

BCI IV Harvill Industrial Center (PPT220001) Noise and Vibration Analysis County of Riverside

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OCTOBER 12, 2022

14231-05 Noise Study



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LIST OF ABBREVIATED TERMS

(1) Reference

ANSI American National Standards Institute

Calveno California Vehicle Noise

CEQA California Environmental Quality Act
CNEL Community Noise Equivalent Level

dBA A-weighted decibels

EPA Environmental Protection Agency
FHWA Federal Highway Administration
FTA Federal Transit Administration

INCE Institute of Noise Control Engineering

L_{eq} Equivalent continuous (average) sound level
L_{max} Maximum level measured over the time interval

mph Miles per hour

PPV Peak Particle Velocity

Project BCI IV Harvill Industrial Center

REMEL Reference Energy Mean Emission Level

RMS Root-mean-square VdB Vibration Decibels



EXECUTIVE SUMMARY

Urban Crossroads, Inc. has prepared this noise study to determine the noise exposure and the necessary noise mitigation measures for the proposed BCI IV Harvill Industrial Center development ("Project"). The Project site is located on the northeast corner of Harvill Avenue and Cajalco Road in the County of Riverside. The Project is proposed to consist of the development of a 99,770 square foot general light industrial building with a 118-stall truck parking lot. This noise study has been prepared to satisfy applicable County of Riverside noise standards and significance criteria based on Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1)

The results of this Noise and Vibration Analysis are summarized below based on the significance criteria in Section 4 of this report consistent with Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1) Table ES-1 shows the findings of significance for each potential noise and/or vibration impact under CEQA before and after any required mitigation measures.

TABLE ES-1: SUMMARY OF CEQA SIGNIFICANCE FINDINGS

Amalusia	Report	Significance Findings				
Analysis	Section	Unmitigated	Mitigated			
Off-Site Traffic Noise	7	Less Than Significant	-			
Operational Noise	9	Less Than Significant	-			
Construction Noise	10	Less Than Significant	-			
Construction Vibration	10	Less Than Significant	-			

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1 INTRODUCTION

This noise analysis has been completed to determine the noise impacts associated with the development of the proposed BCI IV Harvill Industrial Center ("Project"). This noise study briefly describes the proposed Project, provides information regarding noise fundamentals, sets out the local regulatory setting, presents the study methods and procedures for transportation related CNEL traffic noise analysis, and evaluates the future exterior noise environment. In addition, this study includes an analysis of the potential Project-related long-term stationary-source operational noise and short-term construction noise and vibration impacts.

1.1 SITE LOCATION

The proposed Project is located on the northeast corner of Harvill Avenue and Cajalco Road in the County of Riverside, as shown on Exhibit 1-A.

1.2 PROJECT DESCRIPTION

A preliminary site plan for the proposed Project is shown on Exhibit 1-B. The Project is proposed to consist of the development of a 99,770 square foot warehouse building with a 118-stall truck parking lot. Although the latest plan reflects 118-stall truck parking lot, this analysis conservatively assumes a 133-stall truck parking lot which is consistent with the Traffic Analysis and associated trip generation evaluated for the Project. The Project does not propose a cold storage use and therefore is not expected to generate Transport Refrigeration Units (TRUs). The Project site has a General Plan Land Use designation of Light Industrial (LI) and zoning designation of Manufacturing-Service Commercial (M-SC). APNs are 317-130-034 and -035.

The on-site Project-related noise sources are expected to include: loading dock activity, tractor trailer parking, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements. This noise analysis is intended to describe the noise level impacts associated with the expected typical operational activities at the Project site.

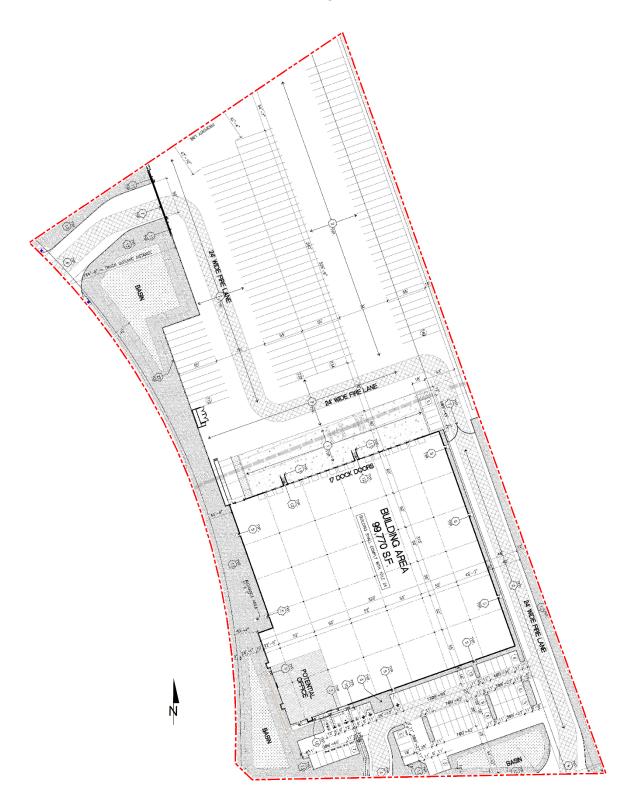


EXHIBIT 1-A: LOCATION MAP





EXHIBIT 1-B: SITE PLAN





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2 FUNDAMENTALS

Noise is simply defined as "unwanted sound." Sound becomes unwanted when it interferes with normal activities, when it causes actual physical harm or when it has adverse effects on health. Noise is measured on a logarithmic scale of sound pressure level known as a decibel (dB). Aweighted decibels (dBA) approximate the subjective response of the human ear to broad frequency noise source by discriminating against very low and very high frequencies of the audible spectrum. They are adjusted to reflect only those frequencies which are audible to the human ear. Exhibit 2-A presents a summary of the typical noise levels and their subjective loudness and effects that are described in more detail below.

EXHIBIT 2-A: TYPICAL NOISE LEVELS

COMMON OUTDOOR ACTIVITIES	COMMON INDOOR ACTIVITIES	A - WEIGHTED SOUND LEVEL dBA	SUBJECTIVE LOUDNESS	EFFECTS OF NOISE	
THRESHOLD OF PAIN		140			
NEAR JET ENGINE		130	INTOLERABLE OR		
		120	DEAFENING	HEARING LOSS	
JET FLY-OVER AT 300m (1000 ft)	ROCK BAND	110			
LOUD AUTO HORN		100			
GAS LAWN MOWER AT 1m (3 ft)		90	VERY NOISY		
DIESEL TRUCK AT 15m (50 ft), at 80 km/hr (50 mph)	FOOD BLENDER AT 1m (3 ft)	80	VERT HOLST		
NOISY URBAN AREA, DAYTIME	VACUUM CLEANER AT 3m (10 ft)	70	LOUD	SPEECH INTERFERENCE	
HEAVY TRAFFIC AT 90m (300 ft)	NORMAL SPEECH AT 1m (3 ft)	60	1000	INTERI ERENCE	
QUIET URBAN DAYTIME	LARGE BUSINESS OFFICE	50	MODERATE	SLEEP	
QUIET URBAN NIGHTTIME	THEATER, LARGE CONFERENCE ROOM (BACKGROUND)	40		DISTURBANCE	
QUIET SUBURBAN NIGHTTIME	LIBRARY	30			
QUIET RURAL NIGHTTIME	BEDROOM AT NIGHT, CONCERT HALL (BACKGROUND)	20	FAINT		
	BROADCAST/RECORDING STUDIO	10	VERY FAINT	NO EFFECT	
LOWEST THRESHOLD OF HUMAN HEARING	LOWEST THRESHOLD OF HUMAN HEARING	0	VERT FAINT		

Source: Environmental Protection Agency Office of Noise Abatement and Control, Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety (EPA/ONAC 550/9-74-004) March 1974.

2.1 RANGE OF NOISE

Since the range of intensities that the human ear can detect is so large, the scale frequently used to measure intensity is a scale based on multiples of 10, the logarithmic scale. The scale for measuring intensity is the decibel scale. Each interval of 10 decibels indicates a sound energy ten times greater than before, which is perceived by the human ear as being roughly twice as loud. (2) The most common sounds vary between 40 dBA (very quiet) to 100 dBA (very loud). Normal conversation at three feet is roughly at 60 dBA, while loud jet engine noises equate to 110 dBA



at approximately 1,000 feet, which can cause serious discomfort. (3) Another important aspect of noise is the duration of the sound and the way it is described and distributed in time.

2.2 Noise Descriptors

Environmental noise descriptors are generally based on averages, rather than instantaneous, noise levels. The most used metric is the equivalent level (L_{eq}). Equivalent sound levels are not measured directly but are calculated from sound pressure levels typically measured in Aweighted decibels (dBA). The equivalent sound level (L_{eq}) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period and is commonly used to describe the "average" noise levels within the environment.

Peak hour or average noise levels, while useful, do not completely describe a given noise environment. Noise levels lower than peak hour may be disturbing if they occur during times when quiet is most desirable, namely evening and nighttime (sleeping) hours. To account for this, the Community Noise Equivalent Level (CNEL), representing a composite 24-hour noise level is utilized. The CNEL is the weighted average of the intensity of a sound, with corrections for time of day, and averaged over 24 hours. The time-of-day corrections require the addition of 5 decibels to dBA L_{eq} sound levels in the evening from 7:00 p.m. to 10:00 p.m., and the addition of 10 decibels to dBA L_{eq} sound levels at night between 10:00 p.m. and 7:00 a.m. These additions are made to account for the noise sensitive time periods during the evening and night hours when noise can become more intrusive. CNEL does not represent the actual sound level heard at any time, but rather represents the total sound exposure. The County of Riverside relies on the 24-hour CNEL level to assess land use compatibility with transportation related noise sources.

2.3 SOUND PROPAGATION

When sound propagates over a distance, it changes in level and frequency content. The way noise reduces with distance depends on the following factors.

2.3.1 GEOMETRIC SPREADING

Sound from a localized source (i.e., a stationary point source) propagates uniformly outward in a spherical pattern. The sound level attenuates (or decreases) at a rate of 6 dB for each doubling of distance from a point source. Highways consist of several localized noise sources on a defined path and hence can be treated as a line source, which approximates the effect of several point sources. Noise from a line source propagates outward in a cylindrical pattern, often referred to as cylindrical spreading. Sound levels attenuate at a rate of 3 dB for each doubling of distance from a line source. (2)

2.3.2 GROUND ABSORPTION

The propagation path of noise from a highway to a receiver is usually very close to the ground. Noise attenuation from ground absorption and reflective wave canceling adds to the attenuation associated with geometric spreading. Traditionally, the excess attenuation has also been expressed in terms of attenuation per doubling of distance. This approximation is usually



sufficiently accurate for distances of less than 200 ft. For acoustically hard sites (i.e., sites with a reflective surface between the source and the receiver, such as a parking lot or body of water), no excess ground attenuation is assumed. For acoustically absorptive or soft sites (i.e., those sites with an absorptive ground surface between the source and the receiver such as soft dirt, grass, or scattered bushes and trees), an excess ground attenuation value of 1.5 dB per doubling of distance is normally assumed. When added to the cylindrical spreading, the excess ground attenuation results in an overall drop-off rate of 4.5 dB per doubling of distance from a line source. (4)

2.3.3 ATMOSPHERIC EFFECTS

Receivers located downwind from a source can be exposed to increased noise levels relative to calm conditions, whereas locations upwind can have lowered noise levels. Sound levels can be increased at large distances (e.g., more than 500 feet) due to atmospheric temperature inversion (i.e., increasing temperature with elevation). Other factors such as air temperature, humidity, and turbulence can also have significant effects. (2)

2.3.4 SHIELDING

A large object or barrier in the path between a noise source and a receiver can substantially attenuate noise levels at the receiver. The amount of attenuation provided by shielding depends on the size of the object and the frequency content of the noise source. Shielding by trees and other such vegetation typically only has an "out of sight, out of mind" effect. That is, the perception of noise impact tends to decrease when vegetation blocks the line-of-sight to nearby residents. However, for vegetation to provide a substantial, or even noticeable, noise reduction, the vegetation area must be at least 15 feet in height, 100 feet wide and dense enough to completely obstruct the line-of-sight between the source and the receiver. This size of vegetation may provide up to 5 dBA of noise reduction. The Federal Highway Administration (FHWA) does not consider the planting of vegetation to be a noise abatement measure. (5)

2.4 Noise Control

Noise control is the process of obtaining an acceptable noise environment for an observation point or receiver by controlling the noise source, transmission path, receiver, or all three. This concept is known as the source-path-receiver concept. In general, noise control measures can be applied to these three elements.

2.5 Noise Barrier Attenuation

Effective noise barriers can reduce noise levels by 10 to 15 dBA, cutting the loudness of traffic noise in half. A noise barrier is most effective when placed close to the noise source or receiver. Noise barriers, however, do have limitations. For a noise barrier to work, it must block the line-of-sight path of sound from the noise source.



2.6 LAND USE COMPATIBILITY WITH NOISE

Some land uses are more tolerant of noise than others. For example, schools, hospitals, churches, and residences are more sensitive to noise intrusion than are commercial or industrial developments and related activities. As ambient noise levels affect the perceived amenity or livability of a development, so too can the mismanagement of noise impacts impair the economic health and growth potential of a community by reducing the area's desirability as a place to live, shop and work. For this reason, land use compatibility with the noise environment is an important consideration in the planning and design process. The FHWA encourages State and Local government to regulate land development in such a way that noise-sensitive land uses are either prohibited from being located adjacent to a highway, or that the developments are planned, designed, and constructed in such a way that noise impacts are minimized. (6)

2.7 COMMUNITY RESPONSE TO NOISE

Approximately sixteen percent of the population has a very low tolerance for noise and will object to any noise not of their making. Consequently, even in the quietest environment, some complaints may occur. Twenty to thirty percent of the population will not complain even in very severe noise environments. (7 pp. 8-6) Thus, a variety of reactions can be expected from people exposed to any given noise environment.

Surveys have shown that community response to noise varies from no reaction to vigorous action for newly introduced noises averaging from 10 dB below existing to 25 dB above existing. (8) According to research originally published in the Noise Effects Handbook (7), the percentage of high annoyance ranges from approximately 0 percent at 45 dB or less, 10 percent are highly annoyed around 60 dB, and increases rapidly to approximately 70 percent being highly annoyed at approximately 85 dB or greater. Despite this variability in behavior on an individual level, the population can be expected to exhibit the following responses to changes in noise levels as shown on Exhibit 2-B. A change of 3 dBA is considered barely perceptible, and changes of 5 dBA are considered readily perceptible. (4)

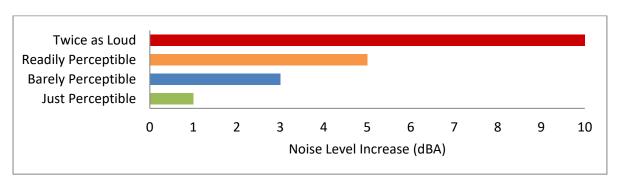


EXHIBIT 2-B: NOISE LEVEL INCREASE PERCEPTION

2.8 VIBRATION

Per the Federal Transit Administration (FTA) *Transit Noise Impact and Vibration Impact Assessment Manual* (8), vibration is the periodic oscillation of a medium or object. The rumbling sound caused by the vibration of room surfaces is called structure-borne noise. Sources of ground-borne vibrations include natural phenomena (e.g., earthquakes, volcanic eruptions, sea waves, landslides) or human-made causes (e.g., explosions, machinery, traffic, trains, construction equipment). Vibration sources may be continuous, such as factory machinery, or transient, such as explosions. As is the case with airborne sound, ground-borne vibrations may be described by amplitude and frequency.

There are several different methods that are used to quantify vibration. The peak particle velocity (PPV) is defined as the maximum instantaneous peak of the vibration signal. The PPV is most frequently used to describe vibration impacts to buildings but is not always suitable for evaluating human response (annoyance) because it takes some time for the human body to respond to vibration signals. Instead, the human body responds to average vibration amplitude often described as the root mean square (RMS). The RMS amplitude is defined as the average of the squared amplitude of the signal and is most frequently used to describe the effect of vibration on the human body. Decibel notation (VdB) is commonly used to measure RMS. Decibel notation (VdB) serves to reduce the range of numbers used to describe human response to vibration. Typically, ground-borne vibration generated by man-made activities attenuates rapidly with distance from the source of the vibration. Sensitive receivers for vibration include structures (especially older masonry structures), people (especially residents, the elderly, and sick), and vibration-sensitive equipment and/or activities.

The background vibration-velocity level in residential areas is generally 50 VdB. Ground-borne vibration is normally perceptible to humans at approximately 65 VdB. For most people, a vibration-velocity level of 75 VdB is the approximate dividing line between barely perceptible and distinctly perceptible levels. Typical outdoor sources of perceptible ground-borne vibration are construction equipment, steel-wheeled trains, and traffic on rough roads. If a roadway is smooth, the ground-borne vibration is rarely perceptible. The range of interest is from approximately 50 VdB, which is the typical background vibration-velocity level, to 100 VdB, which is the general threshold where minor damage can occur in fragile buildings. Exhibit 2-C illustrates common vibration sources and the human and structural response to ground-borne vibration.



Velocity Typical Sources Level* (50 ft from source) Human/Structural Response 100 Threshold, minor cosmetic damage Blasting from construction projects fragile buildings Bulldozers and other heavy tracked construction equipment Difficulty with tasks such as 90 reading a VDT screen Commuter rail, upper range 80 Residential annoyance, infrequent Rapid transit, upper range events (e.g. commuter rail) Commuter rail, typical Residential annoyance, frequent Bus or truck over bump events (e.g. rapid transit) Rapid transit, typical Limit for vibration sensitive equipment. Approx. threshold for Bus or truck, typical human perception of vibration 60 Typical background vibration 50

EXHIBIT 2-C: TYPICAL LEVELS OF GROUND-BORNE VIBRATION

* RMS Vibration Velocity Level in VdB relative to 10-6 inches/second

Source: Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual.



3 REGULATORY SETTING

To limit population exposure to physically and/or psychologically damaging as well as intrusive noise levels, the federal government, the State of California, various county governments, and most municipalities in the state have established standards and ordinances to control noise. In most areas, automobile and truck traffic is the major source of environmental noise. Traffic activity generally produces an average sound level that remains constant with time. Air and rail traffic, and commercial and industrial activities are also major sources of noise in some areas. Federal, state, and local agencies regulate different aspects of environmental noise. Federal and state agencies generally set noise standards for mobile sources such as aircraft and motor vehicles, while regulation of stationary sources is left to local agencies.

3.1 STATE OF CALIFORNIA NOISE REQUIREMENTS

The State of California regulates freeway noise, sets standards for sound transmission, provides occupational noise control criteria, identifies noise standards, and provides guidance for local land use compatibility. State law requires that each county and city adopt a General Plan that includes a Noise Element which is to be prepared per guidelines adopted by the Governor's Office of Planning and Research (OPR). (9) The purpose of the Noise Element is to *limit the exposure of the community to excessive noise levels*. In addition, the California Environmental Quality Act (CEQA) requires that all known environmental effects of a project be analyzed, including environmental noise impacts.

3.2 COUNTY OF RIVERSIDE GENERAL PLAN NOISE ELEMENT

The County of Riverside has adopted a Noise Element of the General Plan to control and abate environmental noise, and to protect the citizens of the County of Riverside from excessive exposure to noise. (10) The Noise Element specifies the maximum allowable exterior noise levels for new developments impacted by transportation noise sources such as arterial roads, freeways, airports, and railroads. In addition, the Noise Element identifies several polices to minimize the impacts of excessive noise levels throughout the community and establishes noise level requirements for all land uses. To protect County of Riverside residents from excessive noise, the Noise Element contains the following policies related to the Project:

- N 1.1 Protect noise-sensitive land uses from high levels of noise by restricting noise-producing land uses from these areas. If the noise-producing land use cannot be relocated, then noise buffers such as setbacks, landscaping, or block walls shall be used.
- N 1.3 Consider the following uses noise-sensitive and discourage these uses in areas in excess of 65 CNEL:
 - Schools
 - Hospitals
 - Rest Homes
 - Long Term Care Facilities
 - Mental Care Facilities
 - Residential Uses
 - Libraries



- Passive Recreation Uses
- Places of Worship
- N 1.5 Prevent and mitigate the adverse impacts of excessive noise exposure on the residents, employees, visitors, and noise-sensitive uses of Riverside County.
- N 4.1 Prohibit facility-related noise, received by any sensitive use, from exceeding the following worst-case noise levels:
 - a. 45 dBA 9-minute L_{eq} between 10:00 p.m. and 7:00 a.m.;
 - b. 65 dBA 9-minute L_{eq} between 7:00 a.m. and 10:00 p.m.
- N 13.1 Minimize the impacts of construction noise on adjacent uses within acceptable standards.
- N 13.2 Ensure that construction activities are regulated to establish hours of operation in order to prevent and/or mitigate the generation of excessive or adverse impacts on surrounding areas.
- N 13.3 Condition subdivision approval adjacent to developed/occupied noise-sensitive land uses (see policy N 1.3) by requiring the developer to submit a construction-related noise mitigation plan to the [County] for review and approval prior to issuance of a grading permit. The plan must depict the location of construction equipment and how the noise from this equipment will be mitigated during construction of this project, through the use of such methods as:
 - i. Temporary noise attenuation fences;
 - ii. Preferential location and equipment; and
 - iii. Use of current noise suppression technology and equipment.
- N 14.1 Enforce the California Building Standards that sets standards for building construction to mitigate interior noise levels to the tolerable 45 CNEL limit. These standards are utilized in conjunction with the Uniform Building Code by the County's Building Department to ensure that noise protection is provided to the public. Some design features may include extra-dense insulation, double-paned windows, and dense construction materials.
- N 16.3 Prohibit exposure of residential dwellings to perceptible ground vibration from passing trains as perceived at the ground or second floor. Perceptible motion shall be presumed to be a motion velocity of 0.01 inches/second over a range of 1 to 100 Hz.

To ensure noise-sensitive land uses are protected from high levels of noise (N 1.1), Table N-1 of the Noise Element identifies guidelines to evaluate proposed developments based on exterior and interior noise level limits for land uses and requires a noise analysis to determine needed mitigation measures if necessary. The Noise Element identifies residential use as a noise-sensitive land use (N 1.3) and discourages new development in areas with transportation related levels of 65 dBA CNEL or greater existing ambient noise levels. To prevent and mitigate noise impacts for its residents (N 1.5), County of Riverside requires exterior noise attenuation measures for sensitive land use exposed to transportation related noise levels higher than 65 dBA CNEL. In addition, the County of Riverside had adopted an interior noise level limit of 45 dBA CNEL (N 14.1).

Policy N 4.1 of the Noise Element sets a stationary-source exterior noise limit to not to be exceeded for a cumulative period of more than ten minutes in any hour of 65 dBA L_{eq} for daytime hours of 7:00 a.m. to 10:00 p.m., and 45 dBA L_{eq} during the noise-sensitive nighttime hours of 10:00 p.m. to 7:00 a.m. To prevent high levels of construction noise from impacting noise-sensitive land uses, policies N 13.1 through 13.3 identify construction noise mitigation



requirements for new development located near existing noise-sensitive land uses. Policy 16.3 establishes the vibration perception threshold for rail-related vibration levels, used in this analysis as a threshold for determining potential vibration impacts due to Project construction. (10)

3.2.1 LAND USE COMPATIBILITY GUIDELINES

The noise criteria identified in the County of Riverside Noise Element (Table N-1) are guidelines to evaluate the land use compatibility of transportation related noise. The compatibility criteria, shown on Exhibit 3-A, provides the County with a planning tool to gauge the compatibility of land uses relative to existing and future exterior noise levels.

The Land Use Compatibility for Community Noise Exposure matrix describes categories of compatibility and not specific noise standards. The warehouse/industrial use of the Project is considered normally acceptable with unmitigated exterior noise levels of less than 70 dBA CNEL based on the Industrial, Manufacturing, Utilities, Agriculture land use compatibility criteria shown on Exhibit 3-A. Residential designated land uses in the Project study area are considered normally acceptable with exterior noise levels below 60 dBA CNEL, and conditionally acceptable with exterior noise levels of up to 70 dBA CNEL. For conditionally acceptable exterior noise levels, of up to 80 dBA CNEL for Project land uses, new construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and the needed noise insulation features are included in the design. Conventional construction, but with closed windows and fresh air supply systems or air conditioning will normally suffice. (10)

3.3.2 COUNTY OF RIVERSIDE STATIONARY NOISE STANDARDS

The County of Riverside has set stationary-source hourly average L_{eq} exterior noise limits to control loading dock activity, tractor trailer parking, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements associated with the development of the proposed BCI IV Harvill Industrial Center. The County considers noise generated using motor vehicles to be a stationary noise source when operated on private property such as at a loading dock. These facility-related noises, as projected to any portion of any surrounding property containing a *habitable dwelling*, *hospital*, *school*, *library or nursing home*, must not exceed the following worst-case noise levels.

Policy N 4.1 of the County of Riverside General Plan Noise Element sets a stationary-source average L_{eq} exterior noise limit not to be exceeded for a cumulative period of more than ten minutes in any hour of 65 dBA L_{eq} for daytime hours of 7:00 a.m. to 10:00 p.m., and 45 dBA L_{eq} during the noise-sensitive nighttime hours of 10:00 p.m. to 7:00 a.m. (10)

The County of Riverside County Code Section 9.52.040 *General sound level standards* (included in Appendix 3.1) identify lower, more restrictive exterior noise level standards, which for the purpose of this report, are used to evaluate potential Project-related operational noise level limits instead of the higher the General Plan exterior noise level standards previously identified. The County of Riverside County Code identifies residential exterior noise level limits of 55 dBA Leq during the daytime hours of 7:00 a.m. to 10:00 p.m., and 45 dBA Leq during the noise-sensitive nighttime hours of 10:00 p.m. to 7:00 a.m., commercial exterior noise level limits of 65 dBA Leq



during the daytime hours, and 55 dBA L_{eq} during the noise-sensitive nighttime hours, and public facility exterior noise level limits of 65 dBA L_{eq} during the daytime hours, and 45 dBA L_{eq} during the noise-sensitive nighttime hours. (11).

LAND USE CATEGORY COMMUNITY NOISE EXPOSURE LEVEL Ldn or CNEL, dBA 65 75 Residential-Low Density Single Family, Duplex, Mobile Homes Residential-Multiple Family Transient Lodging-Motels, Hotels Schools, Libraries, Churches, Hospitals, **Nursing Homes** Auditoriums, Concert Halls, Amphitheaters Sports Arena, Outdoor Spectator Sports Playgrounds, Neighborhood Parks Golf Courses, Riding Stables, Water Recreation. Cemeteries Office Buildings, Businesses, Commercial, and Professional Industrial, Manufacturing, Utilities, Agriculture Conditionally Acceptable: Clearly Unacceptable: New construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and needed noise insulation features included in

EXHIBIT 3-A: LAND USE COMPATIBILITY FOR COMMUNITY NOISE EXPOSURE

Source: County of Riverside General Plan Noise Element, Table N-1.



Based on several discussions with the County of Riverside Department of Environmental Health (DEH), Office of Industrial Hygiene (OIH), it is important to recognize that the County of Riverside County Code noise level standards, incorrectly identify maximum noise level (L_{max}) standards that should instead reflect the average L_{eq} noise levels. Moreover, the County of Riverside DEH OIH's April 15th, 2015 Requirements for determining and mitigating, non-transportation noise source impacts to residential properties also identifies operational (stationary-source) noise level limits using the L_{eq} metric, consistent with the direction of the County of Riverside General Plan guidelines and standards provided in the Noise Element. Therefore, this report has been prepared consistent with direction of the County of Riverside DEH OIH guidelines and standards using the average L_{eq} noise level metric for stationary-source (operational) noise level evaluation.

3.3 CONSTRUCTION NOISE STANDARDS

To control noise impacts associated with the construction of the proposed Project, the County of Riverside has established limits to the hours of construction activities. Riverside County Ordinance No. 847 Regulating Noise Section 2i indicates that noise associated with any private construction activity located within one-quarter of a mile from an inhabited dwelling is considered exempt between the hours of 6:00 a.m. and 6:00 p.m., during the months of June through September, and 7:00 a.m. and 6:00 p.m., during the months of October through May. (11) Neither the County's General Plan nor County Code establish numeric maximum acceptable construction source noise levels at potentially affected receivers for CEQA analysis purposes. Therefore, a numerical construction threshold based on Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment Manual* is used for analysis of daytime construction impacts, as discussed below.

According to the FTA, local noise ordinances are typically not very useful in evaluating construction noise. They usually relate to nuisance and hours of allowed activity, and sometimes specify limits in terms of maximum levels, but are generally not practical for assessing the impact of a construction project. Project construction noise criteria should account for the existing noise environment, the absolute noise levels during construction activities, the duration of the construction, and the adjacent land use. Due to the lack of standardized construction noise thresholds, the FTA provides guidelines that can be considered reasonable criteria for construction noise assessment. The FTA considers a daytime exterior construction noise level of 80 dBA L_{eq} as a reasonable threshold for noise sensitive residential land use with a nighttime exterior construction noise level of 70 dBA L_{eq} (8 p. 179).

3.4 Construction Vibration Standards

Construction activity can result in varying degrees of ground-borne vibration, depending on the equipment and methods used, distance to the affected structures and soil type. Construction vibration is generally associated with pile driving and rock blasting. Other construction equipment such as air compressors, light trucks, hydraulic loaders, etc., generates little or no ground vibration. Occasionally large bulldozers and loaded trucks can cause perceptible vibration levels at close proximity. The County of Riverside does not have vibration standards for temporary construction, but the County's General Plan Noise Element does contain the human



reaction to typical vibration levels. Vibration levels with peak particle velocity of 0.0787 inches per second are considered readily perceptible and above 0.1968 in/sec are considered annoying to people in buildings. Further, County of Riverside General Plan Policy N 16.3 identifies a motion velocity perception threshold for vibration due to passing trains of 0.01 inches per second (in/sec) over the range of one to 100 Hz, which is used in this noise study to assess potential impacts due to Project construction vibration levels. (10)

3.5 MARCH AIR RESERVE BASE/INLAND PORT AIRPORT LAND USE COMPATIBILITY

March Air Reserve Base/Inland Port Airport (MARB/IPA) runway is located approximately 1.4 miles northeast of the Project site boundary. The March Air Reserve Base/Inland Port Airport Land Use Compatibility Plan (MARB/IPA LUCP) includes the policies for determining the land use compatibility of the Project. (12) The MARB/IPA LUCP, Map MA-1, indicates that the Project site is located within Compatibility Zone C2, and the Table MA-1 Compatibility Zone Factors indicates that this area is considered to have a moderate noise impact, and is within the 60 dBA CNEL noise level contour boundaries, but more than 5 miles from runway end. Consistent with the Basic Compatibility Criteria, listed in Table MA-2 of the MARB/IPA LUCP, highly noise-sensitive outdoor nonresidential uses are not permitted. The MARB/IPA LUCP does not identify industrial-use specific noise compatibility standards, and therefore, the Noise/Land Use Noise Compatibility Criteria (Figure N-10) in the County of Riverside General Plan Noise Element is used to assess potential aircraft-related noise levels at the Project site. The Noise/Land Use Noise Compatibility Criteria indicate that industrial uses, such as the Project, are considered normally acceptable with exterior noise levels of up to 70 dBA CNEL. (9) The noise contour boundaries of MARB/IPA are presented on Exhibit 3-B of this report and show that the Project is considered normally acceptable land use since it is located outside the MARB/IPA LUCP 65 dBA CNEL noise level contour boundaries.



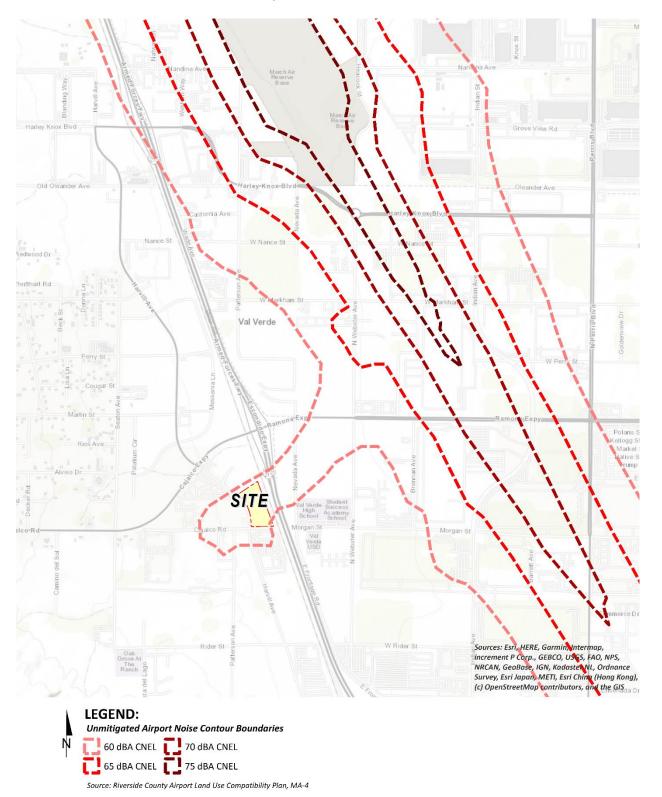


EXHIBIT 3-B: MARB/IPA FUTURE AIRPORT NOISE CONTOURS



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4 SIGNIFICANCE CRITERIA

The following significance criteria are based on currently adopted guidance provided by Appendix G of the Guidelines for Implementation of the California Environmental Quality Act (CEQA) Guidelines. (1) For the purposes of this report, impacts would be potentially significant if the Project results in or causes:

- A. Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- B. Generation of excessive ground-borne vibration or ground-borne noise levels?
- C. For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

4.1 Noise Level Increases (Threshold A)

Noise level increases resulting from the Project are evaluated based on the Appendix G CEQA Guidelines described above at the closest sensitive receiver locations. Under CEQA, consideration must be given to the magnitude of the increase, the existing baseline ambient noise levels, and the location of noise-sensitive receivers to determine if a noise increase represents a significant adverse environmental impact. This approach recognizes that there is no single noise increase that renders the noise impact significant. (13) This is primarily because of the wide variation in individual thresholds of annoyance and differing individual experiences with noise. Thus, an important way of determining a person's subjective reaction to a new noise is the comparison of it to the existing environment to which one has adapted—the so-called ambient environment. In general, the more a new noise exceeds the previously existing ambient noise level, the less acceptable the new noise will typically be judged.

4.1.1 Noise-Sensitive Receivers

The Federal Interagency Committee on Noise (FICON) (14) developed guidance to be used for the assessment of project-generated increases in noise levels that consider the ambient noise level. The FICON recommendations are based on studies that relate aircraft noise levels to the percentage of persons highly annoyed by aircraft noise. Although the FICON recommendations were specifically developed to assess aircraft noise impacts, these recommendations are often used in environmental noise impact assessments involving the use of cumulative noise exposure metrics, such as the average-daily noise level (CNEL) and equivalent continuous noise level (Leq).

As previously stated, the approach used in this noise study recognizes that there is no single noise increase that renders the noise impact significant, based on a 2008 California Court of Appeal ruling on Gray v. County of Madera. (13) For example, if the ambient noise environment is quiet (<60 dBA) and the new noise source greatly increases the noise levels, an impact may occur if the noise criteria may be exceeded. Therefore, for this analysis, a readily perceptible 5 dBA or greater project-related noise level increase is considered a significant impact when the without project



noise levels are below 60 dBA. Per the FICON, in areas where the without project noise levels range from 60 to 65 dBA, a 3 dBA *barely perceptible* noise level increase appears to be appropriate for most people. When the without project noise levels already exceed 65 dBA, any increase in community noise louder than 1.5 dBA or greater is considered a significant impact if the noise criteria for a given land use is exceeded, since it likely contributes to an existing noise exposure exceedance. The FICON guidance provides an established source of criteria to assess the impacts of substantial temporary or permanent increase in baseline ambient noise levels. Based on the FICON criteria, the amount to which a given noise level increase is considered acceptable is reduced when the without Project (baseline) noise levels are already shown to exceed certain land-use specific exterior noise level criteria. The specific levels are based on typical responses to noise level increases of 5 dBA or *readily perceptible*, 3 dBA or *barely perceptible*, and 1.5 dBA depending on the underlying without Project noise levels for noise-sensitive uses. These levels of increases and their perceived acceptance are consistent with guidance provided by both the Federal Highway Administration (4 p. 9) and Caltrans (15 p. 2 48).

4.1.2 Non-Noise-Sensitive Receivers

The County of Riverside General Plan Noise Element, Table N-1, Land Use Compatibility for Community Noise Exposure was used to establish the satisfactory noise levels of significance for non-noise-sensitive land uses in the Project study area. As previously shown on Exhibit 3-A, the normally acceptable exterior noise levels for non-noise-sensitive land uses is 70 dBA CNEL. Noise levels greater than 70 dBA CNEL are considered conditionally acceptable per the Land Use Compatibility for Community Noise Exposure. (10)

To determine if Project-related traffic noise level increases are significant at off-site non-noise-sensitive land uses, a *barely perceptible* 3 dBA criteria is used. When the without Project noise levels are greater than the *normally acceptable* 70 dBA CNEL land use compatibility criteria, a *barely perceptible* 3 dBA or greater noise level increase is considered a significant impact since the noise level criteria is already exceeded. The noise level increases used to determine significant impacts for non-noise-sensitive land uses is generally consistent with the FICON noise level increase thresholds for noise-sensitive land uses but instead rely on the County of Riverside General Plan Noise Element, Table N-1, *Land Use Compatibility for Community Noise Exposure normally acceptable* 70 dBA CNEL exterior noise level criteria.

4.2 VIBRATION (THRESHOLD B)

As described in Section 3.4, the vibration impacts originating from the construction of the BCI IV Harvill Industrial Center are appropriately evaluated the thresholds of significance outlined in the County of Riverside General Plan (10). These guidelines identify a motion velocity perception threshold for vibration due to passing trains of 0.01 inches per second (in/sec) over the range of one to 100 Hz, which is used in this noise study to assess potential impacts due to Project construction vibration levels.



4.3 CEQA Guidelines Not Further Analyzed (Threshold C)

The closest airport which would require additional noise analysis under CEQA Appendix G Guideline C is the MARB/IPA. As previously described in Section 3.5, the Project is in Compatibility Zone C2, and the Table MA-1 Compatibility Zone Factors indicates that this area is considered to have a *moderate* noise impact. In addition, Table MA-2 indicates that the Project land use satisfies the basic compatibility criteria. Therefore, the potential impacts under CEQA Appendix G Guideline C, are *less than significant* and are not further analyzed in this noise study.

4.4 SIGNIFICANCE CRITERIA SUMMARY

Noise impacts shall be considered significant if any of the following occur as a direct result of the proposed development. Table 4-1 shows the significance criteria summary matrix that includes the allowable criteria used to identify potentially significant incremental noise level increases.

TABLE 4-1: SIGNIFICANCE CRITERIA SUMMARY

0 1	Receiving	Condition (a)	Significance Criteria			
Analysis	Land Use	Condition(s)	Daytime	Nighttime		
		If ambient is < 60 dBA CNEL	≥ 5 dBA CNEL F	≥ 5 dBA CNEL Project increase		
	Noise- Sensitive ¹	If ambient is 60 - 65 dBA CNEL	≥ 3 dBA CNEL Project increase			
Off-Site	Sensitive	If ambient is > 65 dBA CNEL	≥ 1.5 dBA CNEL Project increase			
Traffic	Non-Noise- Sensitive ²	If ambient is > 70 dBA CNEL	≥ 3 dBA CNEL Project increase			
		Residential Exterior Noise Level Standards ³	55 dBA L _{eq}	45 dBA L _{eq}		
	Noise- Sensitive	Commercial Exterior Noise Level Standards ³	65 dBA L _{eq}	55 dBA L _{eq}		
Operational		Public Facility Exterior Noise Level Standards ³	65 dBA L _{eq}	45 dBA L _{eq}		
		If ambient is < 60 dBA Leq ¹	≥ 5 dBA L _{eq} Project increase			
		If ambient is 60 - 65 dBA Leq ¹	≥ 3 dBA L _{eq} Project increase			
		If ambient is > 65 dBA Leq ¹	≥ 1.5 dBA L _{eq} Project increase			
Construction	Noise-	Noise Level Threshold ⁴	80 dBA L _{eq}	70 dBA L _{eq}		
Construction	Sensitive	Vibration Level Threshold ⁵	0.01 in/sec RMS			

¹FICON, 1992.



² County of Riverside General Plan Noise Element, Table N-1.

³ County of Riverside General Plan Municipal Code, Section 9.52.040.

⁴ Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual.

⁵ County of Riverside General Plan Noise Element, Policy N 16.3.

[&]quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

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5 EXISTING NOISE LEVEL MEASUREMENTS

To assess the existing noise level environment, 24-hour noise level measurements were taken at four locations in the Project study area. The receiver locations were selected to describe and document the existing noise environment within the Project study area. Exhibit 5-A provides the boundaries of the Project study area and the noise level measurement locations. To fully describe the existing noise conditions, noise level measurements were collected by Urban Crossroads, Inc. on Sunday, June 19th, 2022, and Wednesday, July 21st, 2021. Appendix 5.1 includes study area photos.

5.1 Measurement Procedure and Criteria

To describe the existing noise environment, the hourly noise levels were measured during typical weekday conditions over a 24-hour period. By collecting individual hourly noise level measurements, it is possible to describe the equivalent daytime and nighttime hourly noise levels. The long-term noise readings were recorded using Piccolo Type 2 integrating sound level meter and dataloggers. The Piccolo sound level meters were calibrated using a Larson-Davis calibrator, Model CAL 150. All noise meters were programmed in "slow" mode to record noise levels in "A" weighted form. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (16)

5.2 Noise Measurement Locations

The long-term noise level measurements were positioned as close to the nearest sensitive receiver locations as possible to assess the existing ambient hourly noise levels surrounding the Project site. Both Caltrans and the FTA recognize that it is not reasonable to collect noise level measurements that can fully represent every part of a private yard, patio, deck, or balcony normally used for human activity when estimating impacts for new development projects. This is demonstrated in the Caltrans general site location guidelines which indicate that, sites must be free of noise contamination by sources other than sources of interest. Avoid sites located near sources such as barking dogs, lawnmowers, pool pumps, and air conditioners unless it is the express intent of the analyst to measure these sources. (2) Further, FTA guidance states, that it is not necessary nor recommended that existing noise exposure be determined by measuring at every noise-sensitive location in the project area. Rather, the recommended approach is to characterize the noise environment for clusters of sites based on measurements or estimates at representative locations in the community. (8)

Based on recommendations of Caltrans and the FTA, it is not necessary to collect measurements at each individual building or residence, because each receiver measurement represents a group of buildings that share acoustical equivalence. (8) In other words, the area represented by the receiver shares similar shielding, terrain, and geometric relationship to the reference noise source. Receivers represent a location of noise sensitive areas and are used to estimate the future noise level impacts. Collecting reference ambient noise level measurements at the nearby



sensitive receiver locations allows for a comparison of the before and after Project noise levels and is necessary to assess potential noise impacts due to the Project's contribution to the ambient noise levels.

5.3 Noise Measurement Results

The noise measurements presented below focus on the equivalent or the hourly energy average sound levels (L_{eq}). The equivalent sound level (L_{eq}) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period. Table 5-1 identifies the hourly daytime (7:00 a.m. to 10:00 p.m.) and nighttime (10:00 p.m. to 7:00 a.m.) noise levels at each noise level measurement location.

TABLE 5-1: AMBIENT NOISE LEVEL MEASUREMENTS

Location ¹	Description	Energy Average Noise Level (dBA L _{eq}) ²		
		Daytime	Nighttime	
L1	Located east of the Project site near Val Verde High School at 972 Morgan Street.	57.6	57.2	
L2	Located southwest of the Project site near single-family residence at 23451 Cajalco Road.	50.4	50.0	
L3	Located at the western site boundary.	62.2	58.6	
L4	Located north of the Project site near Marriot Fairfield Hotel at 19310 Harvill Avenue.	55.6	58.3	

¹ See Exhibit 5-A for the noise level measurement locations.

Table 5-1 provides the equivalent noise levels used to describe the daytime and nighttime ambient conditions. These daytime and nighttime energy average noise levels represent the average of all hourly noise levels observed during these time periods expressed as a single number. Appendix 5.2 provides summary worksheets of the noise levels for each of the daytime and nighttime hours.



² Energy (logarithmic) average levels. The long-term 24-hour measurement worksheets are included in Appendix 5.2.

[&]quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

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EXHIBIT 5-A: NOISE MEASUREMENT LOCATIONS





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6 TRAFFIC NOISE METHODS AND PROCEDURES

The following section outlines the methods and procedures used to estimate and analyze the future traffic noise environment. Consistent with County of Riverside Noise Guidelines for Land Use Planning (see Exhibit 3-A), all transportation related noise levels are presented in terms of the 24-hour CNEL's.

6.1 FHWA TRAFFIC NOISE PREDICTION MODEL

The expected roadway noise level increases from vehicular traffic were calculated by Urban Crossroads, Inc. using a computer program that replicates the Federal Highway Administration (FHWA) Traffic Noise Prediction Model- FHWA-RD-77-108. (17) The FHWA Model arrives at a predicted noise level through a series of adjustments to the Reference Energy Mean Emission Level (REMEL). In California the national REMELs are substituted with the California Vehicle Noise (Calveno) Emission Levels. (18) Adjustments are then made to the REMEL to account for: the roadway classification (e.g., collector, secondary, major or arterial), the roadway active width (i.e., the distance between the center of the outermost travel lanes on each side of the roadway), the total average daily traffic (ADT), the travel speed, the percentages of automobiles, medium trucks, and heavy trucks in the traffic volume, the roadway grade, the angle of view (e.g., whether the roadway view is blocked), the site conditions ("hard" or "soft" relates to the absorption of the ground, pavement, or landscaping), and the percentage of total ADT which flows each hour throughout a 24-hour period. Research conducted by Caltrans has shown that the use of soft site conditions is appropriate for the application of the FHWA traffic noise prediction model used in this analysis. (19)

6.1.1 OFF-SITE TRAFFIC NOISE PREDICTION MODEL INPUTS

Table 6-1 presents the roadway parameters used to assess the Project's off-site transportation noise impacts. Table 6-1 identifies the five off-site study area roadway segments, the distance from the centerline to adjacent land use based on the functional roadway classifications per the County of Riverside General Plan Circulation Element, and the vehicle speeds. The ADT volumes used in this study area presented on Table 6-2 are based on the *BCI IV Harvill Industrial Center Traffic Analysis*, prepared by Urban Crossroads, Inc. for the following traffic scenarios (20).

- Existing 2022 Conditions (E)
- Existing plus Project Conditions (E+P)
- Existing plus Ambient Growth 2024 Conditions (EA)
- Existing plus Ambient Growth plus Project 2024 Conditions (EAP)
- Existing plus Ambient Growth plus Cumulative 2024 Conditions (EAC)
- Existing plus Ambient Growth plus Project plus Cumulative 2024 Conditions (EAPC)

The ADT volumes vary for each roadway segment based on the existing traffic volumes and the combination of project traffic distributions. This analysis relies on a comparative evaluation of



the off-site traffic noise impacts at the boundary of the right-of-way of the receiving adjacent land use, without and with project ADT traffic volumes from the Project traffic analysis.

Consistent with the *Traffic Analysis*, the warehouse building has been evaluated assuming general light industrial use in an effort to conduct a conservative off-site noise analysis. The Project is anticipated to generate a net total of 594 two-way trips per day that include 108 truck trips. (actual vehicles). However, if the proposed building were to be occupied by a warehouse user, the Project would generate 278 two-way trips per day with 82 truck trips, which is much lower than the trips evaluated in this analysis.

TABLE 6-1: OFF-SITE ROADWAY PARAMETERS

ID	Roadway	Segment	Receiving Land Use ¹	Classification ²	Distance from Centerline to Receiving Land Use (Feet) ³	Vehicle Speed (mph)
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	Major	59'	50
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	Major	59'	50
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	Major	59'	50
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	Expressway	92'	50
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	Expressway	92'	50

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to adjacent residential land uses.

To quantify the off-site noise levels, the Project related truck trips were added to the heavy truck category in the FHWA noise prediction model. The addition of the Project related truck trips increases the percentage of heavy trucks in the vehicle mix. This approach recognizes that the FHWA noise prediction model is significantly influenced by the number of heavy trucks in the vehicle mix.

TABLE 6-2: AVERAGE DAILY TRAFFIC VOLUMES

	Roadway	Segment	Average Daily Traffic Volumes ¹						
ID			Existing		Existing + Ambient		Existing + Ambient + Cumulative		
			Without Project	With Project	Without Project	With Project	Without Project	With Project	
1	Harvill Av.	n/o Cajalco Exwy.	10,869	10,992	11,308	11,431	25,731	25,854	
2	Harvill Av.	s/o Cajalco Exwy.	14,909	15,235	15,512	15,837	28,600	28,925	
3	Harvill Av.	s/o Cajalco Rd.	12,419	12,688	12,921	13,190	22,143	22,412	
4	Cajalco Exwy.	w/o Harvill Av.	27,605	27,733	28,721	28,849	54,687	54,815	
5	Cajalco Exwy.	e/o Harvill Av.	30,812	30,886	32,057	32,131	72,251	72,325	

¹ BCI IV Harvill Industrial Center (PPT220001) Traffic Analysis, Urban Crossroads, Inc.



² County of Riverside an City of Perris General Plan Circulation Elements functional roadway classification.

³ Distance to receiving land use is based upon the right-of-way distances.

Table 6-3 provides the time of day (daytime, evening, and nighttime) vehicle splits. The daily Project truck trip-ends were assigned to the individual off-site study area roadway segments based on the Project truck trip distribution percentages documented in the *BCI IV Harvill Industrial Center Traffic Analysis*. Using the Project truck trips in combination with the Project trip distribution, Urban Crossroads, Inc. calculated the number of additional Project truck trips and vehicle mix percentages for each of the study area roadway segments. Table 6-4 shows the traffic flow by vehicle type (vehicle mix) used for all without Project traffic scenarios, and Tables 6-5 to 6-7 show the vehicle mixes used for the with Project traffic scenarios.

TABLE 6-3: TIME OF DAY VEHICLE SPLITS

Vahiala Tura		Time of Day Splits ¹		Total of Time of
Vehicle Type	Daytime	Daytime Evening Nighttime		Day Splits
Autos	77.50%	12.90%	9.60%	100.00%
Medium Trucks	84.80%	4.90%	10.30%	100.00%
Heavy Trucks	86.50%	2.70%	10.80%	100.00%

¹ Typical vehicle mix. Values rounded to the nearest one-hundredth.

TABLE 6-4: WITHOUT PROJECT VEHICLE MIX

Classification	Total % Traffic Flow					
Classification	Autos	Medium Trucks	Heavy Trucks	Total		
All Segments	95.34%	1.76%	2.90%	100.00%		

Based on an existing vehicle count taken at Harvill Avenue and Cajalco Expressway (BCI IV Harvill Industrial Center (PPT220001) Traffic Analysis, Urban Crossroads, Inc.). Vehicle mix percentage values rounded to the nearest one-hundredth.

Due to the added Project truck trips, the increase in Project traffic volumes and the distributions of trucks on the study area road segments, the percentage of autos, medium trucks and heavy trucks will vary for each of the traffic scenarios. This explains why the existing and future traffic volumes and vehicle mixes vary between seemingly identical study area roadway segments.

TABLE 6-5: EXISTING WITH PROJECT VEHICLE MIX

			With Project ¹						
ID	Roadway	Segment	Segment Autos		Heavy Trucks	Total ²			
1	Harvill Av.	n/o Cajalco Exwy.	95.24%	1.77%	2.99%	100.00%			
2	Harvill Av.	s/o Cajalco Exwy.	95.16%	1.78%	3.07%	100.00%			
3	Harvill Av.	s/o Cajalco Rd.	94.93%	1.82%	3.25%	100.00%			
4	Cajalco Exwy.	w/o Harvill Av.	95.30%	1.76%	2.93%	100.00%			
5	Cajalco Exwy.	e/o Harvill Av.	95.32%	1.76%	2.92%	100.00%			

¹ BCI IV Harvill Industrial Center (PPT220001) Traffic Analysis, Urban Crossroads, Inc.



[&]quot;Daytime" = 7:00 a.m. to 7:00 p.m.; "Evening" = 7:00 p.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

² Total of vehicle mix percentage values rounded to the nearest one-hundredth.

TABLE 6-6: EA WITH PROJECT VEHICLE MIX

			With Project ¹					
ID	Roadway	Segment	Autos	Medium Trucks	Heavy Trucks	Total ²		
1	Harvill Av.	n/o Cajalco Exwy.	95.25%	1.77%	2.98%	100.00%		
2	Harvill Av.	s/o Cajalco Exwy.	95.16%	1.78%	3.06%	100.00%		
3	Harvill Av.	s/o Cajalco Rd.	94.94%	1.82%	3.24%	100.00%		
4	Cajalco Exwy.	w/o Harvill Av.	95.30%	1.76%	2.93%	100.00%		
5	Cajalco Exwy.	e/o Harvill Av.	95.32%	1.76%	2.92%	100.00%		

¹BCI IV Harvill Industrial Center (PPT220001) Traffic Analysis, Urban Crossroads, Inc.

TABLE 6-7: EAC WITH PROJECT VEHICLE MIX

			With Project ¹						
ID	Roadway	Segment	Autos	Medium Trucks	Heavy Trucks	Total ²			
1	Harvill Av.	n/o Cajalco Exwy.	95.30%	1.77%	2.94%	100.00%			
2	Harvill Av.	s/o Cajalco Exwy.	95.24%	1.77%	2.99%	100.00%			
3	Harvill Av.	s/o Cajalco Rd.	95.11%	1.80%	3.10%	100.00%			
4	Cajalco Exwy.	w/o Harvill Av.	95.32%	1.76%	2.92%	100.00%			
5	Cajalco Exwy.	e/o Harvill Av.	95.33%	1.76%	2.91%	100.00%			

¹BCI IV Harvill Industrial Center (PPT220001) Traffic Analysis, Urban Crossroads, Inc.



² Total of vehicle mix percentage values rounded to the nearest one-hundredth.

 $^{^{\}rm 2}$ Total of vehicle mix percentage values rounded to the nearest one-hundredth.

7 OFF-SITE TRAFFIC NOISE ANALYSIS

To assess the off-site transportation CNEL noise level impacts associated with development of the proposed Project, noise contours were developed based on the BCI IV Harvill Industrial Center Traffic Analysis prepared by Urban Crossroads, Inc. (20) Noise contour boundaries represent the equal levels of noise exposure and are measured in CNEL from the center of the roadway.

7.1 TRAFFIC NOISE CONTOURS

Noise contours were used to assess the Project's incremental traffic-related noise impacts at land uses adjacent to roadways conveying Project traffic. The noise contours represent the distance to noise levels of a constant value and are measured from the center of the roadway for the 70, 65, and 60 dBA noise levels. The noise contours do not consider the effect of any existing noise barriers or topography that may attenuate ambient noise levels. In addition, because the noise contours reflect modeling of vehicular noise on area roadways, they appropriately do not reflect noise contributions from the surrounding stationary noise sources within the Project study area. Tables 7-1 to 7-5 present a summary of the exterior traffic noise levels for each traffic condition. Appendix 7.1 includes the traffic noise level contours worksheets for each traffic condition.

TABLE 7-1: EXISTING WITHOUT PROJECT CONTOURS

-	Dood	Segment Receiving Land Use ¹	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)			
ID	Road		Receiving Land Use (dBA) ²	70 dBA CNEL	65 dBA CNEL	60 dBA CNEL		
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	70.9	68	147	316	
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	72.3	84	181	390	
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	71.5	74	160	346	
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	72.7	139	300	647	
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	73.2	150	323	696	

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

[&]quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-2: EA WITHOUT PROJECT CONTOURS

-	ID Road Segment	Sa ann amh	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)		
טו		Land Use ¹	Receiving Land Use (dBA) ²	70 dBA CNEL	65 dBA CNEL	60 dBA CNEL	
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	71.1	70	151	325
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	72.5	86	186	401
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	71.7	76	165	355
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	72.9	143	308	664
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	73.4	154	332	715

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

TABLE 7-3: EA WITH PROJECT CONTOURS

10	II) I ROAD I SEGMENT I	G	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)		
ID		Land Use ¹	Receiving Land Use (dBA) ²	70 dBA CNEL	65 dBA CNEL	60 dBA CNEL	
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	71.2	71	153	330
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	72.7	89	192	414
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	72.0	81	174	375
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive 72.9 144		144	310	669
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	73.4	155	333	717

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

[&]quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

[&]quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-4: EAC WITHOUT PROJECT CONTOURS

ID	Road	Segment	Receiving	CNEL at Nearest Receiving Land Use (dBA) ²	Distance to Contour from Centerline (Feet)		
טו			Land Use ¹		70 dBA CNEL	65 dBA CNEL	60 dBA CNEL
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	74.7	121	261	562
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	75.1	130	280	603
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	74.0	109	236	508
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	75.7	220	474	1020
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	76.9	265	570	1228

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

TABLE 7-5: EAC WITH PROJECT CONTOURS

ID	Road	Segment Receiving Land Use ¹	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)		
ID	коаа		Land Use ¹	Receiving Land Use (dBA) ²	70 dBA CNEL	65 dBA CNEL	60 dBA CNEL
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	74.7	122	263	566
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	75.3	132	285	614
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	74.2	113	244	525
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive 75.7 221 475		475	1024	
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	76.9	265	571	1231

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

7.2 EA TRAFFIC NOISE LEVEL INCREASES

Table 7-2 presents the Existing plus Ambient Growth (EA) without Project conditions CNEL noise levels. The EA without Project exterior noise levels range from 71.1 to 73.4 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-3 shows that the EA with Project conditions will range from 71.2 to 73.4 dBA CNEL. Table 7-6 shows that the Project off-site traffic noise level increases range from 0.0 to 0.3 dBA CNEL. Based on the significance criteria for off-site traffic noise presented in Table 4-1, land uses adjacent to the study area roadway segments would experience *less than significant* noise level increases on receiving land uses due to the Project-related traffic under EA traffic conditions.

7.3 EAC TRAFFIC NOISE LEVEL INCREASES

Table 7-4 presents the Existing plus Ambient Growth Plus Cumulative (EAC) without Project conditions CNEL noise levels. The EAC without Project exterior noise levels range from 74.0 to



² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

[&]quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

[&]quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

76.9 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-5 shows that the EAC with Project conditions will range from 74.2 to 76.9 dBA CNEL. Table 7-7 shows that the Project off-site traffic noise level increases range from 0.0 to 0.2 dBA CNEL. Based on the significance criteria for off-site traffic noise presented in Table 4-1, land uses adjacent to the study area roadway segments would experience *less than significant* noise level increases on receiving land uses due to the Project-related traffic under EAC traffic conditions.

7.4 OFF-SITE TRAFFIC NOISE IMPACTS

Table 7-8 presents a summary of the cumulative and project incremental noise level increases for each of the study area roadway segments. The cumulative traffic noise level increase increment describes the difference between the EAC with Project conditions and the Existing (baseline) conditions. The Project increment represents the difference between the EAC without Project and the EAC with Project conditions. Based on the significance criteria for off-site traffic noise presented in Table 4-1, land uses adjacent to the study area roadway segments would experience *less than significant* noise level increases on receiving land uses due to the Project-related traffic.



TABLE 7-6: EA WITH PROJECT TRAFFIC NOISE LEVEL INCREASES

ID	Road Segment	Segment	Receiving	CNEL at Receiving Land Use (dBA) ²			Incremental Noise Level Increase Threshold ³	
			Land Use ¹	No Project	With Project	Project Addition	Limit	Exceeded?
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	71.1	71.2	0.1	3.0	No
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	72.5	72.7	0.2	3.0	No
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	71.7	72.0	0.3	1.5	No
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	72.9	72.9	0.0	3.0	No
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	73.4	73.4	0.0	3.0	No

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

TABLE 7-7: EAC WITH PROJECT TRAFFIC NOISE LEVEL INCREASES

ID	Road	Segment	Receiving Land Use ¹		IEL at Receivi and Use (dBA	Incremental Noise Level Increase Threshold ³		
				No Project	With Project	Project Addition	Limit	Exceeded?
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	74.7	74.7	0.0	3.0	No
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	75.1	75.3	0.2	3.0	No
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	74.0	74.2	0.2	1.5	No
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	75.7	75.7	0.0	3.0	No
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	76.9	76.9	0.0	3.0	No

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

³ Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

³ Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

TABLE 7-8: CUMULATIVE AND PROJECT INCREMENTAL NOISE LEVEL INCREASES

			Receiving			IEL at Receiv and Use (dBA	•			ntal Noise ncrease shold ³
ID	Road	Segment	Land Use ¹	Existing No Project (a)	EAC Without (b)	EAC With Project (c)	Cumulative Increase (c-a)	Project Increment (c-b)	Cumulative Limit	Cumulative Impact?
1	Harvill Av.	n/o Cajalco Exwy.	Non-Sensitive	70.9	71.1	71.2	0.3	0.1	3.0	No
2	Harvill Av.	s/o Cajalco Exwy.	Non-Sensitive	72.3	72.5	72.7	0.4	0.2	3.0	No
3	Harvill Av.	s/o Cajalco Rd.	Sensitive	71.5	71.7	72.0	0.5	0.3	1.5	No
4	Cajalco Exwy.	w/o Harvill Av.	Non-Sensitive	72.7	72.9	72.9	0.2	0.0	3.0	No
5	Cajalco Exwy.	e/o Harvill Av.	Non-Sensitive	73.2	73.4	73.4	0.2	0.0	3.0	No

 $^{^{1}}$ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



²The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

³ Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

8 SENSITIVE RECEIVER LOCATIONS

To assess the potential for long-term operational and short-term construction noise impacts, the following sensitive receiver locations, as shown on Exhibit 8-A, were identified as representative locations for analysis. Sensitive receivers are generally defined as locations where people reside or where the presence of unwanted sound could otherwise adversely affect the use of the land. Noise-sensitive land uses are generally considered to include schools, hospitals, single-family dwellings, mobile home parks, churches, libraries, and recreation areas. Moderately noise-sensitive land uses typically include multi-family dwellings, hotels, motels, dormitories, out-patient clinics, cemeteries, golf courses, country clubs, athletic/tennis clubs, and equestrian clubs. Land uses that are considered relatively insensitive to noise include business, commercial, and professional developments. Land uses that are typically not affected by noise include: industrial, manufacturing, utilities, agriculture, undeveloped land, parking lots, warehousing, liquid and solid waste facilities, salvage yards, and transit terminals.

To describe the potential off-site Project noise levels, four receiver locations in the vicinity of the Project site were identified. All distances are measured from the Project site boundary to the outdoor living areas (e.g., private backyards) or at the building façade, whichever is closer to the Project site. The selection of receiver locations is based on FHWA guidelines and is consistent with additional guidance provided by Caltrans and the FTA, as previously described in Section 5.2. Other sensitive land uses in the Project study area that are located at greater distances than those identified in this noise study will experience lower noise levels than those presented in this report due to the additional attenuation from distance and the shielding of intervening structures. Distance is measured in a straight line from the project boundary to each receiver location.

- R1: Location R1 represents the existing noise sensitive Val Verde High School at 972 Morgan Street, approximately 757 feet east of the Project site. Receiver R1 is limited to daytime use with no planned nighttime receivers and is placed at the building façade. A 24-hour noise measurement was taken near this location, L1, to describe the existing ambient noise environment.
- R2: Location R2 represents the vacant noise sensitive residence at 19542 Patterson Avenue, approximately 413 feet southwest of the Project site. Since there are no private outdoor living areas facing the Project site, receiver R2 is placed at the building façade. A 24-hour noise measurement was taken near this location, L2, to describe the existing ambient noise environment.
- R3: Location R3 represents the existing noise sensitive residence at 23451 Cajalco Road, approximately 612 feet southwest of the Project site. R3 is placed in the private outdoor living areas (backyard) facing the Project site. A 24-hour noise measurement was taken near this location, L2, to describe the existing ambient noise environment.
- R4: Location R4 represents the Marriot Fairfield Hotel at 19310 Harvill Avenue, approximately 119 feet north of the Project site. Since there are no private outdoor living areas facing the Project site, receiver R4 is placed at the building façade. A 24-hour noise measurement was taken near this location, L4, to describe the existing ambient noise environment.

757' Site MORGAN ST

EXHIBIT 8-A: RECEIVER LOCATIONS

LEGEND:

Receiver Locations

Distance from receiver to Project site boundary (in feet)

9 OPERATIONAL NOISE IMPACTS

This section analyzes the potential stationary-source operational noise impacts at the nearest receiver locations, identified in Section 8, resulting from the operation of the proposed BCI IV Harvill Industrial Center Project. Exhibit 9-A identifies the noise source locations used to assess the operational noise levels.

9.1 OPERATIONAL NOISE SOURCES

This operational noise analysis is intended to describe noise level impacts associated with the expected typical of daytime and nighttime activities at the Project site. Consistent with similar warehouse uses, the Project business operations would primarily be conducted within the enclosed building, except for traffic movement, parking, as well as loading and unloading of trucks at designated loading bays. The on-site Project-related noise sources are expected to include: loading dock activity, tractor trailer parking, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements.

9.2 REFERENCE NOISE LEVELS

To estimate the Project operational noise impacts, reference noise level measurements were collected from similar types of activities to represent the noise levels expected with the development of the proposed Project. This section provides a detailed description of the reference noise level measurements shown on Table 9-1 used to estimate the Project operational noise impacts. It is important to note that the following projected noise levels assume the worst-case noise environment with the loading dock activity, tractor trailer parking, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements all operating at the same time. These sources of noise activity will likely vary throughout the day.

9.2.1 MEASUREMENT PROCEDURES

The reference noise level measurements presented in this section were collected using a Larson Davis LxT Type 1 precision sound level meter (serial number 01146). The LxT sound level meter was calibrated using a Larson-Davis calibrator, Model CAL 200, was programmed in "slow" mode to record noise levels in "A" weighted form and was located at approximately five feet above the ground elevation for each measurement. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (16)

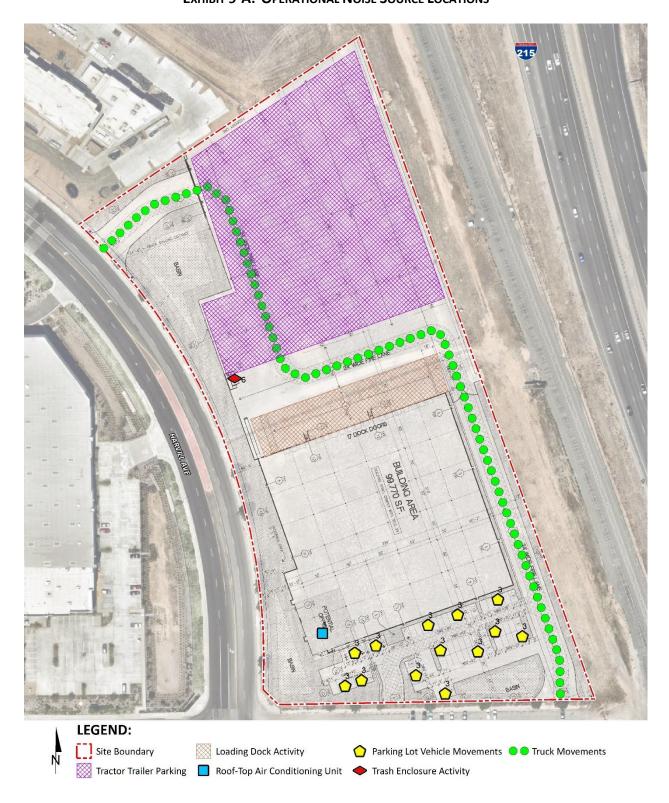


EXHIBIT 9-A: OPERATIONAL NOISE SOURCE LOCATIONS

TABLE 9-1: REFERENCE NOISE LEVEL MEASUREMENTS

Noise Source ¹	Noise Min. Source Hou		-	Reference Noise Level	Sound Power	
Noise Source	Height (Feet)	Day	Night	(dBA L _{eq}) @ 50 Feet	Level (dBA)³	
Loading Dock Activity	8'	60	60	62.8	103.4	
Tractor Trailer Parking	8'	60	60	62.8	103.4	
Roof-Top Air Conditioning Units	5'	39	28	57.2	88.9	
Trash Enclosure Activity	5'	10	10	57.3	89.0	
Parking Lot Vehicle Movements	5'	60	60	56.1	87.8	
Truck Movements	8'	60	60	59.8	93.2	

¹ As measured by Urban Crossroads, Inc.

9.2.2 LOADING DOCK ACTIVITY

The reference loading dock activities are intended to describe the typical operational noise source levels associated with the Project. This includes truck idling, deliveries, backup alarms, unloading/loading, docking including a combination of tractor trailer semi-trucks, two-axle delivery trucks, and background forklift operations. At a uniform reference distance of 50 feet, Urban Crossroads collected a reference noise level of 62.8 dBA L_{eq}. The loading dock activity noise level measurement was taken over a fifteen-minute period and represents multiple noise sources taken from the center of activity. The reference noise level measurement includes employees unloading a docked truck container included the squeaking of the truck's shocks when weight was removed from the truck, employees playing music over a radio, as well as a forklift horn and backup alarm. In addition, during the noise level measurement a truck entered the loading dock area and proceeded to reverse and dock in a nearby loading bay, adding truck engine, idling, air brakes noise, in addition to on-going idling of an already docked truck. Loading dock activity is estimated during all the daytime, evening, and nighttime hours.

9.2.3 TRACTOR TRAILER PARKING

The tractor trailer parking activity noise levels are consistent with the noise source activities at the loading dock. However, for the purpose of this analysis, the tractor trailer noise levels will be limited to the daytime and evening hours from 7:00 a.m. to 10:00 p.m. with no permitted nighttime parking activities between 10:00 p.m. to 7:00 a.m. At a uniform reference distance of 50 feet, Urban Crossroads collected a reference noise level of 62.8 dBA L_{eq}. While tractor trailer parking is permitted in this area during all hours, all noise source activity in this area shall be restricted during the nighttime hours. It is expected that the location of the tractor trailer parking area will act as noise barrier providing addition sound attenuation by blocking the potential nighttime loading dock activities.

² Anticipated duration (minutes within the hour) of noise activity during typical hourly conditions expected at the Project site. "Daytime" = 7:00 a.m. - 10:00 p.m.; "Nighttime" = 10:00 p.m. - 7:00 a.m.

³ Sound power level represents the total amount of acoustical energy (noise level) produced by a sound source independent of distance or surroundings. Sound power levels calculated using the CadnaA noise model at the reference distance to the noise source. Numbers may vary due to size differences between point and area noise sources.

9.2.4 ROOF-TOP AIR CONDITIONING UNITS

The noise level measurements describe a single mechanical roof-top air conditioning unit. The reference noise level represents a Lennox SCA120 series 10-ton model packaged air conditioning unit. At the uniform reference distance of 50 feet, the reference noise levels are 57.2 dBA L_{eq}. Based on the typical operating conditions observed over a four-day measurement period, the roof-top air conditioning units are estimated to operate for and average 39 minutes per hour during the daytime hours, and 28 minutes per hour during the nighttime hours. These operating conditions reflect peak summer cooling requirements with measured temperatures approaching 96 degrees Fahrenheit (°F) with average daytime temperatures of 82°F. For this noise analysis, the air conditioning units are expected to be located on the roof of the Project buildings.

9.2.5 TRASH ENCLOSURE ACTIVITY

To describe the noise levels associated with a trash enclosure activity, Urban Crossroads collected a reference noise level measurement at an existing trash enclosure containing two dumpster bins. The trash enclosure noise levels describe metal gates opening and closing, metal scraping against concrete floor sounds, dumpster movement on metal wheels, and trash dropping into the metal dumpster. The reference noise levels describe trash enclosure noise activities when trash is dropped into an empty metal dumpster, as would occur at the Project Site. The measured reference noise level at the uniform 50-foot reference distance is 57.3 dBA L_{eq} for the trash enclosure activity. The reference noise level describes the expected noise source activities associated with the trash enclosures for the Project's proposed building. Typical trash enclosure activities are estimated to occur for 10 minutes per hour.

9.2.6 PARKING LOT VEHICLE MOVEMENTS

To describe the on-site parking lot activity, a long-term 29-hour reference noise level measurement was collected in the center of activity within the staff parking lot of an Amazon warehouse distribution center. At 50 feet from the center of activity, the parking lot produced a reference noise level of $56.1 \, dBA \, L_{eq}$. Parking activities are expected to take place during the full hour (60 minutes) throughout the daytime and evening hours. The parking lot noise levels are mainly due cars pulling in and out of parking spaces in combination with car doors opening and closing.

9.2.7 TRUCK MOVEMENTS

The truck movements reference noise level measurement was collected over a period of 1 hour and 28 minutes and represents multiple heavy trucks entering and exiting the outdoor loading dock area producing a reference noise level of 59.8 dBA L_{eq} at 50 feet. The noise sources included at this measurement location account for trucks entering and existing the Project driveways and maneuvering in and out of the outdoor loading dock activity area.

9.3 CADNAA NOISE PREDICTION MODEL

To fully describe the exterior operational noise levels from the Project, Urban Crossroads, Inc. developed a noise prediction model using the CadnaA (Computer Aided Noise Abatement)

computer program. CadnaA can analyze multiple types of noise sources using the spatially accurate Project site plan, georeferenced Nearmap aerial imagery, topography, buildings, and barriers in its calculations to predict outdoor noise levels.

Using the ISO 9613-2 protocol, CadnaA will calculate the distance from each noise source to the noise receiver locations, using the ground absorption, distance, and barrier/building attenuation inputs to provide a summary of noise level at each receiver and the partial noise level contributions by noise source. Consistent with the ISO 9613-2 protocol, the CadnaA noise prediction model relies on the reference sound power level (L_w) to describe individual noise sources. While sound pressure levels (e.g., L_{eq}) quantify in decibels the intensity of given sound sources at a reference distance, sound power levels (L_w) are connected to the sound source and are independent of distance. Sound pressure levels vary substantially with distance from the source and diminish because of intervening obstacles and barriers, air absorption, wind, and other factors. Sound power is the acoustical energy emitted by the sound source and is an absolute value that is not affected by the environment.

The operational noise level calculations provided in this noise study account for the distance attenuation provided due to geometric spreading, when sound from a localized stationary source (i.e., a point source) propagates uniformly outward in a spherical pattern. A default ground attenuation factor of 0.5 was used in the CadnaA noise analysis to account for mixed ground representing a combination of hard and soft surfaces. Appendix 9.1 includes the detailed noise model inputs used to estimate the Project operational noise levels presented in this section.

9.4 Project Operational Noise Levels

Using the reference noise levels to represent the proposed Project operations that include loading dock activity, tractor trailer parking, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements, Urban Crossroads, Inc. calculated the operational source noise levels that are expected to be generated at the Project site and the Project-related noise level increases that would be experienced at each of the sensitive receiver locations. Table 9-2 shows the Project operational noise levels during the daytime hours of 7:00 a.m. to 10:00 p.m. The daytime hourly noise levels at the off-site receiver locations are expected to range from 37.6 to 52.2 dBA Leq.

TABLE 9-2: DAYTIME PROJECT OPERATIONAL NOISE LEVELS

Noise Source ¹	Operational Noise Levels by Receiver Location (dBA Leq)					
Noise Source	R1	R2	R3	R4		
Loading Dock Activity	39.5	33.3	25.3	46.2		
Tractor Trailer Parking	41.5	40.2	25.6	50.5		
Roof-Top Air Conditioning Units	20.6	29.0	28.9	22.5		
Trash Enclosure Activity	17.7	20.6	3.2	25.7		
Parking Lot Vehicle Movements	35.3	39.3	36.1	16.4		
Truck Movements	32.5	29.1	22.5	40.8		
Total (All Noise Sources)	44.5	43.6	37.6	52.2		

¹ See Exhibit 9-A for the noise source locations. CadnaA noise model calculations are included in Appendix 9.1.

Tables 9-3 shows the Project operational noise levels during the nighttime hours of $10:00 \, \text{p.m.}$ to $7:00 \, \text{a.m.}$ The nighttime hourly noise levels at the off-site receiver locations are expected to range from $37.3 \, \text{to} \, 52.2 \, \text{dBA} \, L_{\text{eq}}$. The differences between the daytime and nighttime noise levels are largely related to the estimated duration of noise activity as outlined in Table 9-1 and Appendix 9.1.

TABLE 9-3: NIGHTTIME PROJECT OPERATIONAL NOISE LEVELS

Noise Source ¹	Operational Noise Levels by Receiver Location (dBA Leq)					
Noise Source	R1	R2	R3	R4		
Loading Dock Activity	39.5	33.3	25.3	46.2		
Tractor Trailer Parking	41.5	40.2	25.6	50.5		
Roof-Top Air Conditioning Units	18.2	26.6	26.5	20.1		
Trash Enclosure Activity	16.7	19.7	2.2	24.7		
Parking Lot Vehicle Movements	35.3	39.3	36.1	16.4		
Truck Movements	32.5	29.1	22.5	40.8		
Total (All Noise Sources)	44.5	43.5	37.3	52.2		

¹ See Exhibit 9-A for the noise source locations. CadnaA noise model calculations are included in Appendix 9.1.

9.5 Project Operational Noise Level Compliance

To demonstrate compliance with local noise regulations, the Project-only operational noise levels are evaluated against exterior noise level thresholds based on the County of Riverside exterior noise level standards at nearby noise-sensitive receiver locations. Table 9-4 shows the operational noise levels associated with BCI IV Harvill Industrial Center Project will satisfy the County of Riverside daytime and nighttime exterior noise level standards. Therefore, the operational noise impacts are considered *less than significant* at the nearby noise-sensitive receiver locations.

TABLE 9-4: OPERATIONAL NOISE LEVEL COMPLIANCE

Receiver Location ¹		perational s (dBA Leq) ²	Noise Leve (dBA	l Standards Leq) ³		l Standards ded? ⁴
Location	Daytime	Nighttime	Daytime	Nighttime	Daytime	Nighttime
R1	44.5	44.5	65	45 ⁵	No	No ⁵
R2	43.6	43.5	55	45	No	No
R3	37.6	37.3	55	45	No	No
R4	52.2	52.2	65	55	No	No

¹ See Exhibit 8-A for the receiver locations.

² Proposed Project operational noise levels as shown on Tables 9-2 and 9-3.

³ Exterior noise level standards, as shown on Table 4-1.

⁴ Do the estimated Project operational noise source activities exceed the noise level standards?

⁵ Receiver location R1 represents the Val Verde High School and does not include any noise sensitive nighttime receivers.

[&]quot;Daytime" = 7:00 a.m. - 10:00 p.m.; "Nighttime" = 10:00 p.m. - 7:00 a.m.

9.5 Project Operational Noise Level Increases

To describe the Project operational noise level increases, the Project operational noise levels are combined with the existing ambient noise levels measurements for the nearby receiver locations potentially impacted by Project operational noise sources. Since the units used to measure noise, decibels (dB), are logarithmic units, the Project-operational and existing ambient noise levels cannot be combined using standard arithmetic equations. (2) Instead, they must be logarithmically added using the following base equation:

$$\mathsf{SPL}_\mathsf{Total} = \mathsf{10log}_{10}[\mathsf{10}^{\mathsf{SPL1/10}} + \mathsf{10}^{\mathsf{SPL2/10}} + ... \ \mathsf{10}^{\mathsf{SPLn/10}}]$$

Where "SPL1," "SPL2," etc. are equal to the sound pressure levels being combined, or in this case, the Project-operational and existing ambient noise levels. The difference between the combined Project and ambient noise levels describes the Project noise level increases to the existing ambient noise environment. Noise levels that would be experienced at receiver locations when Project-source noise is added to the daytime and nighttime ambient conditions are presented on Tables 9-5 and 9-6, respectively. As indicated on Tables 9-5, the Project will generate a daytime operational noise level increases ranging from 0.2 to 1.6 dBA L_{eq} at the nearest receiver locations. Table 9-6 shows that the Project will generate a nighttime operational noise level increases ranging from 0.2 to 1.0 dBA L_{eq} at the nearest receiver locations. Project-related operational noise level increases will satisfy the operational noise level increase significance criteria presented in Table 4-1, and the increases at the sensitive receiver locations will be *less than significant*.

TABLE 9-5: DAYTIME PROJECT OPERATIONAL NOISE LEVEL INCREASES

Receiver Location ¹	Total Project Operational Noise Level ²	Measurement Location ³	Reference Ambient Noise Levels ⁴	Combined Project and Ambient ⁵	Project Increase ⁶	Increase Criteria ⁷	Increase Criteria Exceeded?
R1	44.5	L1	57.6	57.8	0.2	5.0	No
R2	43.6	L2	50.4	51.2	0.8	5.0	No
R3	37.6	L2	50.4	50.6	0.2	5.0	No
R4	52.2	L4	55.6	57.2	1.6	5.0	No

¹ See Exhibit 8-A for the receiver locations.

TABLE 9-6: NIGHTTIME OPERATIONAL NOISE LEVEL INCREASES

Receiver Location ¹	Total Project Operational Noise Level ²	Measurement Location ³	Reference Ambient Noise Levels ⁴	Combined Project and Ambient ⁵	Project Increase ⁶	Increase Criteria ⁷	Increase Criteria Exceeded?
R1	44.5	L1	57.2	57.4	0.2	5.0	No
R2	43.5	L2	50.0	50.9	0.9	5.0	No
R3	37.3	L2	50.0	50.2	0.2	5.0	No
R4	52.2	L4	58.3	59.3	1.0	5.0	No

¹ See Exhibit 8-A for the receiver locations.



² Total Project daytime operational noise levels as shown on Table 9-2.

³ Reference noise level measurement locations as shown on Exhibit 5-A.

⁴ Observed daytime ambient noise levels as shown on Table 5-1.

⁵ Represents the combined ambient conditions plus the Project activities.

⁶ The noise level increase expected with the addition of the proposed Project activities.

⁷ Significance increase criteria as shown on Table 4-1.

² Total Project nighttime operational noise levels as shown on Table 9-3.

³ Reference noise level measurement locations as shown on Exhibit 5-A.

⁴ Observed nighttime ambient noise levels as shown on Table 5-1.

⁵ Represents the combined ambient conditions plus the Project activities.

⁶ The noise level increase expected with the addition of the proposed Project activities.

⁷ Significance increase criteria as shown on Table 4-1.

10 CONSTRUCTION IMPACTS

This section analyzes potential impacts resulting from the short-term construction activities associated with the development of the Project. Exhibit 10-A shows the construction noise source locations in relation to the nearby sensitive receiver locations previously described in Section 8. According to Riverside County Ordinance No. 847 Regulating Noise Section 2i, noise associated with any private construction activity located within one-quarter of a mile from an inhabited dwelling is considered exempt between the hours of 6:00 a.m. and 6:00 p.m., during the months of June through September, and 7:00 a.m. and 6:00 p.m., during the months of October through May. (11)

In addition, neither the County of Riverside General Plan or County Code establish numeric maximum acceptable construction source noise levels at potentially affected receivers for CEQA analysis purposes. Therefore, a numerical construction threshold based on Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual is used for analysis of daytime construction impacts. The FTA considers a daytime exterior construction noise level of 80 dBA Leq as a reasonable threshold for noise sensitive residential land use (8 p. 179).

10.1 Construction Noise Levels

The FTA *Transit Noise and Vibration Impact Assessment Manual* recognizes that construction projects are accomplished in several different stages and outlines the procedures for assessing noise impacts during construction. Each stage has a specific equipment mix, depending on the work to be completed during that stage. As a result of the equipment mix, each stage has its own noise characteristics; some stages have higher continuous noise levels than others, and some have higher impact noise levels than others. The Project construction activities are expected to occur in the following stages:

- Site Preparation
- Grading
- Building Construction
- Paving
- Architectural Coating

10.2 Construction Reference Noise Levels

To describe construction noise activities, this construction noise analysis was prepared using reference construction equipment noise levels from the Federal Highway Administration (FHWA) published the Roadway Construction Noise Model (RCNM), which includes a national database of construction equipment reference noise emission levels. (21) The RCNM equipment database, provides a comprehensive list of the noise generating characteristics for specific types of construction equipment. In addition, the database provides an acoustical usage factor to estimate the fraction of time each piece of construction equipment is operating at full power (i.e., its loudest condition) during a construction operation.



757' MORGAN ST **LEGEND:**

EXHIBIT 10-A: CONSTRUCTION NOISE SOURCE LOCATIONS



Receiver Locations

Construction Activity — Distance from receiver to construction activity (in feet)

10.3 Construction Noise Analysis

Using the reference construction equipment noise levels and the CadnaA noise prediction model, calculations of the Project construction noise level impacts at the nearby sensitive receiver locations were completed. Consistent with FTA guidance for general construction noise assessment, Table 10-1 presents the combined noise levels for the loudest construction equipment, assuming they operate at the same time. As shown on Table 10-2, the construction noise levels are expected to range from 47.6 to 61.0 dBA Leq at the nearby receiver locations. Appendix 10.1 includes the detailed CadnaA construction noise model inputs.

TABLE 10-1: CONSTRUCTION REFERENCE NOISE LEVELS

Construction Stage	Reference Construction Activity	Reference Noise Level @ 50 Feet (dBA L _{eq}) ¹	Combined Noise Level (dBA L _{eq}) ²	Combined Sound Power Level (PWL) ³	
C'I	Crawler Tractors	78			
Site Preparation	Hauling Trucks	72	80	112	
rreparation	Rubber Tired Dozers	75			
	Graders	81			
Grading	Excavators	77	83	115	
	Compactors	76			
5 11 11	Cranes	73			
Building Construction	Tractors	80	81	113	
Construction	Welders	70			
	Pavers	74			
Paving	Paving Equipment	82	83	115	
	Rollers	73			
	Cranes	73			
Architectural Coating	Air Compressors	74	77	109	
Couting	Generator Sets	70			

¹ FHWA Roadway Construction Noise Model (RCNM).



² Represents the combined noise level for all equipment assuming they operate at the same time consistent with FTA Transit Noise and Vibration Impact Assessment guidance.

³ Sound power level represents the total amount of acoustical energy (noise level) produced by a sound source independent of distance or surroundings. Sound power levels calibrated using the CadnaA noise model at the reference distance to the noise source.

TABLE 10-2: CONSTRUCTION EQUIPMENT NOISE LEVEL SUMMARY

	Construction Noise Levels (dBA L _{eq})							
Receiver Location ¹	Site Preparation	Grading	Building Construction	Paving	Architectural Coating	Highest Levels ²		
R1	50.6	53.6	51.6	53.6	47.6	53.6		
R2	52.2	55.2	53.2	55.2	49.2	55.2		
R3	50.9	53.9	51.9	53.9	47.9	53.9		
R4	58.0	61.0	59.0	61.0	55.0	61.0		

¹ Noise receiver locations are shown on Exhibit 10-A.

10.4 CONSTRUCTION NOISE LEVEL COMPLIANCE

To evaluate whether the Project will generate potentially significant short-term noise levels at nearest receiver locations, a construction-related daytime noise level threshold of 80 dBA L_{eq} is used as a reasonable threshold to assess the daytime construction noise level impacts. The construction noise analysis shows that the nearest receiver locations will satisfy the reasonable daytime 80 dBA L_{eq} significance threshold during Project construction activities as shown on Table 10-3. Therefore, the noise impacts due to Project construction noise are considered *less than significant* at all receiver locations.

TABLE 10-3: CONSTRUCTION NOISE LEVEL COMPLIANCE

	Construction Noise Levels (dBA L _{eq})					
Receiver Location ¹	Highest Construction Noise Levels ²					
R1	53.6	80	No			
R2	55.2	80	No			
R3	53.9	80	No			
R4	61.0	80	No			

¹ Noise receiver locations are shown on Exhibit 10-A.

10.5 NIGHTTIME CONCRETE POUR NOISE ANALYSIS

It is our understanding that nighttime concrete pouring activities will occur as a part of Project building construction activities. Nighttime concrete pouring activities are often used to support reduced concrete mixer truck transit times and lower air temperatures than during the daytime hours and are generally limited to the actual building pad area as shown on Exhibit 10-B. Since the nighttime concrete pours will take place outside the permitted by Riverside County Ordinance No. 847 Regulating Noise Section 2i, the Project Applicant will be required to obtain authorization for nighttime work from the County of Riverside. Any nighttime construction noise



² Construction noise level calculations based on distance from the construction activity, which is measured from the Project site boundary to the nearest receiver locations. CadnaA construction noise model inputs are included in Appendix 10.1.

² Highest construction noise level calculations based on distance from the construction noise source activity to the nearest receiver locations as shown on Table 10-2.

³ Construction noise level thresholds as shown on Table 4-1.

⁴ Do the estimated Project construction noise levels exceed the construction noise level threshold?

activities are evaluated against the FTA nighttime exterior construction noise level threshold of 70 dBA Leq for noise sensitive residential land use (8 p. 179).

10.5.1 NIGHTTIME CONCRETE POUR REFERENCE NOISE LEVEL MEASUREMENTS

To estimate the noise levels due to nighttime concrete pour activities, sample reference noise level measurements were taken during a nighttime concrete pour at a construction site. Urban Crossroads, Inc. collected short-term nighttime concrete pour reference noise level measurements during the noise-sensitive nighttime hours between 1:00 a.m. to 2:00 a.m. at 27334 San Bernardino Avenue in the City of Redlands. The reference noise levels describe the expected concrete pour noise sources that may include concrete mixer truck movements and pouring activities, concrete paving equipment, rear mounted concrete mixer truck backup alarms, engine idling, air brakes, generators, and workers communicating/whistling.

To describe the nighttime concrete pour noise levels associated with the construction of the BCI IV Harvill Industrial Center, this analysis relies on reference sound power level of 100.3 dBA L_w . While the Project noise levels will depend on the actual duration of activities and specific equipment fleet in use at the time of construction, the reference sound power level of 100.3 dBA L_w is used to describe the expected Project nighttime concrete pour noise activities.

10.5.2 NIGHTTIME CONCRETE POUR NOISE LEVEL COMPLIANCE

As shown on Table 10-4, the noise levels associated with the nighttime concrete pour activities are estimated to range from 38.3 to 40.6 dBA $L_{\rm eq}$. The analysis shows that the unmitigated nighttime concrete pour activities will satisfy the FTA 70 dBA $L_{\rm eq}$ nighttime residential noise level threshold at all the nearest noise sensitive receiver locations. Therefore, the noise impacts due to Project construction nighttime concrete pour noise activity are considered *less than significant* at all receiver locations with prior authorization for nighttime work from the County of Riverside. Appendix 10.2 includes the CadnaA nighttime concrete pour noise model inputs.

TABLE 10-4: NIGHTTIME CONCRETE POUR NOISE LEVEL COMPLIANCE

	Concrete Pour Construction Noise Levels (dBA L _{eq})						
Receiver Location ¹	Exterior Noise Levels ²	Threshold ³	Threshold Exceeded? ⁴				
R1	38.3	70	No				
R2	40.6	70	No				
R3	38.7	70	No				
R4	40.1	70	No				

¹ Noise receiver locations are shown on Exhibit 10-B.



² Nighttime Concrete Pour noise model inputs are included in Appendix 10.2.

³ Construction noise level thresholds as shown on Table 4-1.

⁴ Do the estimated Project construction noise levels exceed the construction noise level threshold?

113 215 MORGAN ST LEGEND: Site Boundary Receiver Locations Nighttime Concrete Pour Activity (Building Area) — Distance from receiver to construction activity (in feet)

EXHIBIT 10-B: NIGHTTIME CONCRETE POUR NOISE SOURCE AND RECEIVER LOCATIONS



10.6 Construction Vibration Impacts

Construction activity can result in varying degrees of ground vibration, depending on the equipment and methods used, distance to the affected structures and soil type. It is expected that ground-borne vibration from Project construction activities would cause only intermittent, localized intrusion. Ground-borne vibration levels resulting from typical construction activities occurring within the Project site were estimated by data published by the Federal Transit Administration (FTA) (8). However, while vehicular traffic is rarely perceptible, construction has the potential to result in varying degrees of temporary ground vibration, depending on the specific construction activities and equipment used. Ground vibration levels associated with various types of construction equipment are summarized on Table 10-5. Based on the representative vibration levels presented for various construction equipment types, it is possible to estimate the potential Project construction vibration levels using the following vibration assessment methods defined by the FTA. To describe the human response (annoyance) associated with vibration impacts the FTA provides the following equation: PPV_{equip} = PPV_{ref} x (25/D)^{1.5}

TABLE 10-5: VIBRATION SOURCE LEVELS FOR CONSTRUCTION EQUIPMENT

Equipment	PPV (in/sec) at 25 feet
Small bulldozer	0.003
Jackhammer	0.035
Loaded Trucks	0.076
Large bulldozer	0.089

Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual

Using the vibration source level of construction equipment provided on Table 10-5 and the construction vibration assessment methodology published by the FTA, it is possible to estimate the Project vibration impacts. Table 10-6 presents the expected Project related vibration levels at the nearby receiver locations. At distances ranging from 119 to 757 feet from Project construction activities, construction vibration velocity levels are estimated to range from 0.000 to 0.006 in/sec RMS and will remain below the County of Riverside threshold of 0.01 in/sec RMS at all receiver locations, as shown on Table 10-6. Therefore, the Project-related vibration impacts are considered *less than significant* during the construction activities at the Project site.



TABLE 10-6: PROJECT CONSTRUCTION VIBRATION LEVELS

Receiver ¹	Distance to Const. Activity (Feet)	Receiver Levels (in/sec) RMS ²					Threshold	
		Small Bulldozer	Jack- hammer	Loaded Trucks	Large Bulldozer	Peak Vibration	(in/sec) RMS ⁴	Threshold Exceeded? ⁵
R1	757'	0.000	0.000	0.000	0.000	0.000	0.01	No
R2	413'	0.000	0.000	0.001	0.001	0.001	0.01	No
R3	612'	0.000	0.000	0.000	0.001	0.001	0.01	No
R4	119'	0.000	0.002	0.005	0.006	0.006	0.01	No

¹ Receiver locations are shown on Exhibit 10-A.

Moreover, the vibration levels at the nearest sensitive receiver locations are unlikely to be sustained during the entire construction period but will occur rather only during the times that heavy construction equipment is operating adjacent to the Project site perimeter.



² Based on the Vibration Source Levels of Construction Equipment included on Table 10-4. Vibration levels in PPV are converted to RMS velocity using a 0.71 conversion factor identified in the Caltrans Transportation and Construction Vibration Guidance Manual, September 2013.

³ Source: County of Riverside General Plan Noise Element, Policy N 16.3.

⁴ Does the vibration level exceed the maximum acceptable vibration threshold?

11 REFERENCES

- 1. **State of California.** *California Environmental Quality Act, Appendix G.* 2018.
- 2. California Department of Transportation Environmental Program. *Technical Noise Supplement A Technical Supplement to the Traffic Noise Analysis Protocol.* Sacramento, CA: s.n., September 2013.
- 3. Environmental Protection Agency Office of Noise Abatement and Control. Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety. March 1974. EPA/ONAC 550/9/74-004.
- 4. U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning, Noise and Air Quality Branch. Highway Traffic Noise Analysis and Abatement Policy and Guidance. December 2011.
- 5. **U.S. Department of Transportation Federal Highway Administration.** *Highway Noise Barrier Design Handbook.* 2001.
- 6. **U.S. Department of Transportation, Federal Highway Administration.** *Highway Traffic Noise in the United States, Problem and Response.* April 2000. p. 3.
- 7. **U.S. Environmental Protection Agency Office of Noise Abatement and Control.** *Noise Effects Handbook-A Desk Reference to Health and Welfare Effects of Noise.* October 1979 (revised July 1981). EPA 550/9/82/106.
- 8. **U.S. Department of Transportation, Federal Transit Administration.** *Transit Noise and Vibration Impact Assessment Manual.* September 2018.
- 9. Office of Planning and Research. State of California General Plan Guidelines. 2019.
- 10. County of Riverside. General Plan Noise Element. December 2015.
- 11. . Municipal Code, Chapter 9.52 Noise Regulation.
- 12. **Riverside County Airport Land Use Commission.** *March Air Reserve Base/Inland Port Airport Land Use Compatibility Plan.* November 2014.
- 13. California Court of Appeal. *Gray v. County of Madera, F053661.* 167 Cal.App.4th 1099; Cal.Rptr.3d, October 2008.
- 14. **Federal Interagency Committee on Noise.** Federal Agency Review of Selected Airport Noise Analysis Issues. August 1992.
- 15. California Department of Transportation. Technical Noise Supplement. November 2009.
- 16. American National Standards Institute (ANSI). Specification for Sound Level Meters ANSI S1.4-2014/IEC 61672-1:2013.
- 17. **U.S. Department of Transportation, Federal Highway Administration.** *FHWA Highway Traffic Noise Prediction Model.* December 1978. FHWA-RD-77-108.
- 18. California Department of Transportation Environmental Program, Office of Environmental Engineering. Use of California Vehicle Noise Reference Energy Mean Emission Levels (Calveno REMELs) in FHWA Highway Traffic Noise Prediction. September 1995. TAN 95-03.
- 19. **California Department of Transportation.** *Traffic Noise Attenuation as a Function of Ground and Vegetation Final Report.* June 1995. FHWA/CA/TL-95/23.
- 20. Urban Crossroads, Inc. BCI IV Harvill Industrial Center (PPT220001) Traffic Analysis. September 2022.



21. U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning. FHWA Roadway Construction Noise Model. January, 2006.



12 CERTIFICATION

The contents of this noise study report represent an accurate depiction of the noise environment and impacts associated with the proposed BCI IV Harvill Industrial Center Project. The information contained in this noise study report is based on the best available data at the time of preparation. If you have any questions, please contact me directly at (949) 584-3148.

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EDUCATION

Master of Science in Civil and Environmental Engineering California Polytechnic State University, San Luis Obispo • December, 1993

Bachelor of Science in City and Regional Planning California Polytechnic State University, San Luis Obispo • June, 1992

PROFESSIONAL REGISTRATIONS

PE – Registered Professional Traffic Engineer – TR 2537 • January, 2009

AICP – American Institute of Certified Planners – 013011 • June, 1997–January 1, 2012

PTP – Professional Transportation Planner • May, 2007 – May, 2013

INCE – Institute of Noise Control Engineering • March, 2004

PROFESSIONAL AFFILIATIONS

ASA – Acoustical Society of America ITE – Institute of Transportation Engineers

PROFESSIONAL CERTIFICATIONS

Certified Acoustical Consultant – County of San Diego • March, 2018 Certified Acoustical Consultant – County of Orange • February, 2011 FHWA-NHI-142051 Highway Traffic Noise Certificate of Training • February, 2013



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APPENDIX 3.1:

COUNTY OF RIVERSIDE MUNICIPAL CODE



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Sections:

9.52.010 - Intent.

At certain levels, sound becomes noise and may jeopardize the health, safety or general welfare of Riverside County residents and degrade their quality of life. Pursuant to its police power, the board of supervisors declares that noise shall be regulated in the manner described in this chapter. This chapter is intended to establish county-wide standards regulating noise. This chapter is not intended to establish thresholds of significance for the purpose of any analysis required by the California Environmental Quality Act and no such thresholds are established.

(Ord. 847 § 1, 2006)

9.52.020 - Exemptions.

Sound emanating from the following sources is exempt from the provisions of this chapter:

- A. Facilities owned or operated by or for a governmental agency;
- B. Capital improvement projects of a governmental agency;
- C. The maintenance or repair of public properties;
- D. Public safety personnel in the course of executing their official duties, including, but not limited to, sworn peace officers, emergency personnel and public utility personnel. This exemption includes, without limitation, sound emanating from all equipment used by such personnel, whether stationary or mobile;
- E. Public or private schools and school-sponsored activities;
- F. Agricultural operations on land designated "Agriculture" in the Riverside County general plan, or land zoned A-I (light agriculture), A-P (light agriculture with poultry), A-2 (heavy agriculture), A-D (agriculture-dairy) or C/V (citrus/vineyard), provided such operations are carried out in a manner consistent with accepted industry standards. This exemption includes, without limitation, sound emanating from all equipment used during such operations, whether stationary or mobile;
- G. Wind energy conversion systems (WECS), provided such systems comply with the WECS noise provisions of Riverside County Ordinance No. 348;
- H. Private construction projects located one-quarter of a mile or more from an inhabited dwelling;
- I. Private construction projects located within one-quarter of a mile from an inhabited dwelling, provided that:

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- 1. Construction does not occur between the hours of six p.m. and six a.m. during the months of June through September, and
- 2. Construction does not occur between the hours of six p.m. and seven a.m. during the months of October through May;
- J. Property maintenance, including, but not limited to, the operation of lawnmowers, leaf blowers, etc., provided such maintenance occurs between the hours of seven a.m. and eight p.m.;
- K. Motor vehicles, other than off-highway vehicles. This exemption does not include sound emanating from motor vehicle sound systems;
- L. Heating and air conditioning equipment;
- M. Safety, warning and alarm devices, including, but not limited to, house and car alarms, and other warning devices that are designed to protect the public health, safety, and welfare;
- N. The discharge of firearms consistent with all state laws.

(Ord. 847 § 2, 2006)

9.52.030 - Definitions.

As used in this chapter, the following terms shall have the following meanings:

"Audio equipment" means a television, stereo, radio, tape player, compact disc player, mp3 player, l-POD or other similar device.

"Decibel (dB)" means a unit for measuring the relative amplitude of a sound equal approximately to the smallest difference normally detectable by the human ear, the range of which includes approximately one hundred thirty (130) decibels on a scale beginning with zero decibels for the faintest detectable sound. Decibels are measured with a sound level meter using different methodologies as defined below:

- 1. "A-weighting (dBA)" means the standard A-weighted frequency response of a sound level meter, which de-emphasizes low and high frequencies of sound in a manner similar to the human ear for moderate sounds.
- 2. "Maximum sound level (L $_{\rm max}$)" means the maximum sound level measured on a sound level meter.

"Governmental agency" means the United States, the state of California, Riverside County, any city within Riverside County, any special district within Riverside County or any combination of these agencies.

"Land use permit" means a discretionary permit issued by Riverside County pursuant to Riverside County Ordinance No. 348.

"Motor vehicle" means a vehicle that is self-propelled.

"Motor vehicle sound system" means a stereo, radio, tape player, compact disc player, mp3 player, I-POD or other similar device.

"Noise" means any loud, discordant or disagreeable sound.

"Occupied property" means property upon which is located a residence, business or industrial or manufacturing use.

"Off-highway vehicle" means a motor vehicle designed to travel over any terrain.

"Public or private school" means an institution conducting academic instruction at the preschool, elementary school, junior high school, high school, or college level.

"Public property" means property owned by a governmental agency or held open to the public, including, but not limited to, parks, streets, sidewalks, and alleys.

"Sensitive receptor" means a land use that is identified as sensitive to noise in the noise element of the Riverside County general plan, including, but not limited to, residences, schools, hospitals, churches, rest homes, cemeteries or public libraries.

"Sound-amplifying equipment" means a loudspeaker, microphone, megaphone or other similar device.

"Sound level meter" means an instrument meeting the standards of the American National Standards Institute for Type 1 or Type 2 sound level meters or an instrument that provides equivalent data.

(Ord. 847 § 3, 2006)

9.52.040 - General sound level standards.

No person shall create any sound, or allow the creation of any sound, on any property that causes the exterior sound level on any other occupied property to exceed the sound level standards set forth in Table 1.

TABLE 1
Sound Level Standards (Db L _{max})

GENERAL PLAN	GENERAL	GENERAL	DENSITY	MAXIMUM DECIBEL			
FOUNDATION	PLAN LAND	PLAN LAND		LEVEL			
COMPONENT	USE	USE					
	DESIGNATION	DESIGNATION					
		NAME					
65							

				7 am—10 pm	10 pm—7 am
Community Development	EDR	Estate Density Residential	2 AC	55	45
	VLDR	Very Low Density Residential	1 AC	55	45
	LDR	Low Density Residential	1/2 AC	55	45
	MDR	Medium Density Residential	2—5	55	45
	MHDR	Medium High Density Residential	5—8	55	45
	HDR	High Density Residential	8—14	55	45
	VHDR	Very High Density Residential	14—20	55	45
	H'TDR	Highest Density Residential	20+	55	45
	CR	Retail Commercial		65	55

	СО	Office Commercial		65	55
	СТ	Tourist Commercial		65	55
	СС	Community Center		65	55
	LI	Light Industrial		75	55
	н	Heavy Industrial		75	75
	ВР	Business Park		65	45
	PF	Public Facility		65	45
	SP	Specific Plan- Residential		55	45
		Specific Plan- Commercial		65	55
		Specific Plan- Light Industrial		75	55
		Specific Plan- Heavy Industrial		75	75
Rural Community	EDR	Estate Density Residential	2 AC	55	45
		67			

	VLDR	Very Low Density Residential	1 AC	55	45
	LDR	Low Density Residential	1/2 AC	55	45
Rural	RR	Rural Residential	5 AC	45	45
	RM	Rural Mountainous	10 AC	45	45
	RD	Rural Desert	10 AC	45	45
Agriculture	AG	Agriculture	10 AC	45	45
Open Space	С	Conservation		45	45
	СН	Conservation Habitat		45	45
	REC	Recreation		45	45
	RUR	Rural	20 AC	45	45
	W	Watershed		45	45
	MR	Mineral Resources		75	45

(Ord. 847 § 4, 2006)

9.52.050 - Sound level measurement methodology.

Sound level measurements may be made anywhere within the boundaries of an occupied property. The actual location of a sound level measurement shall be at the discretion of the enforcement officials identified in <u>Section 9.52.080</u> of this chapter. Sound level measurements shall be made with a sound level meter. Immediately before a measurement is made, the sound level meter shall be calibrated utilizing an acoustical calibrator meeting the standards of the American National Standards Institute. Following a sound level measurement, the calibration of the sound level meter shall be re-verified. Sound level meters and calibration equipment shall be certified annually.

(Ord. 847 § 5, 2006)

9.52.060 - Special sound sources standards.

The general sound level standards set forth in <u>Section 9.52.040</u> of this chapter apply to sound emanating from all sources, including the following special sound sources, and the person creating, or allowing the creation of, the sound is subject to the requirements of that section. The following special sound sources are also subject to the following additional standards, the failure to comply with which constitutes separate violations of this chapter:

A. Motor Vehicles.

- 1. Off-Highway Vehicles.
 - a. No person shall operate an off-highway vehicle unless it is equipped with a USDA-qualified spark arrester and a constantly operating and properly maintained muffler. A muffler is not considered constantly operating and properly maintained if it is equipped with a cutout, bypass or similar device.
 - b. No person shall operate an off-highway vehicle unless the noise emitted by the vehicle is not more than ninety-six (96) dBA if the vehicle was manufactured on or after January 1, 1986 or is not more than one hundred one (101) dBA if the vehicle was manufactured before January 1, 1986. For purposes of this subsection, emitted noise shall be measured a distance of twenty (20) inches from the vehicle tailpipe using test procedures established by the Society of Automotive Engineers under Standard J-1287.
- 2. Sound Systems. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, between the hours of ten p.m. and eight a.m., such that the sound system is audible to the human ear inside any inhabited dwelling. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, at any other time such that the sound system is audible to the human ear at a distance greater than one hundred (100) feet from the vehicle.
- B. Power Tools and Equipment. No person shall operate any power tools or equipment between the hours of ten p.m. and eight a.m. such that the power tools or equipment 69

- are audible to the human ear inside an inhabited dwelling other than a dwelling in which the power tools or equipment may be located. No person shall operate any power tools or equipment at any other time such that the power tools or equipment are audible to the human ear at a distance greater than one hundred (100) feet from the power tools or equipment.
- C. Audio Equipment. No person shall operate any audio equipment, whether portable or not, between the hours of ten p.m. and eight a.m. such that the equipment is audible to the human ear inside an inhabited dwelling other than a dwelling in which the equipment may be located. No person shall operate any audio equipment, whether portable or not, at any other time such that the equipment is audible to the human ear at a distance greater than one hundred (100) feet from the equipment.
- D. Sound-Amplifying Equipment and Live Music. No person shall install, use or operate sound-amplifying equipment, or perform, or allow to be performed, live music unless such activities comply with the following requirements. To the extent that these requirements conflict with any conditions of approval attached to an underlying land use permit, these requirements shall control:
 - 1. Sound-amplifying equipment or live music is prohibited between the hours of ten p.m. and eight a.m.
 - 2. Sound emanating from sound-amplifying equipment or live music at any other time shall not be audible to the human ear at a distance greater than two hundred (200) feet from the equipment or music.

(Ord. 847 § 6, 2006)

9.52.070 - Exceptions.

Exceptions may be requested from the standards set forth in <u>Section 9.52.040</u> or <u>9.52.060</u> of this chapter and may be characterized as construction-related, single-event or continuous-events exceptions.

A. Application and Processing.

- Construction-Related Exceptions. An application for a construction-related
 exception shall be made to and considered by the director of building and safety
 on forms provided by the building and safety department and shall be
 accompanied by the appropriate filing fee. No public hearing is required.
- Single-Event Exceptions. An application for a single-event exception shall be made to and considered by the planning director on forms provided by the planning department and shall be accompanied by the appropriate filing fee. No public hearing is required.
- 3. Continuous-Events Exceptions. An application for a continuous-events exception

shall be made to the planning director on forms provided by the planning department and shall be accompanied by the appropriate filing fee. Upon receipt of an application for a continuous-events exception, the planning director shall set the matter for public hearing before the planning commission, notice of which shall be given as provided in Section 18.26c of Riverside County Ordinance No. 348. Notwithstanding the above, an application for a continuous-events exception that is associated with an application for a land use permit shall be processed concurrently with the land use permit in the same manner that the land use permit is required to be processed.

- B. Requirements for Approval. The appropriate decisionmaking body or officer shall not approve an exception application unless the applicant demonstrates that the activities described in the application would not be detrimental to the health, safety or general welfare of the community. In determining whether activities are detrimental to the health, safety or general welfare of the community, the appropriate decisionmaking body or officer shall consider such factors as the proposed duration of the activities and their location in relation to sensitive receptors. If an exception application is approved, reasonable conditions may be imposed to minimize the public detriment, including, but not limited to, restrictions on sound level, sound duration and operating hours.
- C. Appeals. The director of building and safety's decision on an application for a construction-related exception is considered final. The planning director's decision on an application for a single-event exception is considered final. After making a decision on an application for a continuous-events exception, the appropriate decisionmaking body or officer shall mail notice of the decision to the applicant. Within ten (10) calendar days after the mailing of such notice, the applicant or an interested person may appeal the decision to the board of supervisors. Upon receipt of an appeal and payment of the appropriate appeal fee, the clerk of the board shall set the matter for hearing not less than five days nor more than thirty (30) days thereafter and shall give written notice of the hearing in the same manner as notice of the hearing was given by the appropriate hearing officer or body. The board of supervisors shall render its decision within thirty (30) days after the appeal hearing is closed.
- D. Effect of a Pending Continuous-Events Exception Application. For a period of one hundred eighty (180) days from the effective date of this chapter, no person creating any sound prohibited by this chapter shall be considered in violation of this chapter if the sound is related to a use that is operating pursuant to an approved land use permit, if an application for a continuous-events exception has been filed to sanction the sound and if a decision on the application is pending.

(Ord. 847 § 7, 2006)

9.52.080 - Enforcement.

The Riverside County sheriff and code enforcement shall have the primary responsibility for enforcing this chapter; provided, however, the sheriff and code enforcement may be assisted by the public health department. Violations shall be prosecuted as described in <u>Section 9.52.100</u> of this chapter, but nothing in this chapter shall prevent the sheriff, code enforcement or the department of public health from engaging in efforts to obtain voluntary compliance by means of warnings, notices, or educational programs.

(Ord. 847.1 § 1, 2007: Ord. 847 § 8, 2006)

9.52.090 - Duty to cooperate.

No person shall refuse to cooperate with, or obstruct, the enforcement officials identified in <u>Section 9.52.080</u> of this chapter when they are engaged in the process of enforcing the provisions of this chapter. This duty to cooperate may require a person to extinguish a sound source so that it can be determined whether sound emanating from the source violates the provisions of this chapter.

(Ord. 847 § 9, 2006)

9.52.100 - Violations and penalties.

Any person who violates any provision of this chapter once or twice within a one hundred eighty (180) day period shall be guilty of an infraction. Any person who violates any provision of this chapter more than twice within a one hundred eighty (180) day period shall be guilty of a misdemeanor. Each day a violation is committed or permitted to continue shall constitute a separate offense and shall be punishable as such. Penalties shall not exceed the following amounts:

- A. For the first violation within a one hundred eighty (180) day period, the minimum mandatory fine shall be five hundred dollars (\$500.00).
- B. For the second violation within a one hundred eighty (180) day period, the minimum mandatory fine shall be seven hundred fifty dollars (\$750.00).
- C. For any further violations within a one hundred eighty (180) day period, the minimum mandatory fine shall be one thousand dollars (\$1,000.00) or imprisonment in the county jail for a period not exceeding six months, or both.

(Ord. 847 § 10, 2006)

APPENDIX 5.1:

STUDY AREA PHOTOS





JN: 14231 Study Area Photos



L1_E 33, 50' 17.780000"117, 14' 47.060000"



L1_N 33, 50' 17.810000"117, 14' 47.090000"



33, 50' 17.780000"117, 14' 47.090000"



L1_W 33, 50' 17.770000"117, 14' 47.090000"



L2_E 33, 50' 15.070000"117, 15' 13.900000"



L2_N 33, 50' 15.070000"117, 15' 13.900000"

JN: 14231 Study Area Photos



L2_S 33, 50' 15.070000"117, 15' 13.900000"



L2_W 33, 50' 15.070000"117, 15' 13.900000"



33, 50' 19.430000"117, 15' 5.690000"



L3_N 33, 50' 19.430000"117, 15' 5.690000"



L3_S 33, 50' 19.440000"117, 15' 5.690000"



L3_W 33, 50' 19.410000"117, 15' 5.660000"

JN: 14231 Study Area Photos



L4_E 33, 50' 24.100000"117, 15' 6.480000"



L4_N 33, 50' 24.100000"117, 15' 6.480000"



33, 50' 24.100000"117, 15' 6.480000"



L4_W 33, 50' 24.100000"117, 15' 6.480000"



APPENDIX 5.2:

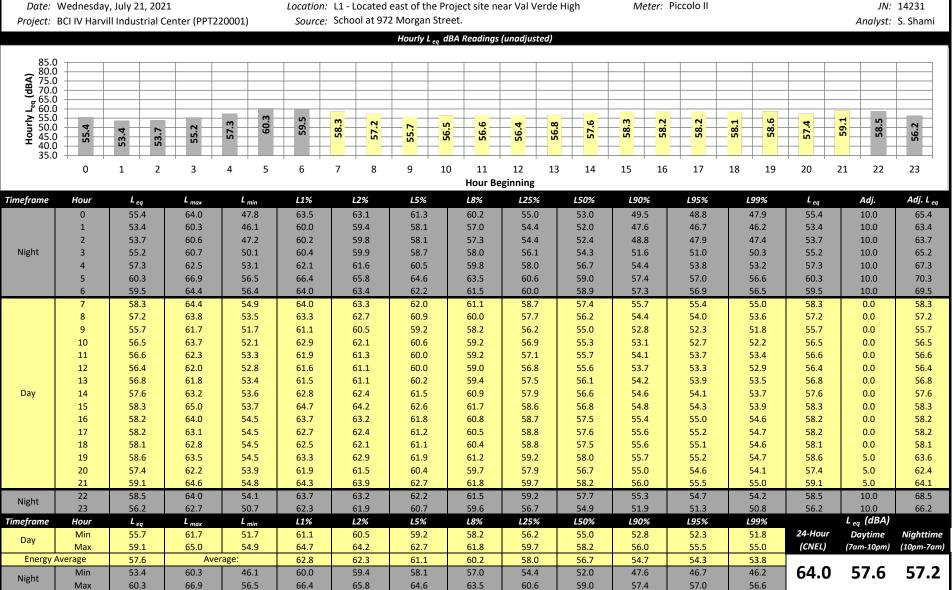
NOISE LEVEL MEASUREMENT WORKSHEETS





24-Hour Noise Level Measurement Summary

Date: Wednesday, July 21, 2021 Location: L1 - Located east of the Project site near Val Verde High Meter: Piccolo II





59.8

57.1

55.4

52.6

52.0

51.5

Average:

62.5

62.0

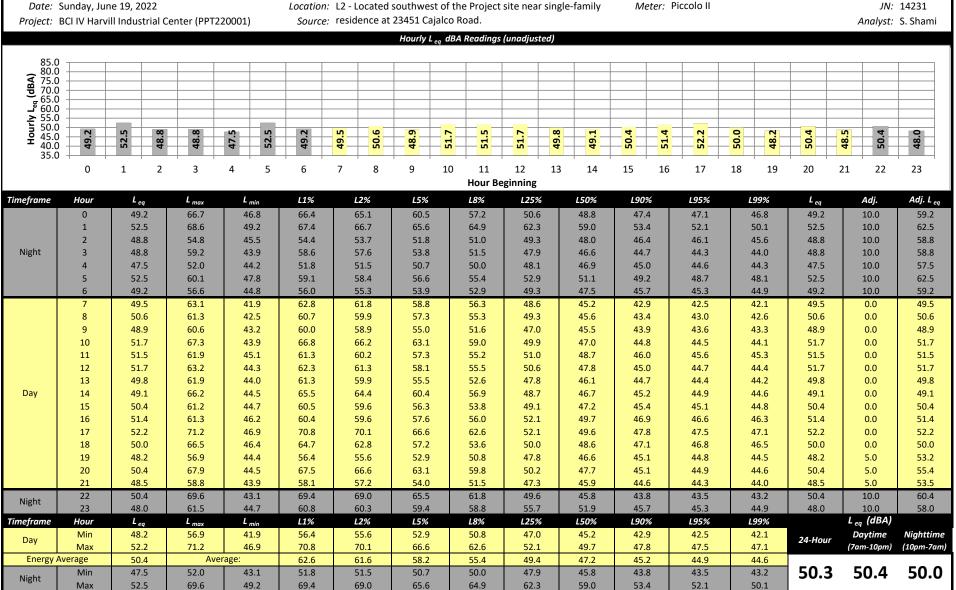
60.7

57.2

Energy Average

24-Hour Noise Level Measurement Summary

Date: Sunday, June 19, 2022 Location: L2 - Located southwest of the Project site near single-family Meter: Piccolo II





55.9

51.7

49.5

46.8

46.4

45.8

Average:

60.4

59.7

57.5

50.0

Energy Average

24-Hour Noise Level Measurement Summary Date: Sunday, June 19, 2022 Meter: Piccolo II JN: 14231 Location: L3 - Located at the western site boundary. Project: BCI IV Harvill Industrial Center (PPT220001) Source: Analyst: S. Shami Hourly Lea dBA Readings (unadjusted) 80.0 (dBA) 75.0 70.0 65.0 **-** 60.0 Form 45.0 63. 63. 58.0 62. 61. 62 62. 59. 40.0 35.0 2 7 0 1 3 5 6 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 **Hour Beginning Timeframe** Hour L_{eq} L1% L2% L5% L8% L25% L50% L90% L95% L99% L_{eq} Adj. Adj. L eq L max L min 0 59.8 69.1 53.2 68.8 68.3 66.2 64.5 59.0 56.3 53.9 53.6 53.3 59.8 10.0 69.8 1 58.1 67.5 51.4 64.1 62.1 51.5 58.1 10.0 68.1 67.2 66.6 57.5 55.2 52.5 52.0 2 49.4 49.5 58.8 58.8 69.4 69.0 68.3 65.8 64.0 57.2 53.9 50.6 50.1 10.0 68.8 Night 3 57.7 67.5 49.4 67.1 66.7 64.6 62.5 56.6 53.7 50.5 50.0 49.5 57.7 10.0 67.7 4 55.8 69.4 49.5 68.9 68.0 65.5 63.3 55.8 53.2 50.6 50.1 49.6 55.8 10.0 65.8 5 58.2 66.9 50.9 66.6 66.1 64.6 63.2 57.5 55.1 52.0 51.4 51.1 58.2 10.0 68.2 6 59.1 68.5 50.6 68.1 65.9 64.5 58.1 51.6 51.2 50.8 59.1 10.0 69.1 67.6 54.5 59.3 68.9 49.5 68.5 68.0 66.1 64.4 58.9 54.3 50.8 50.1 49.7 59.3 0.0 59.3 8 59.7 69.9 49.9 69.5 68.9 66.6 65.2 58.9 54.3 50.8 50.4 50.0 59.7 0.0 59.7 9 71.0 70.7 70.2 68.3 66.8 52.6 51.7 61.7 0.0 61.7 51.5 61.9 57.6 52.1 61.7 10 67.5 61.3 69.8 51.9 69.5 69.0 66.4 62.0 57.1 52.8 52.4 52.1 61.3 0.0 61.3 11 61.8 72.1 53.2 68.6 66.9 58.3 53.4 61.8 0.0 71.8 71.0 62.5 54.4 54.0 61.8 12 62.2 72.0 52.6 71.6 70.9 68.5 67.0 62.4 57.8 53.6 53.1 52.8 62.2 0.0 62.2 13 70.6 62.5 53.2 70.2 69.7 68.2 67.3 59.2 54.2 53.7 53.4 62.5 0.0 62.5 63.4 Dav 14 62.5 75.8 52.9 75.3 74.4 72.2 69.6 63.5 59.2 54.0 53.5 53.0 62.5 0.0 62.5 15 62.5 72.1 52.1 71.7 71.0 68.9 67.6 62.7 57.9 53.1 52.6 52.2 62.5 0.0 62.5 62.5 73.1 53.7 62.5 16 53.6 72.9 72.1 69.3 67.8 63.0 58.5 54.8 54.2 0.0 62.5 17 63.4 72.7 55.3 72.5 72.0 70.4 69.0 64.2 55.4 63.4 0.0 60.1 56.2 55.8 63.4 18 63.3 72.9 55.6 72.1 71.5 69.9 68.6 63.5 59.8 56.6 56.2 55.7 63.3 0.0 63.3 19 63.5 72.3 55.4 71.9 71.5 69.8 68.5 63.8 59.9 56.3 55.9 55.5 63.5 5.0 68.5 20 67.7 55.4 62.9 67.9 62.9 70.8 55.2 70.6 70.2 68.8 63.3 59.7 56.2 55.8 5.0 21 61.7 71.3 54.8 71.0 70.7 69.6 67.7 62.2 58.5 55.6 55.2 54.9 61.7 5.0 66.7 10.0 22 60.5 74.6 53.1 74.3 73.7 71.2 68.8 57.1 54.0 53.6 53.2 60.5 70.5 60.7 Night 23 58.0 66.6 51.3 66.3 65.9 64.3 62.8 57.7 54.7 52.2 51.8 51.4 58.0 10.0 68.0 L eq (dBA) L2% L5% L8% L25% L90% L95% L99% Timeframe Hour L ea L max L min L1% L50% Daytime Min 59.3 68.9 49.5 68.5 68.0 66.1 64.4 58.9 54.3 50.8 50.1 49.7 Nighttime 24-Hour Dav 69.6 55.7 Max 63.5 75.8 55.6 75.3 74.4 72.2 64.2 60.1 56.6 56.2 (7am-10pm) (10pm-7am) **Energy Average** 62.2 Average: 71.3 70.7 68.8 67.4 62.4 58.1 54.1 53.7 53.2 61.2 62.2 58.6 55.8 49.5 Min 66.6 49.4 66.3 65.9 64.1 62.1 55.8 53.2 50.5 50.0 Night Max 60.5 74.6 53.2 74.3 73.7 71.2 68.8 60.7 57.1 54.0 53.6 53.3



64.0

57.8

54.9

52.0

51.5

51.1

Average:

68.5

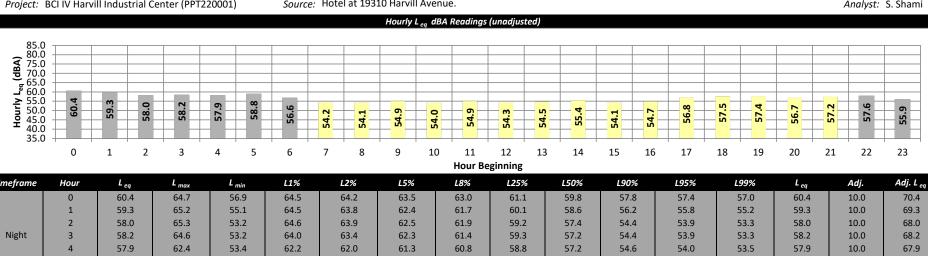
67.9

65.8

58.6

Energy Average

Date: Sunday, June 19, 2022 Project: BCI IV Harvill Industrial Center (PPT220001) Location: L4 - Located north of the Project site near Marriot Fairfield Source: Hotel at 19310 Harvill Avenue. Hourly Leg dBA Readings (unadjusted) Meter: Piccolo II JN: 14231 Analyst: S. Shami



Timeframe	Hour	L_{eq}	L max	L _{min}	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	L_{eq}	Adj.	Adj. L _{eq}
	0	60.4	64.7	56.9	64.5	64.2	63.5	63.0	61.1	59.8	57.8	57.4	57.0	60.4	10.0	70.4
	1	59.3	65.2	55.1	64.5	63.8	62.4	61.7	60.1	58.6	56.2	55.8	55.2	59.3	10.0	69.3
	2	58.0	65.3	53.2	64.6	63.9	62.5	61.9	59.2	57.4	54.4	53.9	53.3	58.0	10.0	68.0
Night	3	58.2	64.6	53.2	64.0	63.4	62.3	61.4	59.3	57.2	54.4	53.9	53.3	58.2	10.0	68.2
	4	57.9	62.4	53.4	62.2	62.0	61.3	60.8	58.8	57.2	54.6	54.0	53.5	57.9	10.0	67.9
	5	58.8	65.2	54.6	64.9	64.7	63.9	63.1	59.6	58.1	55.6	55.1	54.7	58.8	10.0	68.8
	6	56.6	59.8	53.3	59.7	59.5	59.1	58.7	57.4	56.2	54.1	53.8	53.4	56.6	10.0	66.6
	7	54.2	58.6	50.5	58.3	58.1	57.6	57.1	55.0	53.4	51.4	51.0	50.6	54.2	0.0	54.2
	8	54.1	58.9	50.6	58.7	58.4	57.6	56.9	54.8	53.3	51.4	51.1	50.7	54.1	0.0	54.1
	9	54.9	59.6	51.5	59.3	59.0	58.2	57.5	55.5	54.2	52.3	51.9	51.6	54.9	0.0	54.9
	10	54.0	58.7	51.3	58.2	57.8	56.9	56.3	54.5	53.4	52.0	51.7	51.4	54.0	0.0	54.0
	11	54.9	60.6	51.7	60.2	59.8	58.6	57.6	55.3	53.8	52.3	52.1	51.8	54.9	0.0	54.9
	12	54.3	58.7	51.6	58.4	58.0	57.2	56.5	54.8	53.6	52.2	51.9	51.7	54.3	0.0	54.3
	13	54.5	58.7	52.0	58.3	58.0	57.1	56.6	55.1	54.0	52.6	52.3	52.0	54.5	0.0	54.5
Day	14	55.4	62.3	51.6	61.8	61.3	60.0	58.7	55.5	53.9	52.3	52.0	51.7	55.4	0.0	55.4
	15	54.1	58.3	51.4	58.0	57.7	57.0	56.3	54.7	53.6	52.1	51.8	51.5	54.1	0.0	54.1
	16	54.7	59.9	52.3	59.5	59.1	57.8	56.9	55.0	54.1	52.9	52.6	52.4	54.7	0.0	54.7
	17	56.8	63.4	53.6	63.0	62.5	61.0	59.4	57.0	55.7	54.2	54.0	53.7	56.8	0.0	56.8
	18	57.5	66.1	54.5	64.6	63.9	60.8	59.2	57.4	56.5	55.1	54.9	54.6	57.5	0.0	57.5
	19	57.4	61.8	55.1	61.5	61.1	60.1	59.5	57.8	56.8	55.6	55.4	55.1	57.4	5.0	62.4
	20	56.7	59.7	54.4	59.4	59.2	58.8	58.5	57.3	56.3	55.0	54.8	54.5	56.7	5.0	61.7
	21	57.2	62.0	54.5	61.8	61.4	60.6	59.9	57.4	56.5	55.1	54.8	54.6	57.2	5.0	62.2
Night	22	57.6	63.6	53.8	63.3	62.9	62.1	61.5	57.5	56.0	54.5	54.2	53.9	57.6	10.0	67.6
Ť	23	55.9	60.0	53.1	59.8	59.5	59.0	58.5	56.5	55.4	53.7	53.4	53.1	55.9	10.0	65.9
Timeframe	Hour	L _{eq}	L max	L _{min}	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%		L _{eq} (dBA)	
Day	Min	54.0	58.3	50.5	58.0	57.7	56.9	56.3	54.5	53.3	51.4	51.0	50.6	24-Hour	Daytime	Nighttime
Í	Max	57.5	66.1	55.1	64.6	63.9	61.0	59.9	57.8	56.8	55.6	55.4	55.1		(7am-10pm)	(10pm-7am)
Energy A		55.6		rage:	60.1	59.7	58.6	57.8	55.8	54.6	53.1	52.8	52.5	FC 0	FF 6	F0 2
Night	Min	55.9	59.8	53.1	59.7	59.5	59.0	58.5	56.5	55.4	53.7	53.4	53.1	56.8	55.6	58.3
•	Max	60.4	65.3	56.9	64.9	64.7	63.9	63.1	61.1	59.8	57.8	57.4	57.0			
Energy A	Average	58.3	Aver	rage:	63.0	62.7	61.8	61.2	58.8	57.3	55.1	54.6	54.2			

APPENDIX 7.1:

OFF-SITE TRAFFIC NOISE LEVEL CALCULATIONS





	FHWA-RD	-77-108 HIGH	WAY	NOISE I	PREDIC	CTION M	ODEL	(9/12/20	021)		
Scenario Road Name Road Segmen	e: Harvill Av.	Exwy.					Name: umber:		Harvill Ind	ustrial C	Ce
	SPECIFIC IN	PUT DATA							L INPUT	s	
Highway Data	-			S	ite Cor	ditions	(Hara =				
Average Daily	. ,	10,869 vehicle	es					Autos:			
	Percentage:	6.14%				edium Tru		,			
	our Volume:	667 vehicles	3		He	eavy Truc	cks (3+	Axles):	15		
	nicle Speed:	50 mph		ν	ehicle	Mix					
Near/Far Lar	ne Distance:	48 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data							Autos:	71.9%	12.2%	15.99	6 95.34%
Ran	rier Height:	0.0 feet			М	edium Ti	rucks:	75.3%	7.0%	17.79	6 1.76%
Barrier Type (0-Wa	all, 1-Berm):	0.0				Heavy Tr	rucks:	60.4%	12.0%	27.69	6 2.90%
Centerline Dis		59.0 feet		Ν	loise S	ource El	evation	ns (in fe	eet)		
Centerline Dist. t		59.0 feet				Autos	s: 0	.000			
Barrier Distance t	o Observer:	0.0 feet			Mediu	m Trucks	s: 2	.297			
Observer Height (/		5.0 feet			Hear	vy Trucks	s: 8	.004	Grade Ad	justmen	t: 0.0
	d Elevation:	0.0 feet									
	d Elevation:	0.0 feet		L	ane Eq	uivalent			feet)		
F	Road Grade:	0.0%				Autos		.129			
	Left View:	-90.0 degree				m Trucks		1.966			
	Right View:	90.0 degree	es		Hea	vy Trucks	s: 53	3.982			
FHWA Noise Mode	l Calculations	3									
VehicleType	REMEL	Traffic Flow	Dis	tance		Road	Fres		Barrier Att	en Be	rm Atten
Autos:	70.20	-4.26		-0.62		-1.20		-4.69	0.0	000	0.000
Medium Trucks:	81.00	-21.59		-0.60		-1.20		-4.88	0.0	000	0.000
Heavy Trucks:	85.38	-19.43		-0.60		-1.20		-5.35	0.	000	0.000
Unmitigated Noise			_							_	
	Leq Peak Hou		_	Leq Ev			Night		Ldn	_	NEL
Autos:	64.		64.0		62.3		58.		66.	-	66.7
Medium Trucks:	57.		57.7		53.4		52.		60.		60.3
Heavy Trucks:_ Vehicle Noise:	64. 67.		63.3 67.2		62.3 65.6		61.		67. 70.	-	68.2 70.9
Centerline Distanc	e to Noise Co	ntour (in feet)								
zztoriirio ziotario	5 .10.00 00	(70 d	BA	65 (dBA	6	60 dBA	5	5 dBA
			Ldn:		64		139	9	299)	645
		CI	VEL:		68		14	7	316	6	681

	FHWA-R	D - //-108	HIGHWA	TNOISE	PREDIC	TION	MODEL	(9/12/2	021)		
	: EAP 2024								Harvill Ind	ustrial C	е
Road Name Road Segmen	e: Harvill Av.	- Front				JOD I	lumber:	14231			
	SPECIFIC II	NPUT DA	ATA		Site Con				L INPUT	S	
Highway Data					Site Con	aitions	(Hara				
Average Daily	. ,	11,431 \	ehicles					Autos:			
Peak Hour I		6.14%						Axles):			
	our Volume:	702 ve			He	avy iru	icks (3+	Axles):	15		
	nicle Speed:	50 m		Ī	Vehicle	Mix					
Near/Far Lar	e Distance:	48 fe	et	Ī	Veh	icleType	9	Day	Evening	Night	Daily
Site Data							Autos:	71.9%	12.2%	15.9%	95.259
Bar	rier Heiaht:	0.0 f	eet		М	edium 7	rucks:	75.3%	7.0%	17.7%	1.779
Barrier Type (0-Wa	all, 1-Berm):	0.0				Heavy 7	rucks:	60.4%	12.0%	27.6%	2.989
Centerline Dis		59.0 f		ı	Noise S	ource E	levatio	ns (in fe	eet)		
Centerline Dist. t		59.0 f		ı		Auto	s: (0.000			
Barrier Distance t		0.0 f	eet		Mediu	m Truck		2.297			
Observer Height (/		5.0 f	eet			/y Truck		3.004	Grade Ad	justment	0.0
	d Elevation:	0.0 f				•					
	d Elevation:	0.0 f	eet		Lane Eq			_ •	feet)		
F	Road Grade:	0.0%				Auto		1.129			
	Left View:		legrees			m Truck		3.966			
	Right View:	90.0 d	legrees		Hea	ry Truck	(s: 53	3.982			
FHWA Noise Mode											
VehicleType	REMEL	Traffic F		istance		Road	Fres		Barrier Att		m Atten
Autos:	70.20		-4.04	-0.6		-1.20		-4.69		000	0.00
Medium Trucks:	81.00	-	21.35	-0.6	-	-1.20		-4.88		000	0.00
Heavy Trucks:	85.38		19.09	-0.6		-1.20		-5.35	0.0	000	0.00
Unmitigated Noise				_				_			
	Leq Peak Ho		q Day	<u> </u>	vening		Night		Ldn		NEL
Autos:	-	1.3	64.2		62.6		58		66.5	-	67.
Medium Trucks:		7.8	57.9		53.6		52		60.3	-	60.
Heavy Trucks:		1.5	63.6		62.6		61		68.2		68.
Vehicle Noise:	67	7.9	67.5)	65.9		63	.8	70.9	9	71.
Centerline Distanc	e to Noise C	ontour (ir	r feet)	70	-/0.4	-	-10.4	1 .	20 404		-10.4
			1 -1		dBA	65	dBA		60 dBA		dBA
			Ldn. CNFL		67 71		14 15		313 330		674 712

Scenario Road Name Road Segment		Exwv.				Project N Job Nu			Harvill Ind	ustrial Co	Э
SITE S	PECIFIC IN	PUT DATA				NC	DISE N	IODE	L INPUT	s	
Highway Data				S	ite Con	ditions (F	lard =	10, Sc	ft = 15)		
Average Daily T	raffic (Adt):	11,308 vehicles	3					Autos:	15		
Peak Hour F	Percentage:	6.14%			Me	dium Truc	ks (2 A	(xles):	15		
Peak Ho	ur Volume:	694 vehicles			He	avy Truck	s (3+ A	xles):	15		
Veh	icle Speed:	50 mph		1	ehicle I	Miss					
Near/Far Lan	e Distance:	48 feet		V		icleType		Dav	Evening	Night	Dailv
Site Data					* 0			71.9%		15.9%	. ,
	ier Height:	0.0 feet			Ме	edium Tru		75.3%		17.7%	
Barrier Type (0-Wa	-	0.0 reet			F	leavy Tru		60.4%		27.6%	
Centerline Dist	. ,	59.0 feet									
Centerline Dist. to		59.0 feet		٨	loise So	ource Ele			et)		
Barrier Distance to		0.0 feet				Autos:		000			
Observer Height (A		5.0 feet				m Trucks:		297			
	d Elevation:	0.0 feet			Heav	y Trucks:	8.0	004	Grade Ad	iustment	: 0.0
	d Elevation:	0.0 feet		L	ane Eau	uivalent L	Distano	e (in t	feet)		
R	oad Grade:	0.0%				Autos:	54.	129	,		
	Left View:	-90.0 degrees			Mediur	m Trucks:	53.	966			
	Right View:	90.0 degrees			Heav	y Trucks:	53.	982			
FHWA Noise Model	Calculations	·									
VehicleType	REMEL	Traffic Flow	Dis	tance	Finite	Road	Fresn	el	Barrier Att	en Ber	m Atter
Autos:	70.20	-4.09		-0.62		-1.20		-4.69	0.0	000	0.0
Medium Trucks:	81.00	-21.42		-0.60		-1.20		-4.88	0.0	000	0.00
Heavy Trucks:	85.38	-19.26		-0.60		-1.20		-5.35	0.0	000	0.00
Unmitigated Noise	Levels (witho	ut Topo and b	arrie	r attenu	iation)						
VehicleType L	Leq Peak Hou	r Leq Day		Leq Ev	ening	Leq N	ight		Ldn	C	NEL
Autos:	64.	3 6	4.2		62.5		58.9)	66.5	5	66
Medium Trucks:	57.	8 5	7.9		53.6		52.8	}	60.2	2	60
Heavy Trucks:	64.		3.5		62.4		61.3	ļ.	68.		68
Vehicle Noise:	67.	8 6	7.4		65.8		63.6	i	70.8	3	71
Centerline Distance	to Noise Co	ntour (in feet)									
			. L	70 d		65 dl		6	i0 dBA		dBA
		_	dn:		66		143		307		66
		CN	EL:		70		151		325		69

Wednesday, September 14, 2022

FHWA-RI	D-77-108 HIGHV	VAY NOI	SE PREDIC	CTION N	IODEL (9/12	/2021)	
Scenario: EAC 2024 Road Name: Harvill Av. Road Segment: n/o Cajalco	Exwy.				Name: BCI lumber: 142	IV Harvill Indus 31	strial Ce
SITE SPECIFIC IN	IPUT DATA			N	IOISE MOI	EL INPUTS	
Highway Data			Site Con	ditions	(Hard = 10,	Soft = 15)	
Average Daily Traffic (Adt): Peak Hour Percentage: Peak Hour Volume: Vehicle Speed:	25,731 vehicles 6.14% 1,580 vehicles	3			Auto ucks (2 Axle cks (3+ Axle	s): 15	
Near/Far Lane Distance:	50 mph		Vehicle	Mix			
Near/Far Lane Distance:	48 feet		Veh	icleType	Day	Evening I	Night Daily
Site Data	-			,	Autos: 71.9	9% 12.2%	15.9% 95.34%
Barrier Height:	0.0 feet		M	ledium T	rucks: 75.	3% 7.0%	17.7% 1.76%
Barrier Type (0-Wall, 1-Berm):	0.0		4	Heavy T	rucks: 60.4	1% 12.0%	27.6% 2.90%
Centerline Dist. to Barrier:	59.0 feet		Noise So	ource El	evations (in	feet)	
Centerline Dist. to Observer:	59.0 feet			Auto	-	,	
Barrier Distance to Observer:	0.0 feet		Mediu	m Truck	0.000		
Observer Height (Above Pad):	5.0 feet			vy Truck		Grade Adju	stment: 0.0
Pad Elevation:	0.0 feet		77001	vy mack	3. 0.007		
Road Elevation:	0.0 feet		Lane Eq		t Distance (i	n feet)	
Road Grade:	0.0%			Auto			
Left View:	-90.0 degrees	3		m Truck	00.000		
Right View:	90.0 degrees	3	Hear	vy Truck	s: 53.982		
FHWA Noise Model Calculation	s						
VehicleType REMEL	Traffic Flow	Distance	e Finite	Road	Fresnel	Barrier Atter	Berm Atten
Autos: 70.20	-0.52	-(0.62	-1.20	-4.6	9 0.00	0.000
Medium Trucks: 81.00	-17.85	-(0.60	-1.20	-4.8	0.00	0.000
Heavy Trucks: 85.38	-15.69	-(0.60	-1.20	-5.3	5 0.00	0.000
Unmitigated Noise Levels (with	out Topo and b	arrier att	tenuation)				
VehicleType Leq Peak Hot	ur Leq Day	Leg	Evening	Leq	Night	Ldn	CNEL
Autos: 67	7.9 6	7.8	66.1		62.5	70.0	70.5
Medium Trucks: 61	1.4 6	1.4	57.1		56.4	63.8	64.0
		7.0	66.0	1	64.9	71.6	71.9
Vehicle Noise: 71	1.3 7	0.9	69.3		67.2	74.3	74.7
Centerline Distance to Noise Co	ontour (in feet)						
			70 dBA	65	dBA	60 dBA	55 dBA
	_	dn:	115		247	532	1,145
	CN	EL:	121		261	562	1,210

	FHWA-RI	D-77-108 HIGH	IWAY	NOISE	PREDIC	TION N	IODEL (9/12/2	021)		
Road Nan	io: EAPC 2024 ne: Harvill Av. nt: n/o Cajalco						Name: lumber:		Harvill Ind	ustrial C	е
	SPECIFIC IN	NPUT DATA							L INPUT	s	
Highway Data					Site Cor	aitions					
Average Daily	Traffic (Adt):	25,854 vehicl	es					Autos:			
Peak Hour	Percentage:	6.14%					ucks (2)	,			
Peak F	lour Volume:	1,587 vehicle	S		He	avy Tru	cks (3+)	4xles):	15		
Ve	hicle Speed:	50 mph		T	Vehicle	Mix					
Near/Far La	ne Distance:	48 feet		ŀ		icleType		Day	Evening	Night	Daily
Site Data							Autos:	71.9%	12.2%	15.9%	95.30%
Ra	rrier Height:	0.0 feet			М	edium T	rucks:	75.3%	7.0%	17.7%	1.77%
Barrier Type (0-W		0.0				Heavy T	rucks:	60.4%	12.0%	27.6%	2.94%
Centerline Di	st. to Barrier:	59.0 feet			Noise S	ource F	levation	s (in fe	pet)		
Centerline Dist.	to Observer:	59.0 feet		H	140/36 01	Auto		000	,		
Barrier Distance	to Observer:	0.0 feet			Modiu	m Truck		297			
Observer Height	(Above Pad):	5.0 feet				vy Truck		004	Grade Ad	iustmen	- 0.0
P	ad Elevation:	0.0 feet								, ao amon	. 0.0
Ro	ad Elevation:	0.0 feet			Lane Eq	uivalen	t Distan	ce (in i	feet)		
	Road Grade:	0.0%				Auto		129			
	Left View:	-90.0 degre	es		Mediu	m Truck	s: 53.	966			
	Right View:	90.0 degre	es		Hea	y Truck	s: 53.	982			
FHWA Noise Mod	el Calculation	s		- 1							
VehicleType	REMEL	Traffic Flow		stance		Road	Fresr	_	Barrier Att		m Atten
Autos:	70.20			-0.6	_	-1.20		-4.69		000	0.000
Medium Trucks:				-0.6		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-15.61		-0.6	0	-1.20		-5.35	0.0	000	0.000
Unmitigated Nois			barri	er atter	nuation)					,	
VehicleType	Leq Peak Hou			Leq E	vening	Leq	Night		Ldn	_	NEL
Autos:		7.9	67.8		66.1		62.	-	70.	-	70.5
Medium Trucks:	-	1.4	61.5		57.2		56.4		63.8	-	64.1
Heavy Trucks:		3.0	67.1		66.1		65.0		71.		72.0
Vehicle Noise:	71	1.4	71.0		69.4		67.3	3	74.4	4	74.7
Centerline Distan	ce to Noise Co	ontour (in feet)					,		,	
			L	70	dBA	65	dBA	4 - 7	60 dBA		dBA
			Ldn:		115		249		536		1,154
		С	NEL:		122		263		566		1,219

	FHWA-RI	D-77-108 HIGH	WAY	NOISE	PREDIC	CTION N	MODEL (9/	12/20	21)	
	io: EA 2024 e: Harvill Av. nt: s/o Cajalco	Exwy.					t Name: B0 Number: 14		Harvill Indus	trial Ce
SITE	SPECIFIC IN	NPUT DATA					NOISE M	ODEL	INPUTS	
Highway Data				S	ite Cor	nditions	(Hard = 1	0, Soi	ft = 15)	
Peak H	Traffic (Adt): Percentage: our Volume: hicle Speed:	15,512 vehicl 6.14% 952 vehicle 50 mph			He	eavy Tru	Ai rucks (2 Ax icks (3+ Ax		15 15 15	
Near/Far Lai		48 feet		ν	'ehicle					
IVCal/I al Lal	ne Distance.	40 1661			Ver	nicleType	e D	ay	-	light Dail
Site Data Barrier Type (0-W	rier Height: 'all, 1-Berm):	0.0 feet 0.0				ledium 1 Heavy 1	rucks: 7	1.9% 5.3% 0.4%	7.0%	15.9% 95.34 17.7% 1.76 27.6% 2.90
Centerline Dis	st. to Barrier:	59.0 feet		^	loise S	nurce F	levations	(in fe	of)	
Roa	to Observer:	59.0 feet 0.0 feet 5.0 feet 0.0 feet 0.0 feet 0.0% -90.0 degre 90.0 degre		L	Hea ane Eq Mediu	Auto m Truck vy Truck nuivalen Auto m Truck vy Truck	ks: 2.29 ks: 8.00 ht Distance ps: 54.12 ks: 53.96	07 04 (in fe 29 66	Grade Adjus	tment: 0.0
FHWA Noise Mode	el Calculation	s								
VehicleType	REMEL	Traffic Flow	Dis	tance	Finite	Road	Fresne	l E	Barrier Atten	Berm Atte
Autos:	70.20	-2.71		-0.62	2	-1.20	-4	1.69	0.000	0.0
Medium Trucks:	81.00	-20.05		-0.60)	-1.20	-4	1.88	0.000	0.0
Heavy Trucks:	85.38	-17.88		-0.60)	-1.20	-4	5.35	0.000	0.0
Unmitigated Noise	Levels (with	out Topo and	barrie	r atteni	uation)					
VehicleType	Leq Peak Hou	ur Leq Day	V	Leq Ev	ening	Leq	Night		Ldn	CNEL
Autos:	65	5.7	65.6		63.9)	60.3		67.8	6
Medium Trucks:	59	9.2	59.3		54.9)	54.2		61.6	6
Heavy Trucks:	65	5.7	64.8		63.8	}	62.7		69.4	6
Vehicle Noise:	69	9.1	68.7		67.1		65.0		72.1	7:
Centerline Distanc	e to Noise C	ontour (in feet)							
				70 d	BA	65	dBA	60) dBA	55 dBA
			Ldn:		82		176		379	8
		С	NEL:		86		186		401	8

	FRWA-R	D-77-108 HIG	HWAY	NOISE	PREDIC	HON M	ODEL (9/12/2	021)		
Scenario Road Name Road Segmen	e: Harvill Av.	Exwv.					Name: umber:		Harvill Ind	ustrial C	е
		NPUT DATA				N	OISE	MODE	L INPUT	s	
Highway Data				5	Site Con	ditions (Hard =	10, S	oft = 15)		
Average Daily	raffic (Adt):	14,909 vehic	les					Autos:	15		
Peak Hour I	Percentage:	6.14%			Me	dium Tru	icks (2	Axles):	15		
Peak He	our Volume:	915 vehicle	es		He	avy Truc	ks (3+ .	Axles):	15		
Vel	icle Speed:	50 mph		1	/ehicle l	Miv					
Near/Far Lar	e Distance:	48 feet		Ľ.		icleType		Day	Evening	Night	Daily
Site Data							utos:	71.9%	-	15.9%	,
Bar	rier Heiaht:	0.0 feet			M	edium Tr	ucks:	75.3%	7.0%	17.7%	1.76
Barrier Type (0-Wa		0.0			1	Heavy Tr	ucks:	60.4%	12.0%	27.6%	2.90
Centerline Dis	t. to Barrier:	59.0 feet		,	loise So	ource Ele	evation	s (in f	eet)		
Centerline Dist. t	o Observer:	59.0 feet		F		Autos		000	,		
Barrier Distance t	o Observer:	0.0 feet			Mediu	m Trucks		297			
Observer Height (/	,	5.0 feet				v Trucks		004	Grade Ad	iustment	: 0.0
	d Elevation:	0.0 feet		<u> </u>		,					
	d Elevation:	0.0 feet		1	ane Eq	uivalent			feet)		
F	Road Grade:	0.0%				Autos		129			
	Left View:	-90.0 degre				m Trucks		966			
	Right View:	90.0 degre	ees		Heav	y Trucks	: 53	982			
FHWA Noise Mode	l Calculation	s									
Vehicle Type	REMEL	Traffic Flow		stance		Road	Fresi		Barrier Att		rm Atter
Autos:	70.20		-	-0.62	-	-1.20		-4.69		000	0.00
Medium Trucks:	81.00		_	-0.60	-	-1.20		-4.88		000	0.00
Heavy Trucks:	85.38			-0.60		-1.20		-5.35	0.0	000	0.00
Unmitigated Noise	•		_					1			
VehicleType Autos:	Leq Peak Ho		65.4	Leq Ev		Leq I	_	4	Ldn 67.	_	NEL 68
Medium Trucks:		5.5 9.0	59.1		63.7 54.8		60. 54.		61.4		61
		5.5	64.7		63.6		62.	-	69.		69
Heavy Trucks: _ Vehicle Noise:		9.0	68.6		67.0		64.	-	72.		72
Centerline Distanc	e to Noise C	ontour (in fee	t)								
			7	70 d	IBA	65 (iBA		60 dBA	55	dBA
			Ldn:		80		171		369)	79

Wednesday, September 14, 2022

	FHWA-RI	D-77-108 HIGHV	VAY NOI	SE PREDI	CTION N	IODEL (9/12/2	(021)		
	io: EAP 2024 e: Harvill Av. nt: s/o Cajalco	Exwy.				Name: lumber:		/ Harvill Ind	ustrial C	e
	SPECIFIC IN	IPUT DATA						L INPUT	S	
Highway Data				Site Cor	nditions	(Hard =	10, S	oft = 15)		
	Traffic (Adt): Percentage: our Volume:	15,837 vehicles 6.14% 972 vehicles	3		edium Tr eavy Tru	ucks (2)	/	: 15		
Ve	hicle Speed:	50 mph		Vehicle	Miv					
Near/Far Lai	ne Distance:	48 feet			nicleType		Dav	Evening	Night	Dailv
Site Data				707		Autos:	71.99		15.9%	. ,
					1edium T		75.39		17.7%	
Barrier Type (0-W	rier Height: 'all, 1-Berm):	0.0 feet 0.0			Heavy T		60.49		27.6%	
Centerline Dis	st. to Barrier:	59.0 feet		Noise S	ource E	levation.	s (in f	eet)		
Centerline Dist.	to Observer:	59.0 feet		710,000	Auto		000	001)		
Barrier Distance	to Observer:	0.0 feet		Modi	ım Truck	0.	297			
Observer Height (Above Pad):	5.0 feet			vy Truck		004	Grade Ad	iustmen	t 0.0
Pa	ad Elevation:	0.0 feet		Tica	vy IIuck	s. o.	004	0,440,149	401111011	0.0
Roa	ad Elevation:	0.0 feet		Lane Ec	uivalen	t Distan	ce (in	feet)		
F	Road Grade:	0.0%			Auto	s: 54.	129			
	Left View:	-90.0 degrees	S	Mediu	ım Truck	s: 53.	966			
	Right View:	90.0 degrees	3	Hea	vy Truck	s: 53.	982			
FHWA Noise Mode	el Calculation	s		-						
VehicleType	REMEL	Traffic Flow	Distanc	e Finite	Road	Fresr	nel	Barrier Atte	en Be	rm Atten
Autos:	70.20	-2.63	-	0.62	-1.20		-4.69	0.0	000	0.000
Medium Trucks:	81.00	-19.92	-	0.60	-1.20		-4.88	0.0	000	0.000
Heavy Trucks:	85.38	-17.56	-	0.60	-1.20		-5.35	0.0	000	0.000
Unmitigated Noise	Levels (with	out Topo and b	arrier at	tenuation)						
	Leq Peak Hou			q Evening		Night		Ldn		NEL
Autos:	65		5.6	64.0		60.3		67.9		68.4
Medium Trucks:	59		9.4	55.1		54.3	-	61.7		62.0
Heavy Trucks:	66		5.2	64.1		63.0	_	69.8		70.1
Vehicle Noise:	69).3 6	8.9	67.3	3	65.3	3	72.3	3	72.7
Centerline Distance	e to Noise Co	ontour (in feet)		70 dBA	65	dBA		60 dBA		i dBA
		,	dn:	70 aBA 85		ава 182		392		845
		_	an: EL:	89		192		392 414		893
		CN	EL:	89		192		414		893

Wednesday, September 14, 2022

	FHWA-RE	0-77-108 HIGH	WAY	NOISE	PREDIC	CTION N	IODEL	(9/12/2	021)		
Road Nam	io: EAC 2024 ne: Harvill Av. nt: s/o Cajalco	Exwy.					Name: lumber:		Harvill Ind	ustrial C	e
	SPECIFIC IN	PUT DATA							L INPUT	s	
Highway Data					Site Cor	ditions	(Hard :	= 10, Sc	oft = 15)		
Average Daily	Traffic (Adt):	28,600 vehicle	es					Autos:	15		
Peak Hour	Percentage:	6.14%				edium Tr					
Peak H	lour Volume:	1,756 vehicle	S		He	eavy Tru	cks (3+	Axles):	15		
Ve	hicle Speed:	50 mph		T T	Vehicle	Mix					
Near/Far La	ne Distance:	48 feet		Ė		icleType	,	Dav	Evenina	Niaht	Dailv
Site Data							Autos:	71.9%	12.2%	15.9%	95.34%
	rrier Height:	0.0 feet			М	edium T	rucks:	75.3%	7.0%	17.7%	1.76%
Barrier Type (0-W		0.0				Heavy T	rucks:	60.4%	12.0%	27.6%	2.90%
Centerline Di	st. to Barrier:	59.0 feet			Noise S	ource E	lovatio	ne (in fa	not)		
Centerline Dist.	to Observer:	59.0 feet		F		Auto		.000	,,,,		
Barrier Distance	to Observer:	0.0 feet			Mediu	m Truck		297			
Observer Height	(Above Pad):	5.0 feet				vy Truck		.004	Grade Ad	liustmen	t· 0.0
P	ad Elevation:	0.0 feet								juoumom	0.0
Ro	ad Elevation:	0.0 feet			Lane Eq	uivalen	t Distar	ice (in :	feet)		
	Road Grade:	0.0%				Auto	s: 54	.129			
	Left View:	-90.0 degree	es		Mediu	m Truck	s: 53	3.966			
	Right View:	90.0 degree	es		Hea	vy Truck	s: 53	1.982			
FHWA Noise Mode	el Calculations	S									
VehicleType	REMEL	Traffic Flow	Dis	stance	Finite	Road	Fres	nel	Barrier Att	en Be	rm Atten
Autos:	70.20	-0.06		-0.6	2	-1.20		-4.69	0.0	000	0.000
Medium Trucks:	81.00	-17.39		-0.6	0	-1.20		-4.88	0.0	000	0.000
Heavy Trucks:	85.38	-15.23		-0.6	0	-1.20		-5.35	0.0	000	0.000
Unmitigated Noise	e Levels (with	out Topo and	barri	er atter	nuation)						
VehicleType	Leq Peak Hou	r Leq Day	/	Leq E	vening	Leq	Night		Ldn	С	NEL
Autos:	68	.3	68.2		66.5		62	.9	70.	5	70.9
Medium Trucks:	61	.8	61.9		57.6		56	.9	64.	3	64.5
Heavy Trucks:	68	.3	67.5		66.5		65	.3	72.	1	72.4
Vehicle Noise:	71	.8	71.4		69.8		67	.7	74.	8	75.1
Centerline Distance	ce to Noise Co	ntour (in feet)								
				70	dBA	65	dBA	6	60 dBA	55	dBA
			Ldn:		123		26	5	570)	1,229
		C	NEL:		130		28	0	603	3	1,298

	FHWA-RD	-77-108 HIGH	WAY NC	DISE I	PREDIC	TION N	10DEL (9/12/	2021)	
	io: E e: Harvill Av. nt: s/o Cajalco	Rd.					Name: BCI I lumber: 1423	V Harvill Indu 1	strial Ce
	SPECIFIC IN	PUT DATA						EL INPUTS	
Highway Data				S	ite Con	ditions	(Hard = 10, 3	Soft = 15)	
Peak H	Percentage: our Volume:	12,419 vehicle 6.14% 763 vehicles					Auto ucks (2 Axles cks (3+ Axles): 15	
	hicle Speed:	50 mph		ν	ehicle i	Mix			
Near/Far Lai	ne Distance:	48 feet		F		icleType	Dav	Evening	Night Daily
Site Data							Autos: 71.9		15.9% 95.34%
Par	rier Height:	0.0 feet			М	edium T	rucks: 75.3	% 7.0%	17.7% 1.76%
Barrier Type (0-W		0.0			-	Heavy T	rucks: 60.4	% 12.0%	27.6% 2.90%
Centerline Dis	st. to Barrier:	59.0 feet		N	loise So	ource E	levations (in	feet)	
Centerline Dist.	to Observer:	59.0 feet				Auto	-		
Barrier Distance	to Observer:	0.0 feet			Mediu	m Truck			
Observer Height (.	Above Pad):	5.0 feet				vy Truck	0	Grade Adiu	stment: 0.0
Pa	ad Elevation:	0.0 feet							
Roa	ad Elevation:	0.0 feet		L	ane Eq	uivalen	t Distance (ii	ı feet)	
F	Road Grade:	0.0%				Auto			
	Left View:	-90.0 degree	:S			m Truck			
	Right View:	90.0 degree	:S		Heav	ry Truck	s: 53.982		
FHWA Noise Mode	el Calculations	3							
VehicleType	REMEL	Traffic Flow	Distan	се	Finite	Road	Fresnel	Barrier Atte	n Berm Atten
Autos:	70.20	-3.68		-0.62		-1.20	-4.6	9 0.00	0.000
Medium Trucks:	81.00	-21.01		-0.60		-1.20	-4.8	0.00	0.000
Heavy Trucks:	85.38	-18.85		-0.60	1	-1.20	-5.3	5 0.00	0.000
Unmitigated Noise									
	Leq Peak Hou			eq Ev	ening		Night	Ldn	CNEL
Autos:	64.		64.6		62.9		59.3	66.9	67.3
Medium Trucks:	58.		58.3		54.0		53.2	60.6	60.9
Heavy Trucks:	64.		63.9		62.9		61.7	68.5	68.8
Vehicle Noise:	68.		67.8		66.2		64.1	71.2	71.5
Centerline Distanc	e to Noise Co	ntour (in feet)		70 d	D.A	65	dBA	60 dBA	55 dBA
			Ldn:	70 a	<i>BA</i> 70	00	152	327	55 dBA 705
			Lan: JEL:		70		160	346	705
		Cr	VLL.		14		100	346	744

	FHWA-R	D-77-108 HIGH	WAY I	NOISE	PREDIC	TION M	ODEL (9/12/2	021)		
	o: EAPC 202 e: Harvill Av. t: s/o Cajalco						Name: umber:		' Harvill Ind	lustrial C	e
	PECIFIC II	NPUT DATA							L INPUT	s	
Highway Data				S	ite Con	ditions	(Hard =	10, S	oft = 15)		
Average Daily	raffic (Adt):	28,925 vehicl	es					Autos.	15		
Peak Hour I	Percentage:	6.14%			Ме	dium Tru	icks (2	Axles).	15		
Peak He	our Volume:	1,776 vehicle	s		He	avy Truc	ks (3+ .	Axles).	15		
Vel	icle Speed:	50 mph		ν	ehicle l	Mix					
Near/Far Lar	e Distance:	48 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data							lutos:	71.99	6 12.2%	15.9%	95.24
Bar	rier Heiaht:	0.0 feet			М	edium Tr	ucks:	75.39	6 7.0%	17.7%	1.77
Barrier Type (0-Wi		0.0			I	Heavy Tr	ucks:	60.4%	6 12.0%	27.6%	2.99
Centerline Dis	t. to Barrier:	59.0 feet		N	oise So	ource Ele	evation	s (in f	eet)		
Centerline Dist. t	o Observer:	59.0 feet				Autos		000	,		
Barrier Distance t		0.0 feet			Mediu	m Trucks		297			
Observer Height ()	,	5.0 feet			Heav	y Trucks	s: 8.	004	Grade Ad	ljustmen	t: 0.0
	d Elevation:	0.0 feet		-							
	d Elevation:	0.0 feet		L	ane Eq	uivalent			feet)		
F	Road Grade:	0.0%				Autos		.129			
	Left View:	-90.0 degre				m Trucks		.966			
	Right View:	90.0 degre	es		Heav	y Trucks	5.' 53.	.982			
FHWA Noise Mode		-									
VehicleType	REMEL	Traffic Flow		tance		Road	Fresi		Barrier Att		rm Atter
Autos:	70.20			-0.62		-1.20		-4.69		000	0.00
Medium Trucks:	81.00			-0.60		-1.20		-4.88		000	0.00
Heavy Trucks:	85.38			-0.60		-1.20		-5.35	0.	000	0.00
Unmitigated Noise VehicleType	Levels (with Leg Peak Ho			r attenu Leg Ev		100	Night		Ldn		NEL
Autos:		ur Ley Da, 3.4	68.3	Ley Ev	66.6		63.1	n	70.		71
Medium Trucks:		1.9	62.0		57.7		56.	-	64.	-	64
Heavy Trucks:	-	3.5	67.7		66.7		65.	-	72.	-	72
Vehicle Noise:		1.9	71.5		69.9		67.	-	74.		75
Centerline Distanc	e to Noise C	ontour (in fee	t)								
		,		70 di	BA	65 (dBA	-	60 dBA	55	dBA
			Ldn:		125	•	270		581	1	1.25
			Luii.		125		2/(,	581		1,20

Wednesday, September 14, 2022

FH	WA-RD-7	7-108 HIGHV	VAY NO	OISE I	PREDIC	TION	IODEL (9	/12/2	021)	
Scenario: EA 2 Road Name: Harv Road Segment: s/o (/ill Av.	d.					Name: B lumber: 1		Harvill Indus	trial Ce
SITE SPECI	FIC INP	UT DATA				1	IOISE M	ODE	L INPUTS	
Highway Data				S	ite Con	ditions	(Hard = 1	0, S	oft = 15)	
Average Daily Traffic (Peak Hour Percen Peak Hour Vol Vehicle Si	tage: (ume:	2,921 vehicles 3.14% 793 vehicles 50 mph	3		He	avy Tru	A ucks (2 A cks (3+ A	,	15	
Near/Far Lane Dista		48 feet		V	ehicle I				I= . I .	
Site Data					Veh	icleType		Day 11.9%		light Daily 15.9% 95.34%
Barrier He	ight:	0.0 feet		1	М	edium T	rucks: 7	5.3%		17.7% 1.76%
Barrier Type (0-Wall, 1-B		0.0			I	Heavy T	rucks: 6	0.4%	12.0%	27.6% 2.90%
Centerline Dist. to Ba	arrier:	59.0 feet		٨	loise So	ource E	levations	(in f	eet)	
Centerline Dist. to Obse	erver:	59.0 feet		Ë		Auto		•	,	
Barrier Distance to Obse	erver:	0.0 feet			Mediu	m Truck	0.0			
Observer Height (Above	Pad):	5.0 feet				y Truck			Grade Adjus	tment: 0.0
Pad Elevi		0.0 feet		_ <u> </u> _		•				
Road Elevi		0.0 feet		L	ane Eq		t Distance		feet)	
Road G		0.0%				Auto				
		-90.0 degrees				m Truck	00.0			
Right 1	View:	90.0 degrees	3		Heav	y Truck	s: 53.9	82		
FHWA Noise Model Calcu										
VehicleType REN		raffic Flow	Distai		Finite		Fresne		Barrier Atten	
Autos:	70.20	-3.51		-0.62		-1.20		4.69	0.000	
Medium Trucks:	81.00	-20.84		-0.60		-1.20		4.88	0.000	
Heavy Trucks:	85.38	-18.68		-0.60		-1.20	-	5.35	0.000	0.000
VehicleType Leq Pe	s (withou eak Hour	t Topo and b Leg Day		attenu eq Ev		Loa	Night		Ldn	CNEL
Autos:	64.9		4.8	cy Ev	63.1	Leq	59.5		67.0	67.5
Medium Trucks:	58.4	-	8.5		54.1		53.4		60.8	61.1
Heavy Trucks:	64.9	-	4.0		63.0		61.9		68.6	68.9
Vehicle Noise:	68.4	6	7.9		66.3		64.2		71.3	71.7
Centerline Distance to No	oise Cont	our (in feet)								
			, L	70 d		65	dBA	- (60 dBA	55 dBA
		_	dn:		72		156		336	724
		CN	EL:		76		165		355	764

	FHWA-RI	D-77-108 HIGH	WAY I	NOISE	PREDIC	TION N	MODEL	(9/12/2	2021)		
Road Nam	io: EAP 2024 le: Harvill Av. nt: s/o Cajalco	Rd.					t Name: lumber:		/ Harvill Ind	dustrial	Ce
	SPECIFIC IN	NPUT DATA			0				EL INPUT	s	
Highway Data					Site Cor	aitions	(Hara =				
Average Daily	. ,	13,190 vehicle	es					Autos			
	Percentage:	6.14%					rucks (2	,			
	lour Volume:	810 vehicle	S		He	avy Tru	icks (3+	Axles)	: 15		
	hicle Speed:	50 mph		İ	Vehicle	Mix					
Near/Far La	ne Distance:	48 feet		ı	Veh	icleType	9	Day	Evening	Night	Daily
Site Data							Autos:	71.99	6 12.2%	15.9	% 94.94%
Bai	rrier Height:	0.0 feet			М	edium 7	rucks:	75.39	6 7.0%	17.7	% 1.82%
Barrier Type (0-W		0.0				Heavy 7	rucks:	60.49	6 12.0%	27.6	% 3.24%
Centerline Di	st. to Barrier:	59.0 feet		-	Noise S	urco E	lovation	ne (in t	inat)		
Centerline Dist.	to Observer:	59.0 feet		H	NOISE S	Auto		.000	eei)		
Barrier Distance	to Observer:	0.0 feet			Modiu	m Truck		.297			
Observer Height (Above Pad):	5.0 feet				n Truck vy Truck		.004	Grade Ad	livetma	nt: 0.0
Pa	ad Elevation:	0.0 feet			пеа	ry Truck	15. 0	.004	Grade At	ijusune	nt. 0.0
Roa	ad Elevation:	0.0 feet			Lane Eq	uivalen	t Distan	ce (in	feet)		
1	Road Grade:	0.0%				Auto	s: 54	.129			
	Left View:	-90.0 degree	es		Mediu	m Truck	s: 53	.966			
	Right View:	90.0 degree	es		Hea	y Truck	rs: 53	.982			
FHWA Noise Mode	el Calculation	ıs									
VehicleType	REMEL	Traffic Flow	Dist	ance	Finite	Road	Fres	nel	Barrier At	ten B	erm Atten
Autos:	70.20			-0.6	-	-1.20		-4.69		000	0.000
Medium Trucks:	81.00			-0.6		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-18.11		-0.6	30	-1.20		-5.35	0.	000	0.000
Unmitigated Noise	e Levels (with	out Topo and	barrie	r atter	nuation)						
VehicleType	Leq Peak Hou			Leq E	vening	_	Night		Ldn	_	CNEL
Autos:	64	1.9	64.8		63.2		59.	.5	67.	1	67.6
Medium Trucks:			58.7		54.4		53.	-	61.	-	61.3
Heavy Trucks:			64.6		63.6		62.		69.		69.5
Vehicle Noise:	68	3.7	68.2		66.7		64.	.6	71.	7	72.0
Centerline Distance	ce to Noise Co	ontour (in feet)								
			L	70	dBA	65	dBA		60 dBA		55 dBA
			Ldn:		76		16	-	35	-	765
		C	VEL:		81		174	4	375	5	807

	FHWA-RI	D-77-108 HIGH	WAY	NOISE	PREDIC	TION N	ODEL	(9/12/2	(021)		
Road Name	EAPC 2024 Harvill Av.						Name: umber:		/ Harvill Ind	ustrial C	е
Road Segmen	t: s/o Cajaico	Ra.									
	PECIFIC IN	IPUT DATA							L INPUT	S	
Highway Data					Site Con	aitions	(Hara =				
Average Daily 1	. ,	22,412 vehicle	es					Autos			
Peak Hour F		6.14%				dium Tr		,			
	our Volume:	1,376 vehicle	S		не	avy Tru	CKS (3+	Axies)	: 15		
ver Near/Far Lan	icle Speed:	50 mph			Vehicle l	Vix					
Near/Far Lan	e Distance:	48 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data						,	Autos:	71.99		15.9%	95.11%
Bari	rier Height:	0.0 feet			M	edium T	rucks:	75.39	6 7.0%	17.7%	
Barrier Type (0-Wa	all, 1-Berm):	0.0			I	Heavy T	rucks:	60.49	6 12.0%	27.6%	3.10%
Centerline Dis	t. to Barrier:	59.0 feet		- 1	Noise Sc	ource El	evation	s (in f	eet)		
Centerline Dist. t	o Observer:	59.0 feet		F		Auto		.000	000		
Barrier Distance t	o Observer:	0.0 feet			Mediu	m Truck	0	.297			
Observer Height (A	,	5.0 feet				y Truck		.004	Grade Ad	justment	0.0
	d Elevation:	0.0 feet		<u> </u>							
	d Elevation:	0.0 feet		1	Lane Eq				feet)		
R	Road Grade:	0.0%				Auto		.129			
	Left View:	-90.0 degre				m Truck	00	.966			
	Right View:	90.0 degre	es		Heav	y Truck	s: 53	.982			
FHWA Noise Mode											
VehicleType	REMEL	Traffic Flow	Dis	tance	Finite		Fres		Barrier Att		m Atten
Autos:	70.20			-0.6	_	-1.20		-4.69		000	0.000
Medium Trucks:	81.00			-0.6	-	-1.20		-4.88		000	0.000
Heavy Trucks:	85.38			-0.6	-	-1.20		-5.35	0.0	000	0.000
Unmitigated Noise								-			
VehicleType I	Leq Peak Hot 67		67.2	Leq E	vening 65.5	Leq	Night 61.		Ldn 69.4		NEL 69.9
Medium Trucks:			60.9		56.6		55.	-	63.		63.5
Heavy Trucks:			66.7		65.7		55. 64.	-	71.	-	71.6
Vehicle Noise:).9	70.5		68.9		66.		71.		74.2
Centerline Distance											
Contenine Distance	HUISE C	omour (m leet		70	dBA	65	dBA		60 dBA	55	dBA
			Ldn:		107		231	1	497		1,071
	CNEL:						113 244 525				

Barrier Height: 0.0 feet		FHWA-R	D-77-108 HIGH	YAW	NOISE	E PREDI	CTION N	IODEL	(9/12/2	021)		
Average Daily Traffic (Adt): 22,143 vehicles Peak Hour Percentage: 6.14% Autos: 15 Heavy Trucks (24 Axles): 15 Heavy Trucks (24 Axles): 15	Road Name	e: Harvill Av.	Rd.							Harvill Ind	ustrial C	е
Average Daily Traffic (Adt):		SPECIFIC II	NPUT DATA								s	
Peak Hour Percentage:	Highway Data					Site Co.	nditions	(Hard =	= 10, S	oft = 15)		
Peak Hour Volume: Vehicle Speed: 50 mph Near/Far Lane Distance: 48 feet Vehicle Mix Vehicle	Average Daily	Traffic (Adt):	22,143 vehicl	es								
Vehicle Speed: Near/Far Lane Distance: 48 feet Vehicle Mix Vehicle Type Day Evening Night Daily	Peak Hour	Percentage:	6.14%						,			
	Peak H	our Volume:	1,360 vehicle	s		Н	eavy Tru	cks (3+	Axles):	15		
Site Date Day Evening Night Day Signature Night Night Day Night Day Evening Night Day Night Nigh					İ	Vehicle	Mix					
Barrier Height: 0.0 feet	Near/Far Lar	ne Distance:	48 feet			Ve	hicleType	,	Day	Evening	Night	Daily
	Site Data							Autos:	71.9%	12.2%	15.9%	95.349
Barrier Type (0-Wall, 1-Berm):	Bar	rier Heiaht:	0.0 feet			٨	1edium T	rucks:	75.3%	7.0%	17.7%	1.769
Noise Model Calculations Vehicle Type REMEL Traffic Flow Distance Trucks: 81,00 1.17 0.62 -1.20 -4.69 0.000							Heavy T	rucks:	60.4%	12.0%	27.6%	2.909
Autos: 0.000	Centerline Dis	t. to Barrier:	59.0 feet		1	Noise S	ource E	levation	ns (in f	eet)		
Barrier Distance to Observer: 0.0 feet Pad Elevation: 0.0 feet Pad Elevation: 0.0 feet Road Elevation: 0.0 feet Lane Equivalent Distance (in feet)	Centerline Dist. 1	to Observer:	59.0 feet							,		
Distance Helay Trucks: 8.004 Grade Adjustment: 0.0	Barrier Distance t	to Observer:	0.0 feet			Medii						
Pad Elevation: 0.0 feet Cane Equivalent Distance (in feet) Cane Equivalent Di	Observer Height (Above Pad):								Grade Ad	iustmen	: 0.0
Road Grade:	Pa	d Elevation:					,					
						Lane E				feet)		
Right View: 90.0 degrees	F											
			-									
VehicleType		Right View:	90.0 degre	es		Hea	vy Truck	s: 53	.982			
Autos: 70.20	FHWA Noise Mode		-									
Medium Trucks: 81.00 -18.50 -0.60 -1.20 -4.88 0.000 0.00 Heavy Trucks: 85.38 -16.34 -0.60 -1.20 -5.35 0.000 0.00 Unmitigated Noise Levels (without Topo and barrier attenuation)						_		Fres				
Heavy Trucks: 85.38 -16.34 -0.60 -1.20 -5.35 0.000 0.000												
Unmitigated Noise Levels (without Topo and barrier attenuation) VehicleType Leq Peak Hour Leq Day Leq Evening Leq Night Ldn CNEL												
VehicleType Leq Peak Hour Leq Day Leq Evening Leq Night Ldn CNEL Autos: 67.2 67.1 65.4 61.8 69.4 69.4 Medium Trucks: 60.7 60.8 56.5 55.7 63.1 63. Heavy Trucks: 67.2 66.4 65.4 64.2 71.0 71. Vehicle Noise: 70.7 70.3 68.7 66.6 73.7 74. Centerline Distance to Noise Contour (in feet) 70 dBA 65 dBA 60 dBA 55 dBA Ldn: 104 223 481 1,03									-5.35	0.0	000	0.00
Autos: 67.2 67.1 65.4 61.8 69.4 69 Medium Trucks: 60.7 60.8 56.5 55.7 63.1 63 Heavy Trucks: 67.2 66.4 65.4 64.2 71.0 71. Vehicle Noise: 70.7 70.3 68.7 66.6 73.7 74 Centerline Distance to Noise Contour (in feet) 70 dBA 65 dBA 60 dBA 55 dBA Ldn: 104 223 481 1,03				_			_					
Medium Trucks: 60.7 60.8 56.5 55.7 63.1 63. Heavy Trucks: 67.2 66.4 65.4 64.2 71.0 71. Vehicle Noise: 70.7 70.3 68.7 66.6 73.7 74. Centerline Distance to Noise Contour (in feet) 70 dBA 65 dBA 60 dBA 55 dBA Ldn: 104 223 481 1,03				_	Leq E			_				
Heavy Trucks: 67.2 66.4 65.4 64.2 71.0 71		-							-			
Vehicle Noise: 70.7 70.3 68.7 66.6 73.7 74. Centerline Distance to Noise Contour (in feet) 70 dBA 65 dBA 60 dBA 55 dBA Ldn: 104 223 481 1,03							-					
Centerline Distance to Noise Contour (in feet) 70 dBA 65 dBA 60 dBA 55 dBA Ldn: 104 223 481 1,03												
70 dBA 65 dBA 60 dBA 55 dBA Ldn: 104 223 481 1,03						08.	'	06.	.0	/3.	1	/4.
Ldn: 104 223 481 1,031	Centerline Distanc	e to Noise C	ontour (in fee	t)	70	dRΔ	65	dRΔ		SO dBA	56	dRΔ
101 220 101 1,000				I dn	70							
OTALE. 109 230 300 1,09									-			,
			C	· * L L .		108		231	J	300		1,09

Wednesday, September 14, 2022

	FHWA-RI	D-77-108 HIGH	WAY NOIS	E PREDIC	CTION M	ODEL (9/1	2/2021)		
	rio: E ne: Cajalco Ex ent: w/o Harvill					Name: BC umber: 14:	I IV Harvill Ind 231	lustrial C	Э
SITE	SPECIFIC IN	NPUT DATA			N	OISE MC	DEL INPUT	S	
Highway Data				Site Cor	ditions (Hard = 10), Soft = 15)		
Average Daily	Traffic (Adt):	27,605 vehicle	es			Au	tos: 15		
Peak Hou	Percentage:	6.14%		Me	edium Tru	icks (2 Axl	es): 15		
Peak I	Hour Volume:	1,695 vehicles	3	He	eavy Truc	ks (3+ Axl	es): 15		
Ve	ehicle Speed:	50 mph		Vehicle	Miv				
Near/Far La	ane Distance:	102 feet			icleType	Da	ay Evening	Night	Daily
Site Data				VCI			.9% 12.2%	15.9%	,
					edium Tr		5.3% 7.0%	17.7%	
	rrier Height:	0.0 feet			Heavy Tr		0.4% 12.0%	27.6%	
Barrier Type (0-V	. ,	0.0			neavy n	acns. oc	7.470 12.070	21.070	2.5070
Centerline D Centerline Dist	ist. to Barrier:	92.0 feet		Noise S	ource Ele	evations (in feet)		
		92.0 feet			Autos	0.00	0		
Barrier Distance		0.0 feet 5.0 feet		Mediu	m Trucks	2.29	7		
Observer Height	(Above Pad): Pad Flevation:			Hea	vy Trucks	8.00	4 Grade Ad	ljustment	: 0.0
-	ad Elevation:	0.0 feet 0.0 feet		I ane Fo	uivalent	Distance	(in feet)		
AC.	Road Grade:	0.0 reet 0.0%		Lane Lq	Autos		, ,		
	Left View:	-90.0 degree		Mediu	m Trucks				
	Right View:	90.0 degree			vy Trucks		-		
	ragin view.	50.0 degree	75	7700	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	. 70.02	3		
FHWA Noise Mod	lel Calculation	ıs		•					
Vehicle Type	REMEL	Traffic Flow	Distance	Finite	Road	Fresnel	Barrier Att	en Bei	m Atten
Autos	70.20	-0.21	-2	.89	-1.20	-4	.76 0.0	000	0.000
Medium Trucks		-17.54	-2	.88	-1.20	-4	.0.0	000	0.000
Heavy Trucks:	85.38	-15.38	-2	.88	-1.20	-5	.18 0.0	000	0.000
Unmitigated Nois	e Levels (with	out Topo and	barrier atte	enuation)					
VehicleType	Leq Peak Hot	ur Leq Day	Leq	Evening	Leq I	Vight	Ldn	C	NEL
Autos	65	5.9	65.8	64.1		60.5	68.	1	68.5
Medium Trucks:		9.4	59.5	55.2		54.4	61.8	8	62.1
Heavy Trucks:			65.0	64.0		62.9	69.		70.0
Vehicle Noise:	69	9.4	69.0	67.4		65.2	72.3	3	72.7
Centerline Distan	ce to Noise C	ontour (in feet))						
		, ,	70	0 dBA	65 0	BA	60 dBA	55	dBA
			Ldn:	132		284	612	2	1,319
		CI	VEL:	139		300	647	,	1,393

Wednesday, September 14, 2022

	FHWA-RI	D-77-108 HIGH	HWAY	NOISE	PREDIC	TION N	IODEL (9/12/2	021)		
Road Nan	io: EA 2024 ne: Cajalco Ex nt: w/o Harvill						Name: lumber:		Harvill Ind	ustrial C	е
	SPECIFIC IN	IPUT DATA			0:4- 0				L INPUT	S	
Highway Data					Site Con	aitions					
Average Daily	. ,	28,721 vehicl	les					Autos:			
	Percentage:	6.14%					ucks (2)	,			
	lour Volume:	1,763 vehicle	es		He	avy Tru	cks (3+)	Axles):	15		
Ve	hicle Speed:	50 mph		f	Vehicle	Mix					
Near/Far La	ne Distance:	102 feet		ŀ	Veh	icleType		Day	Evening	Night	Daily
Site Data							Autos:	71.9%	12.2%	15.9%	95.34%
Ra	rrier Height:	0.0 feet			М	edium T	rucks:	75.3%	7.0%	17.7%	1.76%
Barrier Type (0-W		0.0				Heavy T	rucks:	60.4%	12.0%	27.6%	2.90%
Centerline Di	st. to Barrier:	92.0 feet		ŀ	Noise So	urce F	lovation	e (in fa	not)		
Centerline Dist.	to Observer:	92.0 feet		F	110/36 00	Auto		000	,		
Barrier Distance	to Observer:	0.0 feet			Modiu	m Truck		297			
Observer Height	(Above Pad):	5.0 feet				ry Truck		004	Grade Ad	iustmen	- 0.0
P	ad Elevation:	0.0 feet		L						, ao amon	. 0.0
Ro	ad Elevation:	0.0 feet		L	Lane Eq	uivalen	t Distan	ce (in i	feet)		
	Road Grade:	0.0%				Auto		733			
	Left View:	-90.0 degre	es		Mediu	m Truck	s: 76.	618			
	Right View:	90.0 degre	es		Heav	y Truck	s: 76.	629			
FHWA Noise Mod	el Calculation	s									
VehicleType	REMEL	Traffic Flow	_	stance		Road	Fresr	_	Barrier Att		m Atten
Autos:	70.20			-2.8	-	-1.20		-4.76		000	0.000
Medium Trucks:				-2.8		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-15.21		-2.8	88	-1.20		-5.18	0.0	000	0.000
Unmitigated Nois	e Levels (with	out Topo and	barri	er atter	nuation)						
VehicleType	Leq Peak Hou		_	Leq E	vening		Night		Ldn	_	NEL
Autos:		5.1	66.0		64.3		60.7		68.2	_	68.7
Medium Trucks:		0.5	59.6		55.3		54.6	-	62.0	-	62.2
Heavy Trucks:		5.1	65.2		64.2		63.		69.8		70.1
Vehicle Noise:	69).5	69.1		67.5		65.4	4	72.	5	72.9
Centerline Distan	ce to Noise Co	ontour (in fee	t)							_	
			L	70	dBA	65	dBA	4 - 7	60 dBA		dBA
			Ldn:		135		292		629		1,354
		С	:NEL:		143		308		664		1,431

	FHWA-RD	0-77-108 HIGH	IWAY	NOISE	PREDIC	CTION N	MODEL	(9/12/2	021)		
Scenario: Road Name: Road Segment:								: BCI IV : 14231	Harvill Ind	ustrial C	е
	ECIFIC IN	IPUT DATA			N/4- O				L INPUT	s	
Average Daily Tra Peak Hour Pe Peak Hou Vehic Near/Far Lane	rcentage: r Volume: le Speed:	54,687 vehicle 6.14% 3,358 vehicle 50 mph			Ме	edium Ti eavy Tru	rucks (2	Autos: Axles): Axles):	15		
Near/Far Lane	Distance:	102 feet			Veh	icleType	е	Day	Evening	Night	Daily
Barrier Type (0-Wall,		0.0 feet 0.0 92.0 feet				edium 1 Heavy 1		71.9% 75.3% 60.4%	7.0%	15.9% 17.7% 27.6%	1.76%
Centerline Dist. to Centerline Dist. to Barrier Distance to Observer Height (Ab	Observer: Observer:	^	Mediu	Auto M Truck Vy Truck	os: (ns (in fe 0.000 2.297 3.004	e et) Grade Adj	justment	: 0.0		
Roa	Elevation: ad Grade: Left View: ight View:	0.0 feet 0.0% -90.0 degre 90.0 degre		L	Mediu	Auto M Truck yy Truck	os: 70 ks: 70	nce (in 1 6.733 6.618 6.629	reetj		
FHWA Noise Model (
Autos: Medium Trucks:	70.20 81.00	2.76 -14.57		-2.89 -2.88	3	-1.20 -1.20		-4.76 -4.88	0.0	000	0.000 0.000
Heavy Trucks:	85.38	-12.41		-2.88		-1.20		-5.18	0.0	000	0.000
Unmitigated Noise L											
VehicleType Le	q Peak Hou 68		68.8	Leq Ev	ening 67.1		Night 63	5	Ldn 71.0		NEL 71.
Medium Trucks: Heavy Trucks:		58.1 67.0		57 65	.4	71.0 64.8 72.6	В	65.0 72.9			
Vehicle Noise:	68 72		71.9		70.3		68		75.3		75.7
Centerline Distance	to Noise Co	ntour (in feet)								
		. ,		70 a	IBA	65	dBA	6	60 dBA	55	dBA
			Ldn:		208		44	-	966		2,081
		С	NEL:		220		47	4	1,020		2,198

	FHWA-RI	D-77-108 HIGH	WAY I	NOISÉ I	PREDIC	TION M	ODEL (9/12/2	021)		
	o: EAP 2024 e: Cajalco Ex t: w/o Harvill						Name: umber:		Harvill Ind	ustrial C	е
	PECIFIC IN	IPUT DATA							L INPUT	S	
Highway Data				S	ite Con	ditions	(Hard =	10, S	oft = 15)		
Average Daily 1	raffic (Adt):	28,849 vehicle	es					Autos:	15		
Peak Hour I	Percentage:	6.14%			Me	edium Tru	ıcks (2	Axles):	15		
Peak Ho	our Volume:	1,771 vehicle	s		He	avy Truc	cks (3+	Axles):	15		
	icle Speed:	50 mph		ν	ehicle	Mix					
Near/Far Lar	e Distance:	102 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data							lutos:	71.9%	12.2%	15.9%	95.309
Ban	rier Heiaht:	0.0 feet			М	edium Ti	rucks:	75.3%	7.0%	17.7%	1.769
Barrier Type (0-Wa	all, 1-Berm):	0.0			1	Heavy Ti	rucks:	60.4%	12.0%	27.6%	2.939
Centerline Dis	t. to Barrier:	92.0 feet			laica S	ource El	ovation	c (in f	not)		
Centerline Dist. t	o Observer:	92.0 feet			10/36 30	Auto:		000	eei)		
Barrier Distance t	o Observer:	0.0 feet			Mediu	m Truck:		297			
Observer Height (A	Above Pad):	5.0 feet				v Truck		004	Grade Ad	iustment	0.0
Pa	d Elevation:	0.0 feet				,					
	d Elevation:	0.0 feet		L	ane Eq	uivalent			feet)		
F	Road Grade:	0.0%				Auto		.733			
	Left View:	-90.0 degre				m Truck		618			
	Right View:	90.0 degre	es		Heav	y Truck:	s: 76	.629			
FHWA Noise Mode											
VehicleType	REMEL	Traffic Flow		ance		Road	Fresi		Barrier Att		m Atten
Autos:	70.20			-2.89		-1.20		-4.76		000	0.00
Medium Trucks:	81.00			-2.88		-1.20		-4.88		000	0.00
Heavy Trucks:	85.38			-2.88		-1.20		-5.18	0.0	000	0.00
Unmitigated Noise	•						N II l- 4	1	Ldn		NFL
VehicleType Autos:	Leq Peak Hou	ur Leq Day	66.0	Leq Ev	ening 64.3		Night 60.	7	Lan 68.3		VEL 68
Medium Trucks:		9.6	59.7		55.4		54.		62.0		62
Heavy Trucks:		3.2	65.3		64.3		63.	-	69.9		70.
Vehicle Noise:		9.6	69.2		67.6		65.		72.6		72
Centerline Distance	e to Noise C	ontour (in feet)								
		. ,		70 d	BA	65	dBA		60 dBA	55	dBA
			Ldn:		136		294		633		1,36

Wednesday, September 14, 2022

FHWA-R	D-77-108 HIGHW	AY NOISI	E PREDIC	TION N	IODEL (9/12/2	(021)		
Scenario: EAPC 202 Road Name: Cajalco Ex Road Segment: w/o Harvill	wy.				Name: lumber:		/ Harvill Ind	ustrial (Ce
SITE SPECIFIC II	NPUT DATA			ı	IOISE	MODE	L INPUT	S	
Highway Data			Site Con	ditions	(Hard =	10, S	oft = 15)		
Average Daily Traffic (Adt):	54,815 vehicles					Autos	: 15		
Peak Hour Percentage:	6.14%		Me	dium Tr	ucks (2	4xles)	: 15		
Peak Hour Volume:	3,366 vehicles		He	avy Tru	cks (3+ .	4xles)	: 15		
Vehicle Speed:	50 mph		Vehicle I	Mix					
Near/Far Lane Distance:	102 feet		Veh	icleType		Dav	Evening	Night	Dailv
Site Data					Autos:	71.99		15.99	6 95.32%
Barrier Height:	0.0 feet		М	edium T		75.39		17.79	
Barrier Type (0-Wall, 1-Berm):	0.0		1	Heavy T	rucks:	60.49	6 12.0%	27.69	6 2.92%
Centerline Dist. to Barrier:	92.0 feet								
Centerline Dist. to Observer:	92.0 feet		Noise So				eet)		
Barrier Distance to Observer:	0.0 feet			Auto	0.	000			
Observer Height (Above Pad):	5.0 feet			m Truck		297	0	·	4.00
Pad Elevation:	0.0 feet		Heav	y Truck	s: 8.	004	Grade Ad	justriier	ii. 0.0
Road Elevation:	0.0 feet		Lane Eq	uivalen	t Distan	ce (in	feet)		
Road Grade:	0.0%			Auto	s: 76	733			
Left View:	-90.0 degrees		Mediu	m Truck	s: 76	618			
Right View:	90.0 degrees		Heav	y Truck	s: 76	629			
FHWA Noise Model Calculation									
VehicleType REMEL	Traffic Flow	Distance		Road	Fresi		Barrier Att		rm Atten
Autos: 70.20		-2.8		-1.20		-4.76		000	0.000
Medium Trucks: 81.00		-2.		-1.20		-4.88		000	0.000
Heavy Trucks: 85.38		-2.8		-1.20		-5.18	0.0	000	0.000
Unmitigated Noise Levels (with					AP 11				
VehicleType Leq Peak Ho			ening	Leq	Night		Ldn		71.5
	3.9 68 2.4 62		67.1 58.1		63. 57.		71. 64.		71.5 65.1
	2.4 62 3.9 68		58.1 67.0		57. 65.		72.	-	65.1 73.0
		2.0	70.4		68.	_	75.		75.7
Centerline Distance to Noise C	ontour (in feet)								
	,,	70	dBA	65	dBA		60 dBA	5	5 dBA
	Lo	in:	209		450	ľ	969)	2,088
	CNE	-1 ·	221				1,024		2.206

September 14, 2022 Wednesday, September 14, 2022

	FHWA-RI	D-77-108 HIGH	WAY	NOISE	PREDIC	TION N	IODEL	9/12/2	021)		
Scenari Road Nam Road Segmer	e: Cajalco Ex						Name: lumber:		Harvill Ind	ustrial (Ce
	SPECIFIC IN	IPUT DATA							L INPUT	s	
Highway Data					Site Con	ditions	(Hard =	10, Sc			
Average Daily	Traffic (Adt):	30,812 vehicle	es					Autos:			
Peak Hour	Percentage:	6.14%				dium Tr		,			
Peak H	our Volume:	1,892 vehicles	3		He	avy Tru	cks (3+	Axles):	15		
	hicle Speed:	50 mph		-	Vehicle i	Wix					
Near/Far La	ne Distance:	102 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data						,	Autos:	71.9%	12.2%	15.99	6 95.34%
Bai	rier Height:	0.0 feet			М	edium T	rucks:	75.3%	7.0%	17.79	6 1.76%
Barrier Type (0-W		0.0				Heavy T	rucks:	60.4%	12.0%	27.69	6 2.90%
Centerline Dis	. ,	92.0 feet			Noise So	urco El	lovation	e (in f	not)		
Centerline Dist.	to Observer:	92.0 feet		Ľ	V0/36 30	Auto		.000	ei)		
Barrier Distance	to Observer:	0.0 feet			Modiu	m Truck		297			
Observer Height (Above Pad):	5.0 feet				y Truck		.004	Grade Ad	liuetmar	t- 0.0
Pa	ad Elevation:	0.0 feet			rica	y IIUCK	3. 0	.004	Orace Au	justinoi	12. 0.0
Ros	ad Elevation:	0.0 feet		1	Lane Eq	uivalent	t Distan	ce (in	feet)		
I	Road Grade:	0.0%				Auto	s: 76	.733			
	Left View:	-90.0 degree	es		Mediu	m Truck	s: 76	.618			
	Right View:	90.0 degree	es		Heav	y Truck	s: 76	.629			
FHWA Noise Mode	el Calculation	s									
VehicleType	REMEL	Traffic Flow	Dis	stance		Road	Fres		Barrier Att		erm Atten
Autos:	70.20	0.27		-2.8	-	-1.20		-4.76	0.0	000	0.000
Medium Trucks:	81.00	-17.07		-2.8	-	-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-14.90		-2.8	8	-1.20		-5.18	0.0	000	0.000
Unmitigated Noise	Levels (with	out Topo and	barrie	er atten	uation)						
	Leq Peak Hou			Leq E		Leq	Night		Ldn		CNEL
Autos:	66		66.3		64.6		61.	-	68.	-	69.0
Medium Trucks:			59.9		55.6		54.	-	62.3	-	62.5
Heavy Trucks:	66		65.5		64.5		63.		70.		70.4
Vehicle Noise:			69.4		67.8		65.	7	72.8	8	73.2
Centerline Distand	e to Noise Co	ontour (in feet)								_	
			L	70 (dBA	65	dBA		60 dBA		5 dBA
			Ldn:		142		306		659		1,419
		CI	VEL:		150		323	3	696	6	1,499

FI	HWA-RD	-77-108 HIGH	WAY	NOISE	PREDIC	CTION	MODEL (9/1	2/2021)		
Scenario: EA Road Name: Caj Road Segment: e/o	alco Exw						t Name: BC Number: 142	I IV Harvill Ind 231	ustrial (Ce
SITE SPEC	IFIC IN	PUT DATA					NOISE MO	DEL INPUT	S	
Highway Data				S	ite Cor	nditions	(Hard = 10	, Soft = 15)		
Average Daily Traffic Peak Hour Perce Peak Hour Vo	ntage: olume:	32,131 vehicle 6.14% 1,973 vehicle					Aut rucks (2 Axle icks (3+ Axle			
Vehicle S	,	50 mph		ν	'ehicle	Mix				
Near/Far Lane Dis	tance:	102 feet			Ver	icleTyp	e Da	y Evening	Night	Daily
Site Data							Autos: 71	.9% 12.2%	15.99	6 95.32%
Barrier H	eiaht:	0.0 feet			M	ledium 1	rucks: 75	.3% 7.0%	17.79	6 1.76%
Barrier Type (0-Wall, 1-L		0.0				Heavy 1	rucks: 60	.4% 12.0%	27.69	6 2.92%
Centerline Dist. to E	arrier:	92.0 feet			loise S	ource F	levations (i	n feet)		
Centerline Dist. to Obs	server:	92.0 feet			0/36 0	Auto				
Barrier Distance to Obs	server:	0.0 feet			Modiu	m Truck	0.000			
Observer Height (Above	Pad):	5.0 feet				vy Truci			liuetmar	t- 0.0
Pad Ele	vation:	0.0 feet			пеа	vy IIuci	15. 0.004	, Orace Au	justinoi	12. 0.0
Road Ele	vation:	0.0 feet		L	ane Eq	uivalen	t Distance	(in feet)		
Road (Grade:	0.0%				Auto	os: 76.73	3		
Left	View:	-90.0 degree	es		Mediu	m Truck	ks: 76.618	3		
Right	View:	90.0 degree	es		Hea	vy Truck	ks: 76.629	9		
FHWA Noise Model Cald	ulations	;								
VehicleType RE	MEL	Traffic Flow	Dis	tance	Finite	Road	Fresnel	Barrier Att	en Be	rm Atten
Autos:	70.20	0.45		-2.89		-1.20	-4.	76 0.	000	0.000
Medium Trucks:	81.00	-16.88		-2.88		-1.20	-4.	88 0.	000	0.000
Heavy Trucks:	85.38	-14.69		-2.88		-1.20	-5.	18 0.	000	0.000
Unmitigated Noise Leve	Is (witho	ut Topo and	barrie	r attenu	ıation)					
VehicleType Leq P	eak Hour	Leq Day	/	Leq Ev	ening	Leg	Night	Ldn	(CNEL
Autos:	66.	6	66.5		64.8	1	61.1	68.	7	69.2
Medium Trucks:	60.	0	60.1		55.8	}	55.1	62.	5	62.7
Heavy Trucks:	66.	6	65.7		64.7		63.6	70.	3	70.7
Vehicle Noise:	70.	0	69.6		68.0)	65.9	73.	0	73.4
Centerline Distance to N	loise Co	ntour (in feet)							
·				70 d	BA	65	dBA	60 dBA	5	5 dBA
			Ldn:		146		315	679)	1,463
		C	NEL:		155		333	717	,	1,546

								9/12/2			
	o: EA 2024								Harvill Ind	ustrial C	e
	e: Cajalco Ex					Job Nu	mber:	14231			
Road Segmen	t: e/o Harvill	AV.									
	SPECIFIC II	NPUT DATA							L INPUT	S	
Highway Data					Site Coi	nditions (l	Hard =	10, Sc	oft = 15)		
Average Daily	Traffic (Adt):	32,057 vehic	les					Autos:	15		
Peak Hour I	Percentage:	6.14%				edium Truc		,			
Peak He	our Volume:	1,968 vehicle	es		H	eavy Truck	(S (3+ A	Axles):	15		
	nicle Speed:	50 mph			Vehicle	Mix					
Near/Far Lar	ne Distance:	102 feet			Vel	nicleType		Day	Evening	Night	Daily
Site Data						Au	ıtos:	71.9%	12.2%	15.9%	95.34
Bar	rier Height:	0.0 feet			N	ledium Tru	icks:	75.3%	7.0%	17.7%	1.76
Barrier Type (0-Wa	-	0.0				Heavy Tru	icks:	60.4%	12.0%	27.6%	2.90
Centerline Dis	t. to Barrier:	92.0 feet			Noise S	ource Ele	vation	s (in f	eet)		
Centerline Dist. t	o Observer:	92.0 feet				Autos		000	,,,,		
Barrier Distance t	o Observer:	0.0 feet			Medii	m Trucks:		297			
Observer Height (/	Above Pad):	5.0 feet				vy Trucks:		004	Grade Ad	iustmen	t: 0.0
Pa	d Elevation:	0.0 feet									
	d Elevation:	0.0 feet			Lane Ec	uivalent l			feet)		
F	Road Grade:	0.0%				Autos:		733			
	Left View:	-90.0 degre				m Trucks:		618			
	Right View:	90.0 degre	ees		Hea	vy Trucks:	76.	629			
FHWA Noise Mode	l Calculation	ıs									
VehicleType	REMEL	Traffic Flow	_	istance		Road	Fresr	_	Barrier Att		rm Atter
Autos:	70.20			-2.		-1.20		-4.76		000	0.00
Medium Trucks:	81.00			-2.		-1.20		-4.88		000	0.00
Heavy Trucks:	85.38	-14.73	3	-2.	88	-1.20		-5.18	0.0	000	0.00
Unmitigated Noise				_							
	Leq Peak Ho		_		Evening	Leq N	•		Ldn		NEL
Autos:	-	6.5	66.4		64.8		61.1	-	68.		69
Medium Trucks:	-	0.0	60.1		55.8		55.1	-	62.	-	62
Heavy Trucks: 66.6 65.7					64.7		63.6		70.3		70
Vehicle Noise:	-	0.0	69.6		68.0)	65.9	9	73.0	J	73
Centerline Distanc	e to Noise C	ontour (in fee	t)	7/) dBA	65 d	D A		60 dBA		dBA
			Ldn			00 a					
			Lan:		146		314		676)	1,45
		-	NEL:		154		332		715		1,53

Wednesday, September 14, 2022

Scenario: EAC 2024 Project Name Road Name: Cajalco Exwy. Road Segment: elo Harvill AV. SITE SPECIFIC INPUT DATA NOISE		Harvill Indu	ustrial C	е
SITE SPECIFIC INDIT DATA NOISE				
Highway Data Site Conditions (Hard		L INPUTS	s	
Average Daily Traffic (Adt): 72,251 vehicles Peak Hour Percentage: 6.14% Medium Trucks (2 Peak Hour Volume: 4.436 vehicles Vehicle Speed: 50 mph Vehicle Mix	Autos: Axles):	15 15		
Near/Far Lane Distance: 102 feet VehicleType	Day	Evening	Night	Daily
Barrier Height: 0.0 feet Medium Trucks: Barrier Type (0-Wall, 1-Berm): 0.0 Heavy Trucks:	71.9% 75.3% 60.4%	7.0%	15.9% 17.7% 27.6%	1.76%
Centerline Dist. to Barrier: 92.0 feet Noise Source Elevatio	ne (in fo	noti		
Centerline Dist. to Observer: 92.0 feet Autos: (Barrier Distance to Observer: 0.0 feet Medium Trucks: : Observer: Heicht (Above Part): 5.0 feet Medium Trucks: :	0.000 2.297 8.004	Grade Adj	justmeni	t: 0.0
Road Elevation: 0.0 feet Lane Equivalent Dista	nce (in t	feet)		
Left View: -90.0 degrees Medium Trucks: 70	6.733 6.618 6.629			
FHWA Noise Model Calculations				
VehicleType REMEL Traffic Flow Distance Finite Road Free	snel	Barrier Atte	en Ber	rm Atten
Autos: 70.20 3.97 -2.89 -1.20	-4.76	0.0	000	0.000
Medium Trucks: 81.00 -13.36 -2.88 -1.20	-4.88	0.0	000	0.000
Heavy Trucks: 85.38 -11.20 -2.88 -1.20	-5.18	0.0	000	0.000
Unmitigated Noise Levels (without Topo and barrier attenuation)				
VehicleType Leq Peak Hour Leq Day Leq Evening Leq Night		Ldn		NEL
	1.7	72.3	-	72.7
	3.6	66.0	-	66.2
Heavy Trucks: 70.1 69.2 68.2 67 Vehicle Noise: 73.6 73.1 71.5 68	7.1).4	73.8 76.5	_	74.1
Centerline Distance to Noise Contour (in feet)				
	-	60 dBA	55	dBA
70 dBA 65 dBA	6			
70 dBA 65 dBA Ldn: 251 54		1,163		2,505

Wednesday, September 14, 2022

Road Nam	io: EAPC 2024 ne: Cajalco Exv nt: e/o Harvill /	wy.				t Name: E lumber: 1		Harvill Indu	ustrial C	е
SITE	SPECIFIC IN	IPUT DATA				NOISE N	IODE	L INPUTS	3	
Highway Data				Site	Conditions	(Hard =	10, So	ft = 15)		
Average Daily	Traffic (Adt):	72,325 vehicle	:S			A	Autos:	15		
Peak Hour	Percentage:	6.14%			Medium Ti	rucks (2 A	xles):	15		
Peak H	lour Volume:	4,441 vehicles	;		Heavy Tru	icks (3+ A	xles):	15		
Ve	hicle Speed:	50 mph		Vohi	cle Mix					
Near/Far La	ne Distance:	102 feet		_	VehicleTyp	9 /	Day	Evening	Night	Daily
Site Data							71.9%		15.9%	
Rai	rrier Height:	0.0 feet			Medium 1	rucks:	75.3%	7.0%	17.7%	
Barrier Type (0-W	-	0.0			Heavy 1	rucks:	60.4%	12.0%	27.6%	2.91
Centerline Di	. ,	92.0 feet								
Centerline Dist		92.0 feet		Nois	e Source E			et)		
Barrier Distance		0.0 feet			Auto					
Observer Height (5.0 feet			edium Truck					
	ad Flevation:	0.0 feet		F	leavy Truck	rs: 8.0	104	Grade Adj	ustment	: 0.0
	ad Elevation:	0.0 feet		Lane	Equivalen	t Distanc	e (in f	eet)		
	Road Grade:	0.0%			Auto			,		
•	Left View:	-90.0 degree	ıs	Me	edium Truck	s: 76.6	18			
	Right View:	90.0 degree		F	leavy Truck	s: 76.6	329			
FHWA Noise Mode	el Calculation	s								
VehicleType	REMEL	Traffic Flow	Distan	ce F	inite Road	Fresne	e/	Barrier Atte	en Ber	m Atten
Autos:	70.20	3.97		-2.89	-1.20		4.76	0.0	00	0.00
Medium Trucks:	81.00	-13.36		-2.88	-1.20		4.88	0.0	00	0.00
Heavy Trucks:	85.38	-11.18		-2.88	-1.20		-5.18	0.0	00	0.00
Unmitigated Noise	e Levels (with	out Topo and	barrier a	ttenuati	on)					
VehicleType	Leq Peak Hou	ır Leq Day	Le	q Evenir	ng Leq	Night		Ldn		NEL
	70		70.0		38.3	64.7		72.3		72
Autos:		.6	63.7		59.3	58.6		66.0		66
Medium Trucks:					38.2	67.1		73.8		74
Medium Trucks: Heavy Trucks:	70		69.2			60.4		76.5		76
Medium Trucks: Heavy Trucks: Vehicle Noise:	70 73	1.6	73.2		71.5	69.4		76.5	i	76
Medium Trucks: Heavy Trucks:	70 73	1.6	73.2		71.5					
Medium Trucks: Heavy Trucks: Vehicle Noise:	70 73	.6 ontour (in feet)	73.2	70 dBA	71.5	69.4 dBA 541		76.5 0 dBA 1.165		76 dBA 2,51



APPENDIX 9.1:

CADNAA OPERATIONAL NOISE MODEL INPUTS





14231 - BCI IV Harvill Industrial Center (PPT220001)

CadnaA Noise Prediction Model: 14231-03.cna

Date: 18.07.22 Analyst: S. Shami

Calculation Configuration

Configurat	ion
Parameter	Value
General	
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	999.99
Min. Length of Section (#(Unit,LEN))	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	-
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier
-	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (FTA/FRA)	
Aircraft (???)	

Receiver Noise Levels

Name	М.	ID		Level Lr		Lir	nit. Valı	ue		Land	l Use	Height		Co	oordinates	
			Day	Night	CNEL	Day	Night	CNEL	Туре	Auto	Noise Type			Х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	44.6	44.6	51.2	65.0	55.0	0.0				5.00	а	6258641.02	2250458.72	5.00
RECEIVERS		R2	43.6	43.5	50.2	55.0	45.0	0.0				5.00	а	6257264.46	2249652.84	5.00
RECEIVERS		R3	37.6	37.3	44.0	55.0	45.0	0.0				5.00	а	6256966.67	2249808.33	5.00
RECEIVERS		R4	52.2	52.2	58.9	65.0	55.0	0.0				5.00	а	6257296.47	2250801.10	5.00

Point Source(s)

Name	M.	ID	R	esult. PW	Ľ		Lw/L	i	Оре	erating Ti	ime	Heigh	t	Coordinates		
			Day	Evening	Night	Туре	Value	norm.	Day	Special	Night			Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(ft)		(ft)	(ft)	(ft)
POINTSOURCE		AC01	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6257656.91	2250019.05	50.00
POINTSOURCE		PARK01	87.8	87.8	87.8	Lw	87.8					5.00	а	6257819.72	2250032.11	5.00
POINTSOURCE		PARK02	87.8	87.8	87.8	Lw	87.8					5.00	а	6257865.12	2250047.80	5.00
POINTSOURCE		PARK03	87.8	87.8	87.8	Lw	87.8					5.00	а	6257927.05	2250071.34	5.00
POINTSOURCE		PARK04	87.8	87.8	87.8	Lw	87.8					5.00	а	6257964.89	2250014.73	5.00
POINTSOURCE		PARK05	87.8	87.8	87.8	Lw	87.8					5.00	а	6257922.85	2250022.30	5.00
POINTSOURCE		PARK06	87.8	87.8	87.8	Lw	87.8					5.00	а	6257896.51	2249991.47	5.00
POINTSOURCE		PARK07	87.8	87.8	87.8	Lw	87.8					5.00	а	6257838.77	2249993.15	5.00
POINTSOURCE		PARK08	87.8	87.8	87.8	Lw	87.8					5.00	а	6257846.06	2249926.45	5.00
POINTSOURCE		PARK09	87.8	87.8	87.8	Lw	87.8					5.00	а	6257800.94	2249954.48	5.00
POINTSOURCE		PARK10	87.8	87.8	87.8	Lw	87.8					5.00	а	6257739.28	2250000.44	5.00
POINTSOURCE		PARK11	87.8	87.8	87.8	Lw	87.8					5.00	а	6257706.77	2249989.23	5.00
POINTSOURCE		PARK12	87.8	87.8	87.8	Lw	87.8					5.00	а	6257717.14	2249946.91	5.00
POINTSOURCE		PARK13	87.8	87.8	87.8	Lw	87.8					5.00	а	6257691.92	2249938.22	5.00

Name	M.	ID	R	Result. PWL			Lw / L	i	Оре	erating Ti	me	Heigh	t	Co	oordinates	
			Day	Evening	Night	Туре	Value	norm.	Day	Special	Night			Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(ft)		(ft)	(ft)	(ft)
POINTSOURCE		TRASH01	89.0	89.0	89.0	Lw	89.0		150.00	0.00	90.00	5.00	a	6257521.48	2250411.90	5.00

Line Source(s)

Name	M.	ID	R	esult. PW	'L	R	esult. PW	'L'		Lw/L	i	Op	erating Ti	me	Moving Pt. Src				Heigh	nt
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	Number			Speed		\Box
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	Day	Evening	Night	(mph)	(ft)	П
LINESOURCE		TRUCK01	93.2	93.2	93.2	67.0	67.0	67.0	Lw	93.2									8	а

Name	H	lei	ght		Coordinat	es	
	Begin		End	х	у	Z	Ground
	(ft)		(ft)	(ft)	(ft)	(ft)	(ft)
LINESOURCE	8.00	а		6257319.15	2250611.95	8.00	0.00
				6257373.16	2250662.74	8.00	0.00
				6257396.79	2250680.01	8.00	0.00
				6257479.48	2250707.27	8.00	0.00
				6257495.83	2250694.55	8.00	0.00
				6257506.74	2250689.10	8.00	0.00
				6257594.88	2250431.94	8.00	0.00
				6257603.97	2250423.76	8.00	0.00
				6257613.96	2250419.22	8.00	0.00
				6257629.41	2250412.86	8.00	0.00
				6257829.32	2250487.37	8.00	0.00
				6257841.13	2250477.37	8.00	0.00
				6258021.96	2249982.14	8.00	0.00
				6258022.87	2249955.79	8.00	0.00
				6258022.87	2249941.25	8.00	0.00
				6258023.84	2249917.14	8.00	0.00

Area Source(s)

Name	M.	ID	R	esult. PW	'L	Re	esult. PW	L"		Lw/L	i	Op	erating Ti	me	Height	t
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)	
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)		
AREASOURCE		DOCK01	103.4	103.4	103.4	71.0	71.0	71.0	Lw	103.4					8	а
AREASOURCE		TRAILER01	103.4	103.4	103.4	63.1	63.1	63.1	Lw	103.4					8	а

Name	ŀ	lei	ght		Coordinat	es	
	Begin		End	х	У	z	Ground
	(ft)		(ft)	(ft)	(ft)	(ft)	(ft)
AREASOURCE	8.00	а		6257545.83	2250349.04	8.00	0.00
				6257832.30	2250450.19	8.00	0.00
				6257850.10	2250391.93	8.00	0.00
				6257568.49	2250290.77	8.00	0.00
AREASOURCE	8.00	а		6257706.06	2250917.12	8.00	0.00
				6257845.25	2250535.97	8.00	0.00
				6257510.23	2250415.39	8.00	0.00
				6257470.57	2250526.26	8.00	0.00
				6257523.98	2250544.87	8.00	0.00
				6257454.39	2250750.42	8.00	0.00

Building(s)

Name	M.	ID	RB	Residents	Absorption	Height			Coordinat	es	
						Begin		х	у	Z	Ground
						(ft)		(ft)	(ft)	(ft)	(ft)
BUILDING		BUILDING00001	х	0		45.00	a	6257558.11	2250289.22	45.00	0.00
								6257845.44	2250389.50	45.00	0.00
								6257951.06	2250093.63	45.00	0.00
							Г	6257641.68	2249985.17	45.00	0.00
								6257596.87	2250111.77	45.00	0.00
								6257617.85	2250118.53	45.00	0.00
BUILDING		BUILDING00002	х	0		45.00	а	6256568.19	2250047.69	45.00	0.00
							Г	6256561.25	2250462.62	45.00	0.00
								6257229.65	2250478.24	45.00	0.00
							Г	6257299.09	2250382.76	45.00	0.00
								6257309.51	2250052.89	45.00	0.00
								6257191.46	2250049.42	45.00	0.00
								6257189.72	2250108.45	45.00	0.00
								6256745.27	2250098.03	45.00	0.00
								6256743.54	2250044.21	45.00	0.00

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APPENDIX 10.1:

CADNAA CONSTRUCTION NOISE MODEL INPUTS





14231 - BCI IV Harvill Industrial Center (PPT220001) CadnaA Noise Prediction Model: 14231-02 - Construction.cna

Date: 18.07.22 Analyst: S. Shami

Calculation Configuration

Configurat	ion
Parameter	Value
General	
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	999.99
Min. Length of Section (#(Unit,LEN))	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (FTA/FRA)	
Railways (FTA/FRA) Aircraft (???)	

Receiver Noise Levels

Name	M.	ID		Level Lr		Lir	nit. Valı	ue		Land	l Use	Height		Co	oordinates	
			Day	Night	CNEL	Day	Night	CNEL	Туре	Auto	Noise Type			Х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	53.6	53.6	60.3	55.0	45.0	0.0				5.00	а	6258641.02	2250458.72	5.00
RECEIVERS		R2	55.2	55.2	61.8	55.0	45.0	0.0				5.00	а	6257264.46	2249652.84	5.00
RECEIVERS		R3	53.9	53.9	60.6	55.0	45.0	0.0				5.00	а	6256966.67	2249808.33	5.00
RECEIVERS		R4	61.0	61.0	67.7	65.0	55.0	0.0				5.00	а	6257296.47	2250801.10	5.00

Area Source(s)

Name	M.	ID	R	esult. PW	L	Re	esult. PW	L"		Lw/L	i	Ope	erating Ti	ime	Heigh	t
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)	
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)		П
SITEBOUNDARY		CONSTRUCTION	115.0	115.0	115.0	69.1	69.1	69.1	Lw	115					8	а

Name	ŀ	lei	ght	Coordinates										
	Begin		End	х	у	z	Ground							
	(ft)		(ft)	(ft)	(ft)	(ft)	(ft)							
SITEBOUNDARY	8.00	a		6257713.38	2250939.21	8.00	0.00							
				6258076.01	2249918.08	8.00	0.00							
				6257588.85	2249909.24	8.00	0.00							
				6257565.59	2249931.98	8.00	0.00							
				6257566.56	2249981.85	8.00	0.00							
				6257564.97	2250031.71	8.00	0.00							
				6257560.83	2250081.41	8.00	0.00							
				6257554.13	2250130.84	8.00	0.00							
				6257544.91	2250179.86	8.00	0.00							

Name	He	ight		Coordinat	es	
	Begin	End	x	у	Z	Ground
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)
			6257533.18	2250228.35	8.00	0.00
			6257518.97	2250276.16	8.00	0.00
			6257502.33	2250323.18	8.00	0.00
			6257485.23	2250363.85	8.00	0.00
			6257466.15	2250403.62	8.00	0.0
			6257445.15	2250442.42	8.00	0.0
			6257422.27	2250480.14	8.00	0.0
			6257397.57	2250516.69	8.00	0.0
			6257371.11	2250551.99	8.00	0.0
			6257342.95	2250585.94	8.00	0.0
			6257313.16	2250618.48	8.00	0.00
			6257281.82	2250649.52	8.00	0.00

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APPENDIX 10.2:

NIGHTTIME CONCRETE POUR NOISE MODEL INPUTS





14231 - BCI IV Harvill Industrial Center (PPT220001)

CadnaA Noise Prediction Model: 14231-02_ConcretePour.cna

Date: 18.07.22 Analyst: S. Shami

Calculation Configuration

Configurat	tion
Parameter	Value
General	
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	999.99
Min. Length of Section (#(Unit,LEN))	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (FTA/FRA)	
Aircraft (???)	
Strictly acc. to AzB	

Receiver Noise Levels

Name	M.	ID		Level Lr		Lir	nit. Valı	ue		Land	l Use	Height		Co	oordinates	
			Day	Night	CNEL	Day	Night	CNEL	Туре	Auto	Noise Type			Х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	38.3	38.3	45.0	65.0	55.0	0.0				5.00	а	6258641.02	2250458.72	5.00
RECEIVERS		R2	40.6	40.6	47.3	55.0	45.0	0.0				5.00	а	6257264.46	2249652.84	5.00
RECEIVERS		R3	38.7	38.7	45.4	55.0	45.0	0.0				5.00	а	6256966.67	2249808.33	5.00
RECEIVERS		R4	40.1	40.1	46.8	65.0	55.0	0.0				5.00	а	6257296.47	2250801.10	5.00

Area Source(s)

_			(-)														
Na	me	M.	ID	R	esult. PW	'L	Re	esult. PW	L"		Lw/L	i	Op	erating Ti	me	Height	t
				Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)	Г
				(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)		Γ
BUILI	DING		CONCRETEPOUR	100.3	100.3	100.3	60.7	60.7	60.7	Lw	100.3					6	а

Name	ŀ	lei	ght		Coordinates									
	Begin	Begin (ft)			х	у	Z	Ground						
	(ft)		(ft)		(ft)	(ft)	(ft)	(ft)						
BUILDING	6.00	а			6257558.11	2250289.22	6.00	0.00						
		Г			6257845.44	2250389.50	6.00	0.00						
					6257951.06	2250093.63	6.00	0.00						
					6257641.68	2249985.17	6.00	0.00						
		Г			6257596.87	2250111.77	6.00	0.00						
					6257617.85	2250118.53	6.00	0.00						

Building(s)

Name	M.	ID	RB	Residents	Absorption	Height	t	Coordinates								
						Begin		х	у	Z	Ground					
						(ft)	Г	(ft)	(ft)	(ft)	(ft)					
BUILDING		BUILDING00002	х	0		45.00	а	6256568.19	2250047.69	45.00	0.00					
								6256561.25	2250462.62	45.00	0.00					
								6257229.65	2250478.24	45.00	0.00					
								6257299.09	2250382.76	45.00	0.00					
								6257309.51	2250052.89	45.00	0.00					
								6257191.46	2250049.42	45.00	0.00					
								6257189.72	2250108.45	45.00	0.00					
								6256745.27	2250098.03	45.00	0.00					
								6256743.54	2250044.21	45.00	0.00					

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