PRELIMINARY DRAINAGE REPORT

FOR

Palisade Temescal Canyon
22740 Temescal Canyon Road
Corona, CA 92883

Prepared For:

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Prepared on: January 10, 2023

DRC Project No. 21-413

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Introduction

A preliminary drainage analysis has been prepared for the Palisade Temescal Canyon project located in Riverside County, California. The project site is located east of Interstate 15 between the Temescal Canyon Road and Weirick Road crossings at 22740 Temescal Canyon Road. The project site encompasses approximately 9.26 acres and Temescal Canyon Wash is immediately adjacent to the project on the east side.

Discussion

This report and the associated analyses have been prepared to present the drainage concept for the project site.

A majority of the project site is currently undeveloped. There is one building and several other scattered structures. Due to the activities that have occurred on the site, there is very little vegetation. Any vegetation that is present is open brush with a poor cover.

The proposed project is a warehouse facility with associated parking, truck parking, truck docks, and landscaped areas.

In the existing condition, the project site generally drains to the east to Temescal Canyon Wash. The proposed condition will generally maintain the existing drainage pattern and discharge to the Temescal Canyon Wash.

Drainage Concept

This project will remove the infiltration basins that served the project to the south. Therefore, 2.54 acres of the project to the south will drain to this project and require drainage mitigation for both water quantity and water quality. As such, the total drainage area associated with this project is 11.80 acres.

Storm drainage from the project site will be collected into inlets and directed in storm drains to one of two underground storage systems. There will be one underground storage system under the truck dock loading / unloading area on the west side of the building and one under the drive aisle on the east side of the building.

The underground storage systems will be designed for both water quality and water quantity mitigation. The system will be designed using a ConTech ConSpan system. For water quality, underground storage system will be designed to capture the Design Capture Volume (DCV) and direct the associated storm flows through a low flow orifice outlet to a volume-based Modular Wetlands System (MWS) for treatment. For water quantity, the underground storage systems will be designed to reduce the discharge from the site and the 2.54 acres of the project to the south to the existing condition level for twelve return frequency / storm duration events.

Hydrologic Analysis

Both rational method and flood hydrograph analyses were prepared. The hydrologic analyses were completed in accordance with the Riverside County Flood Control and Water Conservation District Hydrology Manual.

The rational method analyses developed peak flow estimates. Both existing and proposed condition analyses were prepared. The rational method analyses were prepared for both the 10-year and the 100-year return events. The rational method hydrologic analysis was completed using Advanced Engineering Software (AES).

The flood hydrographs were developed for the underground storage analysis. Both existing and proposed condition analyses were prepared as a comparison. The flood hydrographs were prepared for the 2-, 5-, and 10-year return events. The flood hydrograph hydrologic analysis was completed using CivilDesign software.

The hydrologic soil type is “B” as shown on Plate C-1.28 of the Hydrology Manual.

The relevant soil and rainfall plates from the Hydrology Manual are contained in Technical Appendix A.

Rational Method Analysis

The rational method hydrologic analysis was prepared for both the 10-year and 100-year return events. The following tables summarize the rational method analyses:

Existing Condition

Area (ac)	Tc(10) (min)	Q(10) (cfs)	Tc(100) (min)	Q(100) (cfs)
11.80	17.1	12.0	16.5	20.5

Proposed Condition

Area (ac)	Tc(10) (min)	Q(10) (cfs)	Tc(100) (min)	Q(100) (cfs)
11.80	10.7	22.0	10.7	33.9

The rational method hydrologic analysis is contained in Technical Appendix B and Technical Appendix C.

Flood Hydrograph Analysis

The flood hydrograph hydrologic analysis was prepared for the 2-, 5-, and 10-year return events. Antecedent Moisture Condition (AMC) I was used for the 2- and 5-year analyses and AMC II was used for the 10-year analysis.

There are four separate areas for which flood hydrographs were prepared:
Area Tributary to West Underground Storage System (Nodes 100-131) – 5.31 acres
Area Tributary to West Flow-Based Modular Wetlands System (Node 132) – 0.13 acres
Area Tributary to East Flow-Based Modular Wetlands System (Node 133) – 0.29 acres
Area Tributary to East Underground Storage System (Nodes 140-161) – 6.07 acres

The following tables summarize the flood hydrograph peak flows:

Existing Condition

	2-year				5-year				10-year			
Area (ac)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)
11.80	0.81	3.40	4.48	8.25	1.23	6.29	7.91	12.74	3.61	10.43	12.48	18.18
11.80	**0.81**	**3.40**	**4.48**	**8.25**	**1.23**	**6.29**	**7.91**	**12.74**	**3.61**	**10.43**	**12.48**	**18.18**

Proposed Condition

	2-year				5-year				10-year			
Area (ac)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)
5.31	1.19	3.32	3.79	6.23	1.81	4.69	5.49	8.68	2.33	5.95	6.97	10.75
0.13	0.03	0.09	0.10	0.20	0.04	0.13	0.14	0.28	0.06	0.16	0.18	0.34
0.29	0.07	0.20	0.22	0.45	0.10	0.28	0.32	0.62	0.13	0.35	0.40	0.76
6.07	1.37	3.93	4.45	8.04	2.07	5.58	6.44	11.19	2.66	7.06	8.17	13.80
11.80	**2.65**	**7.53**	**8.56**	**14.91**	**4.02**	**10.67**	**12.38**	**20.77**	**5.17**	**13.53**	**15.72**	**25.65**

The flood hydrograph hydrologic analysis is contained in Technical Appendix D and Technical Appendix E.

Underground Storage Analysis

The underground storage systems are designed for both water quality and water quantity mitigation. Two orifice outlets are provided for each underground storage system. The low flow orifice outlet directs storm flows to a volume-based MWS. The high flow orifice outlet is placed above the depth that corresponds to the DCV, meaning the DCV will be directed to the MWS. The high flow orifice opening is provided to discharge storm flows in excess of the DCV directly to Temescal Canyon Wash.

The underground storage analysis compares the 2-year, 5-year and 10-year return frequencies with 24-hour, 6-hour, 3-hour and 1-hour storm durations for the proposed condition to the existing condition. The underground storage capacity and outlet sizing is designed such that none of these storm events has a higher peak discharge in the proposed condition than in the existing condition.

The following table summarizes the underground storage analysis peak discharges (note that the 5.31 and 6.07 acre areas are the only areas that are mitigated):

Mitigated Condition

	2-year				5-year				10-year			
Area (ac)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)
5.31	0.32	0.30	0.27	0.23	0.47	0.35	0.32	0.26	1.54	0.39	0.36	0.29
0.13	0.03	0.09	0.10	0.20	0.04	0.13	0.14	0.28	0.06	0.16	0.18	0.34
0.29	0.07	0.20	0.22	0.45	0.10	0.28	0.32	0.62	0.13	0.35	0.40	0.76
6.07	0.37	0.34	0.31	0.27	0.55	0.40	0.37	0.30	1.82	0.44	0.41	0.33
11.80	**0.78**	**0.93**	**0.90**	**1.15**	**1.16**	**1.15**	**1.15**	**1.46**	**3.54**	**1.34**	**1.35**	**1.72**

The underground storage analysis is contained in Technical Appendix F.

Summary

The following tables summarize the peak discharges from the project site:

Existing Condition

	2-year				5-year				10-year			
Area (ac)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)
11.80	**0.81**	**3.40**	**4.48**	**8.25**	**1.23**	**6.29**	**7.91**	**12.74**	**3.61**	**10.43**	**12.48**	**18.18**

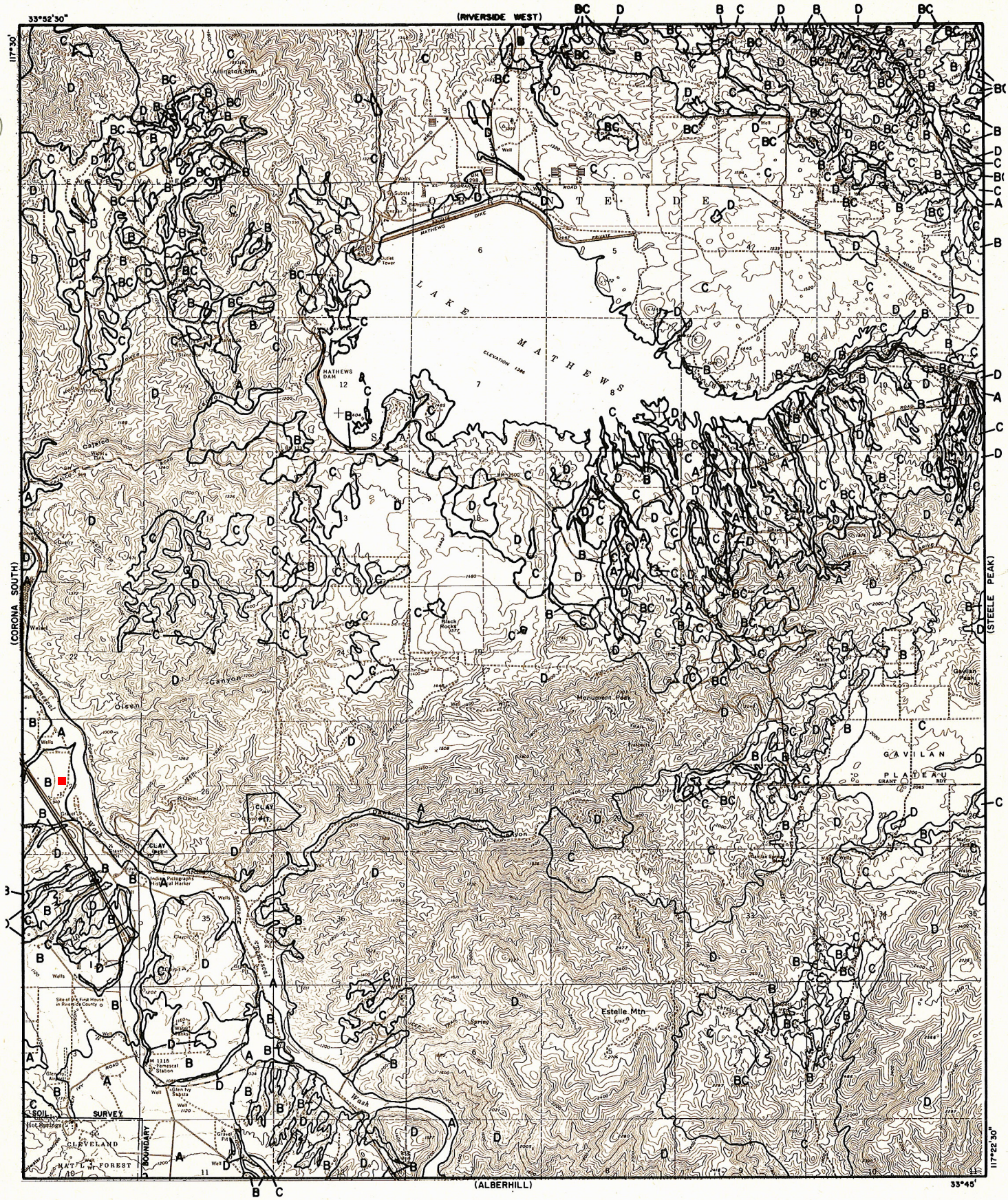
Mitigated Condition

	2-year				5-year				10-year			
Area (ac)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)	24-hr (cfs)	6-hr (cfs)	3-hr (cfs)	1-hr (cfs)
11.80	**0.78**	**0.93**	**0.90**	**1.15**	**1.16**	**1.15**	**1.15**	**1.46**	**3.54**	**1.34**	**1.35**	**1.72**

The underground storage analysis indicates that the proposed condition peak discharges from the project site for the 2-year, 5-year and 10-year return frequencies with 24-hour, 6-hour, 3-hour and 1-hour storm durations does not exceed the existing condition level for any of the twelve return frequency / storm duration combinations that have been analyzed.

Technical Appendix A

References
Soil and Rainfall Plates



LEGEND

—— SOILS GROUP BOUNDARY

A SOILS GROUP DESIGNATION

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0 FEET 5000

HYDROLOGIC SOILS GROUP MAP FOR LAKE MATHEWS

PLATE C-1.28

NOTES:
1. Isohyetals based on NOAA Atlas 2, Volume XI - California, 1973

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RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT

2-YEAR — 1-HOUR PRECIPITATION

DRAWN BY R.A.S.
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DATE
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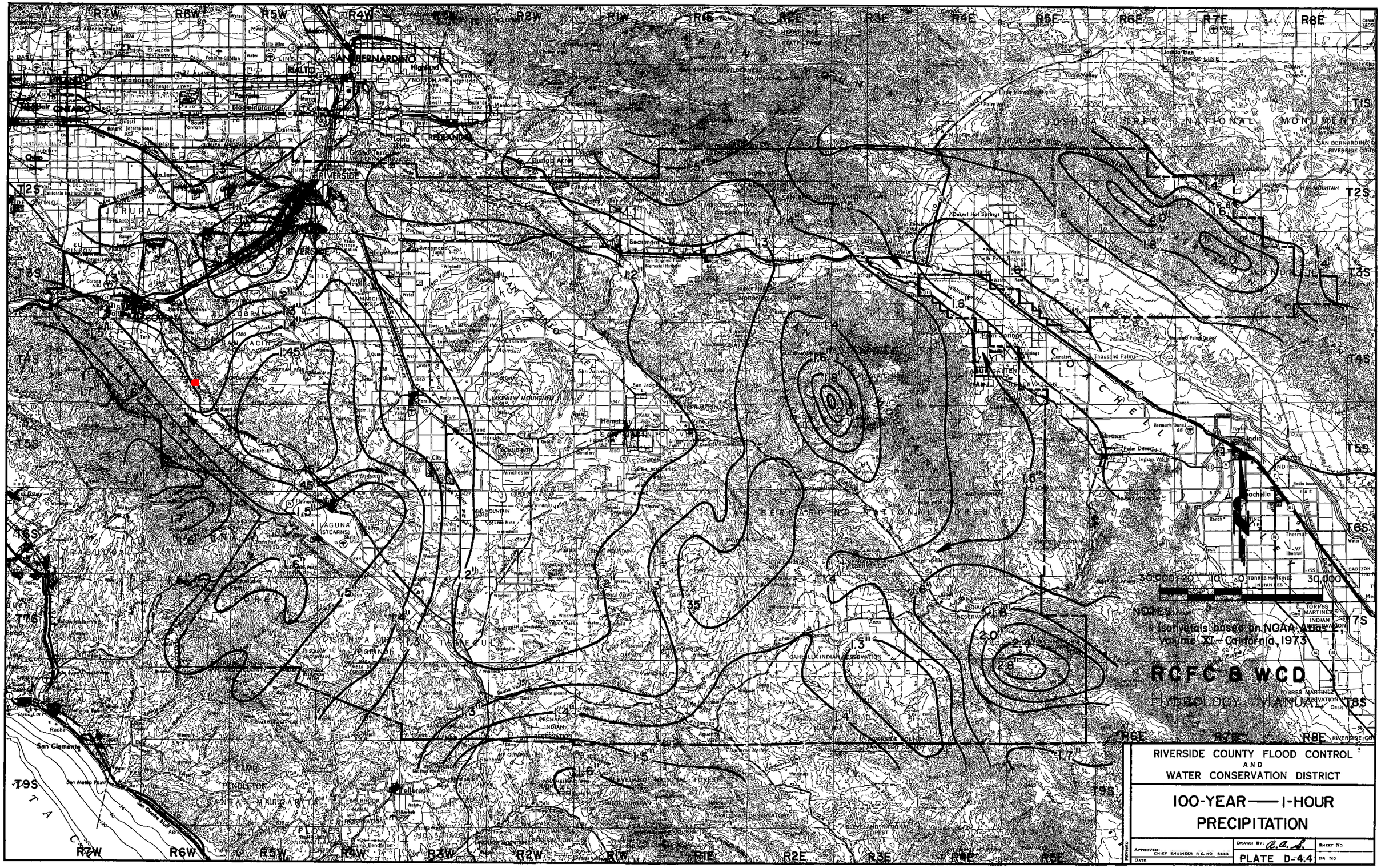
DR NO
PLATE D-4.3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SAN BERNARDINO
RIALTO
RIVERSIDE
RIVERSIDE COUNTY
NORTON AFB
Highland
Redlands
Loma Linda
Colton
Grand Terrace
Bloomington
Fontana
Ontario
Upland
Rancho Cucamonga
Mira Loma
Jurupa
Corona
Norco
Eastvale
Beaumont
Banning
Calimesa
Cherry Valley
Sunnymead
Moreno
Edgemont
Box Springs
Woodcrest
March Field
MARCH AIR RESERVE BASE
Lake Mathews
Lake Perris
Perris
Mead Valley
Good Hope
Winchester
Hemet
San Jacinto
Lakeview
Romoland
Homeland
Green Acres
Valle Vista
Idyllwild
Pine Cove
Mountain Center
Aguanga
Anza
Cahuilla
Thermal
Oasis
Mecca
Coachella
Indio
Palm Springs
Cathedral City
Rancho Mirage
Palm Desert
Indian Wells
La Quinta
Desert Hot Springs
Thousand Palms
Whitewater
Morongo Valley
Yucca Valley
Joshua Tree
Twentynine Palms
Landers
Pioneertown
Big Bear Lake
Big Bear City
Fawnskin
Running Springs
Arrowbear Lake
Crestline
Lake Arrowhead
Rimforest
Twin Peaks
Cedar Glen
Wrightwood
Phelan
Pinon Hills
Oak Hills
Hesperia
Victorville
Apple Valley
Lucerne Valley
Barstow
Yermo
Daggett
Newberry Springs
Ludlow
Amboy
Twentynine Palms
Joshua Tree National Monument
San Bernardino National Forest
Cleveland National Forest
Santa Margarita
Camp Pendleton
Fallbrook
Bonsall
Vista
San Clemente
San Mateo Point
Rancho California
Temecula
Murrieta
Wildomar
Lake Elsinore
Canyon Lake
Menifee
Sun City
Quail Valley
Romoland
Homeland
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Valle Vista
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Pine Cove
Mountain Center
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Fallbrook
Bonsall
Vista
San Clemente
San Mateo Point
Rancho California
Temecula
Murrieta
Wildomar
Lake Elsinore
Canyon Lake
Menifee
Sun City
Quail Valley
SAN JACINTO MOUNTAINS
SAN JACINTO WILDERNESS
SAN JACINTO PEAK
SAN JACINTO RIVER
SANTA ANA RIVER
SANTA MARGARITA RIVER
SAN LUIS REY RIVER
SAN DIEGUITO RIVER
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SAN ANDREAS FAULT
CHINO FAULT
ELSINORE FAULT
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TEMECULA VALLEY
COACHELLA VALLEY
MORONGO VALLEY
LUCERNE VALLEY
MISSION VALLEY
SAN DIEGO AQUEDUCT
COLORADO RIVER AQUEDUCT
METROPOLITAN AQUEDUCT
SANTA ANA MOUNTAINS
SANTA ROSA PLATEAU
LAKEVIEW MOUNTAINS
PECHANGA INDIAN RESERVATION
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TORRES MARTINEZ INDIAN RESERVATION
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NOTES
1. Isohyetals based on NOAA Atlas 2, Volume XI - California, 1973
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RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT
100-YEAR — 1-HOUR PRECIPITATION
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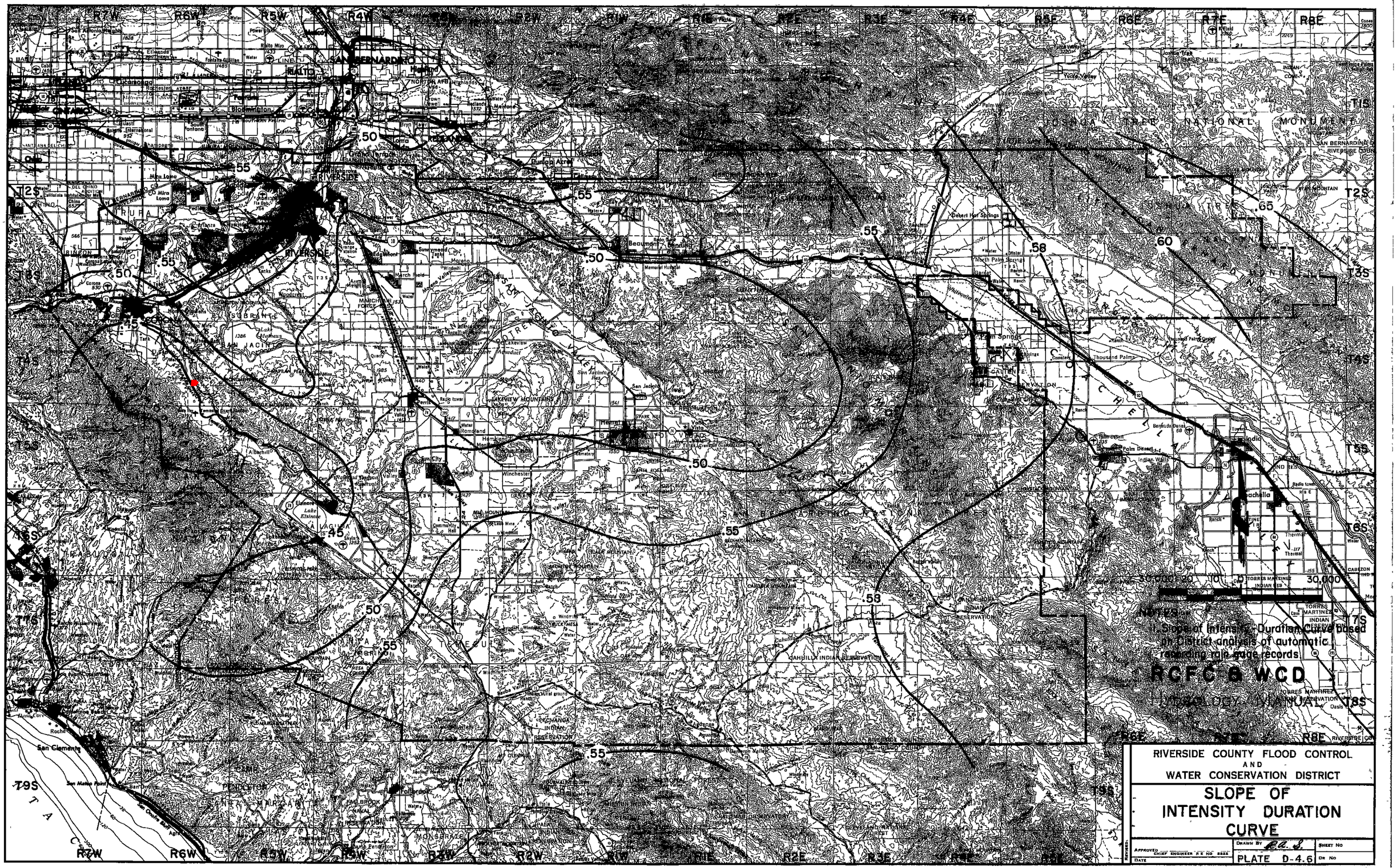

NOTES

1. Slope of Intensity-Duration Curve based on District analysis of automatic recording rain gage records

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SLOPE OF INTENSITY DURATION CURVE

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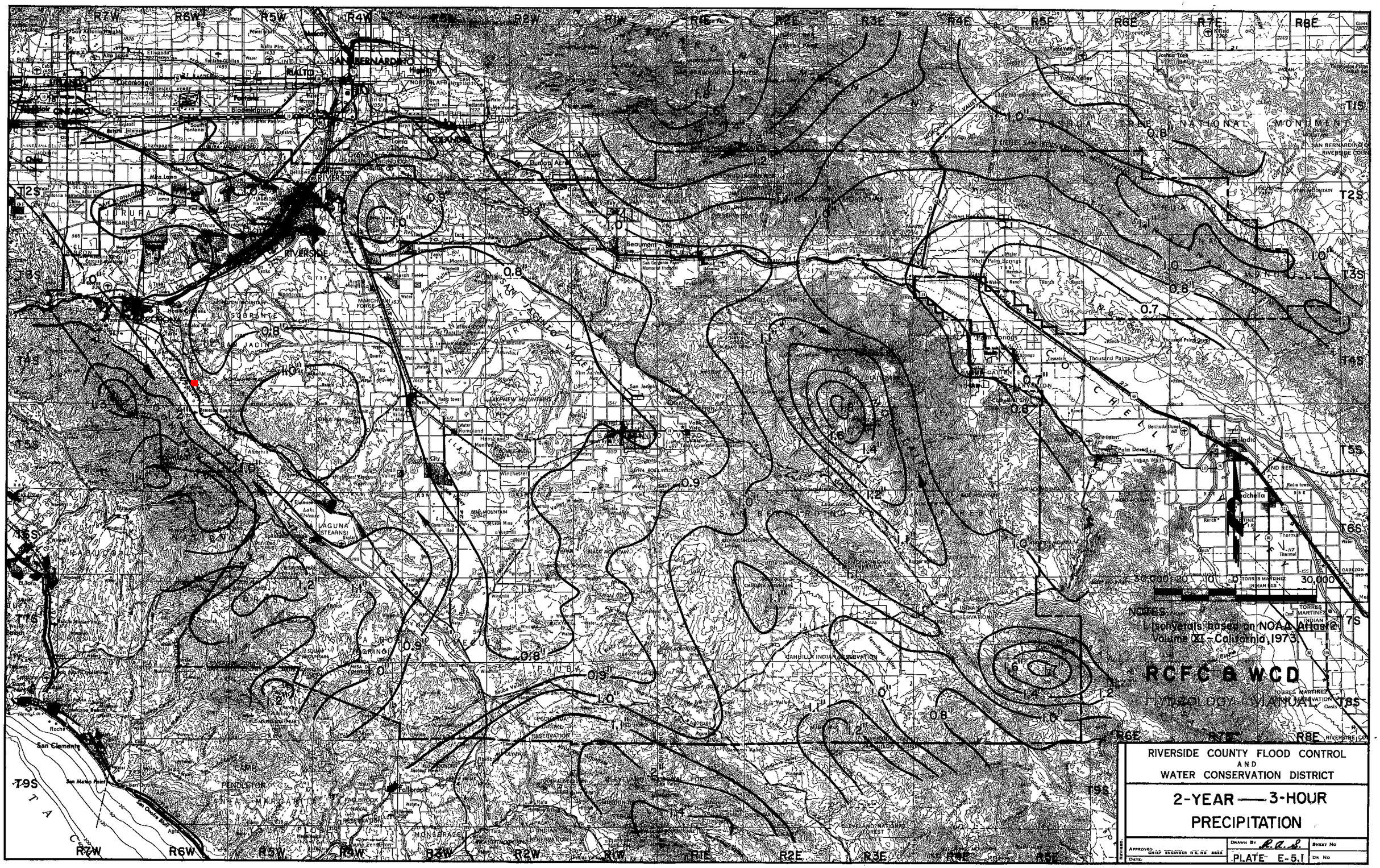

NOTES:

1. Isohyetals based on NOAA Atlas 2, Volume XI - California, 1973.

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2-YEAR —— 3-HOUR PRECIPITATION

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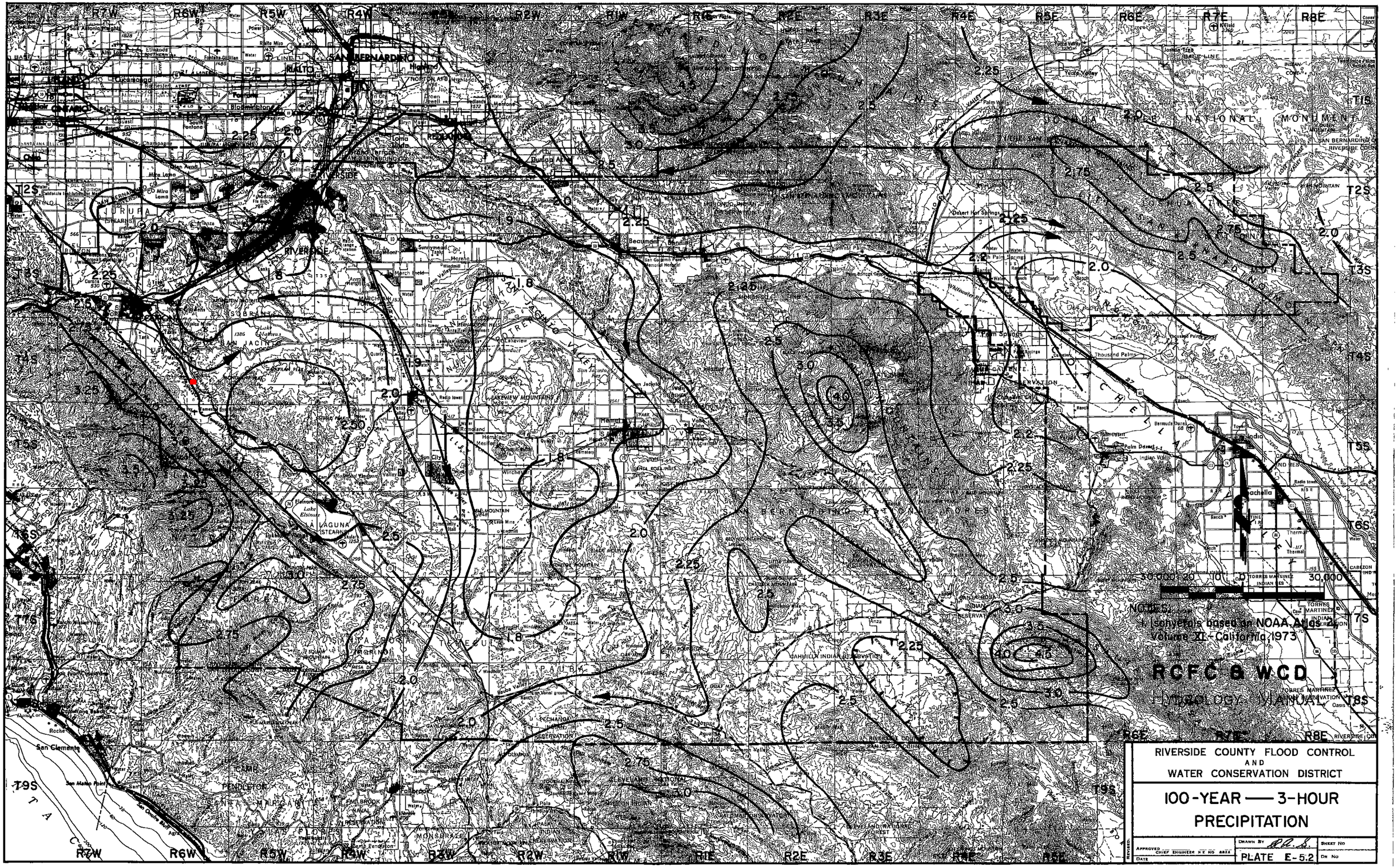

NOTES:

1. Isohyetals based on NOAA Atlas 2, Volume XI - California, 1973

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100-YEAR — 3-HOUR PRECIPITATION

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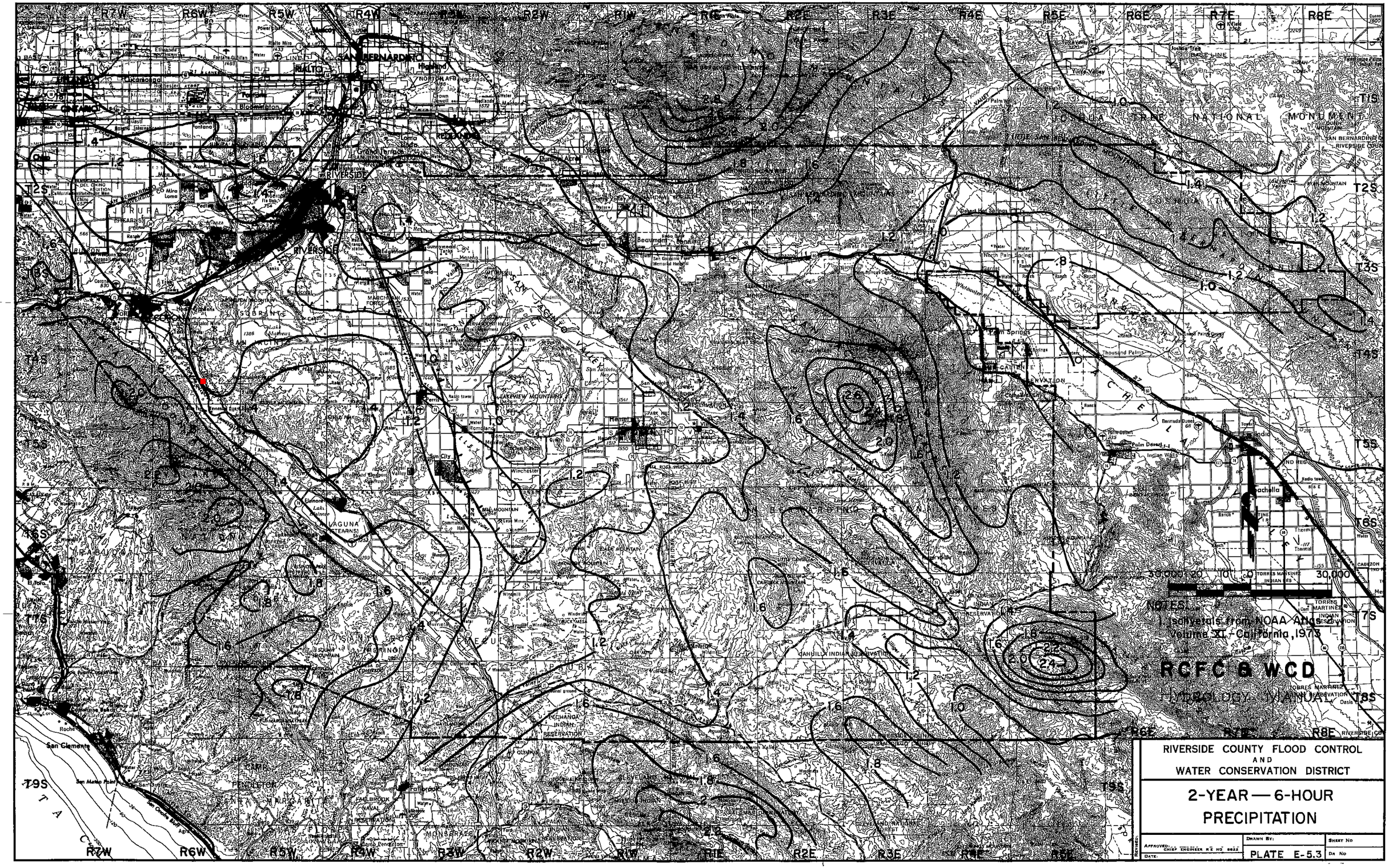

RIVERSIDE COUNTY FLOOD CONTROL
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2-YEAR — 6-HOUR PRECIPITATION

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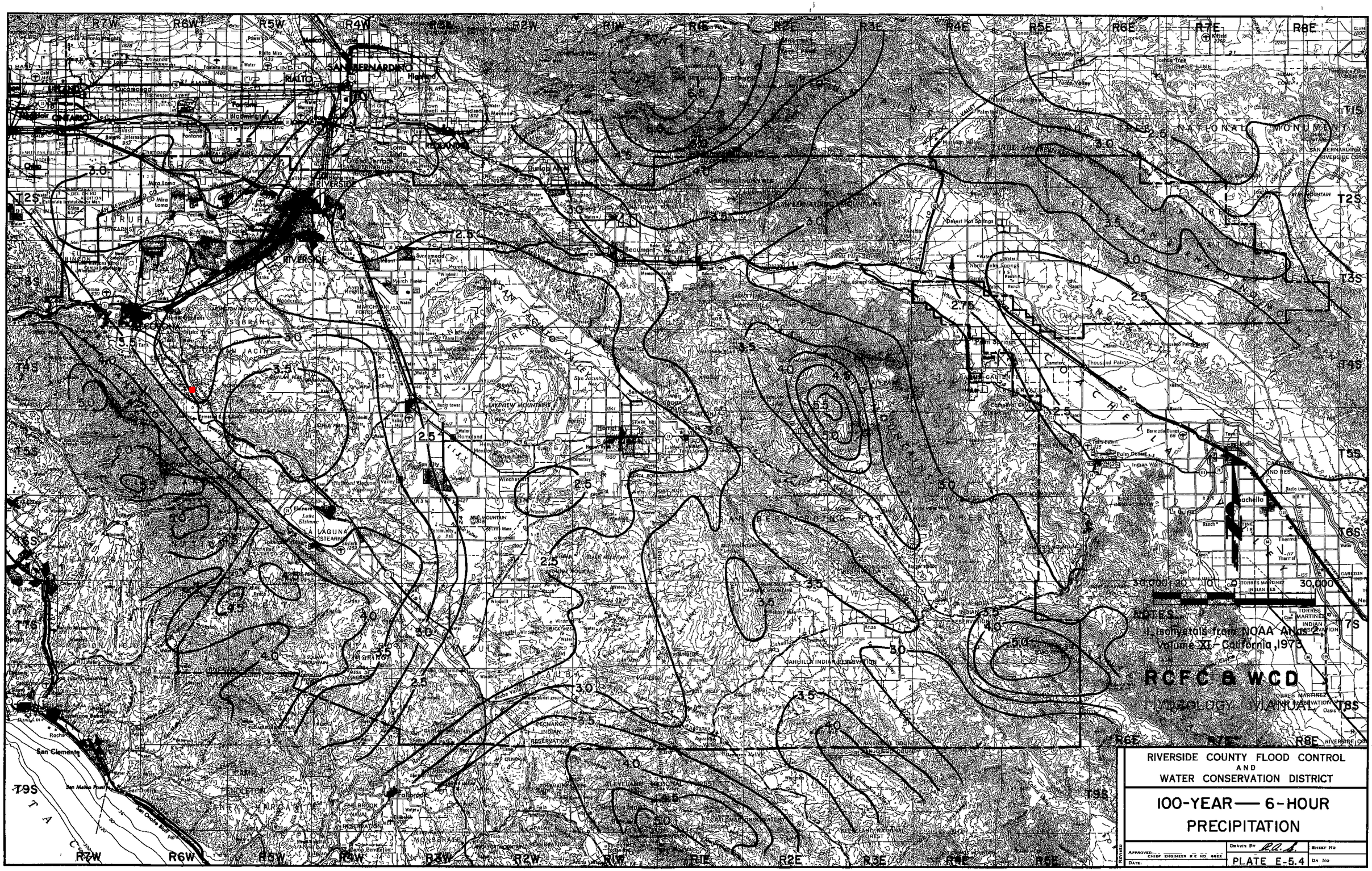

RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT

100-YEAR — 6-HOUR PRECIPITATION

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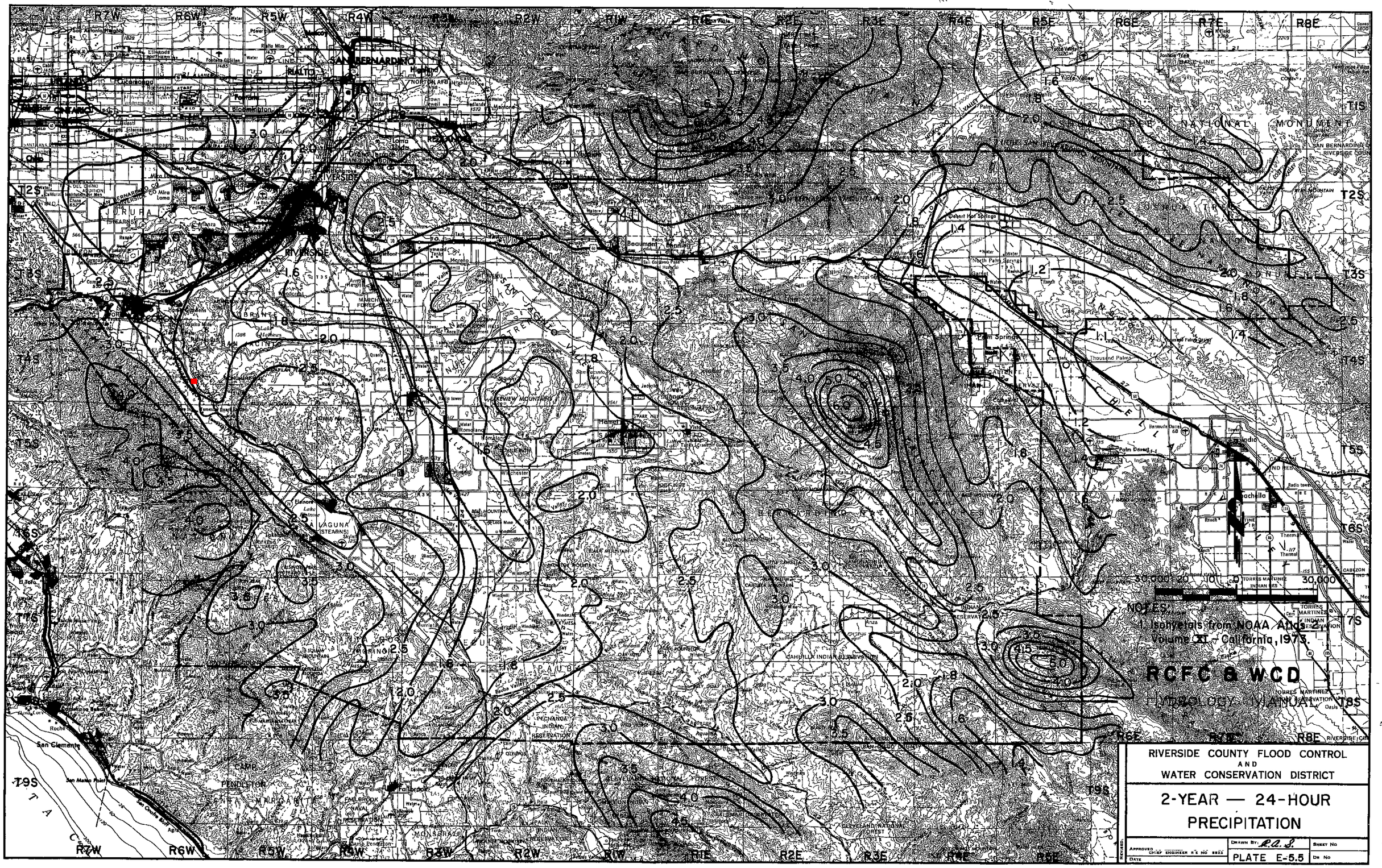

NOTES:
1. Isohyetals from NOAA Atlas 2, Volume XI - California, 1973.

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2-YEAR — 24-HOUR PRECIPITATION

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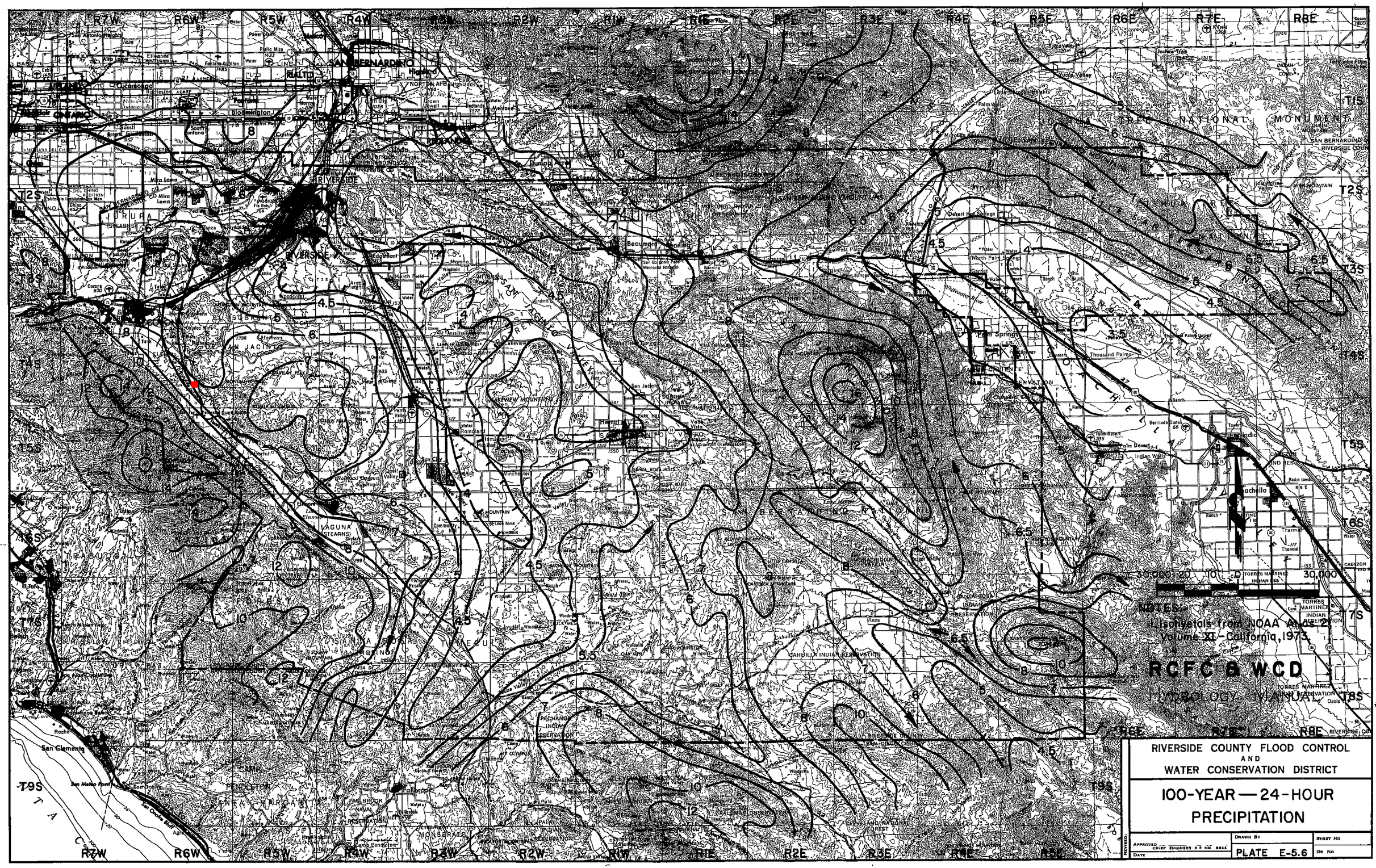
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SAN BERNARDINO
RIALTO
RIVERSIDE
COLTON
LOMA LINDA
REDLANDS
Mira Loma
JURUPA
Corona
Norco
Edgemont
Moreno
Box Springs Mts.
Beaumont
Banning
San Gorgonio Pass
Desert Hot Springs
North Palm Springs
Palm Springs
Thousand Palms
Indio
Bermuda Dunes
Indian Wells
La Quinta
Palm Desert
Coachella
Thermal
Mecca
Salton Sea
Oasis
Valerie
Perris
Lake Perris
Lake Elsinore
Elsinore
Wildomar
Murrieta
Temecula
Winchester
Hemet
San Jacinto
Soboba Indian Reservation
Lakeview Mountains
Double Butte
Santa Rosa Mts.
Santa Rosa Mountains National Forest
Agua Caliente Indian Reservation
Cahuilla Indian Reservation
Torres Martinez Indian Reservation
Pechanga Indian Reservation
Fallbrook
Bonsall
Vista
Oceanside
San Clemente
San Mateo Point
Camp Pendleton
Laguna Mountains
Cleveland National Forest
Palomar Mountain
Anza
Aguanga
Warner Springs
Valley Center
Escondido
Rancho Santa Fe
Del Mar
Poway
Ramona
Julian
Cuyamaca
Descanso
Pine Valley
Jacumba
Boulevard
Campo
Tecate
Mexico
Joshua Tree National Monument
Pinto Mountain
Dos Palmas
Chuckwalla Valley
Chuckwalla Mountains
Palen Mountains
Palo Verde Valley
Blythe
Ripley
Desert Center
Eagle Mountain
Eagle Mountains
Orocopia Mountains
Chocolate Mountains
Coachella Valley
Whitewater River
Whitewater
Mission Creek
Garnet Hill
Morongo Valley
Yucca Valley
Twentynine Palms
Twentynine Palms Indian Reservation
Cabazon
Cabazon Indian Reservation
Torres Martinez Indian Reservation
Oasis
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Temescal Mts.
Gavilan Hills
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Lake Skinner
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Diamond Valley Lake
Domenigoni Valley
Menifee
Sun City
Romoland
Homeland
Green River
Corona
Norco
Eastvale
Jurupa Valley
Mira Loma
Rubidoux
Riverside
Arlington
Canyon Lake
Lake Elsinore
Wildomar
Murrieta
Temecula
Pechanga
Rancho California
Fallbrook
Bonsall
Vista
Oceanside
San Clemente
San Mateo Point
Camp Pendleton
San Onofre State Beach
Interstate 15
Interstate 10
Interstate 215
Interstate 5
Interstate 8
Interstate 405
Interstate 605
State Route 91
State Route 60
State Route 71
State Route 74
State Route 79
State Route 111
State Route 86
State Route 78
State Route 62
State Route 177
State Route 243
State Route 247
State Route 371
State Route 395
State Route 76
State Route 94
State Route 125
State Route 163
State Route 52
State Route 67
State Route 78
State Route 79
State Route 98
State Route 111
State Route 115
State Route 118
State Route 126
State Route 134
State Route 138
State Route 142
State Route 154
State Route 166
State Route 178
State Route 186
State Route 187
State Route 190
State Route 195
State Route 198
State Route 199
State Route 203
State Route 210
State Route 213
State Route 215
State Route 217
State Route 219
State Route 220
State Route 223
State Route 225
State Route 227
State Route 229
State Route 231
State Route 233
State Route 235
State Route 237
State Route 239
State Route 241
State Route 243
State Route 245
State Route 247
State Route

Technical Appendix B

Rational Method Hydrologic Analysis
Existing Condition

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON
         RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT
                      (RCFC&WCD)  1978 HYDROLOGY MANUAL
          (c) Copyright 1982-2003 Advanced Engineering Software (aes)
                      (Rational Tabling Version 5.9D)
                  Release Date: 01/01/2003  License ID 1510

                           Analysis prepared by:

                           DRC Engineering, Inc.
                  160 South Old Springs Road, Suite 210
                     Anaheim Hills, California 92808
                  Tel: 714-685-6860 * Fax: 714-685-6801

 ************************** DESCRIPTION OF STUDY **************************
* TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY                         *
* EXISTING CONDITION                                                      *
* HYDROLOGIC ANALYSIS - 10-YEAR                                           *
 **************************************************************************

  FILE NAME: 2216E010.DAT
  TIME/DATE OF STUDY: 12:00 10/13/2022
--------------------------------------------------------------------------
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
--------------------------------------------------------------------------
  USER SPECIFIED STORM EVENT(YEAR) =   10.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =  12.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
  2-YEAR, 1-HOUR PRECIPITATION(INCH) =  0.540
  100-YEAR, 1-HOUR PRECIPITATION(INCH) =  1.360
  COMPUTED RAINFALL INTENSITY DATA:
  STORM EVENT =   10.00   1-HOUR INTENSITY(INCH/HOUR) =   0.886
  SLOPE OF INTENSITY DURATION CURVE = 0.4800
  RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
  NOTE: CONSIDER ALL CONFLUENCE STREAM COMBINATIONS
        FOR ALL DOWNSTREAM ANALYSES
  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

**************************************************************************
  FLOW PROCESS FROM NODE     10.00 TO NODE     11.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
==========================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   823.00
  UPSTREAM ELEVATION(FEET) =    919.00
  DOWNSTREAM ELEVATION(FEET) =    909.30
  ELEVATION DIFFERENCE(FEET) =      9.70
  TC = 0.303*[(  823.00**3)/(     9.70)]**.2 =   10.801
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.018
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8692
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      3.96
  TOTAL AREA(ACRES) =      2.26   TOTAL RUNOFF(CFS) =      3.96

**************************************************************************
```

```
 FLOW PROCESS FROM NODE     11.00 TO NODE     12.00 IS CODE =  52
----------------------------------------------------------------------------
 >>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =    909.30  DOWNSTREAM(FEET) =    905.00
 CHANNEL LENGTH THRU SUBAREA(FEET) =   547.00   CHANNEL SLOPE =  0.0079
 CHANNEL FLOW THRU SUBAREA(CFS) =      3.96
 FLOW VELOCITY(FEET/SEC) =   1.77 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
 TRAVEL TIME(MIN.) =   5.14   Tc(MIN.) =  15.94
 LONGEST FLOWPATH FROM NODE     10.00 TO NODE     12.00 =  1370.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE     12.00 TO NODE     12.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.674
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8654
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    0.28   SUBAREA RUNOFF(CFS) =    0.41
 TOTAL AREA(ACRES) =      2.54   TOTAL RUNOFF(CFS) =    4.37
 TC(MIN.) =  15.94

****************************************************************************
 FLOW PROCESS FROM NODE     12.00 TO NODE     12.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.674
 UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .5536
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    4.05   SUBAREA RUNOFF(CFS) =    3.75
 TOTAL AREA(ACRES) =      6.59   TOTAL RUNOFF(CFS) =    8.12
 TC(MIN.) =  15.94

****************************************************************************
 FLOW PROCESS FROM NODE     12.00 TO NODE     22.00 IS CODE =  52
----------------------------------------------------------------------------
 >>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =    905.00  DOWNSTREAM(FEET) =    902.90
 CHANNEL LENGTH THRU SUBAREA(FEET) =   178.00   CHANNEL SLOPE =  0.0118
 CHANNEL FLOW THRU SUBAREA(CFS) =      8.12
 FLOW VELOCITY(FEET/SEC) =   2.58 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
 TRAVEL TIME(MIN.) =   1.15   Tc(MIN.) =  17.10
 LONGEST FLOWPATH FROM NODE     10.00 TO NODE     22.00 =  1548.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.619
 UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .5464
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    3.19   SUBAREA RUNOFF(CFS) =    2.82
 TOTAL AREA(ACRES) =      9.78   TOTAL RUNOFF(CFS) =   10.94
 TC(MIN.) =  17.10

****************************************************************************
 FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =   1
----------------------------------------------------------------------------
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
 TOTAL NUMBER OF STREAMS =  2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
 TIME OF CONCENTRATION(MIN.) =  17.10
 RAINFALL INTENSITY(INCH/HR) =   1.62
 TOTAL STREAM AREA(ACRES) =     9.78
 PEAK FLOW RATE(CFS) AT CONFLUENCE =     10.94
```

```
****************************************************************************
  FLOW PROCESS FROM NODE     20.00 TO NODE     21.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS: UNDEVELOPED WITH POOR COVER
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   730.00
  UPSTREAM ELEVATION(FEET) =    917.00
  DOWNSTREAM ELEVATION(FEET) =    903.80
  ELEVATION DIFFERENCE(FEET) =     13.20
  TC = 0.533*[(  730.00**3)/(    13.20)]**.2 =   16.607
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.642
  UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .5494
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      1.64
  TOTAL AREA(ACRES) =      1.82   TOTAL RUNOFF(CFS) =      1.64

****************************************************************************
  FLOW PROCESS FROM NODE     21.00 TO NODE     22.00 IS CODE =  52
----------------------------------------------------------------------------
  >>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =    903.80  DOWNSTREAM(FEET) =    902.90
  CHANNEL LENGTH THRU SUBAREA(FEET) =   537.00   CHANNEL SLOPE =  0.0017
  CHANNEL FLOW THRU SUBAREA(CFS) =      1.64
  FLOW VELOCITY(FEET/SEC) =   0.68 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
  TRAVEL TIME(MIN.) =  13.23   Tc(MIN.) =  29.84
  LONGEST FLOWPATH FROM NODE     20.00 TO NODE     22.00 =  1267.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.239
  UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4877
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.20   SUBAREA RUNOFF(CFS) =    0.12
  TOTAL AREA(ACRES) =      2.02   TOTAL RUNOFF(CFS) =    1.76
  TC(MIN.) =  29.84

****************************************************************************
  FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =  29.84
  RAINFALL INTENSITY(INCH/HR) =   1.24
  TOTAL STREAM AREA(ACRES) =     2.02
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      1.76

  ** CONFLUENCE DATA **
  STREAM     RUNOFF      Tc      INTENSITY      AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
      1       10.94    17.10        1.619          9.78
      2        1.76    29.84        1.239          2.02

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
  STREAM     RUNOFF      Tc      INTENSITY
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
      1       11.95    17.10        1.619
      2       10.14    29.84        1.239
```

```
  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =     11.95   Tc(MIN.) =   17.10
  TOTAL AREA(ACRES) =     11.80
  LONGEST FLOWPATH FROM NODE     10.00 TO NODE     22.00 =  1548.00 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =     11.80  TC(MIN.) =     17.10
  PEAK FLOW RATE(CFS)   =     11.95
  *** PEAK FLOW RATE TABLE ***
         Q(CFS)   Tc(MIN.)
  1       11.95      17.10
  2       10.14      29.84
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
           RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON
        RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT
                    (RCFC&WCD)  1978 HYDROLOGY MANUAL
         (c) Copyright 1982-2003 Advanced Engineering Software (aes)
                    (Rational Tabling Version 5.9D)
                Release Date: 01/01/2003  License ID 1510

                        Analysis prepared by:

                        DRC Engineering, Inc.
                160 South Old Springs Road, Suite 210
                   Anaheim Hills, California 92808
                Tel: 714-685-6860 * Fax: 714-685-6801

 ************************* DESCRIPTION OF STUDY *************************
* TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY                       *
* EXISTING CONDITION                                                    *
* HYDROLOGIC ANALYSIS - 100-YEAR                                        *
 ************************************************************************

  FILE NAME: 2216E100.DAT
  TIME/DATE OF STUDY: 10:00 10/03/2022
------------------------------------------------------------------------
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
------------------------------------------------------------------------
  USER SPECIFIED STORM EVENT(YEAR) =  100.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =  12.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
  2-YEAR, 1-HOUR PRECIPITATION(INCH) =  0.540
  100-YEAR, 1-HOUR PRECIPITATION(INCH) =  1.360
  COMPUTED RAINFALL INTENSITY DATA:
  STORM EVENT =  100.00   1-HOUR INTENSITY(INCH/HOUR) =   1.360
  SLOPE OF INTENSITY DURATION CURVE = 0.4800
  RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
  NOTE: CONSIDER ALL CONFLUENCE STREAM COMBINATIONS
        FOR ALL DOWNSTREAM ANALYSES
  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

**************************************************************************
  FLOW PROCESS FROM NODE     10.00 TO NODE     11.00 IS CODE =  21
------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
========================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   823.00
  UPSTREAM ELEVATION(FEET) =    919.00
  DOWNSTREAM ELEVATION(FEET) =    909.30
  ELEVATION DIFFERENCE(FEET) =      9.70
  TC = 0.303*[(  823.00**3)/(     9.70)]**.2 =   10.801
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.097
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8773
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      6.14
  TOTAL AREA(ACRES) =      2.26   TOTAL RUNOFF(CFS) =      6.14

**************************************************************************
```

```
 FLOW PROCESS FROM NODE     11.00 TO NODE     12.00 IS CODE =  52
----------------------------------------------------------------------------
 >>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =    909.30  DOWNSTREAM(FEET) =    905.00
 CHANNEL LENGTH THRU SUBAREA(FEET) =   547.00   CHANNEL SLOPE =  0.0079
 CHANNEL FLOW THRU SUBAREA(CFS) =      6.14
 FLOW VELOCITY(FEET/SEC) =   1.96 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
 TRAVEL TIME(MIN.) =   4.64   Tc(MIN.) =  15.44
 LONGEST FLOWPATH FROM NODE     10.00 TO NODE     12.00 =  1370.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE     12.00 TO NODE     12.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.609
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8742
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    0.28   SUBAREA RUNOFF(CFS) =    0.64
 TOTAL AREA(ACRES) =      2.54   TOTAL RUNOFF(CFS) =    6.78
 TC(MIN.) =  15.44

****************************************************************************
 FLOW PROCESS FROM NODE     12.00 TO NODE     12.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.609
 UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .6421
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    4.05   SUBAREA RUNOFF(CFS) =    6.79
 TOTAL AREA(ACRES) =      6.59   TOTAL RUNOFF(CFS) =   13.56
 TC(MIN.) =  15.44

****************************************************************************
 FLOW PROCESS FROM NODE     12.00 TO NODE     22.00 IS CODE =  52
----------------------------------------------------------------------------
 >>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =    905.00  DOWNSTREAM(FEET) =    902.90
 CHANNEL LENGTH THRU SUBAREA(FEET) =   178.00   CHANNEL SLOPE =  0.0118
 CHANNEL FLOW THRU SUBAREA(CFS) =     13.56
 FLOW VELOCITY(FEET/SEC) =   2.94 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
 TRAVEL TIME(MIN.) =   1.01   Tc(MIN.) =  16.45
 LONGEST FLOWPATH FROM NODE     10.00 TO NODE     22.00 =  1548.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.531
 UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .6365
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    3.19   SUBAREA RUNOFF(CFS) =    5.14
 TOTAL AREA(ACRES) =      9.78   TOTAL RUNOFF(CFS) =   18.70
 TC(MIN.) =  16.45

****************************************************************************
 FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =   1
----------------------------------------------------------------------------
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
 TOTAL NUMBER OF STREAMS =  2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
 TIME OF CONCENTRATION(MIN.) =  16.45
 RAINFALL INTENSITY(INCH/HR) =   2.53
 TOTAL STREAM AREA(ACRES) =     9.78
 PEAK FLOW RATE(CFS) AT CONFLUENCE =     18.70
```

```
****************************************************************************
  FLOW PROCESS FROM NODE     20.00 TO NODE     21.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS: UNDEVELOPED WITH POOR COVER
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   730.00
  UPSTREAM ELEVATION(FEET) =    917.00
  DOWNSTREAM ELEVATION(FEET) =    903.80
  ELEVATION DIFFERENCE(FEET) =     13.20
  TC = 0.533*[(  730.00**3)/(    13.20)]**.2 =   16.607
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.520
  UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .6357
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      2.91
  TOTAL AREA(ACRES) =      1.82   TOTAL RUNOFF(CFS) =      2.91

****************************************************************************
  FLOW PROCESS FROM NODE     21.00 TO NODE     22.00 IS CODE =  52
----------------------------------------------------------------------------
  >>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =    903.80  DOWNSTREAM(FEET) =    902.90
  CHANNEL LENGTH THRU SUBAREA(FEET) =   537.00   CHANNEL SLOPE =  0.0017
  CHANNEL FLOW THRU SUBAREA(CFS) =      2.91
  FLOW VELOCITY(FEET/SEC) =   0.76 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
  TRAVEL TIME(MIN.) =  11.72   Tc(MIN.) =  28.32
  LONGEST FLOWPATH FROM NODE     20.00 TO NODE     22.00 =  1267.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.950
  UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .5855
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.20   SUBAREA RUNOFF(CFS) =    0.23
  TOTAL AREA(ACRES) =      2.02   TOTAL RUNOFF(CFS) =    3.14
  TC(MIN.) =  28.32

****************************************************************************
  FLOW PROCESS FROM NODE     22.00 TO NODE     22.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =  28.32
  RAINFALL INTENSITY(INCH/HR) =   1.95
  TOTAL STREAM AREA(ACRES) =     2.02
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      3.14

  ** CONFLUENCE DATA **
  STREAM     RUNOFF      Tc      INTENSITY      AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
      1       18.70    16.45        2.531          9.78
      2        3.14    28.32        1.950          2.02

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
  STREAM     RUNOFF      Tc      INTENSITY
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
      1       20.53    16.45       2.531
      2       17.55    28.32       1.950
```

```
  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =     20.53   Tc(MIN.) =   16.45
  TOTAL AREA(ACRES) =     11.80
  LONGEST FLOWPATH FROM NODE     10.00 TO NODE     22.00 =  1548.00 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =     11.80  TC(MIN.) =     16.45
  PEAK FLOW RATE(CFS)   =     20.53
  *** PEAK FLOW RATE TABLE ***
         Q(CFS)   Tc(MIN.)
  1       20.53      16.45
  2       17.55      28.32
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

Technical Appendix C

Rational Method Hydrologic Analysis
Proposed Condition

```
**************************************************************************
           RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON
        RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT
                    (RCFC&WCD)  1978 HYDROLOGY MANUAL
         (c) Copyright 1982-2003 Advanced Engineering Software (aes)
                    (Rational Tabling Version 5.9D)
                Release Date: 01/01/2003  License ID 1510

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 ************************* DESCRIPTION OF STUDY *************************
* TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY                        *
* PROPOSED CONDITION                                                     *
* HYDROLOGIC ANALYSIS - 10-YEAR                                          *
 ************************************************************************

  FILE NAME: 2216P010.DAT
  TIME/DATE OF STUDY: 12:00 10/13/2022
------------------------------------------------------------------------
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
------------------------------------------------------------------------
  USER SPECIFIED STORM EVENT(YEAR) =   10.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =  12.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
  2-YEAR, 1-HOUR PRECIPITATION(INCH) =  0.540
  100-YEAR, 1-HOUR PRECIPITATION(INCH) =  1.360
  COMPUTED RAINFALL INTENSITY DATA:
  STORM EVENT =   10.00   1-HOUR INTENSITY(INCH/HOUR) =   0.886
  SLOPE OF INTENSITY DURATION CURVE = 0.4800
  RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
  NOTE: CONSIDER ALL CONFLUENCE STREAM COMBINATIONS
        FOR ALL DOWNSTREAM ANALYSES
  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

**************************************************************************
  FLOW PROCESS FROM NODE    101.00 TO NODE    101.00 IS CODE =  22
------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
========================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  USER SPECIFIED Tc(MIN.) =    5.000
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.921
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8762
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      0.90
  TOTAL AREA(ACRES) =      0.35   TOTAL RUNOFF(CFS) =      0.90

**************************************************************************
  FLOW PROCESS FROM NODE    101.00 TO NODE    102.00 IS CODE =  31
------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
========================================================================
```

```
  ELEVATION DATA: UPSTREAM(FEET) =   906.80  DOWNSTREAM(FEET) =   906.08
  FLOW LENGTH(FEET) =   142.00   MANNING'S N =  0.012
  ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   4.9 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.00
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      0.90
  PIPE TRAVEL TIME(MIN.) =   0.79    Tc(MIN.) =   5.79
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    102.00 =   142.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    102.00 TO NODE    102.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.723
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8750
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.52   SUBAREA RUNOFF(CFS) =    1.24
  TOTAL AREA(ACRES) =      0.87   TOTAL RUNOFF(CFS) =    2.13
  TC(MIN.) =   5.79

****************************************************************************
  FLOW PROCESS FROM NODE    102.00 TO NODE    103.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   906.08  DOWNSTREAM(FEET) =   905.50
  FLOW LENGTH(FEET) =   115.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   8.3 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.70
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      2.13
  PIPE TRAVEL TIME(MIN.) =   0.52    Tc(MIN.) =   6.31
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    103.00 =   257.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    103.00 TO NODE    103.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.613
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8742
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.63   SUBAREA RUNOFF(CFS) =    1.44
  TOTAL AREA(ACRES) =      1.50   TOTAL RUNOFF(CFS) =    3.57
  TC(MIN.) =   6.31

****************************************************************************
  FLOW PROCESS FROM NODE    103.00 TO NODE    112.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   905.50  DOWNSTREAM(FEET) =   905.37
  FLOW LENGTH(FEET) =    25.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  15.0 INCH PIPE IS   9.7 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   4.28
  ESTIMATED PIPE DIAMETER(INCH) =  15.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      3.57
  PIPE TRAVEL TIME(MIN.) =   0.10    Tc(MIN.) =   6.40
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    112.00 =   282.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    112.00 TO NODE    112.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =   6.40
```

```
 RAINFALL INTENSITY(INCH/HR) =   2.59
 TOTAL STREAM AREA(ACRES) =     1.50
 PEAK FLOW RATE(CFS) AT CONFLUENCE =      3.57

****************************************************************************
 FLOW PROCESS FROM NODE    110.00 TO NODE    111.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
 TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
 INITIAL SUBAREA FLOW-LENGTH(FEET) =   237.00
 UPSTREAM ELEVATION(FEET) =    916.50
 DOWNSTREAM ELEVATION(FEET) =    910.00
 ELEVATION DIFFERENCE(FEET) =      6.50
 TC = 0.303*[(  237.00**3)/(     6.50)]**.2 =    5.544
   10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.779
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8754
 SOIL CLASSIFICATION IS "B"
 SUBAREA RUNOFF(CFS) =      0.61
 TOTAL AREA(ACRES) =      0.25   TOTAL RUNOFF(CFS) =      0.61

****************************************************************************
 FLOW PROCESS FROM NODE    111.00 TO NODE    112.00 IS CODE =  31
----------------------------------------------------------------------------
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =   905.50  DOWNSTREAM(FEET) =   905.37
 FLOW LENGTH(FEET) =    26.00   MANNING'S N =  0.012
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
 DEPTH OF FLOW IN  12.0 INCH PIPE IS   3.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) =   2.71
 ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
 PIPE-FLOW(CFS) =      0.61
 PIPE TRAVEL TIME(MIN.) =   0.16    Tc(MIN.) =   5.70
 LONGEST FLOWPATH FROM NODE    110.00 TO NODE    112.00 =   263.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    112.00 TO NODE    112.00 IS CODE =   1
----------------------------------------------------------------------------
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
 TOTAL NUMBER OF STREAMS =  2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
 TIME OF CONCENTRATION(MIN.) =   5.70
 RAINFALL INTENSITY(INCH/HR) =   2.74
 TOTAL STREAM AREA(ACRES) =     0.25
 PEAK FLOW RATE(CFS) AT CONFLUENCE =      0.61

 ** CONFLUENCE DATA **
 STREAM     RUNOFF      Tc      INTENSITY      AREA
 NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
     1        3.57     6.40        2.594         1.50
     2        0.61     5.70        2.742          0.25

 RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR  2 STREAMS.

 ** PEAK FLOW RATE TABLE **
 STREAM     RUNOFF      Tc      INTENSITY
 NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
     1        3.79     5.70       2.742
     2        4.15     6.40       2.594

 COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) =      4.15   Tc(MIN.) =    6.40
 TOTAL AREA(ACRES) =      1.75
 LONGEST FLOWPATH FROM NODE    101.00 TO NODE    112.00 =   282.00 FEET.
```

```
****************************************************************************
  FLOW PROCESS FROM NODE    112.00 TO NODE    113.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   905.37  DOWNSTREAM(FEET) =   903.83
  FLOW LENGTH(FEET) =    70.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   7.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   7.62
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      4.15
  PIPE TRAVEL TIME(MIN.) =   0.15    Tc(MIN.) =   6.56
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    113.00 =   352.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    113.00 TO NODE    131.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =   6.56
  RAINFALL INTENSITY(INCH/HR) =   2.56
  TOTAL STREAM AREA(ACRES) =     1.75
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      4.15

****************************************************************************
  FLOW PROCESS FROM NODE    120.00 TO NODE    121.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   586.00
  UPSTREAM ELEVATION(FEET) =    915.20
  DOWNSTREAM ELEVATION(FEET) =    906.30
  ELEVATION DIFFERENCE(FEET) =      8.90
  TC = 0.303*[(  586.00**3)/(     8.90)]**.2 =    8.963
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.207
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8710
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      4.52
  TOTAL AREA(ACRES) =      2.35   TOTAL RUNOFF(CFS) =      4.52

****************************************************************************
  FLOW PROCESS FROM NODE    121.00 TO NODE    122.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   903.80  DOWNSTREAM(FEET) =   903.23
  FLOW LENGTH(FEET) =   113.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  15.0 INCH PIPE IS  11.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   4.37
  ESTIMATED PIPE DIAMETER(INCH) =  15.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      4.52
  PIPE TRAVEL TIME(MIN.) =   0.43    Tc(MIN.) =   9.39
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    122.00 =   699.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    122.00 TO NODE    131.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =   9.39
  RAINFALL INTENSITY(INCH/HR) =   2.16
  TOTAL STREAM AREA(ACRES) =     2.35
```

```
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      4.52

  ** CONFLUENCE DATA **
  STREAM     RUNOFF      Tc      INTENSITY      AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
      1        3.79     5.86        2.707          1.75
      1        4.15     6.56        2.564          1.75
      2        4.52     9.39        2.158          2.35

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
  STREAM     RUNOFF      Tc      INTENSITY
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
      1        6.61     5.86       2.707
      2        7.30     6.56       2.564
      3        8.01     9.39       2.158

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =      8.01   Tc(MIN.) =    9.39
  TOTAL AREA(ACRES) =      4.10
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    131.00 =   699.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    131.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.158
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.32   SUBAREA RUNOFF(CFS) =    0.60
  TOTAL AREA(ACRES) =      4.42   TOTAL RUNOFF(CFS) =    8.61
  TC(MIN.) =   9.39

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    131.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.158
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.38   SUBAREA RUNOFF(CFS) =    0.71
  TOTAL AREA(ACRES) =      4.80   TOTAL RUNOFF(CFS) =    9.32
  TC(MIN.) =   9.39

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    131.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.158
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.51   SUBAREA RUNOFF(CFS) =    0.96
  TOTAL AREA(ACRES) =      5.31   TOTAL RUNOFF(CFS) =   10.28
  TC(MIN.) =   9.39

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    132.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   903.25  DOWNSTREAM(FEET) =   902.92
  FLOW LENGTH(FEET) =    31.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  18.0 INCH PIPE IS  13.6 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   7.16
  ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     10.28
```

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  PIPE TRAVEL TIME(MIN.) =   0.07    Tc(MIN.) =   9.47
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    132.00 =   730.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    132.00 TO NODE    132.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.150
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8705
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.13   SUBAREA RUNOFF(CFS) =    0.24
  TOTAL AREA(ACRES) =      5.44   TOTAL RUNOFF(CFS) =   10.53
  TC(MIN.) =   9.47

****************************************************************************
  FLOW PROCESS FROM NODE    132.00 TO NODE    133.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   898.88  DOWNSTREAM(FEET) =   897.91
  FLOW LENGTH(FEET) =   197.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  21.0 INCH PIPE IS  15.9 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   5.39
  ESTIMATED PIPE DIAMETER(INCH) =  21.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     10.53
  PIPE TRAVEL TIME(MIN.) =   0.61    Tc(MIN.) =  10.07
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    133.00 =   927.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    133.00 TO NODE    133.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.087
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8699
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.29   SUBAREA RUNOFF(CFS) =    0.53
  TOTAL AREA(ACRES) =      5.73   TOTAL RUNOFF(CFS) =   11.05
  TC(MIN.) =  10.07

****************************************************************************
  FLOW PROCESS FROM NODE    133.00 TO NODE    162.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   897.89  DOWNSTREAM(FEET) =   897.13
  FLOW LENGTH(FEET) =   157.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  21.0 INCH PIPE IS  16.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   5.37
  ESTIMATED PIPE DIAMETER(INCH) =  21.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     11.05
  PIPE TRAVEL TIME(MIN.) =   0.49    Tc(MIN.) =  10.56
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    162.00 =  1084.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    162.00 IS CODE =  10
----------------------------------------------------------------------------
  >>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
============================================================================

****************************************************************************
  FLOW PROCESS FROM NODE    140.00 TO NODE    141.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
          ASSUMED INITIAL SUBAREA UNIFORM
          DEVELOPMENT IS COMMERCIAL
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   398.00
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```
  UPSTREAM ELEVATION(FEET) =    916.50
  DOWNSTREAM ELEVATION(FEET) =    912.00
  ELEVATION DIFFERENCE(FEET) =      4.50
  TC = 0.303*[(  398.00**3)/(     4.50)]**.2 =    8.145
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.311
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8719
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      1.05
  TOTAL AREA(ACRES) =      0.52   TOTAL RUNOFF(CFS) =      1.05

****************************************************************************
  FLOW PROCESS FROM NODE    141.00 TO NODE    142.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   908.00  DOWNSTREAM(FEET) =   907.77
  FLOW LENGTH(FEET) =    48.00   MANNING'S N =  0.012
  ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   5.4 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.07
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      1.05
  PIPE TRAVEL TIME(MIN.) =   0.26    Tc(MIN.) =   8.41
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    142.00 =   446.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    142.00 TO NODE    142.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.276
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8716
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.28   SUBAREA RUNOFF(CFS) =    0.56
  TOTAL AREA(ACRES) =      0.80   TOTAL RUNOFF(CFS) =    1.60
  TC(MIN.) =   8.41

****************************************************************************
  FLOW PROCESS FROM NODE    142.00 TO NODE    143.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   907.77  DOWNSTREAM(FEET) =   907.25
  FLOW LENGTH(FEET) =   103.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   6.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.48
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      1.60
  PIPE TRAVEL TIME(MIN.) =   0.49    Tc(MIN.) =   8.90
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    143.00 =   549.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    143.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.215
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8711
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.23   SUBAREA RUNOFF(CFS) =    0.44
  TOTAL AREA(ACRES) =      1.03   TOTAL RUNOFF(CFS) =    2.05
  TC(MIN.) =   8.90

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    143.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.215
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8711
```

```
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    2.26   SUBAREA RUNOFF(CFS) =    4.36
  TOTAL AREA(ACRES) =      3.29   TOTAL RUNOFF(CFS) =    6.41
  TC(MIN.) =   8.90

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    144.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   907.25  DOWNSTREAM(FEET) =   907.21
  FLOW LENGTH(FEET) =     9.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  18.0 INCH PIPE IS  13.2 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   4.61
  ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      6.41
  PIPE TRAVEL TIME(MIN.) =   0.03    Tc(MIN.) =   8.93
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    144.00 =   558.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    144.00 TO NODE    144.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.211
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8711
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.21   SUBAREA RUNOFF(CFS) =    0.40
  TOTAL AREA(ACRES) =      3.50   TOTAL RUNOFF(CFS) =    6.81
  TC(MIN.) =   8.93

****************************************************************************
  FLOW PROCESS FROM NODE    144.00 TO NODE    145.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   907.21  DOWNSTREAM(FEET) =   906.56
  FLOW LENGTH(FEET) =   129.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  18.0 INCH PIPE IS  13.2 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   4.90
  ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      6.81
  PIPE TRAVEL TIME(MIN.) =   0.44    Tc(MIN.) =   9.37
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    145.00 =   687.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    161.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =   9.37
  RAINFALL INTENSITY(INCH/HR) =   2.16
  TOTAL STREAM AREA(ACRES) =     3.50
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      6.81

****************************************************************************
  FLOW PROCESS FROM NODE    150.00 TO NODE    151.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   612.00
  UPSTREAM ELEVATION(FEET) =    914.60
  DOWNSTREAM ELEVATION(FEET) =    910.20
  ELEVATION DIFFERENCE(FEET) =      4.40
  TC = 0.303*[(  612.00**3)/(     4.40)]**.2 =   10.591
```

```
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.037
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8694
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      1.68
  TOTAL AREA(ACRES) =      0.95   TOTAL RUNOFF(CFS) =      1.68

****************************************************************************
  FLOW PROCESS FROM NODE    151.00 TO NODE    152.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   906.20  DOWNSTREAM(FEET) =   901.60
  FLOW LENGTH(FEET) =    12.00   MANNING'S N =  0.012
  ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   2.2 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =  16.90
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      1.68
  PIPE TRAVEL TIME(MIN.) =   0.01    Tc(MIN.) =  10.60
  LONGEST FLOWPATH FROM NODE    150.00 TO NODE    152.00 =   624.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    152.00 TO NODE    161.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =  10.60
  RAINFALL INTENSITY(INCH/HR) =   2.04
  TOTAL STREAM AREA(ACRES) =     0.95
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      1.68

  ** CONFLUENCE DATA **
  STREAM     RUNOFF      Tc      INTENSITY      AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
      1        6.81     9.37        2.161          3.50
      2        1.68    10.60        2.036          0.95

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
  STREAM     RUNOFF      Tc      INTENSITY
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
      1        8.30     9.37       2.161
      2        8.10    10.60       2.036

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =      8.30   Tc(MIN.) =    9.37
  TOTAL AREA(ACRES) =      4.45
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    161.00 =   687.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.161
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.24   SUBAREA RUNOFF(CFS) =    0.45
  TOTAL AREA(ACRES) =      4.69   TOTAL RUNOFF(CFS) =    8.75
  TC(MIN.) =   9.37

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
```

```
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.161
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.26   SUBAREA RUNOFF(CFS) =    0.49
  TOTAL AREA(ACRES) =      4.95   TOTAL RUNOFF(CFS) =    9.24
  TC(MIN.) =   9.37

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.161
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.28   SUBAREA RUNOFF(CFS) =    0.53
  TOTAL AREA(ACRES) =      5.23   TOTAL RUNOFF(CFS) =    9.77
  TC(MIN.) =   9.37

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.161
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.22   SUBAREA RUNOFF(CFS) =    0.41
  TOTAL AREA(ACRES) =      5.45   TOTAL RUNOFF(CFS) =   10.18
  TC(MIN.) =   9.37

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.161
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.35   SUBAREA RUNOFF(CFS) =    0.66
  TOTAL AREA(ACRES) =      5.80   TOTAL RUNOFF(CFS) =   10.84
  TC(MIN.) =   9.37

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.161
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8706
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.27   SUBAREA RUNOFF(CFS) =    0.51
  TOTAL AREA(ACRES) =      6.07   TOTAL RUNOFF(CFS) =   11.35
  TC(MIN.) =   9.37

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    162.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   900.95  DOWNSTREAM(FEET) =   897.13
  FLOW LENGTH(FEET) =    14.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   6.7 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =  25.39
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     11.35
  PIPE TRAVEL TIME(MIN.) =   0.01    Tc(MIN.) =   9.38
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    162.00 =   701.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    162.00 IS CODE =  11
```

```
----------------------------------------------------------------------------
  >>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
============================================================================

  ** MAIN STREAM CONFLUENCE DATA **
  STREAM     RUNOFF      Tc       INTENSITY     AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)   (ACRE)
      1       11.35     9.38        2.160        6.07
      2       10.97    10.61        2.035        6.07
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    162.00 =   701.00 FEET.

  ** MEMORY BANK #  1 CONFLUENCE DATA **
  STREAM     RUNOFF      Tc       INTENSITY     AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)   (ACRE)
      1       10.43     7.04        2.479        5.73
      2       10.92     7.73        2.370        5.73
      3       11.05    10.56        2.040        5.73
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    162.00 =  1084.00 FEET.

  ** PEAK FLOW RATE TABLE **
  STREAM    RUNOFF       Tc       INTENSITY
  NUMBER     (CFS)     (MIN.)   (INCH/HOUR)
      1      18.94       7.04        2.479
      2      20.27       7.73        2.370
      3      21.30       9.38        2.160
      4      21.97      10.56        2.040
      5      22.00      10.61        2.035

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =     22.00   Tc(MIN.) =   10.61
  TOTAL AREA(ACRES) =     11.80

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    162.00 IS CODE =  12
----------------------------------------------------------------------------
  >>>>>CLEAR MEMORY BANK # 1 <<<<<
============================================================================

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    163.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   897.11  DOWNSTREAM(FEET) =   897.00
  FLOW LENGTH(FEET) =    24.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  30.0 INCH PIPE IS  19.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   6.42
  ESTIMATED PIPE DIAMETER(INCH) =  30.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     22.00
  PIPE TRAVEL TIME(MIN.) =   0.06    Tc(MIN.) =  10.67
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    163.00 =  1108.00 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =     11.80  TC(MIN.) =     10.67
  PEAK FLOW RATE(CFS)   =     22.00
  *** PEAK FLOW RATE TABLE ***
         Q(CFS)   Tc(MIN.)
  1       18.94       7.10
  2       20.27       7.79
  3       21.30       9.44
  4       21.97      10.62
  5       22.00      10.67
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
           RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON
        RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT
                    (RCFC&WCD)  1978 HYDROLOGY MANUAL
         (c) Copyright 1982-2003 Advanced Engineering Software (aes)
                    (Rational Tabling Version 5.9D)
                Release Date: 01/01/2003  License ID 1510

                        Analysis prepared by:

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 ************************* DESCRIPTION OF STUDY *************************
* TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY                        *
* PROPOSED CONDITION                                                     *
* HYDROLOGIC ANALYSIS - 100-YEAR                                         *
 ************************************************************************

  FILE NAME: 2216P100.DAT
  TIME/DATE OF STUDY: 12:00 07/06/2022
------------------------------------------------------------------------
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
------------------------------------------------------------------------
  USER SPECIFIED STORM EVENT(YEAR) =  100.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =  12.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
  2-YEAR, 1-HOUR PRECIPITATION(INCH) =  0.540
  100-YEAR, 1-HOUR PRECIPITATION(INCH) =  1.360
  COMPUTED RAINFALL INTENSITY DATA:
  STORM EVENT =  100.00   1-HOUR INTENSITY(INCH/HOUR) =   1.360
  SLOPE OF INTENSITY DURATION CURVE = 0.4800
  RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
  NOTE: CONSIDER ALL CONFLUENCE STREAM COMBINATIONS
        FOR ALL DOWNSTREAM ANALYSES
  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

**************************************************************************
  FLOW PROCESS FROM NODE    101.00 TO NODE    101.00 IS CODE =  22
------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
========================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  USER SPECIFIED Tc(MIN.) =    5.000
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.483
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      1.39
  TOTAL AREA(ACRES) =      0.35   TOTAL RUNOFF(CFS) =      1.39

**************************************************************************
  FLOW PROCESS FROM NODE    101.00 TO NODE    102.00 IS CODE =  31
------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
========================================================================
```

```
  ELEVATION DATA: UPSTREAM(FEET) =   906.80  DOWNSTREAM(FEET) =   906.08
  FLOW LENGTH(FEET) =   142.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   6.2 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.38
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      1.39
  PIPE TRAVEL TIME(MIN.) =   0.70    Tc(MIN.) =   5.70
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    102.00 =   142.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    102.00 TO NODE    102.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.209
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8821
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.52   SUBAREA RUNOFF(CFS) =    1.93
  TOTAL AREA(ACRES) =      0.87   TOTAL RUNOFF(CFS) =    3.32
  TC(MIN.) =   5.70

****************************************************************************
  FLOW PROCESS FROM NODE    102.00 TO NODE    103.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   906.08  DOWNSTREAM(FEET) =   905.50
  FLOW LENGTH(FEET) =   115.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  15.0 INCH PIPE IS   9.3 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   4.17
  ESTIMATED PIPE DIAMETER(INCH) =  15.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      3.32
  PIPE TRAVEL TIME(MIN.) =   0.46    Tc(MIN.) =   6.16
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    103.00 =   257.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    103.00 TO NODE    103.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.055
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8815
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.63   SUBAREA RUNOFF(CFS) =    2.25
  TOTAL AREA(ACRES) =      1.50   TOTAL RUNOFF(CFS) =    5.57
  TC(MIN.) =   6.16

****************************************************************************
  FLOW PROCESS FROM NODE    103.00 TO NODE    112.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   905.50  DOWNSTREAM(FEET) =   905.37
  FLOW LENGTH(FEET) =    25.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  18.0 INCH PIPE IS  11.3 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   4.79
  ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      5.57
  PIPE TRAVEL TIME(MIN.) =   0.09    Tc(MIN.) =   6.25
  LONGEST FLOWPATH FROM NODE    101.00 TO NODE    112.00 =   282.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    112.00 TO NODE    112.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =   6.25
  RAINFALL INTENSITY(INCH/HR) =   4.03
```

```
 TOTAL STREAM AREA(ACRES) =     1.50
 PEAK FLOW RATE(CFS) AT CONFLUENCE =      5.57

****************************************************************************
 FLOW PROCESS FROM NODE    110.00 TO NODE    111.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
        ASSUMED INITIAL SUBAREA UNIFORM
        DEVELOPMENT IS COMMERCIAL
 TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
 INITIAL SUBAREA FLOW-LENGTH(FEET) =   237.00
 UPSTREAM ELEVATION(FEET) =    916.50
 DOWNSTREAM ELEVATION(FEET) =    910.00
 ELEVATION DIFFERENCE(FEET) =      6.50
 TC = 0.303*[(  237.00**3)/(     6.50)]**.2 =    5.544
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.266
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8823
 SOIL CLASSIFICATION IS "B"
 SUBAREA RUNOFF(CFS) =      0.94
 TOTAL AREA(ACRES) =      0.25   TOTAL RUNOFF(CFS) =      0.94

****************************************************************************
 FLOW PROCESS FROM NODE    111.00 TO NODE    112.00 IS CODE =  31
----------------------------------------------------------------------------
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =   905.50  DOWNSTREAM(FEET) =   905.37
 FLOW LENGTH(FEET) =    26.00   MANNING'S N =  0.012
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
 DEPTH OF FLOW IN  12.0 INCH PIPE IS   5.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) =   3.04
 ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
 PIPE-FLOW(CFS) =      0.94
 PIPE TRAVEL TIME(MIN.) =   0.14    Tc(MIN.) =   5.69
 LONGEST FLOWPATH FROM NODE    110.00 TO NODE    112.00 =   263.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    112.00 TO NODE    112.00 IS CODE =   1
----------------------------------------------------------------------------
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
 TOTAL NUMBER OF STREAMS =  2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
 TIME OF CONCENTRATION(MIN.) =   5.69
 RAINFALL INTENSITY(INCH/HR) =   4.21
 TOTAL STREAM AREA(ACRES) =     0.25
 PEAK FLOW RATE(CFS) AT CONFLUENCE =      0.94

 ** CONFLUENCE DATA **
 STREAM     RUNOFF      Tc      INTENSITY      AREA
 NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
     1        5.57     6.25        4.028          1.50
     2        0.94     5.69        4.214          0.25

 RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR  2 STREAMS.

 ** PEAK FLOW RATE TABLE **
 STREAM     RUNOFF      Tc      INTENSITY
 NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
     1        6.01     5.69       4.214
     2        6.47     6.25       4.028

 COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) =      6.47   Tc(MIN.) =    6.25
 TOTAL AREA(ACRES) =      1.75
 LONGEST FLOWPATH FROM NODE    101.00 TO NODE    112.00 =   282.00 FEET.

****************************************************************************
```

```
 FLOW PROCESS FROM NODE    112.00 TO NODE    113.00 IS CODE =  31
----------------------------------------------------------------------------
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =   905.37  DOWNSTREAM(FEET) =   903.83
 FLOW LENGTH(FEET) =    70.00   MANNING'S N =  0.012
 DEPTH OF FLOW IN  15.0 INCH PIPE IS   8.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) =   8.57
 ESTIMATED PIPE DIAMETER(INCH) =  15.00    NUMBER OF PIPES =   1
 PIPE-FLOW(CFS) =      6.47
 PIPE TRAVEL TIME(MIN.) =   0.14    Tc(MIN.) =   6.38
 LONGEST FLOWPATH FROM NODE    101.00 TO NODE    113.00 =   352.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    113.00 TO NODE    131.00 IS CODE =   1
----------------------------------------------------------------------------
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
 TOTAL NUMBER OF STREAMS =  2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
 TIME OF CONCENTRATION(MIN.) =   6.38
 RAINFALL INTENSITY(INCH/HR) =   3.99
 TOTAL STREAM AREA(ACRES) =     1.75
 PEAK FLOW RATE(CFS) AT CONFLUENCE =      6.47

****************************************************************************
 FLOW PROCESS FROM NODE    120.00 TO NODE    121.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
        ASSUMED INITIAL SUBAREA UNIFORM
        DEVELOPMENT IS COMMERCIAL
 TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
 INITIAL SUBAREA FLOW-LENGTH(FEET) =   586.00
 UPSTREAM ELEVATION(FEET) =    915.20
 DOWNSTREAM ELEVATION(FEET) =    906.30
 ELEVATION DIFFERENCE(FEET) =      8.90
 TC = 0.303*[(  586.00**3)/(     8.90)]**.2 =    8.963
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.387
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8787
 SOIL CLASSIFICATION IS "B"
 SUBAREA RUNOFF(CFS) =      7.00
 TOTAL AREA(ACRES) =      2.35   TOTAL RUNOFF(CFS) =      7.00

****************************************************************************
 FLOW PROCESS FROM NODE    121.00 TO NODE    122.00 IS CODE =  31
----------------------------------------------------------------------------
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =   903.80  DOWNSTREAM(FEET) =   903.23
 FLOW LENGTH(FEET) =   113.00   MANNING'S N =  0.012
 DEPTH OF FLOW IN  18.0 INCH PIPE IS  13.5 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) =   4.92
 ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
 PIPE-FLOW(CFS) =      7.00
 PIPE TRAVEL TIME(MIN.) =   0.38    Tc(MIN.) =   9.35
 LONGEST FLOWPATH FROM NODE    120.00 TO NODE    122.00 =   699.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    122.00 TO NODE    131.00 IS CODE =   1
----------------------------------------------------------------------------
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
 TOTAL NUMBER OF STREAMS =  2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
 TIME OF CONCENTRATION(MIN.) =   9.35
 RAINFALL INTENSITY(INCH/HR) =   3.32
 TOTAL STREAM AREA(ACRES) =     2.35
 PEAK FLOW RATE(CFS) AT CONFLUENCE =      7.00
```

```
  ** CONFLUENCE DATA **
  STREAM     RUNOFF      Tc      INTENSITY      AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
      1        6.01     5.83        4.166          1.75
      1        6.47     6.38        3.987          1.75
      2        7.00     9.35        3.320          2.35

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
  STREAM     RUNOFF      Tc      INTENSITY
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
      1       10.37     5.83       4.166
      2       11.25     6.38       3.987
      3       12.38     9.35       3.320

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =     12.38   Tc(MIN.) =    9.35
  TOTAL AREA(ACRES) =      4.10
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    131.00 =   699.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    131.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.320
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8784
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.32   SUBAREA RUNOFF(CFS) =    0.93
  TOTAL AREA(ACRES) =      4.42   TOTAL RUNOFF(CFS) =   13.31
  TC(MIN.) =   9.35

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    131.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.320
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8784
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.38   SUBAREA RUNOFF(CFS) =    1.11
  TOTAL AREA(ACRES) =      4.80   TOTAL RUNOFF(CFS) =   14.42
  TC(MIN.) =   9.35

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    131.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.320
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8784
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.51   SUBAREA RUNOFF(CFS) =    1.49
  TOTAL AREA(ACRES) =      5.31   TOTAL RUNOFF(CFS) =   15.91
  TC(MIN.) =   9.35

****************************************************************************
  FLOW PROCESS FROM NODE    131.00 TO NODE    132.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   903.25  DOWNSTREAM(FEET) =   902.92
  FLOW LENGTH(FEET) =    31.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  21.0 INCH PIPE IS  16.3 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   7.95
  ESTIMATED PIPE DIAMETER(INCH) =  21.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     15.91
  PIPE TRAVEL TIME(MIN.) =   0.06    Tc(MIN.) =   9.41
```

```
 LONGEST FLOWPATH FROM NODE    120.00 TO NODE    132.00 =   730.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    132.00 TO NODE    132.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.309
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8784
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    0.13   SUBAREA RUNOFF(CFS) =    0.38
 TOTAL AREA(ACRES) =      5.44   TOTAL RUNOFF(CFS) =   16.29
 TC(MIN.) =   9.41

****************************************************************************
 FLOW PROCESS FROM NODE    132.00 TO NODE    133.00 IS CODE =  31
----------------------------------------------------------------------------
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =   898.88  DOWNSTREAM(FEET) =   897.91
 FLOW LENGTH(FEET) =   197.00   MANNING'S N =  0.012
 DEPTH OF FLOW IN  24.0 INCH PIPE IS  19.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) =   5.92
 ESTIMATED PIPE DIAMETER(INCH) =  24.00    NUMBER OF PIPES =   1
 PIPE-FLOW(CFS) =     16.29
 PIPE TRAVEL TIME(MIN.) =   0.55    Tc(MIN.) =   9.96
 LONGEST FLOWPATH FROM NODE    120.00 TO NODE    133.00 =   927.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    133.00 TO NODE    133.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.219
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8779
 SOIL CLASSIFICATION IS "B"
 SUBAREA AREA(ACRES) =    0.29   SUBAREA RUNOFF(CFS) =    0.82
 TOTAL AREA(ACRES) =      5.73   TOTAL RUNOFF(CFS) =   17.11
 TC(MIN.) =   9.96

****************************************************************************
 FLOW PROCESS FROM NODE    133.00 TO NODE    162.00 IS CODE =  31
----------------------------------------------------------------------------
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
 ELEVATION DATA: UPSTREAM(FEET) =   897.89  DOWNSTREAM(FEET) =   897.13
 FLOW LENGTH(FEET) =   157.00   MANNING'S N =  0.012
 DEPTH OF FLOW IN  27.0 INCH PIPE IS  17.8 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) =   6.15
 ESTIMATED PIPE DIAMETER(INCH) =  27.00    NUMBER OF PIPES =   1
 PIPE-FLOW(CFS) =     17.11
 PIPE TRAVEL TIME(MIN.) =   0.43    Tc(MIN.) =  10.39
 LONGEST FLOWPATH FROM NODE    120.00 TO NODE    162.00 =  1084.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    162.00 TO NODE    162.00 IS CODE =  10
----------------------------------------------------------------------------
 >>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE    140.00 TO NODE    141.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
 TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
 INITIAL SUBAREA FLOW-LENGTH(FEET) =   398.00
 UPSTREAM ELEVATION(FEET) =    916.50
```

```
  DOWNSTREAM ELEVATION(FEET) =    912.00
  ELEVATION DIFFERENCE(FEET) =      4.50
  TC = 0.303*[(  398.00**3)/(     4.50)]**.2 =    8.145
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.547
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8795
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      1.62
  TOTAL AREA(ACRES) =      0.52   TOTAL RUNOFF(CFS) =      1.62

****************************************************************************
  FLOW PROCESS FROM NODE    141.00 TO NODE    142.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   908.00  DOWNSTREAM(FEET) =   907.77
  FLOW LENGTH(FEET) =    48.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   7.0 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.43
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      1.62
  PIPE TRAVEL TIME(MIN.) =   0.23    Tc(MIN.) =   8.38
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    142.00 =   446.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    142.00 TO NODE    142.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.499
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8793
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.28   SUBAREA RUNOFF(CFS) =    0.86
  TOTAL AREA(ACRES) =      0.80   TOTAL RUNOFF(CFS) =    2.48
  TC(MIN.) =   8.38

****************************************************************************
  FLOW PROCESS FROM NODE    142.00 TO NODE    143.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   907.77  DOWNSTREAM(FEET) =   907.25
  FLOW LENGTH(FEET) =   103.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   9.4 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   3.77
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      2.48
  PIPE TRAVEL TIME(MIN.) =   0.45    Tc(MIN.) =   8.83
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    143.00 =   549.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    143.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.411
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8789
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.23   SUBAREA RUNOFF(CFS) =    0.69
  TOTAL AREA(ACRES) =      1.03   TOTAL RUNOFF(CFS) =    3.17
  TC(MIN.) =   8.83

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    143.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.411
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8789
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    2.26   SUBAREA RUNOFF(CFS) =    6.78
```

```
  TOTAL AREA(ACRES) =      3.29   TOTAL RUNOFF(CFS) =    9.95
  TC(MIN.) =   8.83

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    144.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   907.25  DOWNSTREAM(FEET) =   907.21
  FLOW LENGTH(FEET) =     9.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  21.0 INCH PIPE IS  15.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   5.12
  ESTIMATED PIPE DIAMETER(INCH) =  21.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      9.95
  PIPE TRAVEL TIME(MIN.) =   0.03    Tc(MIN.) =   8.86
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    144.00 =   558.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    144.00 TO NODE    144.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.406
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8788
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.21   SUBAREA RUNOFF(CFS) =    0.63
  TOTAL AREA(ACRES) =      3.50   TOTAL RUNOFF(CFS) =   10.58
  TC(MIN.) =   8.86

****************************************************************************
  FLOW PROCESS FROM NODE    144.00 TO NODE    145.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   907.21  DOWNSTREAM(FEET) =   906.56
  FLOW LENGTH(FEET) =   129.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  21.0 INCH PIPE IS  15.8 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   5.45
  ESTIMATED PIPE DIAMETER(INCH) =  21.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     10.58
  PIPE TRAVEL TIME(MIN.) =   0.39    Tc(MIN.) =   9.26
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    145.00 =   687.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    143.00 TO NODE    161.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =   9.26
  RAINFALL INTENSITY(INCH/HR) =   3.34
  TOTAL STREAM AREA(ACRES) =     3.50
  PEAK FLOW RATE(CFS) AT CONFLUENCE =     10.58

****************************************************************************
  FLOW PROCESS FROM NODE    150.00 TO NODE    151.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
         ASSUMED INITIAL SUBAREA UNIFORM
         DEVELOPMENT IS COMMERCIAL
  TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   612.00
  UPSTREAM ELEVATION(FEET) =    914.60
  DOWNSTREAM ELEVATION(FEET) =    910.20
  ELEVATION DIFFERENCE(FEET) =      4.40
  TC = 0.303*[(  612.00**3)/(     4.40)]**.2 =   10.591
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.127
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8774
```

```
  SOIL CLASSIFICATION IS "B"
  SUBAREA RUNOFF(CFS) =      2.61
  TOTAL AREA(ACRES) =      0.95   TOTAL RUNOFF(CFS) =      2.61

****************************************************************************
  FLOW PROCESS FROM NODE    151.00 TO NODE    152.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   906.20  DOWNSTREAM(FEET) =   901.60
  FLOW LENGTH(FEET) =    12.00   MANNING'S N =  0.012
  ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   2.7 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =  19.25
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =      2.61
  PIPE TRAVEL TIME(MIN.) =   0.01    Tc(MIN.) =  10.60
  LONGEST FLOWPATH FROM NODE    150.00 TO NODE    152.00 =   624.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    152.00 TO NODE    161.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =  10.60
  RAINFALL INTENSITY(INCH/HR) =   3.13
  TOTAL STREAM AREA(ACRES) =     0.95
  PEAK FLOW RATE(CFS) AT CONFLUENCE =      2.61

  ** CONFLUENCE DATA **
  STREAM     RUNOFF      Tc      INTENSITY      AREA
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)    (ACRE)
      1       10.58     9.26        3.335          3.50
      2        2.61    10.60        3.125          0.95

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
  STREAM     RUNOFF      Tc      INTENSITY
  NUMBER      (CFS)    (MIN.)   (INCH/HOUR)
      1       12.85     9.26       3.335
      2       12.52    10.60       3.125

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =     12.85   Tc(MIN.) =    9.26
  TOTAL AREA(ACRES) =      4.45
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    161.00 =   687.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.335
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8785
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.24   SUBAREA RUNOFF(CFS) =    0.70
  TOTAL AREA(ACRES) =      4.69   TOTAL RUNOFF(CFS) =   13.56
  TC(MIN.) =   9.26

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.335
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8785
```

```
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.26   SUBAREA RUNOFF(CFS) =    0.76
  TOTAL AREA(ACRES) =      4.95   TOTAL RUNOFF(CFS) =   14.32
  TC(MIN.) =   9.26

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.335
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8785
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.28   SUBAREA RUNOFF(CFS) =    0.82
  TOTAL AREA(ACRES) =      5.23   TOTAL RUNOFF(CFS) =   15.14
  TC(MIN.) =   9.26

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.335
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8785
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.22   SUBAREA RUNOFF(CFS) =    0.64
  TOTAL AREA(ACRES) =      5.45   TOTAL RUNOFF(CFS) =   15.78
  TC(MIN.) =   9.26

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.335
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8785
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.35   SUBAREA RUNOFF(CFS) =    1.03
  TOTAL AREA(ACRES) =      5.80   TOTAL RUNOFF(CFS) =   16.81
  TC(MIN.) =   9.26

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    161.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.335
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8785
  SOIL CLASSIFICATION IS "B"
  SUBAREA AREA(ACRES) =    0.27   SUBAREA RUNOFF(CFS) =    0.79
  TOTAL AREA(ACRES) =      6.07   TOTAL RUNOFF(CFS) =   17.60
  TC(MIN.) =   9.26

****************************************************************************
  FLOW PROCESS FROM NODE    161.00 TO NODE    162.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   900.95  DOWNSTREAM(FEET) =   897.13
  FLOW LENGTH(FEET) =    14.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  12.0 INCH PIPE IS   9.1 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =  27.64
  ESTIMATED PIPE DIAMETER(INCH) =  12.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     17.60
  PIPE TRAVEL TIME(MIN.) =   0.01    Tc(MIN.) =   9.26
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    162.00 =   701.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    162.00 IS CODE =  11
----------------------------------------------------------------------------
  >>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
```

```
==============================================================================

  ** MAIN STREAM CONFLUENCE DATA **
  STREAM     RUNOFF      Tc       INTENSITY     AREA
  NUMBER      (CFS)    (MIN.)    (INCH/HOUR)   (ACRE)
      1       17.60      9.26        3.334        6.07
      2       16.96     10.61        3.124        6.07
  LONGEST FLOWPATH FROM NODE    140.00 TO NODE    162.00 =   701.00 FEET.

  ** MEMORY BANK #  1 CONFLUENCE DATA **
  STREAM     RUNOFF      Tc       INTENSITY     AREA
  NUMBER      (CFS)    (MIN.)    (INCH/HOUR)   (ACRE)
      1       16.30      6.88        3.847        5.73
      2       16.93      7.43        3.707        5.73
      3       17.11     10.39        3.156        5.73
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    162.00 =  1084.00 FEET.

  ** PEAK FLOW RATE TABLE **
  STREAM    RUNOFF        Tc       INTENSITY
  NUMBER     (CFS)      (MIN.)    (INCH/HOUR)
      1      29.37        6.88         3.847
      2      31.04        7.43         3.707
      3      32.85        9.26         3.334
      4      33.77       10.39         3.156
      5      33.90       10.61         3.124

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =     33.90   Tc(MIN.) =   10.61
  TOTAL AREA(ACRES) =     11.80

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    162.00 IS CODE =  12
----------------------------------------------------------------------------
  >>>>>CLEAR MEMORY BANK # 1 <<<<<
============================================================================

****************************************************************************
  FLOW PROCESS FROM NODE    162.00 TO NODE    163.00 IS CODE =  31
----------------------------------------------------------------------------
  >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
  >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
============================================================================
  ELEVATION DATA: UPSTREAM(FEET) =   897.11  DOWNSTREAM(FEET) =   897.00
  FLOW LENGTH(FEET) =    24.00   MANNING'S N =  0.012
  DEPTH OF FLOW IN  33.0 INCH PIPE IS  25.0 INCHES
  PIPE-FLOW VELOCITY(FEET/SEC.) =   7.03
  ESTIMATED PIPE DIAMETER(INCH) =  33.00    NUMBER OF PIPES =   1
  PIPE-FLOW(CFS) =     33.90
  PIPE TRAVEL TIME(MIN.) =   0.06    Tc(MIN.) =  10.67
  LONGEST FLOWPATH FROM NODE    120.00 TO NODE    163.00 =  1108.00 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =     11.80  TC(MIN.) =     10.67
  PEAK FLOW RATE(CFS)   =     33.90
  *** PEAK FLOW RATE TABLE ***
         Q(CFS)   Tc(MIN.)
  1       29.37       6.93
  2       31.04       7.49
  3       32.85       9.32
  4       33.77      10.45
  5       33.90      10.67
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

Technical Appendix D

Flood Hydrograph Hydrologic Analysis
Existing Condition

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E002242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	2.00	23.60

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	6.40	75.52

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(0.731)	0.012	0.004
2	0.17	0.07	0.016	(0.728)	0.012	0.004
3	0.25	0.07	0.016	(0.725)	0.012	0.004
4	0.33	0.10	0.024	(0.722)	0.018	0.006
5	0.42	0.10	0.024	(0.719)	0.018	0.006
6	0.50	0.10	0.024	(0.716)	0.018	0.006
7	0.58	0.10	0.024	(0.714)	0.018	0.006
8	0.67	0.10	0.024	(0.711)	0.018	0.006
9	0.75	0.10	0.024	(0.708)	0.018	0.006
10	0.83	0.13	0.032	(0.705)	0.024	0.008
11	0.92	0.13	0.032	(0.703)	0.024	0.008
12	1.00	0.13	0.032	(0.700)	0.024	0.008
13	1.08	0.10	0.024	(0.697)	0.018	0.006
14	1.17	0.10	0.024	(0.694)	0.018	0.006
15	1.25	0.10	0.024	(0.692)	0.018	0.006
16	1.33	0.10	0.024	(0.689)	0.018	0.006
17	1.42	0.10	0.024	(0.686)	0.018	0.006
18	1.50	0.10	0.024	(0.683)	0.018	0.006
19	1.58	0.10	0.024	(0.681)	0.018	0.006
20	1.67	0.10	0.024	(0.678)	0.018	0.006
21	1.75	0.10	0.024	(0.675)	0.018	0.006
22	1.83	0.13	0.032	(0.672)	0.024	0.008
23	1.92	0.13	0.032	(0.670)	0.024	0.008
24	2.00	0.13	0.032	(0.667)	0.024	0.008
25	2.08	0.13	0.032	(0.664)	0.024	0.008
26	2.17	0.13	0.032	(0.662)	0.024	0.008
27	2.25	0.13	0.032	(0.659)	0.024	0.008
28	2.33	0.13	0.032	(0.656)	0.024	0.008
29	2.42	0.13	0.032	(0.654)	0.024	0.008
30	2.50	0.13	0.032	(0.651)	0.024	0.008
31	2.58	0.17	0.040	(0.648)	0.030	0.010
32	2.67	0.17	0.040	(0.646)	0.030	0.010
33	2.75	0.17	0.040	(0.643)	0.030	0.010
34	2.83	0.17	0.040	(0.640)	0.030	0.010
35	2.92	0.17	0.040	(0.638)	0.030	0.010
36	3.00	0.17	0.040	(0.635)	0.030	0.010

37	3.08	0.17	0.040	(0.632)	0.030	0.010
38	3.17	0.17	0.040	(0.630)	0.030	0.010
39	3.25	0.17	0.040	(0.627)	0.030	0.010
40	3.33	0.17	0.040	(0.624)	0.030	0.010
41	3.42	0.17	0.040	(0.622)	0.030	0.010
42	3.50	0.17	0.040	(0.619)	0.030	0.010
43	3.58	0.17	0.040	(0.617)	0.030	0.010
44	3.67	0.17	0.040	(0.614)	0.030	0.010
45	3.75	0.17	0.040	(0.612)	0.030	0.010
46	3.83	0.20	0.048	(0.609)	0.036	0.012
47	3.92	0.20	0.048	(0.606)	0.036	0.012
48	4.00	0.20	0.048	(0.604)	0.036	0.012
49	4.08	0.20	0.048	(0.601)	0.036	0.012
50	4.17	0.20	0.048	(0.599)	0.036	0.012
51	4.25	0.20	0.048	(0.596)	0.036	0.012
52	4.33	0.23	0.056	(0.594)	0.042	0.014
53	4.42	0.23	0.056	(0.591)	0.042	0.014
54	4.50	0.23	0.056	(0.589)	0.042	0.014
55	4.58	0.23	0.056	(0.586)	0.042	0.014
56	4.67	0.23	0.056	(0.583)	0.042	0.014
57	4.75	0.23	0.056	(0.581)	0.042	0.014
58	4.83	0.27	0.064	(0.578)	0.048	0.016
59	4.92	0.27	0.064	(0.576)	0.048	0.016
60	5.00	0.27	0.064	(0.573)	0.048	0.016
61	5.08	0.20	0.048	(0.571)	0.036	0.012
62	5.17	0.20	0.048	(0.568)	0.036	0.012
63	5.25	0.20	0.048	(0.566)	0.036	0.012
64	5.33	0.23	0.056	(0.564)	0.042	0.014
65	5.42	0.23	0.056	(0.561)	0.042	0.014
66	5.50	0.23	0.056	(0.559)	0.042	0.014
67	5.58	0.27	0.064	(0.556)	0.048	0.016
68	5.67	0.27	0.064	(0.554)	0.048	0.016
69	5.75	0.27	0.064	(0.551)	0.048	0.016
70	5.83	0.27	0.064	(0.549)	0.048	0.016
71	5.92	0.27	0.064	(0.546)	0.048	0.016
72	6.00	0.27	0.064	(0.544)	0.048	0.016
73	6.08	0.30	0.072	(0.542)	0.054	0.018
74	6.17	0.30	0.072	(0.539)	0.054	0.018
75	6.25	0.30	0.072	(0.537)	0.054	0.018
76	6.33	0.30	0.072	(0.534)	0.054	0.018
77	6.42	0.30	0.072	(0.532)	0.054	0.018
78	6.50	0.30	0.072	(0.530)	0.054	0.018
79	6.58	0.33	0.080	(0.527)	0.060	0.020
80	6.67	0.33	0.080	(0.525)	0.060	0.020
81	6.75	0.33	0.080	(0.522)	0.060	0.020
82	6.83	0.33	0.080	(0.520)	0.060	0.020
83	6.92	0.33	0.080	(0.518)	0.060	0.020
84	7.00	0.33	0.080	(0.515)	0.060	0.020
85	7.08	0.33	0.080	(0.513)	0.060	0.020
86	7.17	0.33	0.080	(0.511)	0.060	0.020
87	7.25	0.33	0.080	(0.508)	0.060	0.020
88	7.33	0.37	0.088	(0.506)	0.066	0.022
89	7.42	0.37	0.088	(0.504)	0.066	0.022
90	7.50	0.37	0.088	(0.501)	0.066	0.022
91	7.58	0.40	0.096	(0.499)	0.072	0.024
92	7.67	0.40	0.096	(0.497)	0.072	0.024
93	7.75	0.40	0.096	(0.495)	0.072	0.024
94	7.83	0.43	0.104	(0.492)	0.078	0.026
95	7.92	0.43	0.104	(0.490)	0.078	0.026
96	8.00	0.43	0.104	(0.488)	0.078	0.026
97	8.08	0.50	0.120	(0.485)	0.090	0.030
98	8.17	0.50	0.120	(0.483)	0.090	0.030
99	8.25	0.50	0.120	(0.481)	0.090	0.030
100	8.33	0.50	0.120	(0.479)	0.090	0.030
101	8.42	0.50	0.120	(0.476)	0.090	0.030
102	8.50	0.50	0.120	(0.474)	0.090	0.030
103	8.58	0.53	0.128	(0.472)	0.096	0.032
104	8.67	0.53	0.128	(0.470)	0.096	0.032
105	8.75	0.53	0.128	(0.468)	0.096	0.032
106	8.83	0.57	0.136	(0.465)	0.102	0.034
107	8.92	0.57	0.136	(0.463)	0.102	0.034
108	9.00	0.57	0.136	(0.461)	0.102	0.034

109	9.08	0.63	0.152	(0.459)	0.114	0.038
110	9.17	0.63	0.152	(0.457)	0.114	0.038
111	9.25	0.63	0.152	(0.454)	0.114	0.038
112	9.33	0.67	0.160	(0.452)	0.120	0.040
113	9.42	0.67	0.160	(0.450)	0.120	0.040
114	9.50	0.67	0.160	(0.448)	0.120	0.040
115	9.58	0.70	0.168	(0.446)	0.126	0.042
116	9.67	0.70	0.168	(0.444)	0.126	0.042
117	9.75	0.70	0.168	(0.442)	0.126	0.042
118	9.83	0.73	0.176	(0.439)	0.132	0.044
119	9.92	0.73	0.176	(0.437)	0.132	0.044
120	10.00	0.73	0.176	(0.435)	0.132	0.044
121	10.08	0.50	0.120	(0.433)	0.090	0.030
122	10.17	0.50	0.120	(0.431)	0.090	0.030
123	10.25	0.50	0.120	(0.429)	0.090	0.030
124	10.33	0.50	0.120	(0.427)	0.090	0.030
125	10.42	0.50	0.120	(0.425)	0.090	0.030
126	10.50	0.50	0.120	(0.423)	0.090	0.030
127	10.58	0.67	0.160	(0.421)	0.120	0.040
128	10.67	0.67	0.160	(0.419)	0.120	0.040
129	10.75	0.67	0.160	(0.417)	0.120	0.040
130	10.83	0.67	0.160	(0.414)	0.120	0.040
131	10.92	0.67	0.160	(0.412)	0.120	0.040
132	11.00	0.67	0.160	(0.410)	0.120	0.040
133	11.08	0.63	0.152	(0.408)	0.114	0.038
134	11.17	0.63	0.152	(0.406)	0.114	0.038
135	11.25	0.63	0.152	(0.404)	0.114	0.038
136	11.33	0.63	0.152	(0.402)	0.114	0.038
137	11.42	0.63	0.152	(0.400)	0.114	0.038
138	11.50	0.63	0.152	(0.398)	0.114	0.038
139	11.58	0.57	0.136	(0.396)	0.102	0.034
140	11.67	0.57	0.136	(0.394)	0.102	0.034
141	11.75	0.57	0.136	(0.392)	0.102	0.034
142	11.83	0.60	0.144	(0.391)	0.108	0.036
143	11.92	0.60	0.144	(0.389)	0.108	0.036
144	12.00	0.60	0.144	(0.387)	0.108	0.036
145	12.08	0.83	0.200	(0.385)	0.150	0.050
146	12.17	0.83	0.200	(0.383)	0.150	0.050
147	12.25	0.83	0.200	(0.381)	0.150	0.050
148	12.33	0.87	0.208	(0.379)	0.156	0.052
149	12.42	0.87	0.208	(0.377)	0.156	0.052
150	12.50	0.87	0.208	(0.375)	0.156	0.052
151	12.58	0.93	0.224	(0.373)	0.168	0.056
152	12.67	0.93	0.224	(0.371)	0.168	0.056
153	12.75	0.93	0.224	(0.369)	0.168	0.056
154	12.83	0.97	0.232	(0.368)	0.174	0.058
155	12.92	0.97	0.232	(0.366)	0.174	0.058
156	13.00	0.97	0.232	(0.364)	0.174	0.058
157	13.08	1.13	0.272	(0.362)	0.204	0.068
158	13.17	1.13	0.272	(0.360)	0.204	0.068
159	13.25	1.13	0.272	(0.358)	0.204	0.068
160	13.33	1.13	0.272	(0.357)	0.204	0.068
161	13.42	1.13	0.272	(0.355)	0.204	0.068
162	13.50	1.13	0.272	(0.353)	0.204	0.068
163	13.58	0.77	0.184	(0.351)	0.138	0.046
164	13.67	0.77	0.184	(0.349)	0.138	0.046
165	13.75	0.77	0.184	(0.348)	0.138	0.046
166	13.83	0.77	0.184	(0.346)	0.138	0.046
167	13.92	0.77	0.184	(0.344)	0.138	0.046
168	14.00	0.77	0.184	(0.342)	0.138	0.046
169	14.08	0.90	0.216	(0.341)	0.162	0.054
170	14.17	0.90	0.216	(0.339)	0.162	0.054
171	14.25	0.90	0.216	(0.337)	0.162	0.054
172	14.33	0.87	0.208	(0.335)	0.156	0.052
173	14.42	0.87	0.208	(0.334)	0.156	0.052
174	14.50	0.87	0.208	(0.332)	0.156	0.052
175	14.58	0.87	0.208	(0.330)	0.156	0.052
176	14.67	0.87	0.208	(0.329)	0.156	0.052
177	14.75	0.87	0.208	(0.327)	0.156	0.052
178	14.83	0.83	0.200	(0.325)	0.150	0.050
179	14.92	0.83	0.200	(0.324)	0.150	0.050
180	15.00	0.83	0.200	(0.322)	0.150	0.050

181	15.08	0.80	0.192	(0.320)	0.144	0.048
182	15.17	0.80	0.192	(0.319)	0.144	0.048
183	15.25	0.80	0.192	(0.317)	0.144	0.048
184	15.33	0.77	0.184	(0.315)	0.138	0.046
185	15.42	0.77	0.184	(0.314)	0.138	0.046
186	15.50	0.77	0.184	(0.312)	0.138	0.046
187	15.58	0.63	0.152	(0.311)	0.114	0.038
188	15.67	0.63	0.152	(0.309)	0.114	0.038
189	15.75	0.63	0.152	(0.307)	0.114	0.038
190	15.83	0.63	0.152	(0.306)	0.114	0.038
191	15.92	0.63	0.152	(0.304)	0.114	0.038
192	16.00	0.63	0.152	(0.303)	0.114	0.038
193	16.08	0.13	0.032	(0.301)	0.024	0.008
194	16.17	0.13	0.032	(0.300)	0.024	0.008
195	16.25	0.13	0.032	(0.298)	0.024	0.008
196	16.33	0.13	0.032	(0.297)	0.024	0.008
197	16.42	0.13	0.032	(0.295)	0.024	0.008
198	16.50	0.13	0.032	(0.293)	0.024	0.008
199	16.58	0.10	0.024	(0.292)	0.018	0.006
200	16.67	0.10	0.024	(0.291)	0.018	0.006
201	16.75	0.10	0.024	(0.289)	0.018	0.006
202	16.83	0.10	0.024	(0.288)	0.018	0.006
203	16.92	0.10	0.024	(0.286)	0.018	0.006
204	17.00	0.10	0.024	(0.285)	0.018	0.006
205	17.08	0.17	0.040	(0.283)	0.030	0.010
206	17.17	0.17	0.040	(0.282)	0.030	0.010
207	17.25	0.17	0.040	(0.280)	0.030	0.010
208	17.33	0.17	0.040	(0.279)	0.030	0.010
209	17.42	0.17	0.040	(0.278)	0.030	0.010
210	17.50	0.17	0.040	(0.276)	0.030	0.010
211	17.58	0.17	0.040	(0.275)	0.030	0.010
212	17.67	0.17	0.040	(0.273)	0.030	0.010
213	17.75	0.17	0.040	(0.272)	0.030	0.010
214	17.83	0.13	0.032	(0.271)	0.024	0.008
215	17.92	0.13	0.032	(0.269)	0.024	0.008
216	18.00	0.13	0.032	(0.268)	0.024	0.008
217	18.08	0.13	0.032	(0.267)	0.024	0.008
218	18.17	0.13	0.032	(0.265)	0.024	0.008
219	18.25	0.13	0.032	(0.264)	0.024	0.008
220	18.33	0.13	0.032	(0.263)	0.024	0.008
221	18.42	0.13	0.032	(0.262)	0.024	0.008
222	18.50	0.13	0.032	(0.260)	0.024	0.008
223	18.58	0.10	0.024	(0.259)	0.018	0.006
224	18.67	0.10	0.024	(0.258)	0.018	0.006
225	18.75	0.10	0.024	(0.257)	0.018	0.006
226	18.83	0.07	0.016	(0.255)	0.012	0.004
227	18.92	0.07	0.016	(0.254)	0.012	0.004
228	19.00	0.07	0.016	(0.253)	0.012	0.004
229	19.08	0.10	0.024	(0.252)	0.018	0.006
230	19.17	0.10	0.024	(0.251)	0.018	0.006
231	19.25	0.10	0.024	(0.249)	0.018	0.006
232	19.33	0.13	0.032	(0.248)	0.024	0.008
233	19.42	0.13	0.032	(0.247)	0.024	0.008
234	19.50	0.13	0.032	(0.246)	0.024	0.008
235	19.58	0.10	0.024	(0.245)	0.018	0.006
236	19.67	0.10	0.024	(0.244)	0.018	0.006
237	19.75	0.10	0.024	(0.243)	0.018	0.006
238	19.83	0.07	0.016	(0.241)	0.012	0.004
239	19.92	0.07	0.016	(0.240)	0.012	0.004
240	20.00	0.07	0.016	(0.239)	0.012	0.004
241	20.08	0.10	0.024	(0.238)	0.018	0.006
242	20.17	0.10	0.024	(0.237)	0.018	0.006
243	20.25	0.10	0.024	(0.236)	0.018	0.006
244	20.33	0.10	0.024	(0.235)	0.018	0.006
245	20.42	0.10	0.024	(0.234)	0.018	0.006
246	20.50	0.10	0.024	(0.233)	0.018	0.006
247	20.58	0.10	0.024	(0.232)	0.018	0.006
248	20.67	0.10	0.024	(0.231)	0.018	0.006
249	20.75	0.10	0.024	(0.230)	0.018	0.006
250	20.83	0.07	0.016	(0.229)	0.012	0.004
251	20.92	0.07	0.016	(0.228)	0.012	0.004
252	21.00	0.07	0.016	(0.227)	0.012	0.004

253	21.08	0.10	0.024	(0.227)	0.018	0.006
254	21.17	0.10	0.024	(0.226)	0.018	0.006
255	21.25	0.10	0.024	(0.225)	0.018	0.006
256	21.33	0.07	0.016	(0.224)	0.012	0.004
257	21.42	0.07	0.016	(0.223)	0.012	0.004
258	21.50	0.07	0.016	(0.222)	0.012	0.004
259	21.58	0.10	0.024	(0.221)	0.018	0.006
260	21.67	0.10	0.024	(0.221)	0.018	0.006
261	21.75	0.10	0.024	(0.220)	0.018	0.006
262	21.83	0.07	0.016	(0.219)	0.012	0.004
263	21.92	0.07	0.016	(0.218)	0.012	0.004
264	22.00	0.07	0.016	(0.218)	0.012	0.004
265	22.08	0.10	0.024	(0.217)	0.018	0.006
266	22.17	0.10	0.024	(0.216)	0.018	0.006
267	22.25	0.10	0.024	(0.215)	0.018	0.006
268	22.33	0.07	0.016	(0.215)	0.012	0.004
269	22.42	0.07	0.016	(0.214)	0.012	0.004
270	22.50	0.07	0.016	(0.214)	0.012	0.004
271	22.58	0.07	0.016	(0.213)	0.012	0.004
272	22.67	0.07	0.016	(0.212)	0.012	0.004
273	22.75	0.07	0.016	(0.212)	0.012	0.004
274	22.83	0.07	0.016	(0.211)	0.012	0.004
275	22.92	0.07	0.016	(0.211)	0.012	0.004
276	23.00	0.07	0.016	(0.210)	0.012	0.004
277	23.08	0.07	0.016	(0.210)	0.012	0.004
278	23.17	0.07	0.016	(0.209)	0.012	0.004
279	23.25	0.07	0.016	(0.209)	0.012	0.004
280	23.33	0.07	0.016	(0.208)	0.012	0.004
281	23.42	0.07	0.016	(0.208)	0.012	0.004
282	23.50	0.07	0.016	(0.208)	0.012	0.004
283	23.58	0.07	0.016	(0.207)	0.012	0.004
284	23.67	0.07	0.016	(0.207)	0.012	0.004
285	23.75	0.07	0.016	(0.207)	0.012	0.004
286	23.83	0.07	0.016	(0.206)	0.012	0.004
287	23.92	0.07	0.016	(0.206)	0.012	0.004
288	24.00	0.07	0.016	(0.206)	0.012	0.004

(Loss Rate Not Used)

Sum = 100.0 Sum = 6.0

Flood volume = Effective rainfall 0.50(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 1.50(In)
Total soil loss = 1.475(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 21416.5 Cubic Feet
Total soil loss = 64249.5 Cubic Feet

Peak flow rate of this hydrograph = 0.809(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.04	Q	|	|	|	|
0+15	0.0007	0.04	Q	|	|	|	|
0+20	0.0010	0.05	Q	|	|	|	|
0+25	0.0015	0.07	Q	|	|	|	|
0+30	0.0020	0.07	Q	|	|	|	|
0+35	0.0024	0.07	Q	|	|	|	|
0+40	0.0029	0.07	Q	|	|	|	|
0+45	0.0034	0.07	Q	|	|	|	|
0+50	0.0040	0.08	Q	|	|	|	|
0+55	0.0046	0.09	Q	|	|	|	|
1+ 0	0.0052	0.09	Q	|	|	|	|
1+ 5	0.0058	0.09	Q	|	|	|	|
1+10	0.0063	0.08	Q	|	|	|	|
1+15	0.0069	0.07	Q	|	|	|	|

1+20	0.0074	0.07	Q	|	|	|	|
1+25	0.0078	0.07	Q	|	|	|	|
1+30	0.0083	0.07	Q	|	|	|	|
1+35	0.0088	0.07	Q	|	|	|	|
1+40	0.0093	0.07	Q	|	|	|	|
1+45	0.0098	0.07	Q	|	|	|	|
1+50	0.0104	0.08	Q	|	|	|	|
1+55	0.0110	0.09	Q	|	|	|	|
2+ 0	0.0116	0.09	Q	|	|	|	|
2+ 5	0.0123	0.09	Q	|	|	|	|
2+10	0.0129	0.09	QV	|	|	|	|
2+15	0.0136	0.10	QV	|	|	|	|
2+20	0.0142	0.10	QV	|	|	|	|
2+25	0.0149	0.10	QV	|	|	|	|
2+30	0.0155	0.10	QV	|	|	|	|
2+35	0.0163	0.10	QV	|	|	|	|
2+40	0.0170	0.11	QV	|	|	|	|
2+45	0.0178	0.12	QV	|	|	|	|
2+50	0.0187	0.12	QV	|	|	|	|
2+55	0.0195	0.12	QV	|	|	|	|
3+ 0	0.0203	0.12	QV	|	|	|	|
3+ 5	0.0211	0.12	QV	|	|	|	|
3+10	0.0219	0.12	QV	|	|	|	|
3+15	0.0228	0.12	QV	|	|	|	|
3+20	0.0236	0.12	QV	|	|	|	|
3+25	0.0244	0.12	QV	|	|	|	|
3+30	0.0252	0.12	Q V	|	|	|	|
3+35	0.0260	0.12	Q V	|	|	|	|
3+40	0.0268	0.12	Q V	|	|	|	|
3+45	0.0277	0.12	Q V	|	|	|	|
3+50	0.0285	0.13	Q V	|	|	|	|
3+55	0.0295	0.14	Q V	|	|	|	|
4+ 0	0.0305	0.14	Q V	|	|	|	|
4+ 5	0.0314	0.14	Q V	|	|	|	|
4+10	0.0324	0.14	Q V	|	|	|	|
4+15	0.0334	0.14	Q V	|	|	|	|
4+20	0.0344	0.15	Q V	|	|	|	|
4+25	0.0355	0.16	Q V	|	|	|	|
4+30	0.0367	0.16	Q V	|	|	|	|
4+35	0.0378	0.17	Q V	|	|	|	|
4+40	0.0390	0.17	Q V	|	|	|	|
4+45	0.0401	0.17	Q V	|	|	|	|
4+50	0.0413	0.17	Q V	|	|	|	|
4+55	0.0426	0.19	Q V	|	|	|	|
5+ 0	0.0439	0.19	Q V	|	|	|	|
5+ 5	0.0451	0.17	Q V	|	|	|	|
5+10	0.0461	0.15	Q V	|	|	|	|
5+15	0.0471	0.15	Q V	|	|	|	|
5+20	0.0482	0.15	Q V	|	|	|	|
5+25	0.0493	0.16	Q V	|	|	|	|
5+30	0.0504	0.16	Q V	|	|	|	|
5+35	0.0516	0.17	Q V	|	|	|	|
5+40	0.0529	0.19	Q V	|	|	|	|
5+45	0.0542	0.19	Q V	|	|	|	|
5+50	0.0555	0.19	Q V	|	|	|	|
5+55	0.0568	0.19	Q V	|	|	|	|
6+ 0	0.0581	0.19	Q V	|	|	|	|
6+ 5	0.0595	0.20	Q V	|	|	|	|
6+10	0.0609	0.21	Q V	|	|	|	|
6+15	0.0624	0.21	Q V	|	|	|	|
6+20	0.0639	0.21	Q V	|	|	|	|
6+25	0.0653	0.21	Q V	|	|	|	|
6+30	0.0668	0.21	Q V	|	|	|	|
6+35	0.0683	0.22	Q V	|	|	|	|
6+40	0.0699	0.23	Q V	|	|	|	|
6+45	0.0716	0.24	Q V	|	|	|	|
6+50	0.0732	0.24	Q V	|	|	|	|
6+55	0.0748	0.24	Q V	|	|	|	|
7+ 0	0.0765	0.24	Q V	|	|	|	|
7+ 5	0.0781	0.24	Q V	|	|	|	|
7+10	0.0798	0.24	Q V	|	|	|	|
7+15	0.0814	0.24	Q V	|	|	|	|

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 7+20       0.0831      0.25  Q     V   |           |           |           |
 7+25       0.0849      0.26  |Q    V   |           |           |           |
 7+30       0.0866      0.26  |Q     V  |           |           |           |
 7+35       0.0885      0.27  |Q     V  |           |           |           |
 7+40       0.0904      0.28  |Q     V  |           |           |           |
 7+45       0.0924      0.28  |Q     V  |           |           |           |
 7+50       0.0944      0.29  |Q     V  |           |           |           |
 7+55       0.0965      0.30  |Q     V  |           |           |           |
 8+ 0       0.0986      0.31  |Q      V |           |           |           |
 8+ 5       0.1008      0.32  |Q      V |           |           |           |
 8+10       0.1032      0.35  |Q      V |           |           |           |
 8+15       0.1056      0.35  |Q      V |           |           |           |
 8+20       0.1081      0.35  |Q      V |           |           |           |
 8+25       0.1105      0.36  |Q      V |           |           |           |
 8+30       0.1130      0.36  |Q       V|           |           |           |
 8+35       0.1155      0.36  |Q       V|           |           |           |
 8+40       0.1181      0.38  |Q       V|           |           |           |
 8+45       0.1207      0.38  |Q       V|           |           |           |
 8+50       0.1234      0.39  |Q        V           |           |           |
 8+55       0.1261      0.40  |Q        V           |           |           |
 9+ 0       0.1289      0.40  |Q        V           |           |           |
 9+ 5       0.1318      0.42  |Q        V           |           |           |
 9+10       0.1348      0.44  |Q        V           |           |           |
 9+15       0.1379      0.45  |Q         |V         |           |           |
 9+20       0.1411      0.46  |Q         |V         |           |           |
 9+25       0.1443      0.47  |Q         |V         |           |           |
 9+30       0.1476      0.47  |Q         | V        |           |           |
 9+35       0.1509      0.48  |Q         | V        |           |           |
 9+40       0.1543      0.49  |Q         | V        |           |           |
 9+45       0.1577      0.50  |Q         | V        |           |           |
 9+50       0.1612      0.51  | Q        |  V       |           |           |
 9+55       0.1648      0.52  | Q        |  V       |           |           |
10+ 0       0.1684      0.52  | Q        |  V       |           |           |
10+ 5       0.1716      0.47  |Q         |  V       |           |           |
10+10       0.1743      0.39  |Q         |   V      |           |           |
10+15       0.1768      0.37  |Q         |   V      |           |           |
10+20       0.1793      0.36  |Q         |   V      |           |           |
10+25       0.1818      0.36  |Q         |   V      |           |           |
10+30       0.1843      0.36  |Q         |   V      |           |           |
10+35       0.1870      0.39  |Q         |    V     |           |           |
10+40       0.1901      0.45  |Q         |    V     |           |           |
10+45       0.1933      0.46  |Q         |    V     |           |           |
10+50       0.1966      0.47  |Q         |    V     |           |           |
10+55       0.1998      0.47  |Q         |     V    |           |           |
11+ 0       0.2031      0.48  |Q         |     V    |           |           |
11+ 5       0.2063      0.47  |Q         |     V    |           |           |
11+10       0.2095      0.46  |Q         |      V   |           |           |
11+15       0.2126      0.45  |Q         |      V   |           |           |
11+20       0.2157      0.45  |Q         |      V   |           |           |
11+25       0.2188      0.45  |Q         |      V   |           |           |
11+30       0.2220      0.45  |Q         |       V  |           |           |
11+35       0.2250      0.44  |Q         |       V  |           |           |
11+40       0.2278      0.41  |Q         |       V  |           |           |
11+45       0.2306      0.41  |Q         |       V  |           |           |
11+50       0.2335      0.41  |Q         |       V  |           |           |
11+55       0.2364      0.42  |Q         |        V |           |           |
12+ 0       0.2393      0.43  |Q         |        V |           |           |
12+ 5       0.2426      0.48  |Q         |        V |           |           |
12+10       0.2465      0.56  | Q        |         V           |           |
12+15       0.2505      0.58  | Q        |         V           |           |
12+20       0.2546      0.60  | Q        |         V           |           |
12+25       0.2588      0.61  | Q        |          |V         |           |
12+30       0.2631      0.62  | Q        |          |V         |           |
12+35       0.2674      0.63  | Q        |          |V         |           |
12+40       0.2719      0.66  | Q        |          | V        |           |
12+45       0.2765      0.66  | Q        |          | V        |           |
12+50       0.2811      0.67  | Q        |          | V        |           |
12+55       0.2858      0.68  | Q        |          |  V       |           |
13+ 0       0.2906      0.69  | Q        |          |  V       |           |
13+ 5       0.2956      0.73  | Q        |          |   V      |           |
13+10       0.3010      0.78  |  Q       |          |   V      |           |
13+15       0.3065      0.80  |  Q       |          |   V      |           |
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13+20       0.3120      0.80  |  Q       |          |    V    |          |
13+25       0.3176      0.81  |  Q       |          |    V    |          |
13+30       0.3231      0.81  |  Q       |          |     V   |          |
13+35       0.3281      0.73  | Q        |          |     V   |          |
13+40       0.3323      0.60  | Q        |          |      V  |          |
13+45       0.3362      0.57  | Q        |          |      V  |          |
13+50       0.3401      0.56  | Q        |          |      V  |          |
13+55       0.3439      0.55  | Q        |          |      V  |          |
14+ 0       0.3476      0.55  | Q        |          |       V |          |
14+ 5       0.3516      0.58  | Q        |          |       V |          |
14+10       0.3559      0.62  | Q        |          |       V |          |
14+15       0.3603      0.63  | Q        |          |        V|          |
14+20       0.3646      0.63  | Q        |          |        V|          |
14+25       0.3689      0.62  | Q        |          |         V          |
14+30       0.3732      0.62  | Q        |          |         V          |
14+35       0.3774      0.62  | Q        |          |         V          |
14+40       0.3817      0.62  | Q        |          |          V         |
14+45       0.3860      0.62  | Q        |          |          V         |
14+50       0.3902      0.61  | Q        |          |          V         |
14+55       0.3943      0.60  | Q        |          |           V        |
15+ 0       0.3984      0.60  | Q        |          |           V        |
15+ 5       0.4025      0.59  | Q        |          |           V        |
15+10       0.4064      0.58  | Q        |          |            V       |
15+15       0.4104      0.57  | Q        |          |            V       |
15+20       0.4143      0.56  | Q        |          |            V       |
15+25       0.4181      0.55  | Q        |          |             V      |
15+30       0.4219      0.55  | Q        |          |             V      |
15+35       0.4254      0.52  | Q        |          |             V      |
15+40       0.4287      0.47  |Q         |          |             V      |
15+45       0.4319      0.46  |Q         |          |              V     |
15+50       0.4350      0.46  |Q         |          |              V     |
15+55       0.4381      0.45  |Q         |          |              V     |
16+ 0       0.4412      0.45  |Q         |          |              V     |
16+ 5       0.4436      0.34  |Q         |          |               V    |
16+10       0.4447      0.17  Q          |          |               V    |
16+15       0.4456      0.13  Q          |          |               V    |
16+20       0.4464      0.11  Q          |          |               V    |
16+25       0.4471      0.10  Q          |          |               V    |
16+30       0.4477      0.10  Q          |          |               V    |
16+35       0.4483      0.09  Q          |          |               V    |
16+40       0.4488      0.08  Q          |          |               V    |
16+45       0.4493      0.07  Q          |          |               V    |
16+50       0.4498      0.07  Q          |          |               V    |
16+55       0.4503      0.07  Q          |          |               V    |
17+ 0       0.4508      0.07  Q          |          |               V    |
17+ 5       0.4514      0.09  Q          |          |               V    |
17+10       0.4522      0.11  Q          |          |               V    |
17+15       0.4530      0.11  Q          |          |               V    |
17+20       0.4538      0.12  Q          |          |               V    |
17+25       0.4546      0.12  Q          |          |               V    |
17+30       0.4554      0.12  Q          |          |                V   |
17+35       0.4562      0.12  Q          |          |                V   |
17+40       0.4570      0.12  Q          |          |                V   |
17+45       0.4579      0.12  Q          |          |                V   |
17+50       0.4586      0.11  Q          |          |                V   |
17+55       0.4593      0.10  Q          |          |                V   |
18+ 0       0.4600      0.10  Q          |          |                V   |
18+ 5       0.4607      0.10  Q          |          |                V   |
18+10       0.4613      0.10  Q          |          |                V   |
18+15       0.4620      0.10  Q          |          |                V   |
18+20       0.4626      0.10  Q          |          |                V   |
18+25       0.4633      0.10  Q          |          |                V   |
18+30       0.4639      0.10  Q          |          |                V   |
18+35       0.4645      0.09  Q          |          |                V   |
18+40       0.4651      0.08  Q          |          |                V   |
18+45       0.4656      0.07  Q          |          |                V   |
18+50       0.4660      0.06  Q          |          |                V   |
18+55       0.4664      0.05  Q          |          |                V   |
19+ 0       0.4667      0.05  Q          |          |                V   |
19+ 5       0.4671      0.06  Q          |          |                 V  |
19+10       0.4676      0.07  Q          |          |                 V  |
19+15       0.4680      0.07  Q          |          |                 V  |
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  19+20       0.4686      0.08  Q          |           |           |        V |
  19+25       0.4692      0.09  Q          |           |           |        V |
  19+30       0.4698      0.09  Q          |           |           |        V |
  19+35       0.4704      0.09  Q          |           |           |        V |
  19+40       0.4710      0.08  Q          |           |           |        V |
  19+45       0.4715      0.07  Q          |           |           |        V |
  19+50       0.4719      0.06  Q          |           |           |        V |
  19+55       0.4723      0.05  Q          |           |           |        V |
  20+ 0       0.4726      0.05  Q          |           |           |        V |
  20+ 5       0.4730      0.06  Q          |           |           |        V |
  20+10       0.4735      0.07  Q          |           |           |        V |
  20+15       0.4739      0.07  Q          |           |           |        V |
  20+20       0.4744      0.07  Q          |           |           |        V |
  20+25       0.4749      0.07  Q          |           |           |        V |
  20+30       0.4754      0.07  Q          |           |           |        V |
  20+35       0.4759      0.07  Q          |           |           |        V |
  20+40       0.4764      0.07  Q          |           |           |        V |
  20+45       0.4769      0.07  Q          |           |           |        V |
  20+50       0.4773      0.06  Q          |           |           |        V |
  20+55       0.4777      0.05  Q          |           |           |        V |
  21+ 0       0.4780      0.05  Q          |           |           |        V |
  21+ 5       0.4784      0.06  Q          |           |           |        V |
  21+10       0.4789      0.07  Q          |           |           |        V |
  21+15       0.4794      0.07  Q          |           |           |        V |
  21+20       0.4798      0.06  Q          |           |           |         V|
  21+25       0.4801      0.05  Q          |           |           |         V|
  21+30       0.4805      0.05  Q          |           |           |         V|
  21+35       0.4809      0.06  Q          |           |           |         V|
  21+40       0.4813      0.07  Q          |           |           |         V|
  21+45       0.4818      0.07  Q          |           |           |         V|
  21+50       0.4822      0.06  Q          |           |           |         V|
  21+55       0.4826      0.05  Q          |           |           |         V|
  22+ 0       0.4829      0.05  Q          |           |           |         V|
  22+ 5       0.4833      0.06  Q          |           |           |         V|
  22+10       0.4838      0.07  Q          |           |           |         V|
  22+15       0.4843      0.07  Q          |           |           |         V|
  22+20       0.4847      0.06  Q          |           |           |         V|
  22+25       0.4851      0.05  Q          |           |           |         V|
  22+30       0.4854      0.05  Q          |           |           |         V|
  22+35       0.4857      0.05  Q          |           |           |         V|
  22+40       0.4861      0.05  Q          |           |           |         V|
  22+45       0.4864      0.05  Q          |           |           |         V|
  22+50       0.4867      0.05  Q          |           |           |         V|
  22+55       0.4871      0.05  Q          |           |           |         V|
  23+ 0       0.4874      0.05  Q          |           |           |         V|
  23+ 5       0.4877      0.05  Q          |           |           |         V|
  23+10       0.4880      0.05  Q          |           |           |         V|
  23+15       0.4884      0.05  Q          |           |           |         V|
  23+20       0.4887      0.05  Q          |           |           |         V|
  23+25       0.4890      0.05  Q          |           |           |         V|
  23+30       0.4893      0.05  Q          |           |           |         V|
  23+35       0.4897      0.05  Q          |           |           |         V|
  23+40       0.4900      0.05  Q          |           |           |         V|
  23+45       0.4903      0.05  Q          |           |           |         V|
  23+50       0.4907      0.05  Q          |           |           |         V|
  23+55       0.4910      0.05  Q          |           |           |         V|
  24+ 0       0.4913      0.05  Q          |           |           |         V|
  24+ 5       0.4915      0.03  Q          |           |           |         V|
  24+10       0.4916      0.01  Q          |           |           |         V|
  24+15       0.4916      0.00  Q          |           |           |         V|
  24+20       0.4917      0.00  Q          |           |           |         V|
  24+25       0.4917      0.00  Q          |           |           |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E00262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	1.20	14.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	3.00	35.40

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.200(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.072	(0.412)	0.054	0.018
2	0.17	0.60	0.086	(0.412)	0.065	0.022
3	0.25	0.60	0.086	(0.412)	0.065	0.022
4	0.33	0.60	0.086	(0.412)	0.065	0.022
5	0.42	0.60	0.086	(0.412)	0.065	0.022
6	0.50	0.70	0.101	(0.412)	0.076	0.025
7	0.58	0.70	0.101	(0.412)	0.076	0.025
8	0.67	0.70	0.101	(0.412)	0.076	0.025
9	0.75	0.70	0.101	(0.412)	0.076	0.025
10	0.83	0.70	0.101	(0.412)	0.076	0.025
11	0.92	0.70	0.101	(0.412)	0.076	0.025
12	1.00	0.80	0.115	(0.412)	0.086	0.029
13	1.08	0.80	0.115	(0.412)	0.086	0.029
14	1.17	0.80	0.115	(0.412)	0.086	0.029
15	1.25	0.80	0.115	(0.412)	0.086	0.029
16	1.33	0.80	0.115	(0.412)	0.086	0.029
17	1.42	0.80	0.115	(0.412)	0.086	0.029
18	1.50	0.80	0.115	(0.412)	0.086	0.029
19	1.58	0.80	0.115	(0.412)	0.086	0.029
20	1.67	0.80	0.115	(0.412)	0.086	0.029
21	1.75	0.80	0.115	(0.412)	0.086	0.029
22	1.83	0.80	0.115	(0.412)	0.086	0.029
23	1.92	0.80	0.115	(0.412)	0.086	0.029
24	2.00	0.90	0.130	(0.412)	0.097	0.032
25	2.08	0.80	0.115	(0.412)	0.086	0.029
26	2.17	0.90	0.130	(0.412)	0.097	0.032
27	2.25	0.90	0.130	(0.412)	0.097	0.032
28	2.33	0.90	0.130	(0.412)	0.097	0.032
29	2.42	0.90	0.130	(0.412)	0.097	0.032
30	2.50	0.90	0.130	(0.412)	0.097	0.032
31	2.58	0.90	0.130	(0.412)	0.097	0.032
32	2.67	0.90	0.130	(0.412)	0.097	0.032
33	2.75	1.00	0.144	(0.412)	0.108	0.036
34	2.83	1.00	0.144	(0.412)	0.108	0.036
35	2.92	1.00	0.144	(0.412)	0.108	0.036
36	3.00	1.00	0.144	(0.412)	0.108	0.036

37	3.08	1.00	0.144	(0.412)	0.108	0.036	
38	3.17	1.10	0.158	(0.412)	0.119	0.040	
39	3.25	1.10	0.158	(0.412)	0.119	0.040	
40	3.33	1.10	0.158	(0.412)	0.119	0.040	
41	3.42	1.20	0.173	(0.412)	0.130	0.043	
42	3.50	1.30	0.187	(0.412)	0.140	0.047	
43	3.58	1.40	0.202	(0.412)	0.151	0.050	
44	3.67	1.40	0.202	(0.412)	0.151	0.050	
45	3.75	1.50	0.216	(0.412)	0.162	0.054	
46	3.83	1.50	0.216	(0.412)	0.162	0.054	
47	3.92	1.60	0.230	(0.412)	0.173	0.058	
48	4.00	1.60	0.230	(0.412)	0.173	0.058	
49	4.08	1.70	0.245	(0.412)	0.184	0.061	
50	4.17	1.80	0.259	(0.412)	0.194	0.065	
51	4.25	1.90	0.274	(0.412)	0.205	0.068	
52	4.33	2.00	0.288	(0.412)	0.216	0.072	
53	4.42	2.10	0.302	(0.412)	0.227	0.076	
54	4.50	2.10	0.302	(0.412)	0.227	0.076	
55	4.58	2.20	0.317	(0.412)	0.238	0.079	
56	4.67	2.30	0.331	(0.412)	0.248	0.083	
57	4.75	2.40	0.346	(0.412)	0.259	0.086	
58	4.83	2.40	0.346	(0.412)	0.259	0.086	
59	4.92	2.50	0.360	(0.412)	0.270	0.090	
60	5.00	2.60	0.374	(0.412)	0.281	0.094	
61	5.08	3.10	0.446	(0.412)	0.335	0.112	
62	5.17	3.60	0.518	(0.412)	0.389	0.130	
63	5.25	3.90	0.562	0.412	(0.421)	0.149	
64	5.33	4.20	0.605	0.412	(0.454)	0.193	
65	5.42	4.70	0.677	0.412	(0.508)	0.265	
66	5.50	5.60	0.806	0.412	(0.605)	0.394	
67	5.58	1.90	0.274	(0.412)	0.205	0.068	
68	5.67	0.90	0.130	(0.412)	0.097	0.032	
69	5.75	0.60	0.086	(0.412)	0.065	0.022	
70	5.83	0.50	0.072	(0.412)	0.054	0.018	
71	5.92	0.30	0.043	(0.412)	0.032	0.011	
72	6.00	0.20	0.029	(0.412)	0.022	0.007	

(Loss Rate Not Used)

Sum = 100.0 Sum = 3.9

Flood volume = Effective rainfall 0.33(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.87(In)
Total soil loss = 0.857(Ac.Ft)
Total rainfall = 1.20(In)
Flood volume = 14058.6 Cubic Feet
Total soil loss = 37340.2 Cubic Feet

Peak flow rate of this hydrograph = 3.404(CFS)

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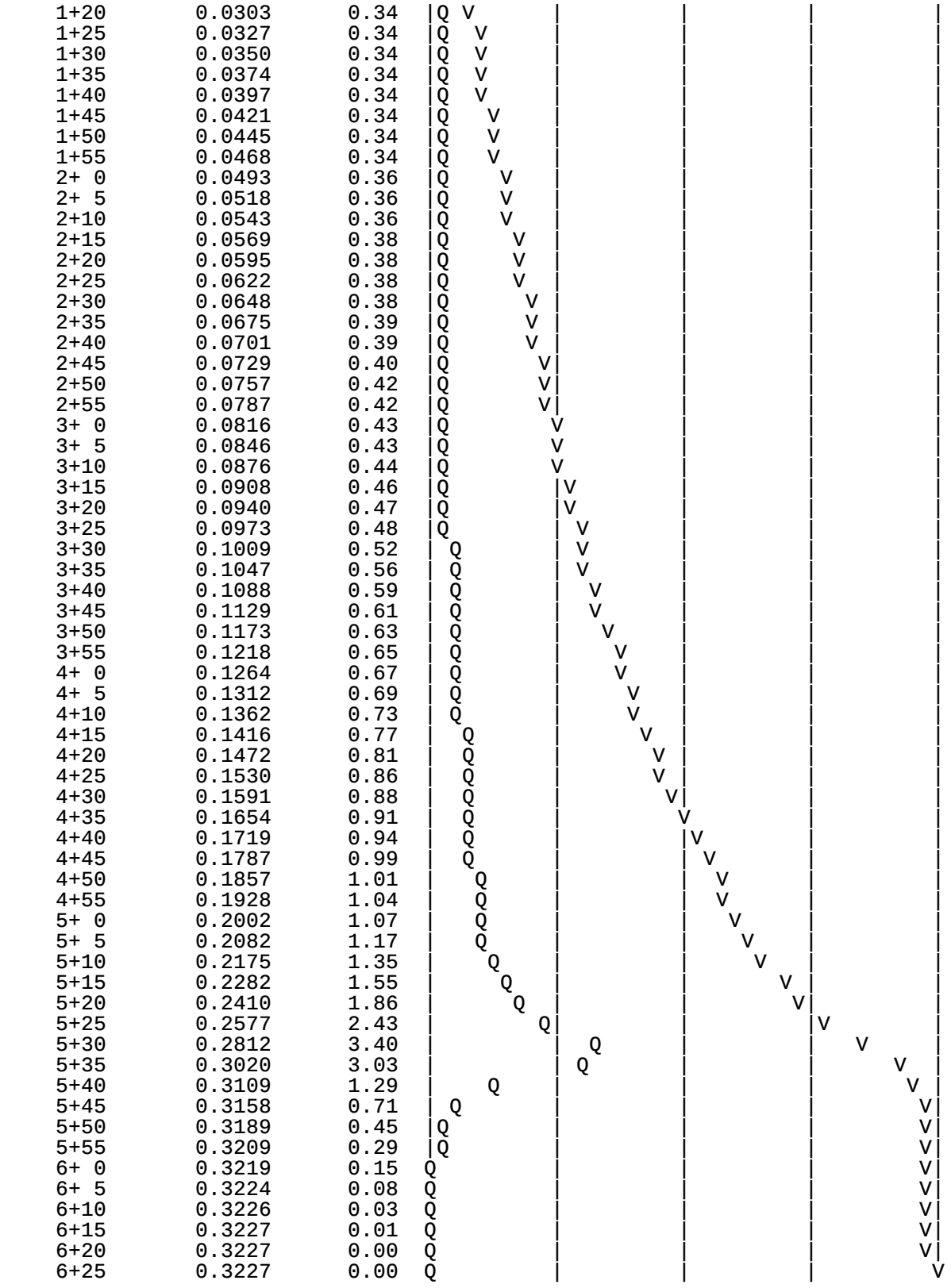
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0005	0.07	Q				
0+10	0.0017	0.18	Q				
0+15	0.0033	0.23	Q				
0+20	0.0050	0.24	Q				
0+25	0.0067	0.25	VQ				
0+30	0.0086	0.27	|Q				
0+35	0.0106	0.29	|Q				
0+40	0.0126	0.30	|Q				
0+45	0.0147	0.30	|Q				
0+50	0.0167	0.30	|QV				
0+55	0.0188	0.30	|QV				
1+ 0	0.0210	0.31	|QV				
1+ 5	0.0233	0.33	|QV				
1+10	0.0256	0.34	|Q V				
1+15	0.0279	0.34	|Q V				


1+20 0.0303 0.34
1+25 0.0327 0.34
1+30 0.0350 0.34
1+35 0.0374 0.34
1+40 0.0397 0.34
1+45 0.0421 0.34
1+50 0.0445 0.34
1+55 0.0468 0.34
2+ 0 0.0493 0.36
2+ 5 0.0518 0.36
2+10 0.0543 0.36
2+15 0.0569 0.38
2+20 0.0595 0.38
2+25 0.0622 0.38
2+30 0.0648 0.38
2+35 0.0675 0.39
2+40 0.0701 0.39
2+45 0.0729 0.40
2+50 0.0757 0.42
2+55 0.0787 0.42
3+ 0 0.0816 0.43
3+ 5 0.0846 0.43
3+10 0.0876 0.44
3+15 0.0908 0.46
3+20 0.0940 0.47
3+25 0.0973 0.48
3+30 0.1009 0.52
3+35 0.1047 0.56
3+40 0.1088 0.59
3+45 0.1129 0.61
3+50 0.1173 0.63
3+55 0.1218 0.65
4+ 0 0.1264 0.67
4+ 5 0.1312 0.69
4+10 0.1362 0.73
4+15 0.1416 0.77
4+20 0.1472 0.81
4+25 0.1530 0.86
4+30 0.1591 0.88
4+35 0.1654 0.91
4+40 0.1719 0.94
4+45 0.1787 0.99
4+50 0.1857 1.01
4+55 0.1928 1.04
5+ 0 0.2002 1.07
5+ 5 0.2082 1.17
5+10 0.2175 1.35
5+15 0.2282 1.55
5+20 0.2410 1.86
5+25 0.2577 2.43
5+30 0.2812 3.40
5+35 0.3020 3.03
5+40 0.3109 1.29
5+45 0.3158 0.71
5+50 0.3189 0.45
5+55 0.3209 0.29
6+ 0 0.3219 0.15
6+ 5 0.3224 0.08
6+10 0.3226 0.03
6+15 0.3227 0.01
6+20 0.3227 0.00
6+25 0.3227 0.00

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E00232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

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EXISTING CONDITION
HYDROLOGIC ANALYSIS
2-YEAR

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Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	0.90	10.62

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	2.35	27.73

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 0.900(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.900(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.140	(0.412)	0.105	0.035
2	0.17	1.30	0.140	(0.412)	0.105	0.035
3	0.25	1.10	0.119	(0.412)	0.089	0.030
4	0.33	1.50	0.162	(0.412)	0.121	0.040
5	0.42	1.50	0.162	(0.412)	0.121	0.040
6	0.50	1.80	0.194	(0.412)	0.146	0.049
7	0.58	1.50	0.162	(0.412)	0.121	0.040
8	0.67	1.80	0.194	(0.412)	0.146	0.049
9	0.75	1.80	0.194	(0.412)	0.146	0.049
10	0.83	1.50	0.162	(0.412)	0.121	0.040
11	0.92	1.60	0.173	(0.412)	0.130	0.043
12	1.00	1.80	0.194	(0.412)	0.146	0.049
13	1.08	2.20	0.238	(0.412)	0.178	0.059
14	1.17	2.20	0.238	(0.412)	0.178	0.059
15	1.25	2.20	0.238	(0.412)	0.178	0.059
16	1.33	2.00	0.216	(0.412)	0.162	0.054
17	1.42	2.60	0.281	(0.412)	0.211	0.070
18	1.50	2.70	0.292	(0.412)	0.219	0.073
19	1.58	2.40	0.259	(0.412)	0.194	0.065
20	1.67	2.70	0.292	(0.412)	0.219	0.073
21	1.75	3.30	0.356	(0.412)	0.267	0.089
22	1.83	3.10	0.335	(0.412)	0.251	0.084
23	1.92	2.90	0.313	(0.412)	0.235	0.078
24	2.00	3.00	0.324	(0.412)	0.243	0.081
25	2.08	3.10	0.335	(0.412)	0.251	0.084
26	2.17	4.20	0.454	(0.412)	0.340	0.113
27	2.25	5.00	0.540	(0.412)	0.405	0.135
28	2.33	3.50	0.378	(0.412)	0.283	0.094
29	2.42	6.80	0.734	0.412	(0.551)	0.322
30	2.50	7.30	0.788	0.412	(0.591)	0.376
31	2.58	8.20	0.886	0.412	(0.664)	0.473
32	2.67	5.90	0.637	0.412	(0.478)	0.225
33	2.75	2.00	0.216	(0.412)	0.162	0.054
34	2.83	1.80	0.194	(0.412)	0.146	0.049
35	2.92	1.80	0.194	(0.412)	0.146	0.049
36	3.00	0.60	0.065	(0.412)	0.049	0.016

(Loss Rate Not Used)

Sum = 100.0 Sum = 3.3

Flood volume = Effective rainfall 0.28(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.62(In)
Total soil loss = 0.612(Ac.Ft)
Total rainfall = 0.90(In)
Flood volume = 11906.0 Cubic Feet
Total soil loss = 26642.6 Cubic Feet

Peak flow rate of this hydrograph = 4.480(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0009	0.13	Q
0+10	0.0032	0.33	VQ
0+15	0.0057	0.36	VQ
0+20	0.0084	0.39	|Q
0+25	0.0115	0.45	|Q
0+30	0.0150	0.50	| Q
0+35	0.0186	0.52	| Q
0+40	0.0222	0.52	| QV
0+45	0.0260	0.56	| QV
0+50	0.0298	0.54	| Q V
0+55	0.0333	0.51	| Q V
1+ 0	0.0370	0.54	| Q V
1+ 5	0.0411	0.61	| Q V
1+10	0.0458	0.67	| Q V
1+15	0.0505	0.69	| Q V
1+20	0.0552	0.68	| Q V
1+25	0.0602	0.72	| Q V
1+30	0.0657	0.81	| Q V
1+35	0.0714	0.81	| Q V
1+40	0.0769	0.81	| Q V
1+45	0.0832	0.91	| Q V
1+50	0.0901	0.99	| Q V
1+55	0.0968	0.97	| Q V
2+ 0	0.1033	0.95	| Q V
2+ 5	0.1100	0.97	| Q V
2+10	0.1176	1.10	| Q V
2+15	0.1269	1.36	| Q V
2+20	0.1363	1.36	| Q V
2+25	0.1505	2.05	| Q V
2+30	0.1746	3.51	| Q V
2+35	0.2055	4.48	| Q V
2+40	0.2350	4.29	| Q V
2+45	0.2520	2.46	| Q V
2+50	0.2606	1.26	| Q V
2+55	0.2667	0.88	| Q V
3+ 0	0.2708	0.59	| Q V
3+ 5	0.2725	0.24	Q V
3+10	0.2730	0.08	Q V
3+15	0.2732	0.03	Q V
3+20	0.2733	0.01	Q V
3+25	0.2733	0.00	Q V

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E00212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	0.54	6.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	1.36	16.05

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.540(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.540(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
		Sum =	100.000 Sum=	11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	4.40	0.285	(0.412)		0.214	0.071
2	0.17	4.50	0.292	(0.412)		0.219	0.073
3	0.25	5.40	0.350	(0.412)		0.262	0.087
4	0.33	5.40	0.350	(0.412)		0.262	0.087
5	0.42	5.70	0.369	(0.412)		0.277	0.092
6	0.50	6.40	0.415	(0.412)		0.311	0.104
7	0.58	7.90	0.512	(0.412)		0.384	0.128
8	0.67	9.10	0.590	0.412	(0.442)		0.178
9	0.75	12.80	0.829	0.412	(0.622)		0.417
10	0.83	25.60	1.659	0.412	(1.244)		1.247
11	0.92	7.90	0.512	(0.412)		0.384	0.128
12	1.00	4.90	0.317	(0.412)		0.238	0.079
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	2.7

Flood volume = Effective rainfall 0.22(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.32(In)
Total soil loss = 0.310(Ac.Ft)
Total rainfall = 0.54(In)
Flood volume = 9608.2 Cubic Feet
Total soil loss = 13519.7 Cubic Feet

Peak flow rate of this hydrograph = 8.247(CFS)

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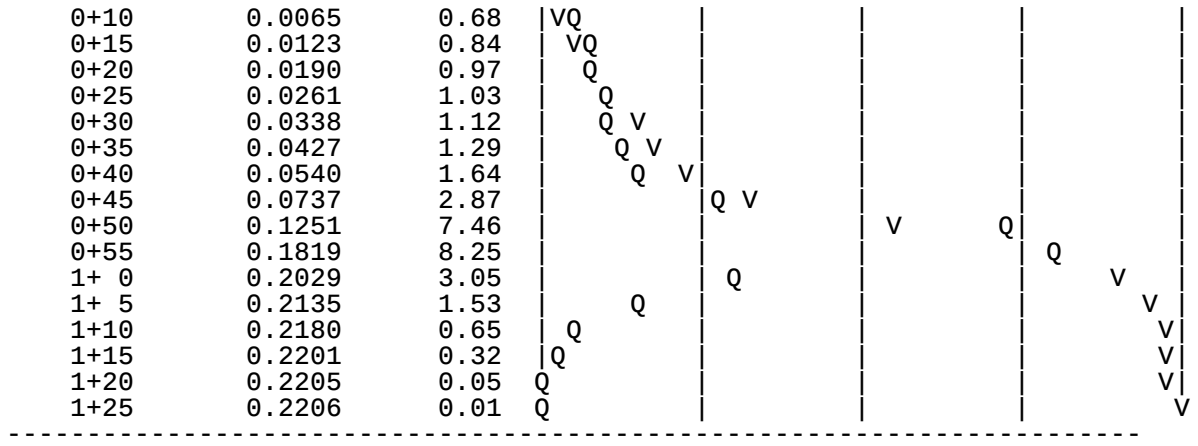
1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0019	0.27	VQ	|	|	|	|


0+10 0.0065 0.68
0+15 0.0123 0.84
0+20 0.0190 0.97
0+25 0.0261 1.03
0+30 0.0338 1.12
0+35 0.0427 1.29
0+40 0.0540 1.64
0+45 0.0737 2.87
0+50 0.1251 7.46
0+55 0.1819 8.25
1+ 0 0.2029 3.05
1+ 5 0.2135 1.53
1+10 0.2180 0.65
1+15 0.2201 0.32
1+20 0.2205 0.05
1+25 0.2206 0.01

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E005245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	2.00	23.60

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	6.40	75.52

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.031(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.031(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.024	(0.731)	0.018	0.006
2	0.17	0.07	0.024	(0.728)	0.018	0.006
3	0.25	0.07	0.024	(0.725)	0.018	0.006
4	0.33	0.10	0.036	(0.722)	0.027	0.009
5	0.42	0.10	0.036	(0.719)	0.027	0.009
6	0.50	0.10	0.036	(0.716)	0.027	0.009
7	0.58	0.10	0.036	(0.714)	0.027	0.009
8	0.67	0.10	0.036	(0.711)	0.027	0.009
9	0.75	0.10	0.036	(0.708)	0.027	0.009
10	0.83	0.13	0.048	(0.705)	0.036	0.012
11	0.92	0.13	0.048	(0.703)	0.036	0.012
12	1.00	0.13	0.048	(0.700)	0.036	0.012
13	1.08	0.10	0.036	(0.697)	0.027	0.009
14	1.17	0.10	0.036	(0.694)	0.027	0.009
15	1.25	0.10	0.036	(0.692)	0.027	0.009
16	1.33	0.10	0.036	(0.689)	0.027	0.009
17	1.42	0.10	0.036	(0.686)	0.027	0.009
18	1.50	0.10	0.036	(0.683)	0.027	0.009
19	1.58	0.10	0.036	(0.681)	0.027	0.009
20	1.67	0.10	0.036	(0.678)	0.027	0.009
21	1.75	0.10	0.036	(0.675)	0.027	0.009
22	1.83	0.13	0.048	(0.672)	0.036	0.012
23	1.92	0.13	0.048	(0.670)	0.036	0.012
24	2.00	0.13	0.048	(0.667)	0.036	0.012
25	2.08	0.13	0.048	(0.664)	0.036	0.012
26	2.17	0.13	0.048	(0.662)	0.036	0.012
27	2.25	0.13	0.048	(0.659)	0.036	0.012
28	2.33	0.13	0.048	(0.656)	0.036	0.012
29	2.42	0.13	0.048	(0.654)	0.036	0.012
30	2.50	0.13	0.048	(0.651)	0.036	0.012
31	2.58	0.17	0.061	(0.648)	0.045	0.015
32	2.67	0.17	0.061	(0.646)	0.045	0.015
33	2.75	0.17	0.061	(0.643)	0.045	0.015
34	2.83	0.17	0.061	(0.640)	0.045	0.015
35	2.92	0.17	0.061	(0.638)	0.045	0.015
36	3.00	0.17	0.061	(0.635)	0.045	0.015

37	3.08	0.17	0.061	(0.632)	0.045	0.015
38	3.17	0.17	0.061	(0.630)	0.045	0.015
39	3.25	0.17	0.061	(0.627)	0.045	0.015
40	3.33	0.17	0.061	(0.624)	0.045	0.015
41	3.42	0.17	0.061	(0.622)	0.045	0.015
42	3.50	0.17	0.061	(0.619)	0.045	0.015
43	3.58	0.17	0.061	(0.617)	0.045	0.015
44	3.67	0.17	0.061	(0.614)	0.045	0.015
45	3.75	0.17	0.061	(0.612)	0.045	0.015
46	3.83	0.20	0.073	(0.609)	0.055	0.018
47	3.92	0.20	0.073	(0.606)	0.055	0.018
48	4.00	0.20	0.073	(0.604)	0.055	0.018
49	4.08	0.20	0.073	(0.601)	0.055	0.018
50	4.17	0.20	0.073	(0.599)	0.055	0.018
51	4.25	0.20	0.073	(0.596)	0.055	0.018
52	4.33	0.23	0.085	(0.594)	0.064	0.021
53	4.42	0.23	0.085	(0.591)	0.064	0.021
54	4.50	0.23	0.085	(0.589)	0.064	0.021
55	4.58	0.23	0.085	(0.586)	0.064	0.021
56	4.67	0.23	0.085	(0.583)	0.064	0.021
57	4.75	0.23	0.085	(0.581)	0.064	0.021
58	4.83	0.27	0.097	(0.578)	0.073	0.024
59	4.92	0.27	0.097	(0.576)	0.073	0.024
60	5.00	0.27	0.097	(0.573)	0.073	0.024
61	5.08	0.20	0.073	(0.571)	0.055	0.018
62	5.17	0.20	0.073	(0.568)	0.055	0.018
63	5.25	0.20	0.073	(0.566)	0.055	0.018
64	5.33	0.23	0.085	(0.564)	0.064	0.021
65	5.42	0.23	0.085	(0.561)	0.064	0.021
66	5.50	0.23	0.085	(0.559)	0.064	0.021
67	5.58	0.27	0.097	(0.556)	0.073	0.024
68	5.67	0.27	0.097	(0.554)	0.073	0.024
69	5.75	0.27	0.097	(0.551)	0.073	0.024
70	5.83	0.27	0.097	(0.549)	0.073	0.024
71	5.92	0.27	0.097	(0.546)	0.073	0.024
72	6.00	0.27	0.097	(0.544)	0.073	0.024
73	6.08	0.30	0.109	(0.542)	0.082	0.027
74	6.17	0.30	0.109	(0.539)	0.082	0.027
75	6.25	0.30	0.109	(0.537)	0.082	0.027
76	6.33	0.30	0.109	(0.534)	0.082	0.027
77	6.42	0.30	0.109	(0.532)	0.082	0.027
78	6.50	0.30	0.109	(0.530)	0.082	0.027
79	6.58	0.33	0.121	(0.527)	0.091	0.030
80	6.67	0.33	0.121	(0.525)	0.091	0.030
81	6.75	0.33	0.121	(0.522)	0.091	0.030
82	6.83	0.33	0.121	(0.520)	0.091	0.030
83	6.92	0.33	0.121	(0.518)	0.091	0.030
84	7.00	0.33	0.121	(0.515)	0.091	0.030
85	7.08	0.33	0.121	(0.513)	0.091	0.030
86	7.17	0.33	0.121	(0.511)	0.091	0.030
87	7.25	0.33	0.121	(0.508)	0.091	0.030
88	7.33	0.37	0.133	(0.506)	0.100	0.033
89	7.42	0.37	0.133	(0.504)	0.100	0.033
90	7.50	0.37	0.133	(0.501)	0.100	0.033
91	7.58	0.40	0.145	(0.499)	0.109	0.036
92	7.67	0.40	0.145	(0.497)	0.109	0.036
93	7.75	0.40	0.145	(0.495)	0.109	0.036
94	7.83	0.43	0.158	(0.492)	0.118	0.039
95	7.92	0.43	0.158	(0.490)	0.118	0.039
96	8.00	0.43	0.158	(0.488)	0.118	0.039
97	8.08	0.50	0.182	(0.485)	0.136	0.045
98	8.17	0.50	0.182	(0.483)	0.136	0.045
99	8.25	0.50	0.182	(0.481)	0.136	0.045
100	8.33	0.50	0.182	(0.479)	0.136	0.045
101	8.42	0.50	0.182	(0.476)	0.136	0.045
102	8.50	0.50	0.182	(0.474)	0.136	0.045
103	8.58	0.53	0.194	(0.472)	0.145	0.048
104	8.67	0.53	0.194	(0.470)	0.145	0.048
105	8.75	0.53	0.194	(0.468)	0.145	0.048
106	8.83	0.57	0.206	(0.465)	0.155	0.052
107	8.92	0.57	0.206	(0.463)	0.155	0.052
108	9.00	0.57	0.206	(0.461)	0.155	0.052

109	9.08	0.63	0.230	(0.459)	0.173	0.058
110	9.17	0.63	0.230	(0.457)	0.173	0.058
111	9.25	0.63	0.230	(0.454)	0.173	0.058
112	9.33	0.67	0.242	(0.452)	0.182	0.061
113	9.42	0.67	0.242	(0.450)	0.182	0.061
114	9.50	0.67	0.242	(0.448)	0.182	0.061
115	9.58	0.70	0.255	(0.446)	0.191	0.064
116	9.67	0.70	0.255	(0.444)	0.191	0.064
117	9.75	0.70	0.255	(0.442)	0.191	0.064
118	9.83	0.73	0.267	(0.439)	0.200	0.067
119	9.92	0.73	0.267	(0.437)	0.200	0.067
120	10.00	0.73	0.267	(0.435)	0.200	0.067
121	10.08	0.50	0.182	(0.433)	0.136	0.045
122	10.17	0.50	0.182	(0.431)	0.136	0.045
123	10.25	0.50	0.182	(0.429)	0.136	0.045
124	10.33	0.50	0.182	(0.427)	0.136	0.045
125	10.42	0.50	0.182	(0.425)	0.136	0.045
126	10.50	0.50	0.182	(0.423)	0.136	0.045
127	10.58	0.67	0.242	(0.421)	0.182	0.061
128	10.67	0.67	0.242	(0.419)	0.182	0.061
129	10.75	0.67	0.242	(0.417)	0.182	0.061
130	10.83	0.67	0.242	(0.414)	0.182	0.061
131	10.92	0.67	0.242	(0.412)	0.182	0.061
132	11.00	0.67	0.242	(0.410)	0.182	0.061
133	11.08	0.63	0.230	(0.408)	0.173	0.058
134	11.17	0.63	0.230	(0.406)	0.173	0.058
135	11.25	0.63	0.230	(0.404)	0.173	0.058
136	11.33	0.63	0.230	(0.402)	0.173	0.058
137	11.42	0.63	0.230	(0.400)	0.173	0.058
138	11.50	0.63	0.230	(0.398)	0.173	0.058
139	11.58	0.57	0.206	(0.396)	0.155	0.052
140	11.67	0.57	0.206	(0.394)	0.155	0.052
141	11.75	0.57	0.206	(0.392)	0.155	0.052
142	11.83	0.60	0.218	(0.391)	0.164	0.055
143	11.92	0.60	0.218	(0.389)	0.164	0.055
144	12.00	0.60	0.218	(0.387)	0.164	0.055
145	12.08	0.83	0.303	(0.385)	0.227	0.076
146	12.17	0.83	0.303	(0.383)	0.227	0.076
147	12.25	0.83	0.303	(0.381)	0.227	0.076
148	12.33	0.87	0.315	(0.379)	0.236	0.079
149	12.42	0.87	0.315	(0.377)	0.236	0.079
150	12.50	0.87	0.315	(0.375)	0.236	0.079
151	12.58	0.93	0.339	(0.373)	0.255	0.085
152	12.67	0.93	0.339	(0.371)	0.255	0.085
153	12.75	0.93	0.339	(0.369)	0.255	0.085
154	12.83	0.97	0.352	(0.368)	0.264	0.088
155	12.92	0.97	0.352	(0.366)	0.264	0.088
156	13.00	0.97	0.352	(0.364)	0.264	0.088
157	13.08	1.13	0.412	(0.362)	0.309	0.103
158	13.17	1.13	0.412	(0.360)	0.309	0.103
159	13.25	1.13	0.412	(0.358)	0.309	0.103
160	13.33	1.13	0.412	(0.357)	0.309	0.103
161	13.42	1.13	0.412	(0.355)	0.309	0.103
162	13.50	1.13	0.412	(0.353)	0.309	0.103
163	13.58	0.77	0.279	(0.351)	0.209	0.070
164	13.67	0.77	0.279	(0.349)	0.209	0.070
165	13.75	0.77	0.279	(0.348)	0.209	0.070
166	13.83	0.77	0.279	(0.346)	0.209	0.070
167	13.92	0.77	0.279	(0.344)	0.209	0.070
168	14.00	0.77	0.279	(0.342)	0.209	0.070
169	14.08	0.90	0.327	(0.341)	0.245	0.082
170	14.17	0.90	0.327	(0.339)	0.245	0.082
171	14.25	0.90	0.327	(0.337)	0.245	0.082
172	14.33	0.87	0.315	(0.335)	0.236	0.079
173	14.42	0.87	0.315	(0.334)	0.236	0.079
174	14.50	0.87	0.315	(0.332)	0.236	0.079
175	14.58	0.87	0.315	(0.330)	0.236	0.079
176	14.67	0.87	0.315	(0.329)	0.236	0.079
177	14.75	0.87	0.315	(0.327)	0.236	0.079
178	14.83	0.83	0.303	(0.325)	0.227	0.076
179	14.92	0.83	0.303	(0.324)	0.227	0.076
180	15.00	0.83	0.303	(0.322)	0.227	0.076

181	15.08	0.80	0.291	(0.320)	0.218	0.073
182	15.17	0.80	0.291	(0.319)	0.218	0.073
183	15.25	0.80	0.291	(0.317)	0.218	0.073
184	15.33	0.77	0.279	(0.315)	0.209	0.070
185	15.42	0.77	0.279	(0.314)	0.209	0.070
186	15.50	0.77	0.279	(0.312)	0.209	0.070
187	15.58	0.63	0.230	(0.311)	0.173	0.058
188	15.67	0.63	0.230	(0.309)	0.173	0.058
189	15.75	0.63	0.230	(0.307)	0.173	0.058
190	15.83	0.63	0.230	(0.306)	0.173	0.058
191	15.92	0.63	0.230	(0.304)	0.173	0.058
192	16.00	0.63	0.230	(0.303)	0.173	0.058
193	16.08	0.13	0.048	(0.301)	0.036	0.012
194	16.17	0.13	0.048	(0.300)	0.036	0.012
195	16.25	0.13	0.048	(0.298)	0.036	0.012
196	16.33	0.13	0.048	(0.297)	0.036	0.012
197	16.42	0.13	0.048	(0.295)	0.036	0.012
198	16.50	0.13	0.048	(0.293)	0.036	0.012
199	16.58	0.10	0.036	(0.292)	0.027	0.009
200	16.67	0.10	0.036	(0.291)	0.027	0.009
201	16.75	0.10	0.036	(0.289)	0.027	0.009
202	16.83	0.10	0.036	(0.288)	0.027	0.009
203	16.92	0.10	0.036	(0.286)	0.027	0.009
204	17.00	0.10	0.036	(0.285)	0.027	0.009
205	17.08	0.17	0.061	(0.283)	0.045	0.015
206	17.17	0.17	0.061	(0.282)	0.045	0.015
207	17.25	0.17	0.061	(0.280)	0.045	0.015
208	17.33	0.17	0.061	(0.279)	0.045	0.015
209	17.42	0.17	0.061	(0.278)	0.045	0.015
210	17.50	0.17	0.061	(0.276)	0.045	0.015
211	17.58	0.17	0.061	(0.275)	0.045	0.015
212	17.67	0.17	0.061	(0.273)	0.045	0.015
213	17.75	0.17	0.061	(0.272)	0.045	0.015
214	17.83	0.13	0.048	(0.271)	0.036	0.012
215	17.92	0.13	0.048	(0.269)	0.036	0.012
216	18.00	0.13	0.048	(0.268)	0.036	0.012
217	18.08	0.13	0.048	(0.267)	0.036	0.012
218	18.17	0.13	0.048	(0.265)	0.036	0.012
219	18.25	0.13	0.048	(0.264)	0.036	0.012
220	18.33	0.13	0.048	(0.263)	0.036	0.012
221	18.42	0.13	0.048	(0.262)	0.036	0.012
222	18.50	0.13	0.048	(0.260)	0.036	0.012
223	18.58	0.10	0.036	(0.259)	0.027	0.009
224	18.67	0.10	0.036	(0.258)	0.027	0.009
225	18.75	0.10	0.036	(0.257)	0.027	0.009
226	18.83	0.07	0.024	(0.255)	0.018	0.006
227	18.92	0.07	0.024	(0.254)	0.018	0.006
228	19.00	0.07	0.024	(0.253)	0.018	0.006
229	19.08	0.10	0.036	(0.252)	0.027	0.009
230	19.17	0.10	0.036	(0.251)	0.027	0.009
231	19.25	0.10	0.036	(0.249)	0.027	0.009
232	19.33	0.13	0.048	(0.248)	0.036	0.012
233	19.42	0.13	0.048	(0.247)	0.036	0.012
234	19.50	0.13	0.048	(0.246)	0.036	0.012
235	19.58	0.10	0.036	(0.245)	0.027	0.009
236	19.67	0.10	0.036	(0.244)	0.027	0.009
237	19.75	0.10	0.036	(0.243)	0.027	0.009
238	19.83	0.07	0.024	(0.241)	0.018	0.006
239	19.92	0.07	0.024	(0.240)	0.018	0.006
240	20.00	0.07	0.024	(0.239)	0.018	0.006
241	20.08	0.10	0.036	(0.238)	0.027	0.009
242	20.17	0.10	0.036	(0.237)	0.027	0.009
243	20.25	0.10	0.036	(0.236)	0.027	0.009
244	20.33	0.10	0.036	(0.235)	0.027	0.009
245	20.42	0.10	0.036	(0.234)	0.027	0.009
246	20.50	0.10	0.036	(0.233)	0.027	0.009
247	20.58	0.10	0.036	(0.232)	0.027	0.009
248	20.67	0.10	0.036	(0.231)	0.027	0.009
249	20.75	0.10	0.036	(0.230)	0.027	0.009
250	20.83	0.07	0.024	(0.229)	0.018	0.006
251	20.92	0.07	0.024	(0.228)	0.018	0.006
252	21.00	0.07	0.024	(0.227)	0.018	0.006

253	21.08	0.10	0.036	(	0.227)	0.027	0.009
254	21.17	0.10	0.036	(	0.226)	0.027	0.009
255	21.25	0.10	0.036	(	0.225)	0.027	0.009
256	21.33	0.07	0.024	(	0.224)	0.018	0.006
257	21.42	0.07	0.024	(	0.223)	0.018	0.006
258	21.50	0.07	0.024	(	0.222)	0.018	0.006
259	21.58	0.10	0.036	(	0.221)	0.027	0.009
260	21.67	0.10	0.036	(	0.221)	0.027	0.009
261	21.75	0.10	0.036	(	0.220)	0.027	0.009
262	21.83	0.07	0.024	(	0.219)	0.018	0.006
263	21.92	0.07	0.024	(	0.218)	0.018	0.006
264	22.00	0.07	0.024	(	0.218)	0.018	0.006
265	22.08	0.10	0.036	(	0.217)	0.027	0.009
266	22.17	0.10	0.036	(	0.216)	0.027	0.009
267	22.25	0.10	0.036	(	0.215)	0.027	0.009
268	22.33	0.07	0.024	(	0.215)	0.018	0.006
269	22.42	0.07	0.024	(	0.214)	0.018	0.006
270	22.50	0.07	0.024	(	0.214)	0.018	0.006
271	22.58	0.07	0.024	(	0.213)	0.018	0.006
272	22.67	0.07	0.024	(	0.212)	0.018	0.006
273	22.75	0.07	0.024	(	0.212)	0.018	0.006
274	22.83	0.07	0.024	(	0.211)	0.018	0.006
275	22.92	0.07	0.024	(	0.211)	0.018	0.006
276	23.00	0.07	0.024	(	0.210)	0.018	0.006
277	23.08	0.07	0.024	(	0.210)	0.018	0.006
278	23.17	0.07	0.024	(	0.209)	0.018	0.006
279	23.25	0.07	0.024	(	0.209)	0.018	0.006
280	23.33	0.07	0.024	(	0.208)	0.018	0.006
281	23.42	0.07	0.024	(	0.208)	0.018	0.006
282	23.50	0.07	0.024	(	0.208)	0.018	0.006
283	23.58	0.07	0.024	(	0.207)	0.018	0.006
284	23.67	0.07	0.024	(	0.207)	0.018	0.006
285	23.75	0.07	0.024	(	0.207)	0.018	0.006
286	23.83	0.07	0.024	(	0.206)	0.018	0.006
287	23.92	0.07	0.024	(	0.206)	0.018	0.006
288	24.00	0.07	0.024	(	0.206)	0.018	0.006

(Loss Rate Not Used)

Sum = 100.0 Sum = 9.1

Flood volume = Effective rainfall 0.76(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.7(Ac.Ft)
Total soil loss = 2.27(In)
Total soil loss = 2.235(Ac.Ft)
Total rainfall = 3.03(In)
Flood volume = 32452.3 Cubic Feet
Total soil loss = 97356.9 Cubic Feet

Peak flow rate of this hydrograph = 1.226(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0002	0.02	Q	|	|	|	|
0+10	0.0006	0.06	Q	|	|	|	|
0+15	0.0010	0.07	Q	|	|	|	|
0+20	0.0016	0.08	Q	|	|	|	|
0+25	0.0022	0.10	Q	|	|	|	|
0+30	0.0030	0.10	Q	|	|	|	|
0+35	0.0037	0.11	Q	|	|	|	|
0+40	0.0044	0.11	Q	|	|	|	|
0+45	0.0052	0.11	Q	|	|	|	|
0+50	0.0060	0.12	Q	|	|	|	|
0+55	0.0070	0.14	Q	|	|	|	|
1+ 0	0.0079	0.14	Q	|	|	|	|
1+ 5	0.0088	0.13	Q	|	|	|	|
1+10	0.0096	0.12	Q	|	|	|	|
1+15	0.0104	0.11	Q	|	|	|	|

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1+20       0.0111      0.11  Q          |          |          |          |
1+25       0.0119      0.11  Q          |          |          |          |
1+30       0.0126      0.11  Q          |          |          |          |
1+35       0.0134      0.11  Q          |          |          |          |
1+40       0.0141      0.11  Q          |          |          |          |
1+45       0.0149      0.11  Q          |          |          |          |
1+50       0.0157      0.12  Q          |          |          |          |
1+55       0.0166      0.14  Q          |          |          |          |
2+ 0       0.0176      0.14  Q          |          |          |          |
2+ 5       0.0186      0.14  Q          |          |          |          |
2+10       0.0196      0.14  QV         |          |          |          |
2+15       0.0206      0.14  QV         |          |          |          |
2+20       0.0216      0.14  QV         |          |          |          |
2+25       0.0226      0.14  QV         |          |          |          |
2+30       0.0236      0.14  QV         |          |          |          |
2+35       0.0246      0.16  QV         |          |          |          |
2+40       0.0258      0.17  QV         |          |          |          |
2+45       0.0270      0.18  QV         |          |          |          |
2+50       0.0283      0.18  QV         |          |          |          |
2+55       0.0295      0.18  QV         |          |          |          |
3+ 0       0.0307      0.18  QV         |          |          |          |
3+ 5       0.0320      0.18  QV         |          |          |          |
3+10       0.0332      0.18  QV         |          |          |          |
3+15       0.0345      0.18  QV         |          |          |          |
3+20       0.0357      0.18  QV         |          |          |          |
3+25       0.0370      0.18  QV         |          |          |          |
3+30       0.0382      0.18  Q V        |          |          |          |
3+35       0.0394      0.18  Q V        |          |          |          |
3+40       0.0407      0.18  Q V        |          |          |          |
3+45       0.0419      0.18  Q V        |          |          |          |
3+50       0.0432      0.19  Q V        |          |          |          |
3+55       0.0447      0.21  Q V        |          |          |          |
4+ 0       0.0462      0.21  Q V        |          |          |          |
4+ 5       0.0476      0.21  Q V        |          |          |          |
4+10       0.0491      0.22  Q V        |          |          |          |
4+15       0.0506      0.22  Q V        |          |          |          |
4+20       0.0522      0.23  Q V        |          |          |          |
4+25       0.0539      0.24  Q V        |          |          |          |
4+30       0.0556      0.25  Q V        |          |          |          |
4+35       0.0573      0.25  |Q V        |          |          |          |
4+40       0.0590      0.25  |Q V        |          |          |          |
4+45       0.0608      0.25  |Q V        |          |          |          |
4+50       0.0626      0.26  |Q V        |          |          |          |
4+55       0.0645      0.28  |Q V        |          |          |          |
5+ 0       0.0665      0.29  |Q V        |          |          |          |
5+ 5       0.0683      0.26  |Q V        |          |          |          |
5+10       0.0699      0.23  Q  V        |          |          |          |
5+15       0.0714      0.22  Q  V        |          |          |          |
5+20       0.0730      0.23  Q  V        |          |          |          |
5+25       0.0747      0.25  Q   V       |          |          |          |
5+30       0.0764      0.25  Q   V       |          |          |          |
5+35       0.0782      0.26  |Q  V       |          |          |          |
5+40       0.0802      0.28  |Q  V       |          |          |          |
5+45       0.0821      0.29  |Q  V       |          |          |          |
5+50       0.0841      0.29  |Q  V       |          |          |          |
5+55       0.0861      0.29  |Q  V       |          |          |          |
6+ 0       0.0881      0.29  |Q  V       |          |          |          |
6+ 5       0.0902      0.30  |Q  V       |          |          |          |
6+10       0.0923      0.32  |Q  V       |          |          |          |
6+15       0.0945      0.32  |Q   V      |          |          |          |
6+20       0.0968      0.32  |Q   V      |          |          |          |
6+25       0.0990      0.32  |Q   V      |          |          |          |
6+30       0.1012      0.32  |Q   V      |          |          |          |
6+35       0.1036      0.34  |Q   V      |          |          |          |
6+40       0.1060      0.35  |Q   V      |          |          |          |
6+45       0.1084      0.36  |Q   V      |          |          |          |
6+50       0.1109      0.36  |Q   V      |          |          |          |
6+55       0.1134      0.36  |Q    V     |          |          |          |
7+ 0       0.1159      0.36  |Q    V     |          |          |          |
7+ 5       0.1184      0.36  |Q    V     |          |          |          |
7+10       0.1208      0.36  |Q    V     |          |          |          |
7+15       0.1233      0.36  |Q    V     |          |          |          |
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 7+20       0.1259      0.37  |Q    V   |          |          |          |
 7+25       0.1286      0.39  |Q    V   |          |          |          |
 7+30       0.1313      0.39  |Q     V  |          |          |          |
 7+35       0.1341      0.41  |Q     V  |          |          |          |
 7+40       0.1370      0.42  |Q     V  |          |          |          |
 7+45       0.1400      0.43  |Q     V  |          |          |          |
 7+50       0.1430      0.44  |Q     V  |          |          |          |
 7+55       0.1462      0.46  |Q     V  |          |          |          |
 8+ 0       0.1494      0.47  |Q      V |          |          |          |
 8+ 5       0.1528      0.49  |Q      V |          |          |          |
 8+10       0.1564      0.53  | Q     V |          |          |          |
 8+15       0.1601      0.53  | Q     V |          |          |          |
 8+20       0.1638      0.54  | Q     V |          |          |          |
 8+25       0.1675      0.54  | Q     V |          |          |          |
 8+30       0.1712      0.54  | Q      V|          |          |          |
 8+35       0.1750      0.55  | Q      V|          |          |          |
 8+40       0.1789      0.57  | Q      V|          |          |          |
 8+45       0.1829      0.57  | Q      V|          |          |          |
 8+50       0.1869      0.59  | Q       V          |          |          |
 8+55       0.1911      0.60  | Q       V          |          |          |
 9+ 0       0.1953      0.61  | Q       V          |          |          |
 9+ 5       0.1997      0.63  | Q       V          |          |          |
 9+10       0.2043      0.67  | Q       V          |          |          |
 9+15       0.2090      0.68  | Q       |V         |          |          |
 9+20       0.2137      0.69  | Q       |V         |          |          |
 9+25       0.2186      0.71  | Q       |V         |          |          |
 9+30       0.2236      0.72  | Q       | V        |          |          |
 9+35       0.2286      0.73  | Q       | V        |          |          |
 9+40       0.2338      0.75  | Q       | V        |          |          |
 9+45       0.2390      0.75  |  Q      | V        |          |          |
 9+50       0.2443      0.77  |  Q      |  V       |          |          |
 9+55       0.2497      0.79  |  Q      |  V       |          |          |
10+ 0       0.2551      0.79  |  Q      |  V       |          |          |
10+ 5       0.2600      0.71  | Q       |  V       |          |          |
10+10       0.2641      0.59  | Q       |   V      |          |          |
10+15       0.2680      0.56  | Q       |   V      |          |          |
10+20       0.2718      0.55  | Q       |   V      |          |          |
10+25       0.2755      0.54  | Q       |   V      |          |          |
10+30       0.2792      0.54  | Q       |   V      |          |          |
10+35       0.2834      0.60  | Q       |    V     |          |          |
10+40       0.2881      0.68  | Q       |    V     |          |          |
10+45       0.2929      0.70  | Q       |    V     |          |          |
10+50       0.2978      0.71  | Q       |    V     |          |          |
10+55       0.3028      0.72  | Q       |     V    |          |          |
11+ 0       0.3078      0.72  | Q       |     V    |          |          |
11+ 5       0.3126      0.71  | Q       |     V    |          |          |
11+10       0.3174      0.69  | Q       |      V   |          |          |
11+15       0.3222      0.69  | Q       |      V   |          |          |
11+20       0.3269      0.69  | Q       |      V   |          |          |
11+25       0.3316      0.69  | Q       |      V   |          |          |
11+30       0.3363      0.69  | Q       |       V  |          |          |
11+35       0.3409      0.66  | Q       |       V  |          |          |
11+40       0.3452      0.63  | Q       |       V  |          |          |
11+45       0.3495      0.62  | Q       |       V  |          |          |
11+50       0.3538      0.63  | Q       |       V  |          |          |
11+55       0.3582      0.64  | Q       |        V |          |          |
12+ 0       0.3627      0.65  | Q       |        V |          |          |
12+ 5       0.3677      0.73  | Q       |        V |          |          |
12+10       0.3735      0.85  |  Q      |         V|          |          |
12+15       0.3796      0.88  |  Q      |         V|          |          |
12+20       0.3858      0.90  |  Q      |         V|          |          |
12+25       0.3922      0.93  |  Q      |          |V         |          |
12+30       0.3986      0.93  |  Q      |          |V         |          |
12+35       0.4052      0.96  |  Q      |          |V         |          |
12+40       0.4121      0.99  |  Q      |          | V        |          |
12+45       0.4190      1.00  |   Q     |          | V        |          |
12+50       0.4260      1.02  |   Q     |          | V        |          |
12+55       0.4331      1.04  |   Q     |          |  V       |          |
13+ 0       0.4403      1.04  |   Q     |          |  V       |          |
13+ 5       0.4479      1.10  |   Q     |          |   V      |          |
13+10       0.4561      1.19  |   Q     |          |   V      |          |
13+15       0.4644      1.21  |   Q     |          |   V      |          |
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13+20       0.4728      1.22  |   Q     |          |    V    |          |
13+25       0.4812      1.22  |   Q     |          |    V    |          |
13+30       0.4897      1.23  |   Q     |          |     V   |          |
13+35       0.4972      1.10  |   Q     |          |     V   |          |
13+40       0.5035      0.91  |  Q      |          |      V  |          |
13+45       0.5095      0.87  |  Q      |          |      V  |          |
13+50       0.5153      0.85  |  Q      |          |      V  |          |
13+55       0.5210      0.84  |  Q      |          |      V  |          |
14+ 0       0.5268      0.83  |  Q      |          |       V |          |
14+ 5       0.5328      0.88  |  Q      |          |       V |          |
14+10       0.5393      0.94  |  Q      |          |       V |          |
14+15       0.5459      0.96  |  Q      |          |        V|          |
14+20       0.5525      0.96  |  Q      |          |        V|          |
14+25       0.5590      0.94  |  Q      |          |         V          |
14+30       0.5655      0.94  |  Q      |          |         V          |
14+35       0.5719      0.94  |  Q      |          |         V          |
14+40       0.5784      0.94  |  Q      |          |         |V         |
14+45       0.5848      0.94  |  Q      |          |         |V         |
14+50       0.5912      0.93  |  Q      |          |         |V         |
14+55       0.5975      0.91  |  Q      |          |         | V        |
15+ 0       0.6037      0.90  |  Q      |          |         | V        |
15+ 5       0.6098      0.89  |  Q      |          |         | V        |
15+10       0.6159      0.87  |  Q      |          |         |  V       |
15+15       0.6218      0.87  |  Q      |          |         |  V       |
15+20       0.6277      0.86  |  Q      |          |         |  V       |
15+25       0.6335      0.84  |  Q      |          |         |   V      |
15+30       0.6392      0.83  |  Q      |          |         |   V      |
15+35       0.6446      0.78  |  Q      |          |         |   V      |
15+40       0.6496      0.72  | Q       |          |         |   V      |
15+45       0.6544      0.70  | Q       |          |         |    V     |
15+50       0.6591      0.69  | Q       |          |         |    V     |
15+55       0.6639      0.69  | Q       |          |         |    V     |
16+ 0       0.6686      0.69  | Q       |          |         |    V     |
16+ 5       0.6721      0.51  | Q       |          |         |     V    |
16+10       0.6739      0.26  |Q        |          |         |     V    |
16+15       0.6752      0.19  Q         |          |         |     V    |
16+20       0.6764      0.17  Q         |          |         |     V    |
16+25       0.6774      0.15  Q         |          |         |     V    |
16+30       0.6784      0.14  Q         |          |         |     V    |
16+35       0.6793      0.13  Q         |          |         |     V    |
16+40       0.6801      0.12  Q         |          |         |     V    |
16+45       0.6809      0.11  Q         |          |         |     V    |
16+50       0.6816      0.11  Q         |          |         |     V    |
16+55       0.6824      0.11  Q         |          |         |     V    |
17+ 0       0.6831      0.11  Q         |          |         |     V    |
17+ 5       0.6840      0.13  Q         |          |         |     V    |
17+10       0.6852      0.17  Q         |          |         |     V    |
17+15       0.6864      0.17  Q         |          |         |     V    |
17+20       0.6876      0.18  Q         |          |         |     V    |
17+25       0.6888      0.18  Q         |          |         |     V    |
17+30       0.6901      0.18  Q         |          |         |      V   |
17+35       0.6913      0.18  Q         |          |         |      V   |
17+40       0.6926      0.18  Q         |          |         |      V   |
17+45       0.6938      0.18  Q         |          |         |      V   |
17+50       0.6950      0.17  Q         |          |         |      V   |
17+55       0.6960      0.15  Q         |          |         |      V   |
18+ 0       0.6970      0.15  Q         |          |         |      V   |
18+ 5       0.6980      0.15  Q         |          |         |      V   |
18+10       0.6990      0.14  Q         |          |         |      V   |
18+15       0.7000      0.14  Q         |          |         |      V   |
18+20       0.7010      0.14  Q         |          |         |      V   |
18+25       0.7020      0.14  Q         |          |         |      V   |
18+30       0.7030      0.14  Q         |          |         |      V   |
18+35       0.7039      0.13  Q         |          |         |      V   |
18+40       0.7047      0.12  Q         |          |         |      V   |
18+45       0.7055      0.11  Q         |          |         |      V   |
18+50       0.7062      0.10  Q         |          |         |      V   |
18+55       0.7067      0.08  Q         |          |         |      V   |
19+ 0       0.7072      0.08  Q         |          |         |      V   |
19+ 5       0.7078      0.09  Q         |          |         |       V  |
19+10       0.7085      0.10  Q         |          |         |       V  |
19+15       0.7092      0.10  Q         |          |         |       V  |
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  19+20       0.7100      0.12  Q          |           |           |        V |
  19+25       0.7110      0.14  Q          |           |           |        V |
  19+30       0.7120      0.14  Q          |           |           |        V |
  19+35       0.7129      0.13  Q          |           |           |        V |
  19+40       0.7136      0.12  Q          |           |           |        V |
  19+45       0.7144      0.11  Q          |           |           |        V |
  19+50       0.7151      0.10  Q          |           |           |        V |
  19+55       0.7156      0.08  Q          |           |           |        V |
  20+ 0       0.7162      0.08  Q          |           |           |        V |
  20+ 5       0.7167      0.09  Q          |           |           |        V |
  20+10       0.7174      0.10  Q          |           |           |        V |
  20+15       0.7182      0.10  Q          |           |           |        V |
  20+20       0.7189      0.11  Q          |           |           |        V |
  20+25       0.7196      0.11  Q          |           |           |        V |
  20+30       0.7204      0.11  Q          |           |           |        V |
  20+35       0.7211      0.11  Q          |           |           |        V |
  20+40       0.7219      0.11  Q          |           |           |        V |
  20+45       0.7226      0.11  Q          |           |           |        V |
  20+50       0.7233      0.10  Q          |           |           |        V |
  20+55       0.7238      0.08  Q          |           |           |        V |
  21+ 0       0.7244      0.08  Q          |           |           |        V |
  21+ 5       0.7249      0.09  Q          |           |           |        V |
  21+10       0.7256      0.10  Q          |           |           |        V |
  21+15       0.7264      0.10  Q          |           |           |        V |
  21+20       0.7270      0.10  Q          |           |           |         V|
  21+25       0.7276      0.08  Q          |           |           |         V|
  21+30       0.7281      0.08  Q          |           |           |         V|
  21+35       0.7287      0.09  Q          |           |           |         V|
  21+40       0.7294      0.10  Q          |           |           |         V|
  21+45       0.7301      0.10  Q          |           |           |         V|
  21+50       0.7307      0.10  Q          |           |           |         V|
  21+55       0.7313      0.08  Q          |           |           |         V|
  22+ 0       0.7318      0.08  Q          |           |           |         V|
  22+ 5       0.7324      0.09  Q          |           |           |         V|
  22+10       0.7331      0.10  Q          |           |           |         V|
  22+15       0.7338      0.10  Q          |           |           |         V|
  22+20       0.7345      0.10  Q          |           |           |         V|
  22+25       0.7350      0.08  Q          |           |           |         V|
  22+30       0.7355      0.08  Q          |           |           |         V|
  22+35       0.7360      0.07  Q          |           |           |         V|
  22+40       0.7365      0.07  Q          |           |           |         V|
  22+45       0.7370      0.07  Q          |           |           |         V|
  22+50       0.7375      0.07  Q          |           |           |         V|
  22+55       0.7380      0.07  Q          |           |           |         V|
  23+ 0       0.7385      0.07  Q          |           |           |         V|
  23+ 5       0.7390      0.07  Q          |           |           |         V|
  23+10       0.7395      0.07  Q          |           |           |         V|
  23+15       0.7400      0.07  Q          |           |           |         V|
  23+20       0.7405      0.07  Q          |           |           |         V|
  23+25       0.7410      0.07  Q          |           |           |         V|
  23+30       0.7415      0.07  Q          |           |           |         V|
  23+35       0.7420      0.07  Q          |           |           |         V|
  23+40       0.7425      0.07  Q          |           |           |         V|
  23+45       0.7430      0.07  Q          |           |           |         V|
  23+50       0.7435      0.07  Q          |           |           |         V|
  23+55       0.7440      0.07  Q          |           |           |         V|
  24+ 0       0.7445      0.07  Q          |           |           |         V|
  24+ 5       0.7448      0.05  Q          |           |           |         V|
  24+10       0.7449      0.01  Q          |           |           |         V|
  24+15       0.7450      0.01  Q          |           |           |         V|
  24+20       0.7450      0.00  Q          |           |           |         V|
  24+25       0.7450      0.00  Q          |           |           |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E00565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	1.20	14.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	3.00	35.40

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.622(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.622(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.097	(0.412)	0.073	0.024
2	0.17	0.60	0.117	(0.412)	0.088	0.029
3	0.25	0.60	0.117	(0.412)	0.088	0.029
4	0.33	0.60	0.117	(0.412)	0.088	0.029
5	0.42	0.60	0.117	(0.412)	0.088	0.029
6	0.50	0.70	0.136	(0.412)	0.102	0.034
7	0.58	0.70	0.136	(0.412)	0.102	0.034
8	0.67	0.70	0.136	(0.412)	0.102	0.034
9	0.75	0.70	0.136	(0.412)	0.102	0.034
10	0.83	0.70	0.136	(0.412)	0.102	0.034
11	0.92	0.70	0.136	(0.412)	0.102	0.034
12	1.00	0.80	0.156	(0.412)	0.117	0.039
13	1.08	0.80	0.156	(0.412)	0.117	0.039
14	1.17	0.80	0.156	(0.412)	0.117	0.039
15	1.25	0.80	0.156	(0.412)	0.117	0.039
16	1.33	0.80	0.156	(0.412)	0.117	0.039
17	1.42	0.80	0.156	(0.412)	0.117	0.039
18	1.50	0.80	0.156	(0.412)	0.117	0.039
19	1.58	0.80	0.156	(0.412)	0.117	0.039
20	1.67	0.80	0.156	(0.412)	0.117	0.039
21	1.75	0.80	0.156	(0.412)	0.117	0.039
22	1.83	0.80	0.156	(0.412)	0.117	0.039
23	1.92	0.80	0.156	(0.412)	0.117	0.039
24	2.00	0.90	0.175	(0.412)	0.131	0.044
25	2.08	0.80	0.156	(0.412)	0.117	0.039
26	2.17	0.90	0.175	(0.412)	0.131	0.044
27	2.25	0.90	0.175	(0.412)	0.131	0.044
28	2.33	0.90	0.175	(0.412)	0.131	0.044
29	2.42	0.90	0.175	(0.412)	0.131	0.044
30	2.50	0.90	0.175	(0.412)	0.131	0.044
31	2.58	0.90	0.175	(0.412)	0.131	0.044
32	2.67	0.90	0.175	(0.412)	0.131	0.044
33	2.75	1.00	0.195	(0.412)	0.146	0.049
34	2.83	1.00	0.195	(0.412)	0.146	0.049
35	2.92	1.00	0.195	(0.412)	0.146	0.049
36	3.00	1.00	0.195	(0.412)	0.146	0.049

37	3.08	1.00	0.195	(	0.412)	0.146	0.049
38	3.17	1.10	0.214	(	0.412)	0.161	0.054
39	3.25	1.10	0.214	(	0.412)	0.161	0.054
40	3.33	1.10	0.214	(	0.412)	0.161	0.054
41	3.42	1.20	0.234	(	0.412)	0.175	0.058
42	3.50	1.30	0.253	(	0.412)	0.190	0.063
43	3.58	1.40	0.272	(	0.412)	0.204	0.068
44	3.67	1.40	0.272	(	0.412)	0.204	0.068
45	3.75	1.50	0.292	(	0.412)	0.219	0.073
46	3.83	1.50	0.292	(	0.412)	0.219	0.073
47	3.92	1.60	0.311	(	0.412)	0.234	0.078
48	4.00	1.60	0.311	(	0.412)	0.234	0.078
49	4.08	1.70	0.331	(	0.412)	0.248	0.083
50	4.17	1.80	0.350	(	0.412)	0.263	0.088
51	4.25	1.90	0.370	(	0.412)	0.277	0.092
52	4.33	2.00	0.389	(	0.412)	0.292	0.097
53	4.42	2.10	0.409	(	0.412)	0.306	0.102
54	4.50	2.10	0.409	(	0.412)	0.306	0.102
55	4.58	2.20	0.428	(	0.412)	0.321	0.107
56	4.67	2.30	0.448	(	0.412)	0.336	0.112
57	4.75	2.40	0.467	(	0.412)	0.350	0.117
58	4.83	2.40	0.467	(	0.412)	0.350	0.117
59	4.92	2.50	0.486	(	0.412)	0.365	0.122
60	5.00	2.60	0.506	(	0.412)	0.379	0.126
61	5.08	3.10	0.603		0.412	(0.452)	0.191
62	5.17	3.60	0.701		0.412	(0.525)	0.288
63	5.25	3.90	0.759		0.412	(0.569)	0.347
64	5.33	4.20	0.817		0.412	(0.613)	0.405
65	5.42	4.70	0.915		0.412	(0.686)	0.502
66	5.50	5.60	1.090		0.412	(0.817)	0.678
67	5.58	1.90	0.370	(	0.412)	0.277	0.092
68	5.67	0.90	0.175	(	0.412)	0.131	0.044
69	5.75	0.60	0.117	(	0.412)	0.088	0.029
70	5.83	0.50	0.097	(	0.412)	0.073	0.024
71	5.92	0.30	0.058	(	0.412)	0.044	0.015
72	6.00	0.20	0.039	(	0.412)	0.029	0.010

(Loss Rate Not Used)

Sum = 100.0 Sum = 6.1

Flood volume = Effective rainfall 0.50(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 1.12(In)
Total soil loss = 1.098(Ac.Ft)
Total rainfall = 1.62(In)
Flood volume = 21613.3 Cubic Feet
Total soil loss = 47843.7 Cubic Feet

Peak flow rate of this hydrograph = 6.294(CFS)

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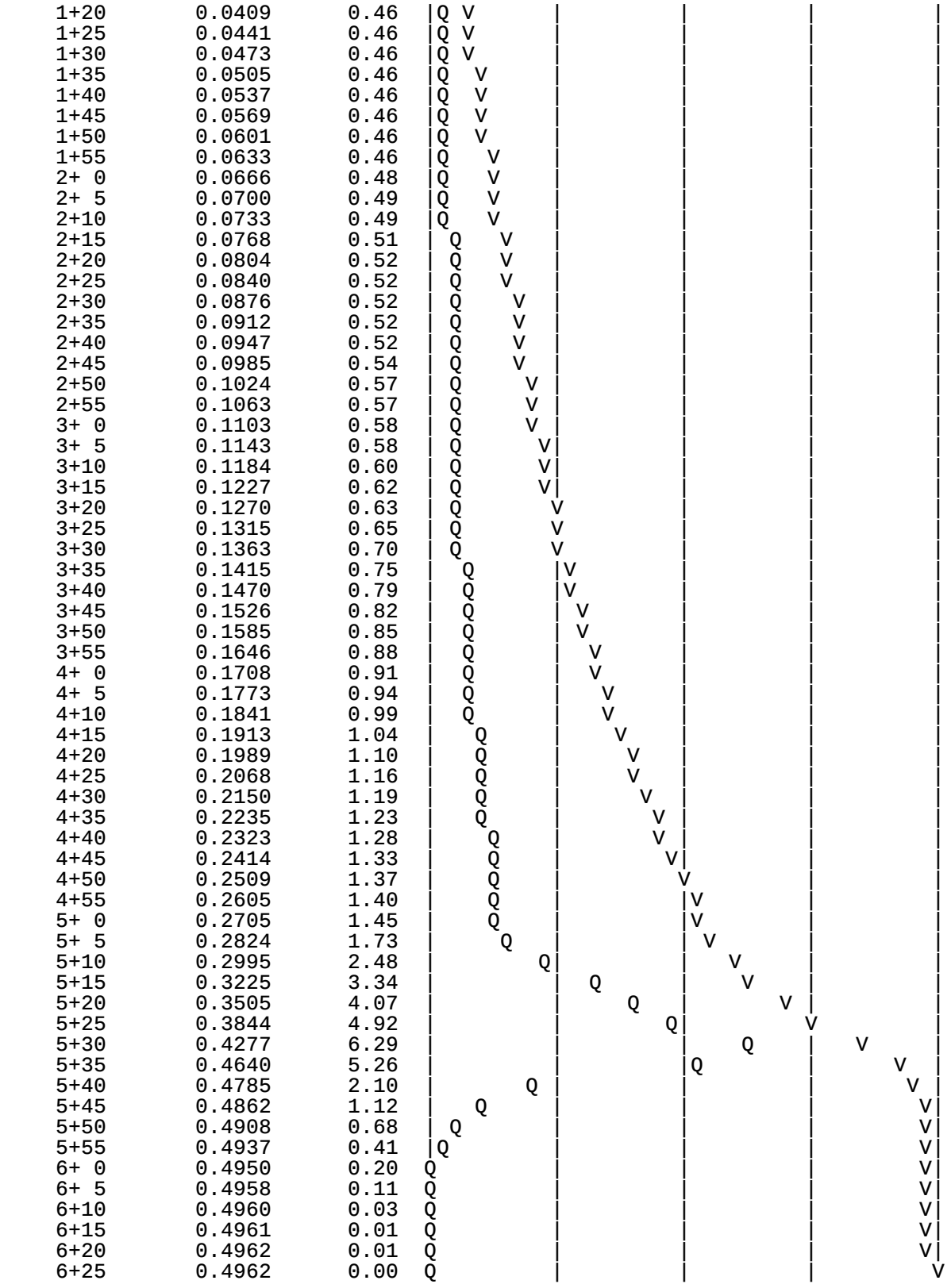
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0006	0.09	Q				
0+10	0.0023	0.25	Q				
0+15	0.0045	0.31	VQ				
0+20	0.0067	0.33	VQ				
0+25	0.0091	0.34	VQ				
0+30	0.0116	0.36	VQ				
0+35	0.0143	0.39	|Q				
0+40	0.0171	0.40	|Q				
0+45	0.0198	0.40	|Q				
0+50	0.0226	0.40	|Q				
0+55	0.0254	0.41	|QV				
1+ 0	0.0283	0.42	|QV				
1+ 5	0.0314	0.45	|QV				
1+10	0.0346	0.46	|QV				
1+15	0.0378	0.46	|Q V				


1+20 0.0409 0.46
1+25 0.0441 0.46
1+30 0.0473 0.46
1+35 0.0505 0.46
1+40 0.0537 0.46
1+45 0.0569 0.46
1+50 0.0601 0.46
1+55 0.0633 0.46
2+ 0 0.0666 0.48
2+ 5 0.0700 0.49
2+10 0.0733 0.49
2+15 0.0768 0.51
2+20 0.0804 0.52
2+25 0.0840 0.52
2+30 0.0876 0.52
2+35 0.0912 0.52
2+40 0.0947 0.52
2+45 0.0985 0.54
2+50 0.1024 0.57
2+55 0.1063 0.57
3+ 0 0.1103 0.58
3+ 5 0.1143 0.58
3+10 0.1184 0.60
3+15 0.1227 0.62
3+20 0.1270 0.63
3+25 0.1315 0.65
3+30 0.1363 0.70
3+35 0.1415 0.75
3+40 0.1470 0.79
3+45 0.1526 0.82
3+50 0.1585 0.85
3+55 0.1646 0.88
4+ 0 0.1708 0.91
4+ 5 0.1773 0.94
4+10 0.1841 0.99
4+15 0.1913 1.04
4+20 0.1989 1.10
4+25 0.2068 1.16
4+30 0.2150 1.19
4+35 0.2235 1.23
4+40 0.2323 1.28
4+45 0.2414 1.33
4+50 0.2509 1.37
4+55 0.2605 1.40
5+ 0 0.2705 1.45
5+ 5 0.2824 1.73
5+10 0.2995 2.48
5+15 0.3225 3.34
5+20 0.3505 4.07
5+25 0.3844 4.92
5+30 0.4277 6.29
5+35 0.4640 5.26
5+40 0.4785 2.10
5+45 0.4862 1.12
5+50 0.4908 0.68
5+55 0.4937 0.41
6+ 0 0.4950 0.20
6+ 5 0.4958 0.11
6+10 0.4960 0.03
6+15 0.4961 0.01
6+20 0.4962 0.01
6+25 0.4962 0.00

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E00535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	0.90	10.62

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	2.35	27.73

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.240(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.240(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.193	(0.412)	0.145	0.048
2	0.17	1.30	0.193	(0.412)	0.145	0.048
3	0.25	1.10	0.164	(0.412)	0.123	0.041
4	0.33	1.50	0.223	(0.412)	0.167	0.056
5	0.42	1.50	0.223	(0.412)	0.167	0.056
6	0.50	1.80	0.268	(0.412)	0.201	0.067
7	0.58	1.50	0.223	(0.412)	0.167	0.056
8	0.67	1.80	0.268	(0.412)	0.201	0.067
9	0.75	1.80	0.268	(0.412)	0.201	0.067
10	0.83	1.50	0.223	(0.412)	0.167	0.056
11	0.92	1.60	0.238	(0.412)	0.178	0.059
12	1.00	1.80	0.268	(0.412)	0.201	0.067
13	1.08	2.20	0.327	(0.412)	0.245	0.082
14	1.17	2.20	0.327	(0.412)	0.245	0.082
15	1.25	2.20	0.327	(0.412)	0.245	0.082
16	1.33	2.00	0.297	(0.412)	0.223	0.074
17	1.42	2.60	0.387	(0.412)	0.290	0.097
18	1.50	2.70	0.402	(0.412)	0.301	0.100
19	1.58	2.40	0.357	(0.412)	0.268	0.089
20	1.67	2.70	0.402	(0.412)	0.301	0.100
21	1.75	3.30	0.491	(0.412)	0.368	0.123
22	1.83	3.10	0.461	(0.412)	0.346	0.115
23	1.92	2.90	0.431	(0.412)	0.324	0.108
24	2.00	3.00	0.446	(0.412)	0.335	0.112
25	2.08	3.10	0.461	(0.412)	0.346	0.115
26	2.17	4.20	0.625	0.412	(0.469)	0.213
27	2.25	5.00	0.744	0.412	(0.558)	0.332
28	2.33	3.50	0.521	(0.412)	0.390	0.130
29	2.42	6.80	1.011	0.412	(0.759)	0.599
30	2.50	7.30	1.086	0.412	(0.814)	0.674
31	2.58	8.20	1.220	0.412	(0.915)	0.808
32	2.67	5.90	0.878	0.412	(0.658)	0.465
33	2.75	2.00	0.297	(0.412)	0.223	0.074
34	2.83	1.80	0.268	(0.412)	0.201	0.067
35	2.92	1.80	0.268	(0.412)	0.201	0.067
36	3.00	0.60	0.089	(0.412)	0.067	0.022

(Loss Rate Not Used)
Sum = 100.0 Sum = 5.4
Flood volume = Effective rainfall 0.45(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.79(In)
Total soil loss = 0.775(Ac.Ft)
Total rainfall = 1.24(In)
Flood volume = 19340.9 Cubic Feet
Total soil loss = 33754.5 Cubic Feet

Peak flow rate of this hydrograph = 7.907(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0013	0.18	Q
0+10	0.0044	0.46	VQ
0+15	0.0078	0.49	VQ
0+20	0.0115	0.54	|VQ
0+25	0.0158	0.63	|VQ
0+30	0.0206	0.69	|VQ
0+35	0.0256	0.72	| Q
0+40	0.0305	0.72	| Q
0+45	0.0359	0.78	| Q
0+50	0.0410	0.75	| QV
0+55	0.0458	0.70	| Q V
1+ 0	0.0509	0.74	| Q V
1+ 5	0.0567	0.84	| Q V
1+10	0.0631	0.93	| Q V
1+15	0.0696	0.95	| Q V
1+20	0.0761	0.94	| Q V
1+25	0.0829	0.99	| Q V
1+30	0.0906	1.12	| Q V
1+35	0.0983	1.12	| Q V
1+40	0.1060	1.12	| Q V
1+45	0.1146	1.26	| Q V
1+50	0.1241	1.37	| Q |V
1+55	0.1333	1.33	| Q | V
2+ 0	0.1423	1.31	| Q | V
2+ 5	0.1515	1.34	| Q | V
2+10	0.1635	1.73	| Q | V
2+15	0.1823	2.74	| Q V
2+20	0.2015	2.78	| |Q V
2+25	0.2266	3.65	| Q V
2+30	0.2707	6.40	| VQ
2+35	0.3252	7.91	| V|Q
2+40	0.3782	7.70	| Q V
2+45	0.4100	4.62	| Q V
2+50	0.4246	2.11	| Q V
2+55	0.4341	1.39	| Q V
3+ 0	0.4403	0.89	| Q V
3+ 5	0.4428	0.37	|Q V
3+10	0.4435	0.11	Q V
3+15	0.4438	0.05	Q V
3+20	0.4440	0.02	Q V
3+25	0.4440	0.00	Q V

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E00515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	0.54	6.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	1.36	16.05

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.732(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.732(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	0.215	0.029
76.0	58.2	0.488	0.000	0.488	0.785	0.383
					Sum (F) =	0.412

Area averaged mean soil loss (F) (In/Hr) = 0.412
Minimum soil loss rate ((In/Hr)) = 0.206
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
		Sum =	100.000 Sum=	11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.386	(0.412)	0.290	0.097
2	0.17	4.50	0.395	(0.412)	0.296	0.099
3	0.25	5.40	0.474	(0.412)	0.356	0.119
4	0.33	5.40	0.474	(0.412)	0.356	0.119
5	0.42	5.70	0.501	(0.412)	0.376	0.125
6	0.50	6.40	0.562	0.412	(0.422)	0.150
7	0.58	7.90	0.694	0.412	(0.520)	0.282
8	0.67	9.10	0.799	0.412	(0.599)	0.387
9	0.75	12.80	1.124	0.412	(0.843)	0.712
10	0.83	25.60	2.249	0.412	(1.686)	1.837
11	0.92	7.90	0.694	0.412	(0.520)	0.282
12	1.00	4.90	0.430	(0.412)	0.323	0.108
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	4.3

Flood volume = Effective rainfall 0.36(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.37(In)
Total soil loss = 0.366(Ac.Ft)
Total rainfall = 0.73(In)
Flood volume = 15402.5 Cubic Feet
Total soil loss = 15951.4 Cubic Feet

Peak flow rate of this hydrograph = 12.741(CFS)

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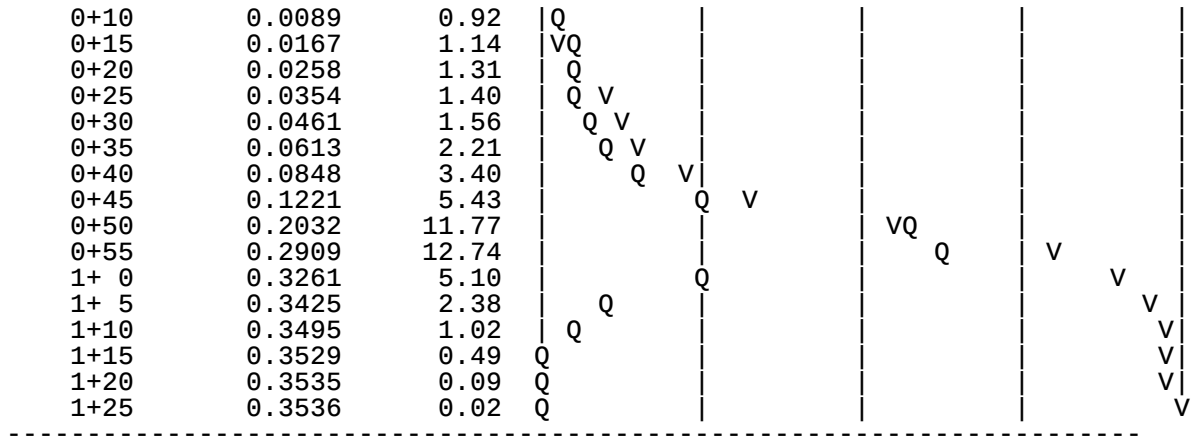
1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0025	0.37	Q	|	|	|	|


0+10 0.0089 0.92
0+15 0.0167 1.14
0+20 0.0258 1.31
0+25 0.0354 1.40
0+30 0.0461 1.56
0+35 0.0613 2.21
0+40 0.0848 3.40
0+45 0.1221 5.43
0+50 0.2032 11.77
0+55 0.2909 12.74
1+ 0 0.3261 5.10
1+ 5 0.3425 2.38
1+10 0.3495 1.02
1+15 0.3529 0.49
1+20 0.3535 0.09
1+25 0.3536 0.02

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E0102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	2.00	23.60

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	6.40	75.52

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.810(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.810(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	0.215	0.021
76.0	76.0	0.291	0.000	0.291	0.785	0.229
					Sum (F) =	0.249

Area averaged mean soil loss (F) (In/Hr) = 0.249
Minimum soil loss rate ((In/Hr)) = 0.125
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.030	(0.442)	0.023	0.008
2	0.17	0.07	0.030	(0.440)	0.023	0.008
3	0.25	0.07	0.030	(0.439)	0.023	0.008
4	0.33	0.10	0.046	(0.437)	0.034	0.011
5	0.42	0.10	0.046	(0.435)	0.034	0.011
6	0.50	0.10	0.046	(0.434)	0.034	0.011
7	0.58	0.10	0.046	(0.432)	0.034	0.011
8	0.67	0.10	0.046	(0.430)	0.034	0.011
9	0.75	0.10	0.046	(0.429)	0.034	0.011
10	0.83	0.13	0.061	(0.427)	0.046	0.015
11	0.92	0.13	0.061	(0.425)	0.046	0.015
12	1.00	0.13	0.061	(0.424)	0.046	0.015
13	1.08	0.10	0.046	(0.422)	0.034	0.011
14	1.17	0.10	0.046	(0.420)	0.034	0.011
15	1.25	0.10	0.046	(0.418)	0.034	0.011
16	1.33	0.10	0.046	(0.417)	0.034	0.011
17	1.42	0.10	0.046	(0.415)	0.034	0.011
18	1.50	0.10	0.046	(0.414)	0.034	0.011
19	1.58	0.10	0.046	(0.412)	0.034	0.011
20	1.67	0.10	0.046	(0.410)	0.034	0.011
21	1.75	0.10	0.046	(0.409)	0.034	0.011
22	1.83	0.13	0.061	(0.407)	0.046	0.015
23	1.92	0.13	0.061	(0.405)	0.046	0.015
24	2.00	0.13	0.061	(0.404)	0.046	0.015
25	2.08	0.13	0.061	(0.402)	0.046	0.015
26	2.17	0.13	0.061	(0.400)	0.046	0.015
27	2.25	0.13	0.061	(0.399)	0.046	0.015
28	2.33	0.13	0.061	(0.397)	0.046	0.015
29	2.42	0.13	0.061	(0.396)	0.046	0.015
30	2.50	0.13	0.061	(0.394)	0.046	0.015
31	2.58	0.17	0.076	(0.392)	0.057	0.019
32	2.67	0.17	0.076	(0.391)	0.057	0.019
33	2.75	0.17	0.076	(0.389)	0.057	0.019
34	2.83	0.17	0.076	(0.387)	0.057	0.019
35	2.92	0.17	0.076	(0.386)	0.057	0.019
36	3.00	0.17	0.076	(0.384)	0.057	0.019

37	3.08	0.17	0.076	(0.383)	0.057	0.019
38	3.17	0.17	0.076	(0.381)	0.057	0.019
39	3.25	0.17	0.076	(0.380)	0.057	0.019
40	3.33	0.17	0.076	(0.378)	0.057	0.019
41	3.42	0.17	0.076	(0.376)	0.057	0.019
42	3.50	0.17	0.076	(0.375)	0.057	0.019
43	3.58	0.17	0.076	(0.373)	0.057	0.019
44	3.67	0.17	0.076	(0.372)	0.057	0.019
45	3.75	0.17	0.076	(0.370)	0.057	0.019
46	3.83	0.20	0.091	(0.369)	0.069	0.023
47	3.92	0.20	0.091	(0.367)	0.069	0.023
48	4.00	0.20	0.091	(0.365)	0.069	0.023
49	4.08	0.20	0.091	(0.364)	0.069	0.023
50	4.17	0.20	0.091	(0.362)	0.069	0.023
51	4.25	0.20	0.091	(0.361)	0.069	0.023
52	4.33	0.23	0.107	(0.359)	0.080	0.027
53	4.42	0.23	0.107	(0.358)	0.080	0.027
54	4.50	0.23	0.107	(0.356)	0.080	0.027
55	4.58	0.23	0.107	(0.355)	0.080	0.027
56	4.67	0.23	0.107	(0.353)	0.080	0.027
57	4.75	0.23	0.107	(0.352)	0.080	0.027
58	4.83	0.27	0.122	(0.350)	0.091	0.030
59	4.92	0.27	0.122	(0.349)	0.091	0.030
60	5.00	0.27	0.122	(0.347)	0.091	0.030
61	5.08	0.20	0.091	(0.346)	0.069	0.023
62	5.17	0.20	0.091	(0.344)	0.069	0.023
63	5.25	0.20	0.091	(0.343)	0.069	0.023
64	5.33	0.23	0.107	(0.341)	0.080	0.027
65	5.42	0.23	0.107	(0.340)	0.080	0.027
66	5.50	0.23	0.107	(0.338)	0.080	0.027
67	5.58	0.27	0.122	(0.337)	0.091	0.030
68	5.67	0.27	0.122	(0.335)	0.091	0.030
69	5.75	0.27	0.122	(0.334)	0.091	0.030
70	5.83	0.27	0.122	(0.332)	0.091	0.030
71	5.92	0.27	0.122	(0.331)	0.091	0.030
72	6.00	0.27	0.122	(0.329)	0.091	0.030
73	6.08	0.30	0.137	(0.328)	0.103	0.034
74	6.17	0.30	0.137	(0.326)	0.103	0.034
75	6.25	0.30	0.137	(0.325)	0.103	0.034
76	6.33	0.30	0.137	(0.323)	0.103	0.034
77	6.42	0.30	0.137	(0.322)	0.103	0.034
78	6.50	0.30	0.137	(0.320)	0.103	0.034
79	6.58	0.33	0.152	(0.319)	0.114	0.038
80	6.67	0.33	0.152	(0.318)	0.114	0.038
81	6.75	0.33	0.152	(0.316)	0.114	0.038
82	6.83	0.33	0.152	(0.315)	0.114	0.038
83	6.92	0.33	0.152	(0.313)	0.114	0.038
84	7.00	0.33	0.152	(0.312)	0.114	0.038
85	7.08	0.33	0.152	(0.310)	0.114	0.038
86	7.17	0.33	0.152	(0.309)	0.114	0.038
87	7.25	0.33	0.152	(0.308)	0.114	0.038
88	7.33	0.37	0.168	(0.306)	0.126	0.042
89	7.42	0.37	0.168	(0.305)	0.126	0.042
90	7.50	0.37	0.168	(0.303)	0.126	0.042
91	7.58	0.40	0.183	(0.302)	0.137	0.046
92	7.67	0.40	0.183	(0.301)	0.137	0.046
93	7.75	0.40	0.183	(0.299)	0.137	0.046
94	7.83	0.43	0.198	(0.298)	0.149	0.050
95	7.92	0.43	0.198	(0.297)	0.149	0.050
96	8.00	0.43	0.198	(0.295)	0.149	0.050
97	8.08	0.50	0.229	(0.294)	0.171	0.057
98	8.17	0.50	0.229	(0.292)	0.171	0.057
99	8.25	0.50	0.229	(0.291)	0.171	0.057
100	8.33	0.50	0.229	(0.290)	0.171	0.057
101	8.42	0.50	0.229	(0.288)	0.171	0.057
102	8.50	0.50	0.229	(0.287)	0.171	0.057
103	8.58	0.53	0.244	(0.286)	0.183	0.061
104	8.67	0.53	0.244	(0.284)	0.183	0.061
105	8.75	0.53	0.244	(0.283)	0.183	0.061
106	8.83	0.57	0.259	(0.282)	0.194	0.065
107	8.92	0.57	0.259	(0.280)	0.194	0.065
108	9.00	0.57	0.259	(0.279)	0.194	0.065

109	9.08	0.63	0.290	(	0.278)	0.217		0.072
110	9.17	0.63	0.290	(	0.276)	0.217		0.072
111	9.25	0.63	0.290	(	0.275)	0.217		0.072
112	9.33	0.67	0.305	(	0.274)	0.229		0.076
113	9.42	0.67	0.305	(	0.272)	0.229		0.076
114	9.50	0.67	0.305	(	0.271)	0.229		0.076
115	9.58	0.70	0.320	(	0.270)	0.240		0.080
116	9.67	0.70	0.320	(	0.269)	0.240		0.080
117	9.75	0.70	0.320	(	0.267)	0.240		0.080
118	9.83	0.73	0.335	(	0.266)	0.251		0.084
119	9.92	0.73	0.335	(	0.265)	0.251		0.084
120	10.00	0.73	0.335	(	0.263)	0.251		0.084
121	10.08	0.50	0.229	(	0.262)	0.171		0.057
122	10.17	0.50	0.229	(	0.261)	0.171		0.057
123	10.25	0.50	0.229	(	0.260)	0.171		0.057
124	10.33	0.50	0.229	(	0.258)	0.171		0.057
125	10.42	0.50	0.229	(	0.257)	0.171		0.057
126	10.50	0.50	0.229	(	0.256)	0.171		0.057
127	10.58	0.67	0.305	(	0.255)	0.229		0.076
128	10.67	0.67	0.305	(	0.253)	0.229		0.076
129	10.75	0.67	0.305	(	0.252)	0.229		0.076
130	10.83	0.67	0.305	(	0.251)	0.229		0.076
131	10.92	0.67	0.305	(	0.250)	0.229		0.076
132	11.00	0.67	0.305	(	0.248)	0.229		0.076
133	11.08	0.63	0.290	(	0.247)	0.217		0.072
134	11.17	0.63	0.290	(	0.246)	0.217		0.072
135	11.25	0.63	0.290	(	0.245)	0.217		0.072
136	11.33	0.63	0.290	(	0.244)	0.217		0.072
137	11.42	0.63	0.290	(	0.242)	0.217		0.072
138	11.50	0.63	0.290	(	0.241)	0.217		0.072
139	11.58	0.57	0.259	(	0.240)	0.194		0.065
140	11.67	0.57	0.259	(	0.239)	0.194		0.065
141	11.75	0.57	0.259	(	0.238)	0.194		0.065
142	11.83	0.60	0.274	(	0.236)	0.206		0.069
143	11.92	0.60	0.274	(	0.235)	0.206		0.069
144	12.00	0.60	0.274	(	0.234)	0.206		0.069
145	12.08	0.83	0.381		0.233	(	0.286)	0.148
146	12.17	0.83	0.381		0.232	(	0.286)	0.149
147	12.25	0.83	0.381		0.230	(	0.286)	0.151
148	12.33	0.87	0.396		0.229	(	0.297)	0.167
149	12.42	0.87	0.396		0.228	(	0.297)	0.168
150	12.50	0.87	0.396		0.227	(	0.297)	0.169
151	12.58	0.93	0.427		0.226	(	0.320)	0.201
152	12.67	0.93	0.427		0.225	(	0.320)	0.202
153	12.75	0.93	0.427		0.224	(	0.320)	0.203
154	12.83	0.97	0.442		0.222	(	0.331)	0.219
155	12.92	0.97	0.442		0.221	(	0.331)	0.221
156	13.00	0.97	0.442		0.220	(	0.331)	0.222
157	13.08	1.13	0.518		0.219	(	0.389)	0.299
158	13.17	1.13	0.518		0.218	(	0.389)	0.300
159	13.25	1.13	0.518		0.217	(	0.389)	0.301
160	13.33	1.13	0.518		0.216	(	0.389)	0.302
161	13.42	1.13	0.518		0.215	(	0.389)	0.303
162	13.50	1.13	0.518		0.214	(	0.389)	0.305
163	13.58	0.77	0.351		0.213	(	0.263)	0.138
164	13.67	0.77	0.351		0.211	(	0.263)	0.139
165	13.75	0.77	0.351		0.210	(	0.263)	0.140
166	13.83	0.77	0.351		0.209	(	0.263)	0.141
167	13.92	0.77	0.351		0.208	(	0.263)	0.142
168	14.00	0.77	0.351		0.207	(	0.263)	0.143
169	14.08	0.90	0.411		0.206	(	0.309)	0.205
170	14.17	0.90	0.411		0.205	(	0.309)	0.206
171	14.25	0.90	0.411		0.204	(	0.309)	0.207
172	14.33	0.87	0.396		0.203	(	0.297)	0.193
173	14.42	0.87	0.396		0.202	(	0.297)	0.194
174	14.50	0.87	0.396		0.201	(	0.297)	0.195
175	14.58	0.87	0.396		0.200	(	0.297)	0.196
176	14.67	0.87	0.396		0.199	(	0.297)	0.197
177	14.75	0.87	0.396		0.198	(	0.297)	0.198
178	14.83	0.83	0.381		0.197	(	0.286)	0.184
179	14.92	0.83	0.381		0.196	(	0.286)	0.185
180	15.00	0.83	0.381		0.195	(	0.286)	0.186

181	15.08	0.80	0.366		0.194	(	0.274)	0.172
182	15.17	0.80	0.366		0.193	(	0.274)	0.173
183	15.25	0.80	0.366		0.192	(	0.274)	0.174
184	15.33	0.77	0.351		0.191	(	0.263)	0.160
185	15.42	0.77	0.351		0.190	(	0.263)	0.161
186	15.50	0.77	0.351		0.189	(	0.263)	0.162
187	15.58	0.63	0.290		0.188	(	0.217)	0.102
188	15.67	0.63	0.290		0.187	(	0.217)	0.103
189	15.75	0.63	0.290		0.186	(	0.217)	0.104
190	15.83	0.63	0.290		0.185	(	0.217)	0.105
191	15.92	0.63	0.290		0.184	(	0.217)	0.105
192	16.00	0.63	0.290		0.183	(	0.217)	0.106
193	16.08	0.13	0.061	(	0.182)		0.046	0.015
194	16.17	0.13	0.061	(	0.181)		0.046	0.015
195	16.25	0.13	0.061	(	0.180)		0.046	0.015
196	16.33	0.13	0.061	(	0.179)		0.046	0.015
197	16.42	0.13	0.061	(	0.179)		0.046	0.015
198	16.50	0.13	0.061	(	0.178)		0.046	0.015
199	16.58	0.10	0.046	(	0.177)		0.034	0.011
200	16.67	0.10	0.046	(	0.176)		0.034	0.011
201	16.75	0.10	0.046	(	0.175)		0.034	0.011
202	16.83	0.10	0.046	(	0.174)		0.034	0.011
203	16.92	0.10	0.046	(	0.173)		0.034	0.011
204	17.00	0.10	0.046	(	0.172)		0.034	0.011
205	17.08	0.17	0.076	(	0.171)		0.057	0.019
206	17.17	0.17	0.076	(	0.171)		0.057	0.019
207	17.25	0.17	0.076	(	0.170)		0.057	0.019
208	17.33	0.17	0.076	(	0.169)		0.057	0.019
209	17.42	0.17	0.076	(	0.168)		0.057	0.019
210	17.50	0.17	0.076	(	0.167)		0.057	0.019
211	17.58	0.17	0.076	(	0.166)		0.057	0.019
212	17.67	0.17	0.076	(	0.165)		0.057	0.019
213	17.75	0.17	0.076	(	0.165)		0.057	0.019
214	17.83	0.13	0.061	(	0.164)		0.046	0.015
215	17.92	0.13	0.061	(	0.163)		0.046	0.015
216	18.00	0.13	0.061	(	0.162)		0.046	0.015
217	18.08	0.13	0.061	(	0.161)		0.046	0.015
218	18.17	0.13	0.061	(	0.161)		0.046	0.015
219	18.25	0.13	0.061	(	0.160)		0.046	0.015
220	18.33	0.13	0.061	(	0.159)		0.046	0.015
221	18.42	0.13	0.061	(	0.158)		0.046	0.015
222	18.50	0.13	0.061	(	0.158)		0.046	0.015
223	18.58	0.10	0.046	(	0.157)		0.034	0.011
224	18.67	0.10	0.046	(	0.156)		0.034	0.011
225	18.75	0.10	0.046	(	0.155)		0.034	0.011
226	18.83	0.07	0.030	(	0.155)		0.023	0.008
227	18.92	0.07	0.030	(	0.154)		0.023	0.008
228	19.00	0.07	0.030	(	0.153)		0.023	0.008
229	19.08	0.10	0.046	(	0.152)		0.034	0.011
230	19.17	0.10	0.046	(	0.152)		0.034	0.011
231	19.25	0.10	0.046	(	0.151)		0.034	0.011
232	19.33	0.13	0.061	(	0.150)		0.046	0.015
233	19.42	0.13	0.061	(	0.150)		0.046	0.015
234	19.50	0.13	0.061	(	0.149)		0.046	0.015
235	19.58	0.10	0.046	(	0.148)		0.034	0.011
236	19.67	0.10	0.046	(	0.147)		0.034	0.011
237	19.75	0.10	0.046	(	0.147)		0.034	0.011
238	19.83	0.07	0.030	(	0.146)		0.023	0.008
239	19.92	0.07	0.030	(	0.145)		0.023	0.008
240	20.00	0.07	0.030	(	0.145)		0.023	0.008
241	20.08	0.10	0.046	(	0.144)		0.034	0.011
242	20.17	0.10	0.046	(	0.144)		0.034	0.011
243	20.25	0.10	0.046	(	0.143)		0.034	0.011
244	20.33	0.10	0.046	(	0.142)		0.034	0.011
245	20.42	0.10	0.046	(	0.142)		0.034	0.011
246	20.50	0.10	0.046	(	0.141)		0.034	0.011
247	20.58	0.10	0.046	(	0.141)		0.034	0.011
248	20.67	0.10	0.046	(	0.140)		0.034	0.011
249	20.75	0.10	0.046	(	0.139)		0.034	0.011
250	20.83	0.07	0.030	(	0.139)		0.023	0.008
251	20.92	0.07	0.030	(	0.138)		0.023	0.008
252	21.00	0.07	0.030	(	0.138)		0.023	0.008

253	21.08	0.10	0.046	(0.137)	0.034	0.011
254	21.17	0.10	0.046	(0.137)	0.034	0.011
255	21.25	0.10	0.046	(0.136)	0.034	0.011
256	21.33	0.07	0.030	(0.136)	0.023	0.008
257	21.42	0.07	0.030	(0.135)	0.023	0.008
258	21.50	0.07	0.030	(0.135)	0.023	0.008
259	21.58	0.10	0.046	(0.134)	0.034	0.011
260	21.67	0.10	0.046	(0.134)	0.034	0.011
261	21.75	0.10	0.046	(0.133)	0.034	0.011
262	21.83	0.07	0.030	(0.133)	0.023	0.008
263	21.92	0.07	0.030	(0.132)	0.023	0.008
264	22.00	0.07	0.030	(0.132)	0.023	0.008
265	22.08	0.10	0.046	(0.131)	0.034	0.011
266	22.17	0.10	0.046	(0.131)	0.034	0.011
267	22.25	0.10	0.046	(0.130)	0.034	0.011
268	22.33	0.07	0.030	(0.130)	0.023	0.008
269	22.42	0.07	0.030	(0.130)	0.023	0.008
270	22.50	0.07	0.030	(0.129)	0.023	0.008
271	22.58	0.07	0.030	(0.129)	0.023	0.008
272	22.67	0.07	0.030	(0.128)	0.023	0.008
273	22.75	0.07	0.030	(0.128)	0.023	0.008
274	22.83	0.07	0.030	(0.128)	0.023	0.008
275	22.92	0.07	0.030	(0.127)	0.023	0.008
276	23.00	0.07	0.030	(0.127)	0.023	0.008
277	23.08	0.07	0.030	(0.127)	0.023	0.008
278	23.17	0.07	0.030	(0.127)	0.023	0.008
279	23.25	0.07	0.030	(0.126)	0.023	0.008
280	23.33	0.07	0.030	(0.126)	0.023	0.008
281	23.42	0.07	0.030	(0.126)	0.023	0.008
282	23.50	0.07	0.030	(0.126)	0.023	0.008
283	23.58	0.07	0.030	(0.125)	0.023	0.008
284	23.67	0.07	0.030	(0.125)	0.023	0.008
285	23.75	0.07	0.030	(0.125)	0.023	0.008
286	23.83	0.07	0.030	(0.125)	0.023	0.008
287	23.92	0.07	0.030	(0.125)	0.023	0.008
288	24.00	0.07	0.030	(0.125)	0.023	0.008

(Loss Rate Not Used)

Sum = 100.0 Sum = 15.6

Flood volume = Effective rainfall 1.30(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 1.3(Ac.Ft)
Total soil loss = 2.51(In)
Total soil loss = 2.470(Ac.Ft)
Total rainfall = 3.81(In)
Flood volume = 55622.4 Cubic Feet
Total soil loss = 107579.8 Cubic Feet

Peak flow rate of this hydrograph = 3.610(CFS)

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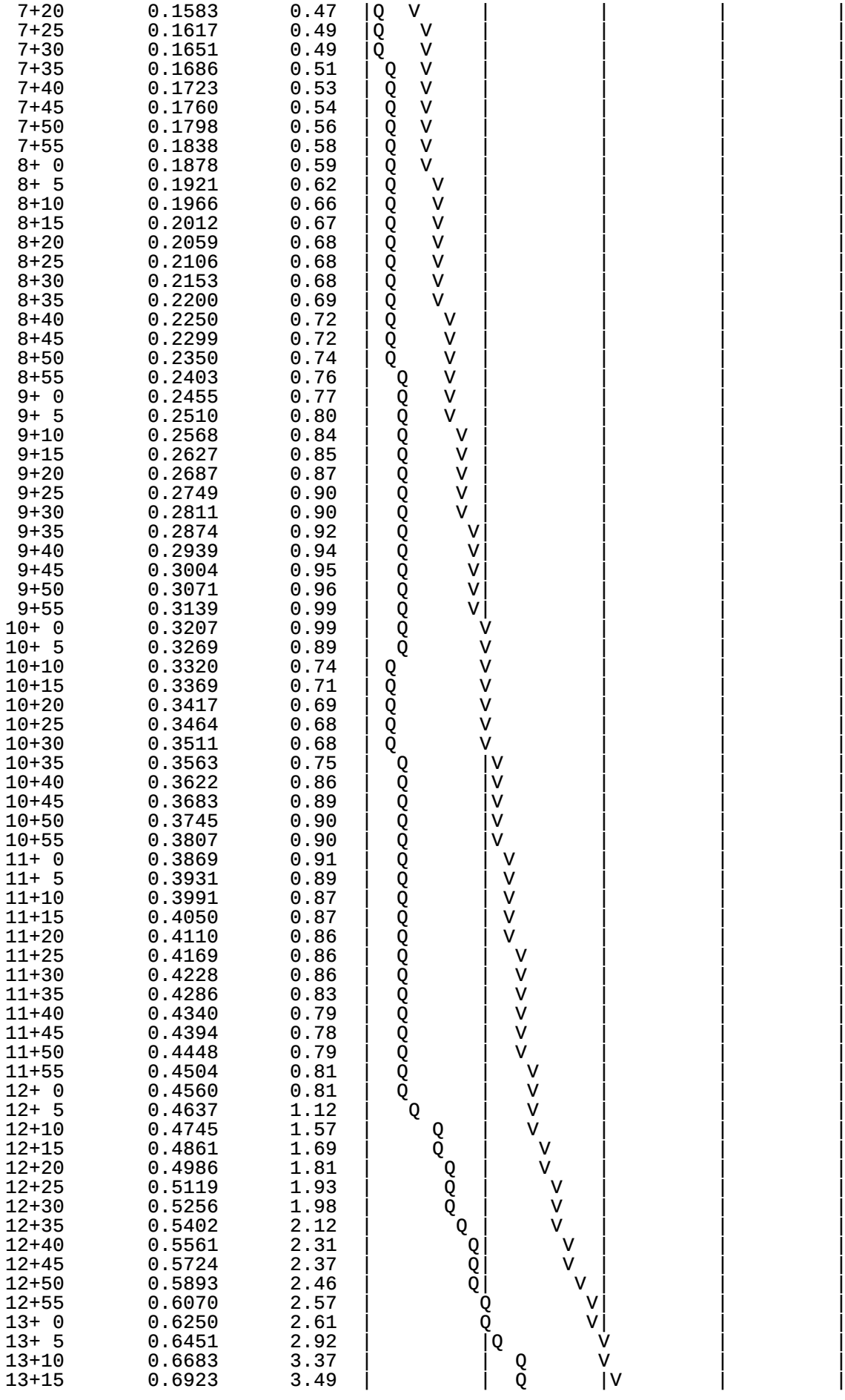
24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0002	0.03	Q				
0+10	0.0007	0.07	Q				
0+15	0.0013	0.08	Q				
0+20	0.0020	0.10	Q				
0+25	0.0028	0.13	Q				
0+30	0.0037	0.13	Q				
0+35	0.0047	0.13	Q				
0+40	0.0056	0.14	Q				
0+45	0.0065	0.14	Q				
0+50	0.0076	0.15	Q				
0+55	0.0087	0.17	Q				
1+ 0	0.0100	0.18	Q				
1+ 5	0.0111	0.16	Q				
1+10	0.0121	0.14	Q				
1+15	0.0131	0.14	Q				

```
1+20       0.0140      0.14  Q          |           |           |           |
1+25       0.0150      0.14  Q          |           |           |           |
1+30       0.0159      0.14  Q          |           |           |           |
1+35       0.0168      0.14  Q          |           |           |           |
1+40       0.0178      0.14  Q          |           |           |           |
1+45       0.0187      0.14  Q          |           |           |           |
1+50       0.0197      0.15  Q          |           |           |           |
1+55       0.0209      0.17  Q          |           |           |           |
2+ 0       0.0221      0.18  Q          |           |           |           |
2+ 5       0.0234      0.18  Q          |           |           |           |
2+10       0.0246      0.18  Q          |           |           |           |
2+15       0.0259      0.18  Q          |           |           |           |
2+20       0.0271      0.18  Q          |           |           |           |
2+25       0.0284      0.18  Q          |           |           |           |
2+30       0.0296      0.18  Q          |           |           |           |
2+35       0.0310      0.20  Q          |           |           |           |
2+40       0.0325      0.22  QV         |           |           |           |
2+45       0.0340      0.22  QV         |           |           |           |
2+50       0.0355      0.22  QV         |           |           |           |
2+55       0.0371      0.23  QV         |           |           |           |
3+ 0       0.0387      0.23  QV         |           |           |           |
3+ 5       0.0402      0.23  QV         |           |           |           |
3+10       0.0418      0.23  QV         |           |           |           |
3+15       0.0433      0.23  QV         |           |           |           |
3+20       0.0449      0.23  QV         |           |           |           |
3+25       0.0465      0.23  QV         |           |           |           |
3+30       0.0480      0.23  QV         |           |           |           |
3+35       0.0496      0.23  QV         |           |           |           |
3+40       0.0511      0.23  QV         |           |           |           |
3+45       0.0527      0.23  QV         |           |           |           |
3+50       0.0544      0.24  QV         |           |           |           |
3+55       0.0562      0.26  |Q         |           |           |           |
4+ 0       0.0580      0.27  |Q         |           |           |           |
4+ 5       0.0599      0.27  |Q         |           |           |           |
4+10       0.0618      0.27  |Q         |           |           |           |
4+15       0.0636      0.27  |Q         |           |           |           |
4+20       0.0656      0.29  |QV        |           |           |           |
4+25       0.0677      0.31  |QV        |           |           |           |
4+30       0.0699      0.31  |QV        |           |           |           |
4+35       0.0720      0.32  |QV        |           |           |           |
4+40       0.0742      0.32  |QV        |           |           |           |
4+45       0.0764      0.32  |QV        |           |           |           |
4+50       0.0787      0.33  |QV        |           |           |           |
4+55       0.0811      0.35  |QV        |           |           |           |
5+ 0       0.0836      0.36  |QV        |           |           |           |
5+ 5       0.0859      0.33  |QV        |           |           |           |
5+10       0.0879      0.29  |QV        |           |           |           |
5+15       0.0898      0.28  |QV        |           |           |           |
5+20       0.0918      0.29  |QV        |           |           |           |
5+25       0.0939      0.31  |QV        |           |           |           |
5+30       0.0961      0.31  |Q V       |           |           |           |
5+35       0.0984      0.33  |Q V       |           |           |           |
5+40       0.1008      0.35  |Q V       |           |           |           |
5+45       0.1033      0.36  |Q V       |           |           |           |
5+50       0.1058      0.36  |Q V       |           |           |           |
5+55       0.1082      0.36  |Q V       |           |           |           |
6+ 0       0.1107      0.36  |Q V       |           |           |           |
6+ 5       0.1133      0.38  |Q V       |           |           |           |
6+10       0.1161      0.40  |Q V       |           |           |           |
6+15       0.1189      0.40  |Q V       |           |           |           |
6+20       0.1217      0.41  |Q V       |           |           |           |
6+25       0.1245      0.41  |Q V       |           |           |           |
6+30       0.1273      0.41  |Q V       |           |           |           |
6+35       0.1302      0.42  |Q  V      |           |           |           |
6+40       0.1333      0.44  |Q  V      |           |           |           |
6+45       0.1363      0.45  |Q  V      |           |           |           |
6+50       0.1395      0.45  |Q  V      |           |           |           |
6+55       0.1426      0.45  |Q  V      |           |           |           |
7+ 0       0.1457      0.45  |Q  V      |           |           |           |
7+ 5       0.1488      0.45  |Q  V      |           |           |           |
7+10       0.1519      0.45  |Q  V      |           |           |           |
7+15       0.1551      0.45  |Q  V      |           |           |           |
```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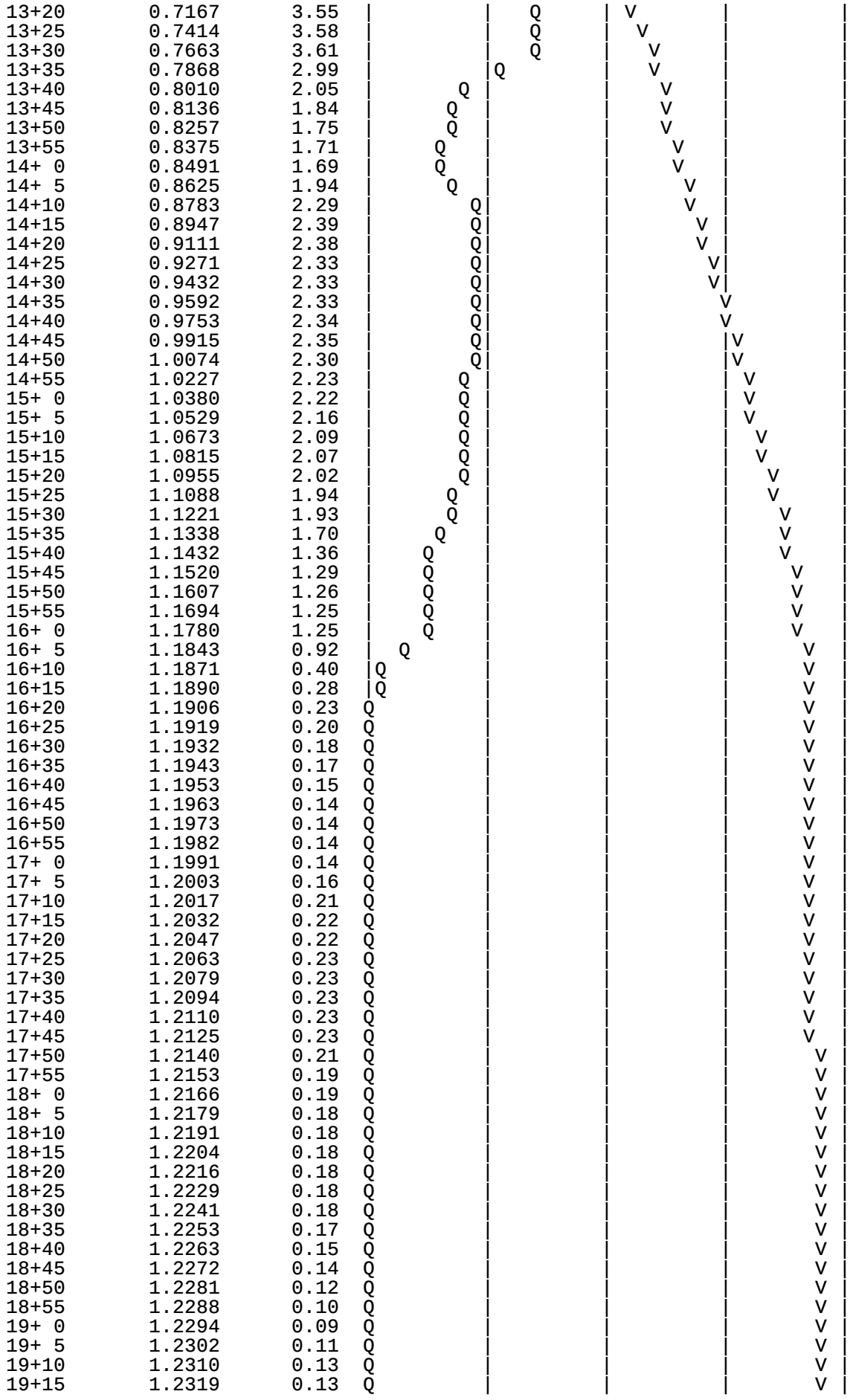
7+25 0.1617 0.49
7+30 0.1651 0.49
7+35 0.1686 0.51
7+40 0.1723 0.53
7+45 0.1760 0.54
7+50 0.1798 0.56
7+55 0.1838 0.58
8+ 0 0.1878 0.59
8+ 5 0.1921 0.62
8+10 0.1966 0.66
8+15 0.2012 0.67
8+20 0.2059 0.68
8+25 0.2106 0.68
8+30 0.2153 0.68
8+35 0.2200 0.69
8+40 0.2250 0.72
8+45 0.2299 0.72
8+50 0.2350 0.74
8+55 0.2403 0.76
9+ 0 0.2455 0.77
9+ 5 0.2510 0.80
9+10 0.2568 0.84
9+15 0.2627 0.85
9+20 0.2687 0.87
9+25 0.2749 0.90
9+30 0.2811 0.90
9+35 0.2874 0.92
9+40 0.2939 0.94
9+45 0.3004 0.95
9+50 0.3071 0.96
9+55 0.3139 0.99
10+ 0 0.3207 0.99
10+ 5 0.3269 0.89
10+10 0.3320 0.74
10+15 0.3369 0.71
10+20 0.3417 0.69
10+25 0.3464 0.68
10+30 0.3511 0.68
10+35 0.3563 0.75
10+40 0.3622 0.86
10+45 0.3683 0.89
10+50 0.3745 0.90
10+55 0.3807 0.90
11+ 0 0.3869 0.91
11+ 5 0.3931 0.89
11+10 0.3991 0.87
11+15 0.4050 0.87
11+20 0.4110 0.86
11+25 0.4169 0.86
11+30 0.4228 0.86
11+35 0.4286 0.83
11+40 0.4340 0.79
11+45 0.4394 0.78
11+50 0.4448 0.79
11+55 0.4504 0.81
12+ 0 0.4560 0.81
12+ 5 0.4637 1.12
12+10 0.4745 1.57
12+15 0.4861 1.69
12+20 0.4986 1.81
12+25 0.5119 1.93
12+30 0.5256 1.98
12+35 0.5402 2.12
12+40 0.5561 2.31
12+45 0.5724 2.37
12+50 0.5893 2.46
12+55 0.6070 2.57
13+ 0 0.6250 2.61
13+ 5 0.6451 2.92
13+10 0.6683 3.37
13+15 0.6923 3.49



13+20	0.7167	3.55	
13+25	0.7414	3.58	
13+30	0.7663	3.61	
13+35	0.7868	2.99	
13+40	0.8010	2.05	
13+45	0.8136	1.84	
13+50	0.8257	1.75	
13+55	0.8375	1.71	
14+ 0	0.8491	1.69	
14+ 5	0.8625	1.94	
14+10	0.8783	2.29	
14+15	0.8947	2.39	
14+20	0.9111	2.38	
14+25	0.9271	2.33	
14+30	0.9432	2.33	
14+35	0.9592	2.33	
14+40	0.9753	2.34	
14+45	0.9915	2.35	
14+50	1.0074	2.30	
14+55	1.0227	2.23	
15+ 0	1.0380	2.22	
15+ 5	1.0529	2.16	
15+10	1.0673	2.09	
15+15	1.0815	2.07	
15+20	1.0955	2.02	
15+25	1.1088	1.94	
15+30	1.1221	1.93	
15+35	1.1338	1.70	
15+40	1.1432	1.36	
15+45	1.1520	1.29	
15+50	1.1607	1.26	
15+55	1.1694	1.25	
16+ 0	1.1780	1.25	
16+ 5	1.1843	0.92	
16+10	1.1871	0.40	
16+15	1.1890	0.28	
16+20	1.1906	0.23	
16+25	1.1919	0.20	
16+30	1.1932	0.18	
16+35	1.1943	0.17	
16+40	1.1953	0.15	
16+45	1.1963	0.14	
16+50	1.1973	0.14	
16+55	1.1982	0.14	
17+ 0	1.1991	0.14	
17+ 5	1.2003	0.16	
17+10	1.2017	0.21	
17+15	1.2032	0.22	
17+20	1.2047	0.22	
17+25	1.2063	0.23	
17+30	1.2079	0.23	
17+35	1.2094	0.23	
17+40	1.2110	0.23	
17+45	1.2125	0.23	
17+50	1.2140	0.21	
17+55	1.2153	0.19	
18+ 0	1.2166	0.19	
18+ 5	1.2179	0.18	
18+10	1.2191	0.18	
18+15	1.2204	0.18	
18+20	1.2216	0.18	
18+25	1.2229	0.18	
18+30	1.2241	0.18	
18+35	1.2253	0.17	
18+40	1.2263	0.15	
18+45	1.2272	0.14	
18+50	1.2281	0.12	
18+55	1.2288	0.10	
19+ 0	1.2294	0.09	
19+ 5	1.2302	0.11	
19+10	1.2310	0.13	
19+15	1.2319	0.13	

```
  19+20       1.2330      0.15  Q          |           |           |        V |
  19+25       1.2341      0.17  Q          |           |           |        V |
  19+30       1.2354      0.18  Q          |           |           |        V |
  19+35       1.2365      0.16  Q          |           |           |        V |
  19+40       1.2375      0.14  Q          |           |           |        V |
  19+45       1.2385      0.14  Q          |           |           |        V |
  19+50       1.2393      0.12  Q          |           |           |        V |
  19+55       1.2400      0.10  Q          |           |           |        V |
  20+ 0       1.2407      0.09  Q          |           |           |        V |
  20+ 5       1.2414      0.11  Q          |           |           |        V |
  20+10       1.2423      0.13  Q          |           |           |        V |
  20+15       1.2432      0.13  Q          |           |           |        V |
  20+20       1.2441      0.13  Q          |           |           |        V |
  20+25       1.2450      0.14  Q          |           |           |         V|
  20+30       1.2460      0.14  Q          |           |           |         V|
  20+35       1.2469      0.14  Q          |           |           |         V|
  20+40       1.2478      0.14  Q          |           |           |         V|
  20+45       1.2488      0.14  Q          |           |           |         V|
  20+50       1.2496      0.12  Q          |           |           |         V|
  20+55       1.2503      0.10  Q          |           |           |         V|
  21+ 0       1.2510      0.09  Q          |           |           |         V|
  21+ 5       1.2517      0.11  Q          |           |           |         V|
  21+10       1.2526      0.13  Q          |           |           |         V|
  21+15       1.2535      0.13  Q          |           |           |         V|
  21+20       1.2543      0.12  Q          |           |           |         V|
  21+25       1.2550      0.10  Q          |           |           |         V|
  21+30       1.2556      0.09  Q          |           |           |         V|
  21+35       1.2564      0.11  Q          |           |           |         V|
  21+40       1.2573      0.13  Q          |           |           |         V|
  21+45       1.2582      0.13  Q          |           |           |         V|
  21+50       1.2590      0.12  Q          |           |           |         V|
  21+55       1.2597      0.10  Q          |           |           |         V|
  22+ 0       1.2603      0.09  Q          |           |           |         V|
  22+ 5       1.2611      0.11  Q          |           |           |         V|
  22+10       1.2619      0.13  Q          |           |           |         V|
  22+15       1.2628      0.13  Q          |           |           |         V|
  22+20       1.2637      0.12  Q          |           |           |         V|
  22+25       1.2644      0.10  Q          |           |           |         V|
  22+30       1.2650      0.09  Q          |           |           |         V|
  22+35       1.2656      0.09  Q          |           |           |         V|
  22+40       1.2663      0.09  Q          |           |           |         V|
  22+45       1.2669      0.09  Q          |           |           |         V|
  22+50       1.2675      0.09  Q          |           |           |         V|
  22+55       1.2681      0.09  Q          |           |           |         V|
  23+ 0       1.2688      0.09  Q          |           |           |         V|
  23+ 5       1.2694      0.09  Q          |           |           |         V|
  23+10       1.2700      0.09  Q          |           |           |         V|
  23+15       1.2706      0.09  Q          |           |           |         V|
  23+20       1.2713      0.09  Q          |           |           |         V|
  23+25       1.2719      0.09  Q          |           |           |         V|
  23+30       1.2725      0.09  Q          |           |           |         V|
  23+35       1.2731      0.09  Q          |           |           |         V|
  23+40       1.2738      0.09  Q          |           |           |         V|
  23+45       1.2744      0.09  Q          |           |           |         V|
  23+50       1.2750      0.09  Q          |           |           |         V|
  23+55       1.2756      0.09  Q          |           |           |         V|
  24+ 0       1.2763      0.09  Q          |           |           |         V|
  24+ 5       1.2767      0.06  Q          |           |           |         V|
  24+10       1.2768      0.02  Q          |           |           |         V|
  24+15       1.2769      0.01  Q          |           |           |         V|
  24+20       1.2769      0.00  Q          |           |           |         V|
  24+25       1.2769      0.00  Q          |           |           |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E010610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	1.20	14.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	3.00	35.40

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.941(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.940(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	0.215	0.021
76.0	76.0	0.291	0.000	0.291	0.785	0.229
					Sum (F) =	0.249

Area averaged mean soil loss (F) (In/Hr) = 0.249
Minimum soil loss rate ((In/Hr)) = 0.125
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.50	0.116	(0.249)		0.087	0.029
2	0.17	0.60	0.140	(0.249)		0.105	0.035
3	0.25	0.60	0.140	(0.249)		0.105	0.035
4	0.33	0.60	0.140	(0.249)		0.105	0.035
5	0.42	0.60	0.140	(0.249)		0.105	0.035
6	0.50	0.70	0.163	(0.249)		0.122	0.041
7	0.58	0.70	0.163	(0.249)		0.122	0.041
8	0.67	0.70	0.163	(0.249)		0.122	0.041
9	0.75	0.70	0.163	(0.249)		0.122	0.041
10	0.83	0.70	0.163	(0.249)		0.122	0.041
11	0.92	0.70	0.163	(0.249)		0.122	0.041
12	1.00	0.80	0.186	(0.249)		0.140	0.047
13	1.08	0.80	0.186	(0.249)		0.140	0.047
14	1.17	0.80	0.186	(0.249)		0.140	0.047
15	1.25	0.80	0.186	(0.249)		0.140	0.047
16	1.33	0.80	0.186	(0.249)		0.140	0.047
17	1.42	0.80	0.186	(0.249)		0.140	0.047
18	1.50	0.80	0.186	(0.249)		0.140	0.047
19	1.58	0.80	0.186	(0.249)		0.140	0.047
20	1.67	0.80	0.186	(0.249)		0.140	0.047
21	1.75	0.80	0.186	(0.249)		0.140	0.047
22	1.83	0.80	0.186	(0.249)		0.140	0.047
23	1.92	0.80	0.186	(0.249)		0.140	0.047
24	2.00	0.90	0.210	(0.249)		0.157	0.052
25	2.08	0.80	0.186	(0.249)		0.140	0.047
26	2.17	0.90	0.210	(0.249)		0.157	0.052
27	2.25	0.90	0.210	(0.249)		0.157	0.052
28	2.33	0.90	0.210	(0.249)		0.157	0.052
29	2.42	0.90	0.210	(0.249)		0.157	0.052
30	2.50	0.90	0.210	(0.249)		0.157	0.052
31	2.58	0.90	0.210	(0.249)		0.157	0.052
32	2.67	0.90	0.210	(0.249)		0.157	0.052
33	2.75	1.00	0.233	(0.249)		0.175	0.058
34	2.83	1.00	0.233	(0.249)		0.175	0.058
35	2.92	1.00	0.233	(0.249)		0.175	0.058
36	3.00	1.00	0.233	(0.249)		0.175	0.058

37	3.08	1.00	0.233	(	0.249)	0.175		0.058
38	3.17	1.10	0.256	(	0.249)	0.192		0.064
39	3.25	1.10	0.256	(	0.249)	0.192		0.064
40	3.33	1.10	0.256	(	0.249)	0.192		0.064
41	3.42	1.20	0.279	(	0.249)	0.210		0.070
42	3.50	1.30	0.303	(	0.249)	0.227		0.076
43	3.58	1.40	0.326	(	0.249)	0.244		0.081
44	3.67	1.40	0.326	(	0.249)	0.244		0.081
45	3.75	1.50	0.349		0.249	(0.262)		0.100
46	3.83	1.50	0.349		0.249	(0.262)		0.100
47	3.92	1.60	0.373		0.249	(0.279)		0.123
48	4.00	1.60	0.373		0.249	(0.279)		0.123
49	4.08	1.70	0.396		0.249	(0.297)		0.146
50	4.17	1.80	0.419		0.249	(0.314)		0.170
51	4.25	1.90	0.442		0.249	(0.332)		0.193
52	4.33	2.00	0.466		0.249	(0.349)		0.216
53	4.42	2.10	0.489		0.249	(0.367)		0.240
54	4.50	2.10	0.489		0.249	(0.367)		0.240
55	4.58	2.20	0.512		0.249	(0.384)		0.263
56	4.67	2.30	0.536		0.249	(0.402)		0.286
57	4.75	2.40	0.559		0.249	(0.419)		0.309
58	4.83	2.40	0.559		0.249	(0.419)		0.309
59	4.92	2.50	0.582		0.249	(0.437)		0.333
60	5.00	2.60	0.605		0.249	(0.454)		0.356
61	5.08	3.10	0.722		0.249	(0.541)		0.472
62	5.17	3.60	0.838		0.249	(0.629)		0.589
63	5.25	3.90	0.908		0.249	(0.681)		0.659
64	5.33	4.20	0.978		0.249	(0.733)		0.729
65	5.42	4.70	1.094		0.249	(0.821)		0.845
66	5.50	5.60	1.304		0.249	(0.978)		1.055
67	5.58	1.90	0.442		0.249	(0.332)		0.193
68	5.67	0.90	0.210	(	0.249)	0.157		0.052
69	5.75	0.60	0.140	(	0.249)	0.105		0.035
70	5.83	0.50	0.116	(	0.249)	0.087		0.029
71	5.92	0.30	0.070	(	0.249)	0.052		0.017
72	6.00	0.20	0.047	(	0.249)	0.035		0.012

(Loss Rate Not Used)

Sum = 100.0 Sum = 10.4

Flood volume = Effective rainfall 0.87(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.9(Ac.Ft)
Total soil loss = 1.07(In)
Total soil loss = 1.054(Ac.Ft)
Total rainfall = 1.94(In)
Flood volume = 37207.4 Cubic Feet
Total soil loss = 45910.0 Cubic Feet

Peak flow rate of this hydrograph = 10.432(CFS)

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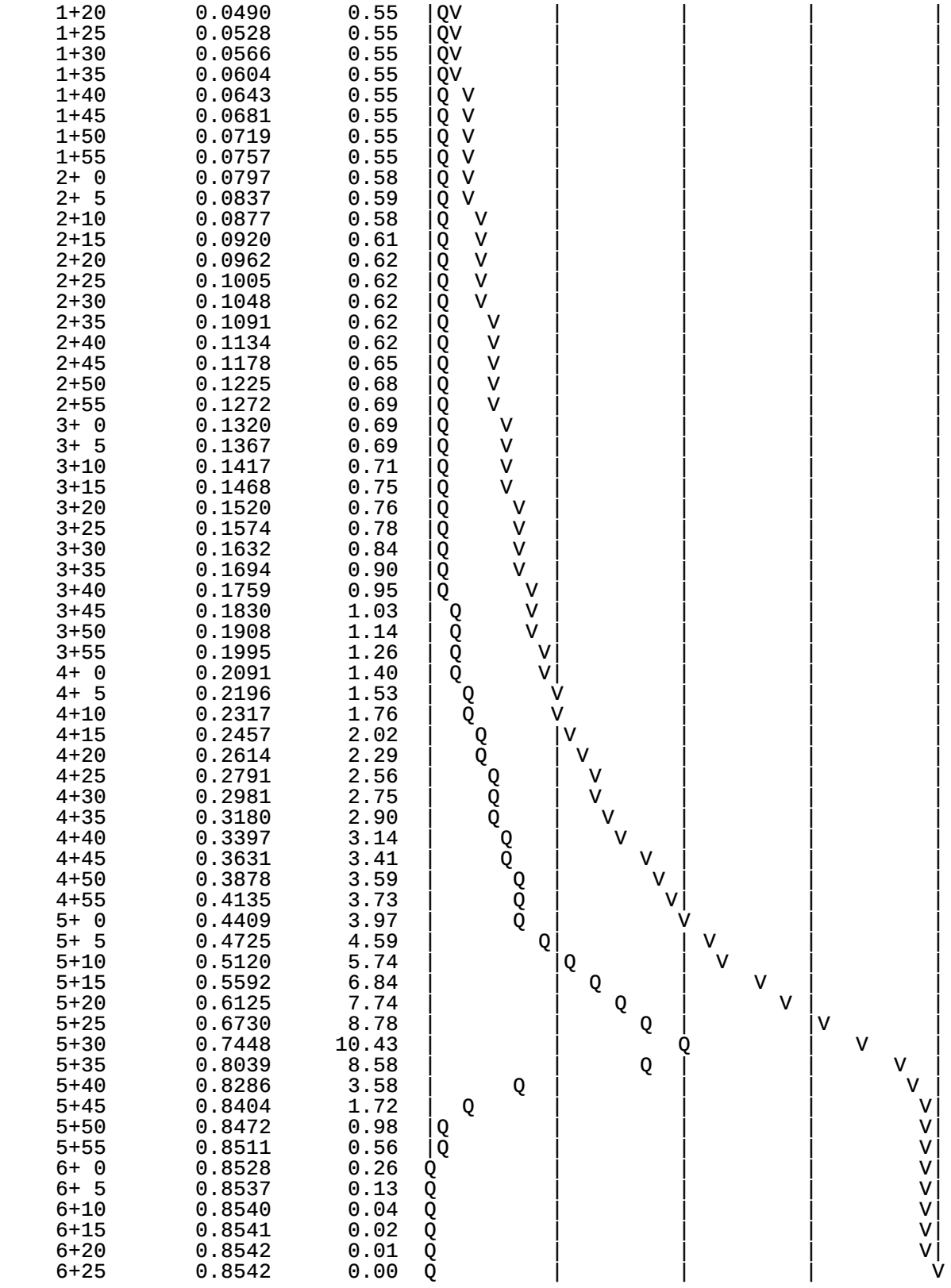
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0008	0.11	Q				
0+10	0.0028	0.30	Q				
0+15	0.0054	0.37	Q				
0+20	0.0081	0.39	Q				
0+25	0.0109	0.41	Q				
0+30	0.0139	0.44	Q				
0+35	0.0171	0.47	Q				
0+40	0.0204	0.48	Q				
0+45	0.0237	0.48	QV				
0+50	0.0271	0.48	QV				
0+55	0.0304	0.48	QV				
1+ 0	0.0339	0.51	|Q				
1+ 5	0.0376	0.54	|Q				
1+10	0.0414	0.55	|Q				
1+15	0.0452	0.55	|QV				


1+20 0.0490 0.55
1+25 0.0528 0.55
1+30 0.0566 0.55
1+35 0.0604 0.55
1+40 0.0643 0.55
1+45 0.0681 0.55
1+50 0.0719 0.55
1+55 0.0757 0.55
2+ 0 0.0797 0.58
2+ 5 0.0837 0.59
2+10 0.0877 0.58
2+15 0.0920 0.61
2+20 0.0962 0.62
2+25 0.1005 0.62
2+30 0.1048 0.62
2+35 0.1091 0.62
2+40 0.1134 0.62
2+45 0.1178 0.65
2+50 0.1225 0.68
2+55 0.1272 0.69
3+ 0 0.1320 0.69
3+ 5 0.1367 0.69
3+10 0.1417 0.71
3+15 0.1468 0.75
3+20 0.1520 0.76
3+25 0.1574 0.78
3+30 0.1632 0.84
3+35 0.1694 0.90
3+40 0.1759 0.95
3+45 0.1830 1.03
3+50 0.1908 1.14
3+55 0.1995 1.26
4+ 0 0.2091 1.40
4+ 5 0.2196 1.53
4+10 0.2317 1.76
4+15 0.2457 2.02
4+20 0.2614 2.29
4+25 0.2791 2.56
4+30 0.2981 2.75
4+35 0.3180 2.90
4+40 0.3397 3.14
4+45 0.3631 3.41
4+50 0.3878 3.59
4+55 0.4135 3.73
5+ 0 0.4409 3.97
5+ 5 0.4725 4.59
5+10 0.5120 5.74
5+15 0.5592 6.84
5+20 0.6125 7.74
5+25 0.6730 8.78
5+30 0.7448 10.43
5+35 0.8039 8.58
5+40 0.8286 3.58
5+45 0.8404 1.72
5+50 0.8472 0.98
5+55 0.8511 0.56
6+ 0 0.8528 0.26
6+ 5 0.8537 0.13
6+10 0.8540 0.04
6+15 0.8541 0.02
6+20 0.8542 0.01
6+25 0.8542 0.00

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E010310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	0.90	10.62

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	2.35	27.73

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.497(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.496(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	0.215	0.021
76.0	76.0	0.291	0.000	0.291	0.785	0.229
					Sum (F) =	0.249

Area averaged mean soil loss (F) (In/Hr) = 0.249
Minimum soil loss rate ((In/Hr)) = 0.125
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
			Sum = 100.000	Sum= 11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.233	(0.249)	0.175	0.058
2	0.17	1.30	0.233	(0.249)	0.175	0.058
3	0.25	1.10	0.198	(0.249)	0.148	0.049
4	0.33	1.50	0.269	(0.249)	0.202	0.067
5	0.42	1.50	0.269	(0.249)	0.202	0.067
6	0.50	1.80	0.323	(0.249)	0.242	0.081
7	0.58	1.50	0.269	(0.249)	0.202	0.067
8	0.67	1.80	0.323	(0.249)	0.242	0.081
9	0.75	1.80	0.323	(0.249)	0.242	0.081
10	0.83	1.50	0.269	(0.249)	0.202	0.067
11	0.92	1.60	0.287	(0.249)	0.215	0.072
12	1.00	1.80	0.323	(0.249)	0.242	0.081
13	1.08	2.20	0.395	0.249	(0.296)	0.146
14	1.17	2.20	0.395	0.249	(0.296)	0.146
15	1.25	2.20	0.395	0.249	(0.296)	0.146
16	1.33	2.00	0.359	0.249	(0.269)	0.110
17	1.42	2.60	0.467	0.249	(0.350)	0.217
18	1.50	2.70	0.485	0.249	(0.364)	0.235
19	1.58	2.40	0.431	0.249	(0.323)	0.182
20	1.67	2.70	0.485	0.249	(0.364)	0.235
21	1.75	3.30	0.593	0.249	(0.444)	0.343
22	1.83	3.10	0.557	0.249	(0.418)	0.307
23	1.92	2.90	0.521	0.249	(0.391)	0.271
24	2.00	3.00	0.539	0.249	(0.404)	0.289
25	2.08	3.10	0.557	0.249	(0.418)	0.307
26	2.17	4.20	0.754	0.249	(0.566)	0.505
27	2.25	5.00	0.898	0.249	(0.673)	0.648
28	2.33	3.50	0.629	0.249	(0.471)	0.379
29	2.42	6.80	1.221	0.249	(0.916)	0.972
30	2.50	7.30	1.311	0.249	(0.983)	1.061
31	2.58	8.20	1.473	0.249	(1.104)	1.223
32	2.67	5.90	1.059	0.249	(0.795)	0.810
33	2.75	2.00	0.359	0.249	(0.269)	0.110
34	2.83	1.80	0.323	(0.249)	0.242	0.081
35	2.92	1.80	0.323	(0.249)	0.242	0.081
36	3.00	0.60	0.108	(0.249)	0.081	0.027

(Loss Rate Not Used)
Sum = 100.0 Sum = 9.7
Flood volume = Effective rainfall 0.81(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.8(Ac.Ft)
Total soil loss = 0.69(In)
Total soil loss = 0.680(Ac.Ft)
Total rainfall = 1.50(In)
Flood volume = 34491.0 Cubic Feet
Total soil loss = 29608.5 Cubic Feet

Peak flow rate of this hydrograph = 12.482(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 5.0 10.0 15.0 20.0
0+ 5	0.0015	0.22	Q
0+10	0.0053	0.55	VQ
0+15	0.0094	0.60	VQ
0+20	0.0139	0.65	VQ
0+25	0.0191	0.76	VQ
0+30	0.0249	0.84	|Q
0+35	0.0309	0.87	|Q
0+40	0.0368	0.87	|Q
0+45	0.0433	0.94	|QV
0+50	0.0495	0.90	|QV
0+55	0.0553	0.85	|QV
1+ 0	0.0615	0.89	|Q V
1+ 5	0.0696	1.19	| QV
1+10	0.0804	1.56	| QV
1+15	0.0918	1.66	| QV
1+20	0.1026	1.56	| Q V
1+25	0.1149	1.79	| Q V
1+30	0.1317	2.43	| Q V
1+35	0.1485	2.45	| Q V
1+40	0.1653	2.43	| Q V
1+45	0.1867	3.11	| Q V|
1+50	0.2118	3.65	| Q V
1+55	0.2357	3.47	| Q |V
2+ 0	0.2589	3.36	| Q | V
2+ 5	0.2830	3.50	| Q | V
2+10	0.3131	4.37	| Q | V
2+15	0.3547	6.04	| | Q V
2+20	0.3968	6.11	| | Q V
2+25	0.4462	7.17	| | Q | V
2+30	0.5194	10.63	| | |Q V
2+35	0.6054	12.48	| | | Q V
2+40	0.6897	12.24	| | | Q | V
2+45	0.7425	7.66	| | Q | | V
2+50	0.7650	3.27	| Q | | | V
2+55	0.7786	1.97	| Q | | | V
3+ 0	0.7869	1.21	| Q | | | V
3+ 5	0.7903	0.49	Q | | | V
3+10	0.7912	0.13	Q | | | V
3+15	0.7916	0.06	Q | | | V
3+20	0.7918	0.02	Q | | | V
3+25	0.7918	0.00	Q | | | V

U n i t H y d r o g r a p h A n a l y s i s

Study date 12/28/22 File: 2216E010110.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
EXISTING CONDITION
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 11.80(Ac.) = 0.018 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 11.80(Ac.) = 0.018 Sq. Mi.
Length along longest watercourse = 1548.00(Ft.)
Length along longest watercourse measured to centroid = 500.00(Ft.)
Length along longest watercourse = 0.293 Mi.
Length along longest watercourse measured to centroid = 0.095 Mi.
Difference in elevation = 16.10(Ft.)
Slope along watercourse = 54.9147 Ft./Mi.
Average Manning's 'N' = 0.020
Lag time = 0.057 Hr.
Lag time = 3.45 Min.
25% of lag time = 0.86 Min.
40% of lag time = 1.38 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	0.54	6.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
11.80	1.36	16.05

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.877(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.877(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
2.540	56.00	0.900
9.260	76.00	0.000

Total Area Entered = 11.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	0.215	0.021
76.0	76.0	0.291	0.000	0.291	0.785	0.229
					Sum (F) =	0.249

Area averaged mean soil loss (F) (In/Hr) = 0.249
Minimum soil loss rate ((In/Hr)) = 0.125
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.750

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	145.077	31.965	3.801
2	0.167	290.154	47.363	5.632
3	0.250	435.231	11.478	1.365
4	0.333	580.308	5.035	0.599
5	0.417	725.385	2.615	0.311
6	0.500	870.462	1.544	0.184
		Sum =	100.000 Sum=	11.892

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.463	0.249	(0.347)	0.214
2	0.17	4.50	0.474	0.249	(0.355)	0.224
3	0.25	5.40	0.568	0.249	(0.426)	0.319
4	0.33	5.40	0.568	0.249	(0.426)	0.319
5	0.42	5.70	0.600	0.249	(0.450)	0.351
6	0.50	6.40	0.674	0.249	(0.505)	0.424
7	0.58	7.90	0.832	0.249	(0.624)	0.582
8	0.67	9.10	0.958	0.249	(0.718)	0.709
9	0.75	12.80	1.347	0.249	(1.011)	1.098
10	0.83	25.60	2.695	0.249	(2.021)	2.446
11	0.92	7.90	0.832	0.249	(0.624)	0.582
12	1.00	4.90	0.516	0.249	(0.387)	0.266
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.5

Flood volume = Effective rainfall 0.63(In)
times area 11.8(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.25(In)
Total soil loss = 0.245(Ac.Ft)
Total rainfall = 0.88(In)
Flood volume = 26893.4 Cubic Feet
Total soil loss = 10683.2 Cubic Feet

Peak flow rate of this hydrograph = 18.179(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0056	0.81	VQ	|	|	|	|

```
    0+10       0.0198      2.06  |V  Q     |          |          |          |
    0+15       0.0388      2.77  | V  Q    |          |          |          |
    0+20       0.0626      3.45  |   V Q   |          |          |          |
    0+25       0.0885      3.77  |    V Q  |          |          |          |
    0+30       0.1183      4.33  |      VQ |          |          |          |
    0+35       0.1556      5.42  |         Q          |          |          |
    0+40       0.2033      6.92  |          |  Q      |          |          |
    0+45       0.2679      9.39  |          |      VQ |          |          |
    0+50       0.3850     17.00  |          |         |   V      |   Q      |
    0+55       0.5102     18.18  |          |         |          |  V  Q    |
    1+ 0       0.5696      8.62  |          |      Q  |          |     V    |
    1+ 5       0.5988      4.23  |         Q |         |          |       V  |
    1+10       0.6103      1.68  |  Q       |         |          |         V|
    1+15       0.6157      0.79  |Q         |         |          |         V|
    1+20       0.6171      0.19  Q          |         |          |         V|
    1+25       0.6174      0.05  Q          |         |          |          V
-------------------------------------------------------------------------
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Technical Appendix E

Flood Hydrograph Hydrologic Analysis
Proposed Condition

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA02242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	2.00	10.62

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	6.40	33.98

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(0.238)	0.003	0.013
2	0.17	0.07	0.016	(0.237)	0.003	0.013
3	0.25	0.07	0.016	(0.236)	0.003	0.013
4	0.33	0.10	0.024	(0.235)	0.004	0.020
5	0.42	0.10	0.024	(0.234)	0.004	0.020
6	0.50	0.10	0.024	(0.233)	0.004	0.020
7	0.58	0.10	0.024	(0.232)	0.004	0.020
8	0.67	0.10	0.024	(0.231)	0.004	0.020
9	0.75	0.10	0.024	(0.230)	0.004	0.020
10	0.83	0.13	0.032	(0.230)	0.006	0.026
11	0.92	0.13	0.032	(0.229)	0.006	0.026
12	1.00	0.13	0.032	(0.228)	0.006	0.026
13	1.08	0.10	0.024	(0.227)	0.004	0.020
14	1.17	0.10	0.024	(0.226)	0.004	0.020
15	1.25	0.10	0.024	(0.225)	0.004	0.020
16	1.33	0.10	0.024	(0.224)	0.004	0.020
17	1.42	0.10	0.024	(0.223)	0.004	0.020
18	1.50	0.10	0.024	(0.222)	0.004	0.020
19	1.58	0.10	0.024	(0.222)	0.004	0.020
20	1.67	0.10	0.024	(0.221)	0.004	0.020
21	1.75	0.10	0.024	(0.220)	0.004	0.020
22	1.83	0.13	0.032	(0.219)	0.006	0.026
23	1.92	0.13	0.032	(0.218)	0.006	0.026
24	2.00	0.13	0.032	(0.217)	0.006	0.026
25	2.08	0.13	0.032	(0.216)	0.006	0.026
26	2.17	0.13	0.032	(0.215)	0.006	0.026
27	2.25	0.13	0.032	(0.214)	0.006	0.026
28	2.33	0.13	0.032	(0.214)	0.006	0.026
29	2.42	0.13	0.032	(0.213)	0.006	0.026
30	2.50	0.13	0.032	(0.212)	0.006	0.026
31	2.58	0.17	0.040	(0.211)	0.007	0.033
32	2.67	0.17	0.040	(0.210)	0.007	0.033
33	2.75	0.17	0.040	(0.209)	0.007	0.033
34	2.83	0.17	0.040	(0.208)	0.007	0.033
35	2.92	0.17	0.040	(0.208)	0.007	0.033
36	3.00	0.17	0.040	(0.207)	0.007	0.033
37	3.08	0.17	0.040	(0.206)	0.007	0.033
38	3.17	0.17	0.040	(0.205)	0.007	0.033
39	3.25	0.17	0.040	(0.204)	0.007	0.033
40	3.33	0.17	0.040	(0.203)	0.007	0.033
41	3.42	0.17	0.040	(0.202)	0.007	0.033

42	3.50	0.17	0.040	(0.202)	0.007	0.033
43	3.58	0.17	0.040	(0.201)	0.007	0.033
44	3.67	0.17	0.040	(0.200)	0.007	0.033
45	3.75	0.17	0.040	(0.199)	0.007	0.033
46	3.83	0.20	0.048	(0.198)	0.009	0.039
47	3.92	0.20	0.048	(0.197)	0.009	0.039
48	4.00	0.20	0.048	(0.197)	0.009	0.039
49	4.08	0.20	0.048	(0.196)	0.009	0.039
50	4.17	0.20	0.048	(0.195)	0.009	0.039
51	4.25	0.20	0.048	(0.194)	0.009	0.039
52	4.33	0.23	0.056	(0.193)	0.010	0.046
53	4.42	0.23	0.056	(0.192)	0.010	0.046
54	4.50	0.23	0.056	(0.192)	0.010	0.046
55	4.58	0.23	0.056	(0.191)	0.010	0.046
56	4.67	0.23	0.056	(0.190)	0.010	0.046
57	4.75	0.23	0.056	(0.189)	0.010	0.046
58	4.83	0.27	0.064	(0.188)	0.012	0.052
59	4.92	0.27	0.064	(0.187)	0.012	0.052
60	5.00	0.27	0.064	(0.187)	0.012	0.052
61	5.08	0.20	0.048	(0.186)	0.009	0.039
62	5.17	0.20	0.048	(0.185)	0.009	0.039
63	5.25	0.20	0.048	(0.184)	0.009	0.039
64	5.33	0.23	0.056	(0.183)	0.010	0.046
65	5.42	0.23	0.056	(0.183)	0.010	0.046
66	5.50	0.23	0.056	(0.182)	0.010	0.046
67	5.58	0.27	0.064	(0.181)	0.012	0.052
68	5.67	0.27	0.064	(0.180)	0.012	0.052
69	5.75	0.27	0.064	(0.179)	0.012	0.052
70	5.83	0.27	0.064	(0.179)	0.012	0.052
71	5.92	0.27	0.064	(0.178)	0.012	0.052
72	6.00	0.27	0.064	(0.177)	0.012	0.052
73	6.08	0.30	0.072	(0.176)	0.013	0.059
74	6.17	0.30	0.072	(0.175)	0.013	0.059
75	6.25	0.30	0.072	(0.175)	0.013	0.059
76	6.33	0.30	0.072	(0.174)	0.013	0.059
77	6.42	0.30	0.072	(0.173)	0.013	0.059
78	6.50	0.30	0.072	(0.172)	0.013	0.059
79	6.58	0.33	0.080	(0.172)	0.014	0.066
80	6.67	0.33	0.080	(0.171)	0.014	0.066
81	6.75	0.33	0.080	(0.170)	0.014	0.066
82	6.83	0.33	0.080	(0.169)	0.014	0.066
83	6.92	0.33	0.080	(0.169)	0.014	0.066
84	7.00	0.33	0.080	(0.168)	0.014	0.066
85	7.08	0.33	0.080	(0.167)	0.014	0.066
86	7.17	0.33	0.080	(0.166)	0.014	0.066
87	7.25	0.33	0.080	(0.165)	0.014	0.066
88	7.33	0.37	0.088	(0.165)	0.016	0.072
89	7.42	0.37	0.088	(0.164)	0.016	0.072
90	7.50	0.37	0.088	(0.163)	0.016	0.072
91	7.58	0.40	0.096	(0.162)	0.017	0.079
92	7.67	0.40	0.096	(0.162)	0.017	0.079
93	7.75	0.40	0.096	(0.161)	0.017	0.079
94	7.83	0.43	0.104	(0.160)	0.019	0.085
95	7.92	0.43	0.104	(0.159)	0.019	0.085
96	8.00	0.43	0.104	(0.159)	0.019	0.085
97	8.08	0.50	0.120	(0.158)	0.022	0.098
98	8.17	0.50	0.120	(0.157)	0.022	0.098
99	8.25	0.50	0.120	(0.157)	0.022	0.098
100	8.33	0.50	0.120	(0.156)	0.022	0.098
101	8.42	0.50	0.120	(0.155)	0.022	0.098
102	8.50	0.50	0.120	(0.154)	0.022	0.098
103	8.58	0.53	0.128	(0.154)	0.023	0.105
104	8.67	0.53	0.128	(0.153)	0.023	0.105
105	8.75	0.53	0.128	(0.152)	0.023	0.105
106	8.83	0.57	0.136	(0.151)	0.024	0.112
107	8.92	0.57	0.136	(0.151)	0.024	0.112
108	9.00	0.57	0.136	(0.150)	0.024	0.112
109	9.08	0.63	0.152	(0.149)	0.027	0.125
110	9.17	0.63	0.152	(0.149)	0.027	0.125
111	9.25	0.63	0.152	(0.148)	0.027	0.125
112	9.33	0.67	0.160	(0.147)	0.029	0.131
113	9.42	0.67	0.160	(0.147)	0.029	0.131

114	9.50	0.67	0.160	(0.146)	0.029	0.131
115	9.58	0.70	0.168	(0.145)	0.030	0.138
116	9.67	0.70	0.168	(0.144)	0.030	0.138
117	9.75	0.70	0.168	(0.144)	0.030	0.138
118	9.83	0.73	0.176	(0.143)	0.032	0.144
119	9.92	0.73	0.176	(0.142)	0.032	0.144
120	10.00	0.73	0.176	(0.142)	0.032	0.144
121	10.08	0.50	0.120	(0.141)	0.022	0.098
122	10.17	0.50	0.120	(0.140)	0.022	0.098
123	10.25	0.50	0.120	(0.140)	0.022	0.098
124	10.33	0.50	0.120	(0.139)	0.022	0.098
125	10.42	0.50	0.120	(0.138)	0.022	0.098
126	10.50	0.50	0.120	(0.138)	0.022	0.098
127	10.58	0.67	0.160	(0.137)	0.029	0.131
128	10.67	0.67	0.160	(0.136)	0.029	0.131
129	10.75	0.67	0.160	(0.136)	0.029	0.131
130	10.83	0.67	0.160	(0.135)	0.029	0.131
131	10.92	0.67	0.160	(0.134)	0.029	0.131
132	11.00	0.67	0.160	(0.134)	0.029	0.131
133	11.08	0.63	0.152	(0.133)	0.027	0.125
134	11.17	0.63	0.152	(0.132)	0.027	0.125
135	11.25	0.63	0.152	(0.132)	0.027	0.125
136	11.33	0.63	0.152	(0.131)	0.027	0.125
137	11.42	0.63	0.152	(0.130)	0.027	0.125
138	11.50	0.63	0.152	(0.130)	0.027	0.125
139	11.58	0.57	0.136	(0.129)	0.024	0.112
140	11.67	0.57	0.136	(0.128)	0.024	0.112
141	11.75	0.57	0.136	(0.128)	0.024	0.112
142	11.83	0.60	0.144	(0.127)	0.026	0.118
143	11.92	0.60	0.144	(0.126)	0.026	0.118
144	12.00	0.60	0.144	(0.126)	0.026	0.118
145	12.08	0.83	0.200	(0.125)	0.036	0.164
146	12.17	0.83	0.200	(0.125)	0.036	0.164
147	12.25	0.83	0.200	(0.124)	0.036	0.164
148	12.33	0.87	0.208	(0.123)	0.037	0.171
149	12.42	0.87	0.208	(0.123)	0.037	0.171
150	12.50	0.87	0.208	(0.122)	0.037	0.171
151	12.58	0.93	0.224	(0.121)	0.040	0.184
152	12.67	0.93	0.224	(0.121)	0.040	0.184
153	12.75	0.93	0.224	(0.120)	0.040	0.184
154	12.83	0.97	0.232	(0.120)	0.042	0.190
155	12.92	0.97	0.232	(0.119)	0.042	0.190
156	13.00	0.97	0.232	(0.118)	0.042	0.190
157	13.08	1.13	0.272	(0.118)	0.049	0.223
158	13.17	1.13	0.272	(0.117)	0.049	0.223
159	13.25	1.13	0.272	(0.117)	0.049	0.223
160	13.33	1.13	0.272	(0.116)	0.049	0.223
161	13.42	1.13	0.272	(0.115)	0.049	0.223
162	13.50	1.13	0.272	(0.115)	0.049	0.223
163	13.58	0.77	0.184	(0.114)	0.033	0.151
164	13.67	0.77	0.184	(0.114)	0.033	0.151
165	13.75	0.77	0.184	(0.113)	0.033	0.151
166	13.83	0.77	0.184	(0.113)	0.033	0.151
167	13.92	0.77	0.184	(0.112)	0.033	0.151
168	14.00	0.77	0.184	(0.111)	0.033	0.151
169	14.08	0.90	0.216	(0.111)	0.039	0.177
170	14.17	0.90	0.216	(0.110)	0.039	0.177
171	14.25	0.90	0.216	(0.110)	0.039	0.177
172	14.33	0.87	0.208	(0.109)	0.037	0.171
173	14.42	0.87	0.208	(0.109)	0.037	0.171
174	14.50	0.87	0.208	(0.108)	0.037	0.171
175	14.58	0.87	0.208	(0.107)	0.037	0.171
176	14.67	0.87	0.208	(0.107)	0.037	0.171
177	14.75	0.87	0.208	(0.106)	0.037	0.171
178	14.83	0.83	0.200	(0.106)	0.036	0.164
179	14.92	0.83	0.200	(0.105)	0.036	0.164
180	15.00	0.83	0.200	(0.105)	0.036	0.164
181	15.08	0.80	0.192	(0.104)	0.035	0.157
182	15.17	0.80	0.192	(0.104)	0.035	0.157
183	15.25	0.80	0.192	(0.103)	0.035	0.157
184	15.33	0.77	0.184	(0.103)	0.033	0.151
185	15.42	0.77	0.184	(0.102)	0.033	0.151

186	15.50	0.77	0.184	(0.102)	0.033	0.151
187	15.58	0.63	0.152	(0.101)	0.027	0.125
188	15.67	0.63	0.152	(0.101)	0.027	0.125
189	15.75	0.63	0.152	(0.100)	0.027	0.125
190	15.83	0.63	0.152	(0.100)	0.027	0.125
191	15.92	0.63	0.152	(0.099)	0.027	0.125
192	16.00	0.63	0.152	(0.099)	0.027	0.125
193	16.08	0.13	0.032	(0.098)	0.006	0.026
194	16.17	0.13	0.032	(0.098)	0.006	0.026
195	16.25	0.13	0.032	(0.097)	0.006	0.026
196	16.33	0.13	0.032	(0.097)	0.006	0.026
197	16.42	0.13	0.032	(0.096)	0.006	0.026
198	16.50	0.13	0.032	(0.096)	0.006	0.026
199	16.58	0.10	0.024	(0.095)	0.004	0.020
200	16.67	0.10	0.024	(0.095)	0.004	0.020
201	16.75	0.10	0.024	(0.094)	0.004	0.020
202	16.83	0.10	0.024	(0.094)	0.004	0.020
203	16.92	0.10	0.024	(0.093)	0.004	0.020
204	17.00	0.10	0.024	(0.093)	0.004	0.020
205	17.08	0.17	0.040	(0.092)	0.007	0.033
206	17.17	0.17	0.040	(0.092)	0.007	0.033
207	17.25	0.17	0.040	(0.091)	0.007	0.033
208	17.33	0.17	0.040	(0.091)	0.007	0.033
209	17.42	0.17	0.040	(0.090)	0.007	0.033
210	17.50	0.17	0.040	(0.090)	0.007	0.033
211	17.58	0.17	0.040	(0.089)	0.007	0.033
212	17.67	0.17	0.040	(0.089)	0.007	0.033
213	17.75	0.17	0.040	(0.089)	0.007	0.033
214	17.83	0.13	0.032	(0.088)	0.006	0.026
215	17.92	0.13	0.032	(0.088)	0.006	0.026
216	18.00	0.13	0.032	(0.087)	0.006	0.026
217	18.08	0.13	0.032	(0.087)	0.006	0.026
218	18.17	0.13	0.032	(0.086)	0.006	0.026
219	18.25	0.13	0.032	(0.086)	0.006	0.026
220	18.33	0.13	0.032	(0.086)	0.006	0.026
221	18.42	0.13	0.032	(0.085)	0.006	0.026
222	18.50	0.13	0.032	(0.085)	0.006	0.026
223	18.58	0.10	0.024	(0.084)	0.004	0.020
224	18.67	0.10	0.024	(0.084)	0.004	0.020
225	18.75	0.10	0.024	(0.084)	0.004	0.020
226	18.83	0.07	0.016	(0.083)	0.003	0.013
227	18.92	0.07	0.016	(0.083)	0.003	0.013
228	19.00	0.07	0.016	(0.082)	0.003	0.013
229	19.08	0.10	0.024	(0.082)	0.004	0.020
230	19.17	0.10	0.024	(0.082)	0.004	0.020
231	19.25	0.10	0.024	(0.081)	0.004	0.020
232	19.33	0.13	0.032	(0.081)	0.006	0.026
233	19.42	0.13	0.032	(0.080)	0.006	0.026
234	19.50	0.13	0.032	(0.080)	0.006	0.026
235	19.58	0.10	0.024	(0.080)	0.004	0.020
236	19.67	0.10	0.024	(0.079)	0.004	0.020
237	19.75	0.10	0.024	(0.079)	0.004	0.020
238	19.83	0.07	0.016	(0.079)	0.003	0.013
239	19.92	0.07	0.016	(0.078)	0.003	0.013
240	20.00	0.07	0.016	(0.078)	0.003	0.013
241	20.08	0.10	0.024	(0.078)	0.004	0.020
242	20.17	0.10	0.024	(0.077)	0.004	0.020
243	20.25	0.10	0.024	(0.077)	0.004	0.020
244	20.33	0.10	0.024	(0.077)	0.004	0.020
245	20.42	0.10	0.024	(0.076)	0.004	0.020
246	20.50	0.10	0.024	(0.076)	0.004	0.020
247	20.58	0.10	0.024	(0.076)	0.004	0.020
248	20.67	0.10	0.024	(0.075)	0.004	0.020
249	20.75	0.10	0.024	(0.075)	0.004	0.020
250	20.83	0.07	0.016	(0.075)	0.003	0.013
251	20.92	0.07	0.016	(0.074)	0.003	0.013
252	21.00	0.07	0.016	(0.074)	0.003	0.013
253	21.08	0.10	0.024	(0.074)	0.004	0.020
254	21.17	0.10	0.024	(0.073)	0.004	0.020
255	21.25	0.10	0.024	(0.073)	0.004	0.020
256	21.33	0.07	0.016	(0.073)	0.003	0.013
257	21.42	0.07	0.016	(0.073)	0.003	0.013

258	21.50	0.07	0.016	(0.072)	0.003	0.013
259	21.58	0.10	0.024	(0.072)	0.004	0.020
260	21.67	0.10	0.024	(0.072)	0.004	0.020
261	21.75	0.10	0.024	(0.072)	0.004	0.020
262	21.83	0.07	0.016	(0.071)	0.003	0.013
263	21.92	0.07	0.016	(0.071)	0.003	0.013
264	22.00	0.07	0.016	(0.071)	0.003	0.013
265	22.08	0.10	0.024	(0.071)	0.004	0.020
266	22.17	0.10	0.024	(0.070)	0.004	0.020
267	22.25	0.10	0.024	(0.070)	0.004	0.020
268	22.33	0.07	0.016	(0.070)	0.003	0.013
269	22.42	0.07	0.016	(0.070)	0.003	0.013
270	22.50	0.07	0.016	(0.069)	0.003	0.013
271	22.58	0.07	0.016	(0.069)	0.003	0.013
272	22.67	0.07	0.016	(0.069)	0.003	0.013
273	22.75	0.07	0.016	(0.069)	0.003	0.013
274	22.83	0.07	0.016	(0.069)	0.003	0.013
275	22.92	0.07	0.016	(0.069)	0.003	0.013
276	23.00	0.07	0.016	(0.068)	0.003	0.013
277	23.08	0.07	0.016	(0.068)	0.003	0.013
278	23.17	0.07	0.016	(0.068)	0.003	0.013
279	23.25	0.07	0.016	(0.068)	0.003	0.013
280	23.33	0.07	0.016	(0.068)	0.003	0.013
281	23.42	0.07	0.016	(0.068)	0.003	0.013
282	23.50	0.07	0.016	(0.068)	0.003	0.013
283	23.58	0.07	0.016	(0.067)	0.003	0.013
284	23.67	0.07	0.016	(0.067)	0.003	0.013
285	23.75	0.07	0.016	(0.067)	0.003	0.013
286	23.83	0.07	0.016	(0.067)	0.003	0.013
287	23.92	0.07	0.016	(0.067)	0.003	0.013
288	24.00	0.07	0.016	(0.067)	0.003	0.013

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.7

Flood volume = Effective rainfall 1.64(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.7(Ac.Ft)
Total soil loss = 0.36(In)
Total soil loss = 0.159(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 31611.2 Cubic Feet
Total soil loss = 6939.0 Cubic Feet

Peak flow rate of this hydrograph = 1.194(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0003	0.04	Q	|	|	|	|
0+10	0.0007	0.07	Q	|	|	|	|
0+15	0.0012	0.07	Q	|	|	|	|
0+20	0.0018	0.09	Q	|	|	|	|
0+25	0.0026	0.10	Q	|	|	|	|
0+30	0.0033	0.11	Q	|	|	|	|
0+35	0.0040	0.11	Q	|	|	|	|
0+40	0.0047	0.11	Q	|	|	|	|
0+45	0.0055	0.11	Q	|	|	|	|
0+50	0.0063	0.13	Q	|	|	|	|
0+55	0.0073	0.14	Q	|	|	|	|
1+ 0	0.0082	0.14	Q	|	|	|	|
1+ 5	0.0091	0.12	Q	|	|	|	|
1+10	0.0098	0.11	Q	|	|	|	|
1+15	0.0105	0.11	Q	|	|	|	|
1+20	0.0113	0.11	Q	|	|	|	|
1+25	0.0120	0.11	Q	|	|	|	|
1+30	0.0127	0.11	Q	|	|	|	|
1+35	0.0134	0.11	Q	|	|	|	|
1+40	0.0142	0.11	Q	|	|	|	|

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1+45       0.0149      0.11  Q         |          |          |          |
1+50       0.0158      0.13  Q         |          |          |          |
1+55       0.0167      0.14  Q         |          |          |          |
2+ 0       0.0177      0.14  Q         |          |          |          |
2+ 5       0.0186      0.14  QV        |          |          |          |
2+10       0.0196      0.14  QV        |          |          |          |
2+15       0.0206      0.14  QV        |          |          |          |
2+20       0.0215      0.14  QV        |          |          |          |
2+25       0.0225      0.14  QV        |          |          |          |
2+30       0.0235      0.14  QV        |          |          |          |
2+35       0.0246      0.16  QV        |          |          |          |
2+40       0.0258      0.17  QV        |          |          |          |
2+45       0.0270      0.18  QV        |          |          |          |
2+50       0.0282      0.18  QV        |          |          |          |
2+55       0.0294      0.18  QV        |          |          |          |
3+ 0       0.0306      0.18  QV        |          |          |          |
3+ 5       0.0318      0.18  QV        |          |          |          |
3+10       0.0330      0.18  QV        |          |          |          |
3+15       0.0343      0.18  QV        |          |          |          |
3+20       0.0355      0.18  QV        |          |          |          |
3+25       0.0367      0.18  Q V       |          |          |          |
3+30       0.0379      0.18  Q V       |          |          |          |
3+35       0.0391      0.18  Q V       |          |          |          |
3+40       0.0403      0.18  Q V       |          |          |          |
3+45       0.0415      0.18  Q V       |          |          |          |
3+50       0.0429      0.20  Q V       |          |          |          |
3+55       0.0443      0.21  Q V       |          |          |          |
4+ 0       0.0457      0.21  Q V       |          |          |          |
4+ 5       0.0472      0.21  Q V       |          |          |          |
4+10       0.0487      0.21  Q V       |          |          |          |
4+15       0.0501      0.21  Q V       |          |          |          |
4+20       0.0517      0.23  Q V       |          |          |          |
4+25       0.0534      0.24  Q V       |          |          |          |
4+30       0.0551      0.25  Q  V      |          |          |          |
4+35       0.0568      0.25  Q  V      |          |          |          |
4+40       0.0585      0.25  Q  V      |          |          |          |
4+45       0.0601      0.25  Q  V      |          |          |          |
4+50       0.0620      0.27  |Q V      |          |          |          |
4+55       0.0639      0.28  |Q V      |          |          |          |
5+ 0       0.0658      0.28  |Q V      |          |          |          |
5+ 5       0.0675      0.24  Q  V      |          |          |          |
5+10       0.0690      0.21  Q  V      |          |          |          |
5+15       0.0704      0.21  Q  V      |          |          |          |
5+20       0.0720      0.23  Q  V      |          |          |          |
5+25       0.0737      0.24  Q   V     |          |          |          |
5+30       0.0754      0.25  Q   V     |          |          |          |
5+35       0.0772      0.27  |Q  V     |          |          |          |
5+40       0.0791      0.28  |Q  V     |          |          |          |
5+45       0.0811      0.28  |Q  V     |          |          |          |
5+50       0.0830      0.28  |Q  V     |          |          |          |
5+55       0.0849      0.28  |Q  V     |          |          |          |
6+ 0       0.0869      0.28  |Q  V     |          |          |          |
6+ 5       0.0890      0.30  |Q  V     |          |          |          |
6+10       0.0911      0.31  |Q   V    |          |          |          |
6+15       0.0933      0.32  |Q   V    |          |          |          |
6+20       0.0955      0.32  |Q   V    |          |          |          |
6+25       0.0977      0.32  |Q   V    |          |          |          |
6+30       0.0998      0.32  |Q   V    |          |          |          |
6+35       0.1021      0.34  |Q   V    |          |          |          |
6+40       0.1046      0.35  |Q   V    |          |          |          |
6+45       0.1070      0.35  |Q   V    |          |          |          |
6+50       0.1094      0.35  |Q    V   |          |          |          |
6+55       0.1118      0.35  |Q    V   |          |          |          |
7+ 0       0.1142      0.35  |Q    V   |          |          |          |
7+ 5       0.1166      0.35  |Q    V   |          |          |          |
7+10       0.1191      0.35  |Q    V   |          |          |          |
7+15       0.1215      0.35  |Q    V   |          |          |          |
7+20       0.1240      0.37  |Q    V   |          |          |          |
7+25       0.1267      0.38  |Q    V   |          |          |          |
7+30       0.1294      0.39  |Q     V  |          |          |          |
7+35       0.1322      0.41  |Q     V  |          |          |          |
7+40       0.1350      0.42  |Q     V  |          |          |          |
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7+45	0.1379	0.42	Q	V			
7+50	0.1410	0.44	Q	V			
7+55	0.1441	0.45	Q	V			
8+ 0	0.1473	0.46	Q	V			
8+ 5	0.1507	0.50	Q	V			
8+10	0.1543	0.52	Q	V			
8+15	0.1579	0.53	Q	V			
8+20	0.1615	0.53	Q	V			
8+25	0.1652	0.53	Q	V			
8+30	0.1688	0.53	Q	V			
8+35	0.1726	0.55	Q	V			
8+40	0.1764	0.56	Q	V			
8+45	0.1803	0.56	Q	V			
8+50	0.1843	0.58	Q	V			
8+55	0.1884	0.60	Q	V			
9+ 0	0.1925	0.60	Q	V			
9+ 5	0.1969	0.64	Q	V			
9+10	0.2015	0.66	Q	V			
9+15	0.2061	0.67	Q	V			
9+20	0.2108	0.69	Q	V			
9+25	0.2156	0.70	Q	V			
9+30	0.2205	0.70	Q	V			
9+35	0.2255	0.72	Q	V			
9+40	0.2305	0.74	Q	V			
9+45	0.2356	0.74	Q	V			
9+50	0.2408	0.76	Q	V			
9+55	0.2461	0.77	Q	V			
10+ 0	0.2514	0.77	Q	V			
10+ 5	0.2558	0.63	Q	V			
10+10	0.2595	0.54	Q	V			
10+15	0.2631	0.53	Q	V			
10+20	0.2668	0.53	Q	V			
10+25	0.2704	0.53	Q	V			
10+30	0.2740	0.53	Q	V			
10+35	0.2784	0.63	Q	V			
10+40	0.2831	0.69	Q	V			
10+45	0.2880	0.70	Q	V			
10+50	0.2928	0.70	Q	V			
10+55	0.2976	0.70	Q	V			
11+ 0	0.3025	0.70	Q	V			
11+ 5	0.3072	0.68	Q	V			
11+10	0.3118	0.67	Q	V			
11+15	0.3164	0.67	Q	V			
11+20	0.3210	0.67	Q	V			
11+25	0.3256	0.67	Q	V			
11+30	0.3302	0.67	Q	V			
11+35	0.3345	0.63	Q	V			
11+40	0.3386	0.60	Q	V			
11+45	0.3427	0.60	Q	V			
11+50	0.3470	0.62	Q	V			
11+55	0.3513	0.63	Q	V			
12+ 0	0.3557	0.63	Q	V			
12+ 5	0.3610	0.77	Q	V			
12+10	0.3670	0.86	Q	V			
12+15	0.3730	0.88	Q	V			
12+20	0.3792	0.90	Q	V			
12+25	0.3855	0.91	Q	V			
12+30	0.3918	0.91	Q	V			
12+35	0.3983	0.95	Q	V			
12+40	0.4051	0.98	Q	V			
12+45	0.4119	0.98	Q	V			
12+50	0.4188	1.00	Q	V			
12+55	0.4258	1.02	Q	V			
13+ 0	0.4328	1.02	Q	V			
13+ 5	0.4405	1.12	Q	V			
13+10	0.4487	1.18	Q	V			
13+15	0.4569	1.19	Q	V			
13+20	0.4651	1.19	Q	V			
13+25	0.4733	1.19	Q	V			
13+30	0.4816	1.19	Q	V			
13+35	0.4882	0.97	Q	V			
13+40	0.4940	0.83	Q	V			

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13+45       0.4995      0.81  |  Q       |          |       V  |          |
13+50       0.5051      0.81  |  Q       |          |       V  |          |
13+55       0.5106      0.81  |  Q       |          |        V |          |
14+ 0       0.5162      0.81  |  Q       |          |        V |          |
14+ 5       0.5223      0.89  |  Q       |          |        V |          |
14+10       0.5288      0.94  |  Q       |          |         V|          |
14+15       0.5353      0.95  |  Q       |          |         V|          |
14+20       0.5417      0.93  |  Q       |          |         V|          |
14+25       0.5480      0.92  |  Q       |          |          V          |
14+30       0.5543      0.91  |  Q       |          |          V          |
14+35       0.5606      0.91  |  Q       |          |          V          |
14+40       0.5669      0.91  |  Q       |          |          |V         |
14+45       0.5732      0.91  |  Q       |          |          |V         |
14+50       0.5793      0.89  |  Q       |          |          |V         |
14+55       0.5854      0.88  |  Q       |          |          | V        |
15+ 0       0.5914      0.88  |  Q       |          |          | V        |
15+ 5       0.5974      0.86  |  Q       |          |          | V        |
15+10       0.6032      0.84  |  Q       |          |          |  V       |
15+15       0.6090      0.84  |  Q       |          |          |  V       |
15+20       0.6146      0.82  |  Q       |          |          |  V       |
15+25       0.6202      0.81  |  Q       |          |          |   V      |
15+30       0.6258      0.81  |  Q       |          |          |   V      |
15+35       0.6308      0.73  | Q        |          |          |   V      |
15+40       0.6354      0.68  | Q        |          |          |    V     |
15+45       0.6400      0.67  | Q        |          |          |    V     |
15+50       0.6446      0.67  | Q        |          |          |    V     |
15+55       0.6492      0.67  | Q        |          |          |    V     |
16+ 0       0.6538      0.67  | Q        |          |          |     V    |
16+ 5       0.6563      0.36  |Q         |          |          |     V    |
16+10       0.6575      0.17  Q          |          |          |     V    |
16+15       0.6585      0.14  Q          |          |          |     V    |
16+20       0.6594      0.14  Q          |          |          |     V    |
16+25       0.6604      0.14  Q          |          |          |     V    |
16+30       0.6614      0.14  Q          |          |          |     V    |
16+35       0.6622      0.12  Q          |          |          |     V    |
16+40       0.6629      0.11  Q          |          |          |     V    |
16+45       0.6637      0.11  Q          |          |          |     V    |
16+50       0.6644      0.11  Q          |          |          |     V    |
16+55       0.6651      0.11  Q          |          |          |     V    |
17+ 0       0.6658      0.11  Q          |          |          |     V    |
17+ 5       0.6668      0.15  Q          |          |          |     V    |
17+10       0.6680      0.17  Q          |          |          |     V    |
17+15       0.6692      0.18  Q          |          |          |     V    |
17+20       0.6704      0.18  Q          |          |          |     V    |
17+25       0.6717      0.18  Q          |          |          |      V   |
17+30       0.6729      0.18  Q          |          |          |      V   |
17+35       0.6741      0.18  Q          |          |          |      V   |
17+40       0.6753      0.18  Q          |          |          |      V   |
17+45       0.6765      0.18  Q          |          |          |      V   |
17+50       0.6776      0.16  Q          |          |          |      V   |
17+55       0.6785      0.14  Q          |          |          |      V   |
18+ 0       0.6795      0.14  Q          |          |          |      V   |
18+ 5       0.6805      0.14  Q          |          |          |      V   |
18+10       0.6814      0.14  Q          |          |          |      V   |
18+15       0.6824      0.14  Q          |          |          |      V   |
18+20       0.6834      0.14  Q          |          |          |      V   |
18+25       0.6843      0.14  Q          |          |          |      V   |
18+30       0.6853      0.14  Q          |          |          |      V   |
18+35       0.6861      0.12  Q          |          |          |      V   |
18+40       0.6869      0.11  Q          |          |          |      V   |
18+45       0.6876      0.11  Q          |          |          |      V   |
18+50       0.6882      0.09  Q          |          |          |      V   |
18+55       0.6887      0.07  Q          |          |          |      V   |
19+ 0       0.6892      0.07  Q          |          |          |      V   |
19+ 5       0.6898      0.09  Q          |          |          |       V  |
19+10       0.6905      0.10  Q          |          |          |       V  |
19+15       0.6912      0.11  Q          |          |          |       V  |
19+20       0.6921      0.13  Q          |          |          |       V  |
19+25       0.6931      0.14  Q          |          |          |       V  |
19+30       0.6940      0.14  Q          |          |          |       V  |
19+35       0.6949      0.12  Q          |          |          |       V  |
19+40       0.6956      0.11  Q          |          |          |       V  |
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  19+45       0.6963      0.11  Q          |           |           |        V |
  19+50       0.6969      0.09  Q          |           |           |        V |
  19+55       0.6974      0.07  Q          |           |           |        V |
  20+ 0       0.6979      0.07  Q          |           |           |        V |
  20+ 5       0.6985      0.09  Q          |           |           |        V |
  20+10       0.6992      0.10  Q          |           |           |        V |
  20+15       0.6999      0.11  Q          |           |           |        V |
  20+20       0.7007      0.11  Q          |           |           |        V |
  20+25       0.7014      0.11  Q          |           |           |        V |
  20+30       0.7021      0.11  Q          |           |           |        V |
  20+35       0.7028      0.11  Q          |           |           |        V |
  20+40       0.7036      0.11  Q          |           |           |        V |
  20+45       0.7043      0.11  Q          |           |           |        V |
  20+50       0.7049      0.09  Q          |           |           |        V |
  20+55       0.7054      0.07  Q          |           |           |        V |
  21+ 0       0.7059      0.07  Q          |           |           |        V |
  21+ 5       0.7065      0.09  Q          |           |           |        V |
  21+10       0.7072      0.10  Q          |           |           |        V |
  21+15       0.7079      0.11  Q          |           |           |         V|
  21+20       0.7085      0.09  Q          |           |           |         V|
  21+25       0.7090      0.07  Q          |           |           |         V|
  21+30       0.7095      0.07  Q          |           |           |         V|
  21+35       0.7101      0.09  Q          |           |           |         V|
  21+40       0.7108      0.10  Q          |           |           |         V|
  21+45       0.7116      0.11  Q          |           |           |         V|
  21+50       0.7121      0.09  Q          |           |           |         V|
  21+55       0.7126      0.07  Q          |           |           |         V|
  22+ 0       0.7131      0.07  Q          |           |           |         V|
  22+ 5       0.7137      0.09  Q          |           |           |         V|
  22+10       0.7145      0.10  Q          |           |           |         V|
  22+15       0.7152      0.11  Q          |           |           |         V|
  22+20       0.7158      0.09  Q          |           |           |         V|
  22+25       0.7163      0.07  Q          |           |           |         V|
  22+30       0.7168      0.07  Q          |           |           |         V|
  22+35       0.7172      0.07  Q          |           |           |         V|
  22+40       0.7177      0.07  Q          |           |           |         V|
  22+45       0.7182      0.07  Q          |           |           |         V|
  22+50       0.7187      0.07  Q          |           |           |         V|
  22+55       0.7192      0.07  Q          |           |           |         V|
  23+ 0       0.7197      0.07  Q          |           |           |         V|
  23+ 5       0.7201      0.07  Q          |           |           |         V|
  23+10       0.7206      0.07  Q          |           |           |         V|
  23+15       0.7211      0.07  Q          |           |           |         V|
  23+20       0.7216      0.07  Q          |           |           |         V|
  23+25       0.7221      0.07  Q          |           |           |         V|
  23+30       0.7226      0.07  Q          |           |           |         V|
  23+35       0.7230      0.07  Q          |           |           |         V|
  23+40       0.7235      0.07  Q          |           |           |         V|
  23+45       0.7240      0.07  Q          |           |           |         V|
  23+50       0.7245      0.07  Q          |           |           |         V|
  23+55       0.7250      0.07  Q          |           |           |         V|
  24+ 0       0.7255      0.07  Q          |           |           |         V|
  24+ 5       0.7257      0.03  Q          |           |           |         V|
  24+10       0.7257      0.00  Q          |           |           |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA0262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	1.20	6.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	3.00	15.93

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.200(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.50	0.072	(0.134)		0.013	0.059
2	0.17	0.60	0.086	(0.134)		0.016	0.071
3	0.25	0.60	0.086	(0.134)		0.016	0.071
4	0.33	0.60	0.086	(0.134)		0.016	0.071
5	0.42	0.60	0.086	(0.134)		0.016	0.071
6	0.50	0.70	0.101	(0.134)		0.018	0.083
7	0.58	0.70	0.101	(0.134)		0.018	0.083
8	0.67	0.70	0.101	(0.134)		0.018	0.083
9	0.75	0.70	0.101	(0.134)		0.018	0.083
10	0.83	0.70	0.101	(0.134)		0.018	0.083
11	0.92	0.70	0.101	(0.134)		0.018	0.083
12	1.00	0.80	0.115	(0.134)		0.021	0.094
13	1.08	0.80	0.115	(0.134)		0.021	0.094
14	1.17	0.80	0.115	(0.134)		0.021	0.094
15	1.25	0.80	0.115	(0.134)		0.021	0.094
16	1.33	0.80	0.115	(0.134)		0.021	0.094
17	1.42	0.80	0.115	(0.134)		0.021	0.094
18	1.50	0.80	0.115	(0.134)		0.021	0.094
19	1.58	0.80	0.115	(0.134)		0.021	0.094
20	1.67	0.80	0.115	(0.134)		0.021	0.094
21	1.75	0.80	0.115	(0.134)		0.021	0.094
22	1.83	0.80	0.115	(0.134)		0.021	0.094
23	1.92	0.80	0.115	(0.134)		0.021	0.094
24	2.00	0.90	0.130	(0.134)		0.023	0.106
25	2.08	0.80	0.115	(0.134)		0.021	0.094
26	2.17	0.90	0.130	(0.134)		0.023	0.106
27	2.25	0.90	0.130	(0.134)		0.023	0.106
28	2.33	0.90	0.130	(0.134)		0.023	0.106
29	2.42	0.90	0.130	(0.134)		0.023	0.106
30	2.50	0.90	0.130	(0.134)		0.023	0.106
31	2.58	0.90	0.130	(0.134)		0.023	0.106
32	2.67	0.90	0.130	(0.134)		0.023	0.106
33	2.75	1.00	0.144	(0.134)		0.026	0.118
34	2.83	1.00	0.144	(0.134)		0.026	0.118
35	2.92	1.00	0.144	(0.134)		0.026	0.118
36	3.00	1.00	0.144	(0.134)		0.026	0.118
37	3.08	1.00	0.144	(0.134)		0.026	0.118
38	3.17	1.10	0.158	(0.134)		0.029	0.130
39	3.25	1.10	0.158	(0.134)		0.029	0.130
40	3.33	1.10	0.158	(0.134)		0.029	0.130
41	3.42	1.20	0.173	(0.134)		0.031	0.142

42	3.50	1.30	0.187	(	0.134)	0.034	0.154
43	3.58	1.40	0.202	(	0.134)	0.036	0.165
44	3.67	1.40	0.202	(	0.134)	0.036	0.165
45	3.75	1.50	0.216	(	0.134)	0.039	0.177
46	3.83	1.50	0.216	(	0.134)	0.039	0.177
47	3.92	1.60	0.230	(	0.134)	0.041	0.189
48	4.00	1.60	0.230	(	0.134)	0.041	0.189
49	4.08	1.70	0.245	(	0.134)	0.044	0.201
50	4.17	1.80	0.259	(	0.134)	0.047	0.213
51	4.25	1.90	0.274	(	0.134)	0.049	0.224
52	4.33	2.00	0.288	(	0.134)	0.052	0.236
53	4.42	2.10	0.302	(	0.134)	0.054	0.248
54	4.50	2.10	0.302	(	0.134)	0.054	0.248
55	4.58	2.20	0.317	(	0.134)	0.057	0.260
56	4.67	2.30	0.331	(	0.134)	0.060	0.272
57	4.75	2.40	0.346	(	0.134)	0.062	0.283
58	4.83	2.40	0.346	(	0.134)	0.062	0.283
59	4.92	2.50	0.360	(	0.134)	0.065	0.295
60	5.00	2.60	0.374	(	0.134)	0.067	0.307
61	5.08	3.10	0.446	(	0.134)	0.080	0.366
62	5.17	3.60	0.518	(	0.134)	0.093	0.425
63	5.25	3.90	0.562	(	0.134)	0.101	0.461
64	5.33	4.20	0.605	(	0.134)	0.109	0.496
65	5.42	4.70	0.677	(	0.134)	0.122	0.555
66	5.50	5.60	0.806		0.134	(0.145)	0.672
67	5.58	1.90	0.274	(	0.134)	0.049	0.224
68	5.67	0.90	0.130	(	0.134)	0.023	0.106
69	5.75	0.60	0.086	(	0.134)	0.016	0.071
70	5.83	0.50	0.072	(	0.134)	0.013	0.059
71	5.92	0.30	0.043	(	0.134)	0.008	0.035
72	6.00	0.20	0.029	(	0.134)	0.005	0.024

(Loss Rate Not Used)

Sum = 100.0 Sum = 11.8

Flood volume = Effective rainfall 0.98(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.22(In)
Total soil loss = 0.095(Ac.Ft)
Total rainfall = 1.20(In)
Flood volume = 18984.2 Cubic Feet
Total soil loss = 4145.7 Cubic Feet

Peak flow rate of this hydrograph = 3.317(CFS)

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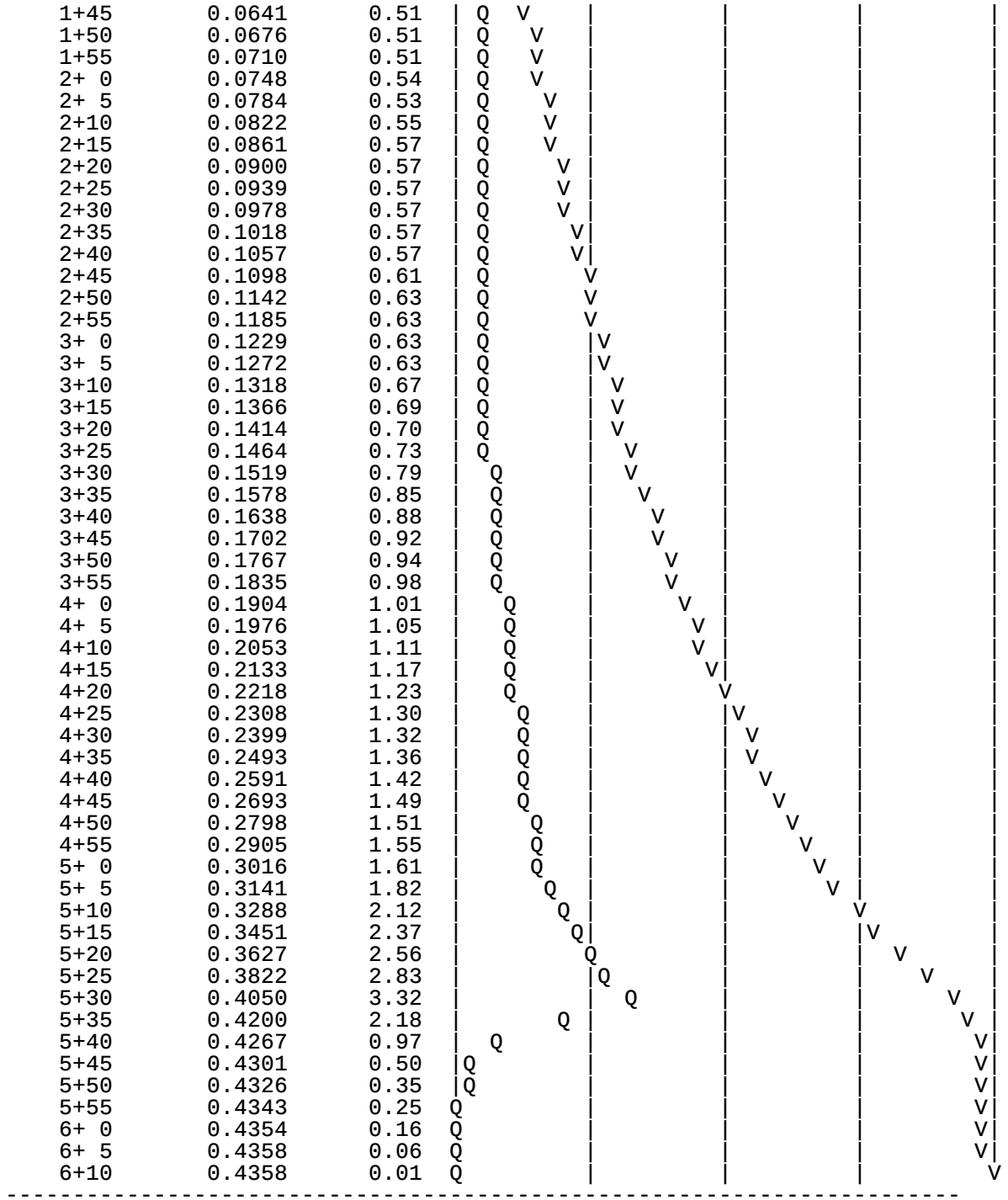
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0013	0.18	Q				
0+10	0.0036	0.33	VQ				
0+15	0.0062	0.38	VQ				
0+20	0.0088	0.38	VQ				
0+25	0.0114	0.38	|Q				
0+30	0.0142	0.42	|Q				
0+35	0.0173	0.44	|Q				
0+40	0.0203	0.44	|Q				
0+45	0.0234	0.44	|QV				
0+50	0.0264	0.44	|QV				
0+55	0.0295	0.44	|QV				
1+ 0	0.0328	0.48	|Q V				
1+ 5	0.0362	0.50	| QV				
1+10	0.0397	0.51	| QV				
1+15	0.0432	0.51	| QV				
1+20	0.0467	0.51	| Q V				
1+25	0.0501	0.51	| Q V				
1+30	0.0536	0.51	| Q V				
1+35	0.0571	0.51	| Q V				
1+40	0.0606	0.51	| Q V				


1+45 0.0641 0.51
1+50 0.0676 0.51
1+55 0.0710 0.51
2+ 0 0.0748 0.54
2+ 5 0.0784 0.53
2+10 0.0822 0.55
2+15 0.0861 0.57
2+20 0.0900 0.57
2+25 0.0939 0.57
2+30 0.0978 0.57
2+35 0.1018 0.57
2+40 0.1057 0.57
2+45 0.1098 0.61
2+50 0.1142 0.63
2+55 0.1185 0.63
3+ 0 0.1229 0.63
3+ 5 0.1272 0.63
3+10 0.1318 0.67
3+15 0.1366 0.69
3+20 0.1414 0.70
3+25 0.1464 0.73
3+30 0.1519 0.79
3+35 0.1578 0.85
3+40 0.1638 0.88
3+45 0.1702 0.92
3+50 0.1767 0.94
3+55 0.1835 0.98
4+ 0 0.1904 1.01
4+ 5 0.1976 1.05
4+10 0.2053 1.11
4+15 0.2133 1.17
4+20 0.2218 1.23
4+25 0.2308 1.30
4+30 0.2399 1.32
4+35 0.2493 1.36
4+40 0.2591 1.42
4+45 0.2693 1.49
4+50 0.2798 1.51
4+55 0.2905 1.55
5+ 0 0.3016 1.61
5+ 5 0.3141 1.82
5+10 0.3288 2.12
5+15 0.3451 2.37
5+20 0.3627 2.56
5+25 0.3822 2.83
5+30 0.4050 3.32
5+35 0.4200 2.18
5+40 0.4267 0.97
5+45 0.4301 0.50
5+50 0.4326 0.35
5+55 0.4343 0.25
6+ 0 0.4354 0.16
6+ 5 0.4358 0.06
6+10 0.4358 0.01

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA0232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	0.90	4.78

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	2.35	12.48

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 0.900(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.900(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.140	(0.134)	0.025	0.115
2	0.17	1.30	0.140	(0.134)	0.025	0.115
3	0.25	1.10	0.119	(0.134)	0.021	0.097
4	0.33	1.50	0.162	(0.134)	0.029	0.133
5	0.42	1.50	0.162	(0.134)	0.029	0.133
6	0.50	1.80	0.194	(0.134)	0.035	0.159
7	0.58	1.50	0.162	(0.134)	0.029	0.133
8	0.67	1.80	0.194	(0.134)	0.035	0.159
9	0.75	1.80	0.194	(0.134)	0.035	0.159
10	0.83	1.50	0.162	(0.134)	0.029	0.133
11	0.92	1.60	0.173	(0.134)	0.031	0.142
12	1.00	1.80	0.194	(0.134)	0.035	0.159
13	1.08	2.20	0.238	(0.134)	0.043	0.195
14	1.17	2.20	0.238	(0.134)	0.043	0.195
15	1.25	2.20	0.238	(0.134)	0.043	0.195
16	1.33	2.00	0.216	(0.134)	0.039	0.177
17	1.42	2.60	0.281	(0.134)	0.051	0.230
18	1.50	2.70	0.292	(0.134)	0.052	0.239
19	1.58	2.40	0.259	(0.134)	0.047	0.213
20	1.67	2.70	0.292	(0.134)	0.052	0.239
21	1.75	3.30	0.356	(0.134)	0.064	0.292
22	1.83	3.10	0.335	(0.134)	0.060	0.275
23	1.92	2.90	0.313	(0.134)	0.056	0.257
24	2.00	3.00	0.324	(0.134)	0.058	0.266
25	2.08	3.10	0.335	(0.134)	0.060	0.275
26	2.17	4.20	0.454	(0.134)	0.082	0.372
27	2.25	5.00	0.540	(0.134)	0.097	0.443
28	2.33	3.50	0.378	(0.134)	0.068	0.310
29	2.42	6.80	0.734	(0.134)	0.132	0.602
30	2.50	7.30	0.788	0.134	(0.142)	0.654
31	2.58	8.20	0.886	0.134	(0.159)	0.751
32	2.67	5.90	0.637	(0.134)	0.115	0.522
33	2.75	2.00	0.216	(0.134)	0.039	0.177
34	2.83	1.80	0.194	(0.134)	0.035	0.159
35	2.92	1.80	0.194	(0.134)	0.035	0.159
36	3.00	0.60	0.065	(0.134)	0.012	0.053
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.9

Flood volume = Effective rainfall 0.74(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.16(In)

Total soil loss = 0.070(Ac.Ft)
Total rainfall = 0.90(In)
Flood volume = 14277.9 Cubic Feet
Total soil loss = 3069.5 Cubic Feet

Peak flow rate of this hydrograph = 3.788(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0025	0.36	VQ
0+10	0.0065	0.58	V Q
0+15	0.0103	0.56	|VQ
0+20	0.0147	0.64	|VQ
0+25	0.0195	0.70	| Q
0+30	0.0250	0.79	| Q
0+35	0.0303	0.76	| Q
0+40	0.0358	0.80	| QV
0+45	0.0416	0.85	| Q V
0+50	0.0469	0.77	| Q V
0+55	0.0521	0.75	| Q V
1+ 0	0.0576	0.81	| Q V
1+ 5	0.0642	0.96	| Q V
1+10	0.0713	1.03	| Q V
1+15	0.0785	1.04	| Q V|
1+20	0.0853	0.99	| Q V
1+25	0.0930	1.12	| Q |V
1+30	0.1016	1.24	| Q | V
1+35	0.1098	1.20	| Q | V
1+40	0.1183	1.23	| Q | V
1+45	0.1282	1.44	| Q | V
1+50	0.1385	1.49	| Q | V
1+55	0.1483	1.42	| Q | V
2+ 0	0.1580	1.41	| Q | V|
2+ 5	0.1679	1.45	| Q | V
2+10	0.1801	1.77	| Q | |V
2+15	0.1951	2.18	| Q | V
2+20	0.2085	1.94	| Q | V
2+25	0.2264	2.60	| Q V |
2+30	0.2491	3.30	| | Q | V
2+35	0.2752	3.79	| | Q | V
2+40	0.2978	3.29	| | Q | V
2+45	0.3102	1.80	| Q | V
2+50	0.3171	1.00	| Q | V
2+55	0.3230	0.86	| Q | V|
3+ 0	0.3266	0.52	| Q | V|
3+ 5	0.3277	0.15	Q | V|
3+10	0.3278	0.02	Q | V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA0212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	0.54	2.87

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	1.36	7.22

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.540(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.540(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

```
      RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
      AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
      56.0  36.0      0.706     0.900        0.134       1.000      0.134
                                                       Sum (F) =   0.134
      Area averaged mean soil loss (F) (In/Hr) =  0.134
      Minimum soil loss rate ((In/Hr)) =  0.067
      (for 24 hour storm duration)
      Soil low loss rate (decimal) =   0.180
      ------------------------------------------------------------------------
      Slope of intensity-duration curve for a 1 hour storm =0.4800
      ------------------------------------------------------------------------

                    U n i t  H y d r o g r a p h
                           VALLEY S-Curve
      ------------------------------------------------------------------------
                    Unit Hydrograph Data
      ------------------------------------------------------------------------
      Unit time period   Time % of lag   Distribution   Unit Hydrograph
          (hrs)                          Graph %           (CFS)
      ------------------------------------------------------------------------
          1   0.083        311.341         57.815             3.094
          2   0.167        622.682         36.513             1.954
          3   0.250        934.022          5.672             0.304
                                   Sum = 100.000   Sum=       5.351
-------------------------------------------------------------------------------


 The following loss rate calculations reflect use of the minimum calculated loss
 rate subtracted from the Storm Rain to produce the maximum Effective Rain value

  Unit Time   Pattern   Storm Rain     Loss rate(In./Hr)     Effective
       (Hr.)  Percent   (In/Hr)         Max   |   Low         (In/Hr)
   1   0.08     4.40      0.285       (  0.134)       0.051        0.234
   2   0.17     4.50      0.292       (  0.134)       0.052        0.239
   3   0.25     5.40      0.350       (  0.134)       0.063        0.287
   4   0.33     5.40      0.350       (  0.134)       0.063        0.287
   5   0.42     5.70      0.369       (  0.134)       0.066        0.303
   6   0.50     6.40      0.415       (  0.134)       0.075        0.340
   7   0.58     7.90      0.512       (  0.134)       0.092        0.420
   8   0.67     9.10      0.590       (  0.134)       0.106        0.484
   9   0.75    12.80      0.829          0.134    (  0.149)       0.695
  10   0.83    25.60      1.659          0.134    (  0.299)       1.525
  11   0.92     7.90      0.512       (  0.134)       0.092        0.420
  12   1.00     4.90      0.318       (  0.134)       0.057        0.260
               (Loss Rate Not Used)
     Sum =     100.0                                  Sum =     5.5
       Flood volume = Effective rainfall      0.46(In)
        times area       5.3(Ac.)/[(In)/(Ft.)] =       0.2(Ac.Ft)
       Total soil loss =      0.08(In)
       Total soil loss =     0.036(Ac.Ft)
       Total rainfall =      0.54(In)
       Flood volume =        8823.2 Cubic Feet
       Total soil loss =        1585.0 Cubic Feet
       ---------------------------------------------------------------------
        Peak flow rate of this hydrograph =      6.226(CFS)
       ---------------------------------------------------------------------
       +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          1 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
       ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

       ---------------------------------------------------------------------
  Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
  ----------------------------------------------------------------------
    0+ 5       0.0050      0.72  V Q       |         |         |         |
    0+10       0.0132      1.20  | V Q     |         |         |         |
    0+15       0.0231      1.43  |   VQ    |         |         |         |
    0+20       0.0335      1.52  |     Q   |         |         |         |
    0+25       0.0445      1.59  |     Q V |         |         |         |
    0+30       0.0564      1.73  |     Q   |V        |         |         |
```

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   0+35       0.0705      2.06  |        Q |  V       |          |          |
   0+40       0.0872      2.42  |         Q|       V  |          |          |
   0+45       0.1094      3.22  |          | Q        |V         |          |
   0+50       0.1523      6.23  |          |          |   Q      V          |
   0+55       0.1832      4.49  |          |       Q  |          |     V    |
   1+ 0       0.1976      2.09  |        Q |          |          |          V|
   1+ 5       0.2020      0.64  | Q        |          |          |          V|
   1+10       0.2026      0.08  Q          |          |          |           V
-------------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA05245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	2.00	10.62

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	6.40	33.98

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.031(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.031(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.024	(0.238)	0.004	0.020
2	0.17	0.07	0.024	(0.237)	0.004	0.020
3	0.25	0.07	0.024	(0.236)	0.004	0.020
4	0.33	0.10	0.036	(0.235)	0.007	0.030
5	0.42	0.10	0.036	(0.234)	0.007	0.030
6	0.50	0.10	0.036	(0.233)	0.007	0.030
7	0.58	0.10	0.036	(0.232)	0.007	0.030
8	0.67	0.10	0.036	(0.231)	0.007	0.030
9	0.75	0.10	0.036	(0.230)	0.007	0.030
10	0.83	0.13	0.048	(0.230)	0.009	0.040
11	0.92	0.13	0.048	(0.229)	0.009	0.040
12	1.00	0.13	0.048	(0.228)	0.009	0.040
13	1.08	0.10	0.036	(0.227)	0.007	0.030
14	1.17	0.10	0.036	(0.226)	0.007	0.030
15	1.25	0.10	0.036	(0.225)	0.007	0.030
16	1.33	0.10	0.036	(0.224)	0.007	0.030
17	1.42	0.10	0.036	(0.223)	0.007	0.030
18	1.50	0.10	0.036	(0.222)	0.007	0.030
19	1.58	0.10	0.036	(0.222)	0.007	0.030
20	1.67	0.10	0.036	(0.221)	0.007	0.030
21	1.75	0.10	0.036	(0.220)	0.007	0.030
22	1.83	0.13	0.048	(0.219)	0.009	0.040
23	1.92	0.13	0.048	(0.218)	0.009	0.040
24	2.00	0.13	0.048	(0.217)	0.009	0.040
25	2.08	0.13	0.048	(0.216)	0.009	0.040
26	2.17	0.13	0.048	(0.215)	0.009	0.040
27	2.25	0.13	0.048	(0.214)	0.009	0.040
28	2.33	0.13	0.048	(0.214)	0.009	0.040
29	2.42	0.13	0.048	(0.213)	0.009	0.040
30	2.50	0.13	0.048	(0.212)	0.009	0.040
31	2.58	0.17	0.061	(0.211)	0.011	0.050
32	2.67	0.17	0.061	(0.210)	0.011	0.050
33	2.75	0.17	0.061	(0.209)	0.011	0.050
34	2.83	0.17	0.061	(0.208)	0.011	0.050
35	2.92	0.17	0.061	(0.208)	0.011	0.050
36	3.00	0.17	0.061	(0.207)	0.011	0.050
37	3.08	0.17	0.061	(0.206)	0.011	0.050
38	3.17	0.17	0.061	(0.205)	0.011	0.050
39	3.25	0.17	0.061	(0.204)	0.011	0.050
40	3.33	0.17	0.061	(0.203)	0.011	0.050
41	3.42	0.17	0.061	(0.202)	0.011	0.050

42	3.50	0.17	0.061	(0.202)	0.011	0.050
43	3.58	0.17	0.061	(0.201)	0.011	0.050
44	3.67	0.17	0.061	(0.200)	0.011	0.050
45	3.75	0.17	0.061	(0.199)	0.011	0.050
46	3.83	0.20	0.073	(0.198)	0.013	0.060
47	3.92	0.20	0.073	(0.197)	0.013	0.060
48	4.00	0.20	0.073	(0.197)	0.013	0.060
49	4.08	0.20	0.073	(0.196)	0.013	0.060
50	4.17	0.20	0.073	(0.195)	0.013	0.060
51	4.25	0.20	0.073	(0.194)	0.013	0.060
52	4.33	0.23	0.085	(0.193)	0.015	0.070
53	4.42	0.23	0.085	(0.192)	0.015	0.070
54	4.50	0.23	0.085	(0.192)	0.015	0.070
55	4.58	0.23	0.085	(0.191)	0.015	0.070
56	4.67	0.23	0.085	(0.190)	0.015	0.070
57	4.75	0.23	0.085	(0.189)	0.015	0.070
58	4.83	0.27	0.097	(0.188)	0.017	0.080
59	4.92	0.27	0.097	(0.187)	0.017	0.080
60	5.00	0.27	0.097	(0.187)	0.017	0.080
61	5.08	0.20	0.073	(0.186)	0.013	0.060
62	5.17	0.20	0.073	(0.185)	0.013	0.060
63	5.25	0.20	0.073	(0.184)	0.013	0.060
64	5.33	0.23	0.085	(0.183)	0.015	0.070
65	5.42	0.23	0.085	(0.183)	0.015	0.070
66	5.50	0.23	0.085	(0.182)	0.015	0.070
67	5.58	0.27	0.097	(0.181)	0.017	0.080
68	5.67	0.27	0.097	(0.180)	0.017	0.080
69	5.75	0.27	0.097	(0.179)	0.017	0.080
70	5.83	0.27	0.097	(0.179)	0.017	0.080
71	5.92	0.27	0.097	(0.178)	0.017	0.080
72	6.00	0.27	0.097	(0.177)	0.017	0.080
73	6.08	0.30	0.109	(0.176)	0.020	0.089
74	6.17	0.30	0.109	(0.175)	0.020	0.089
75	6.25	0.30	0.109	(0.175)	0.020	0.089
76	6.33	0.30	0.109	(0.174)	0.020	0.089
77	6.42	0.30	0.109	(0.173)	0.020	0.089
78	6.50	0.30	0.109	(0.172)	0.020	0.089
79	6.58	0.33	0.121	(0.172)	0.022	0.099
80	6.67	0.33	0.121	(0.171)	0.022	0.099
81	6.75	0.33	0.121	(0.170)	0.022	0.099
82	6.83	0.33	0.121	(0.169)	0.022	0.099
83	6.92	0.33	0.121	(0.169)	0.022	0.099
84	7.00	0.33	0.121	(0.168)	0.022	0.099
85	7.08	0.33	0.121	(0.167)	0.022	0.099
86	7.17	0.33	0.121	(0.166)	0.022	0.099
87	7.25	0.33	0.121	(0.165)	0.022	0.099
88	7.33	0.37	0.133	(0.165)	0.024	0.109
89	7.42	0.37	0.133	(0.164)	0.024	0.109
90	7.50	0.37	0.133	(0.163)	0.024	0.109
91	7.58	0.40	0.145	(0.162)	0.026	0.119
92	7.67	0.40	0.145	(0.162)	0.026	0.119
93	7.75	0.40	0.145	(0.161)	0.026	0.119
94	7.83	0.43	0.158	(0.160)	0.028	0.129
95	7.92	0.43	0.158	(0.159)	0.028	0.129
96	8.00	0.43	0.158	(0.159)	0.028	0.129
97	8.08	0.50	0.182	(0.158)	0.033	0.149
98	8.17	0.50	0.182	(0.157)	0.033	0.149
99	8.25	0.50	0.182	(0.157)	0.033	0.149
100	8.33	0.50	0.182	(0.156)	0.033	0.149
101	8.42	0.50	0.182	(0.155)	0.033	0.149
102	8.50	0.50	0.182	(0.154)	0.033	0.149
103	8.58	0.53	0.194	(0.154)	0.035	0.159
104	8.67	0.53	0.194	(0.153)	0.035	0.159
105	8.75	0.53	0.194	(0.152)	0.035	0.159
106	8.83	0.57	0.206	(0.151)	0.037	0.169
107	8.92	0.57	0.206	(0.151)	0.037	0.169
108	9.00	0.57	0.206	(0.150)	0.037	0.169
109	9.08	0.63	0.230	(0.149)	0.041	0.189
110	9.17	0.63	0.230	(0.149)	0.041	0.189
111	9.25	0.63	0.230	(0.148)	0.041	0.189
112	9.33	0.67	0.242	(0.147)	0.044	0.199
113	9.42	0.67	0.242	(0.147)	0.044	0.199

114	9.50	0.67	0.242	(0.146)	0.044	0.199
115	9.58	0.70	0.255	(0.145)	0.046	0.209
116	9.67	0.70	0.255	(0.144)	0.046	0.209
117	9.75	0.70	0.255	(0.144)	0.046	0.209
118	9.83	0.73	0.267	(0.143)	0.048	0.219
119	9.92	0.73	0.267	(0.142)	0.048	0.219
120	10.00	0.73	0.267	(0.142)	0.048	0.219
121	10.08	0.50	0.182	(0.141)	0.033	0.149
122	10.17	0.50	0.182	(0.140)	0.033	0.149
123	10.25	0.50	0.182	(0.140)	0.033	0.149
124	10.33	0.50	0.182	(0.139)	0.033	0.149
125	10.42	0.50	0.182	(0.138)	0.033	0.149
126	10.50	0.50	0.182	(0.138)	0.033	0.149
127	10.58	0.67	0.242	(0.137)	0.044	0.199
128	10.67	0.67	0.242	(0.136)	0.044	0.199
129	10.75	0.67	0.242	(0.136)	0.044	0.199
130	10.83	0.67	0.242	(0.135)	0.044	0.199
131	10.92	0.67	0.242	(0.134)	0.044	0.199
132	11.00	0.67	0.242	(0.134)	0.044	0.199
133	11.08	0.63	0.230	(0.133)	0.041	0.189
134	11.17	0.63	0.230	(0.132)	0.041	0.189
135	11.25	0.63	0.230	(0.132)	0.041	0.189
136	11.33	0.63	0.230	(0.131)	0.041	0.189
137	11.42	0.63	0.230	(0.130)	0.041	0.189
138	11.50	0.63	0.230	(0.130)	0.041	0.189
139	11.58	0.57	0.206	(0.129)	0.037	0.169
140	11.67	0.57	0.206	(0.128)	0.037	0.169
141	11.75	0.57	0.206	(0.128)	0.037	0.169
142	11.83	0.60	0.218	(0.127)	0.039	0.179
143	11.92	0.60	0.218	(0.126)	0.039	0.179
144	12.00	0.60	0.218	(0.126)	0.039	0.179
145	12.08	0.83	0.303	(0.125)	0.055	0.249
146	12.17	0.83	0.303	(0.125)	0.055	0.249
147	12.25	0.83	0.303	(0.124)	0.055	0.249
148	12.33	0.87	0.315	(0.123)	0.057	0.258
149	12.42	0.87	0.315	(0.123)	0.057	0.258
150	12.50	0.87	0.315	(0.122)	0.057	0.258
151	12.58	0.93	0.339	(0.121)	0.061	0.278
152	12.67	0.93	0.339	(0.121)	0.061	0.278
153	12.75	0.93	0.339	(0.120)	0.061	0.278
154	12.83	0.97	0.352	(0.120)	0.063	0.288
155	12.92	0.97	0.352	(0.119)	0.063	0.288
156	13.00	0.97	0.352	(0.118)	0.063	0.288
157	13.08	1.13	0.412	(0.118)	0.074	0.338
158	13.17	1.13	0.412	(0.117)	0.074	0.338
159	13.25	1.13	0.412	(0.117)	0.074	0.338
160	13.33	1.13	0.412	(0.116)	0.074	0.338
161	13.42	1.13	0.412	(0.115)	0.074	0.338
162	13.50	1.13	0.412	(0.115)	0.074	0.338
163	13.58	0.77	0.279	(0.114)	0.050	0.229
164	13.67	0.77	0.279	(0.114)	0.050	0.229
165	13.75	0.77	0.279	(0.113)	0.050	0.229
166	13.83	0.77	0.279	(0.113)	0.050	0.229
167	13.92	0.77	0.279	(0.112)	0.050	0.229
168	14.00	0.77	0.279	(0.111)	0.050	0.229
169	14.08	0.90	0.327	(0.111)	0.059	0.268
170	14.17	0.90	0.327	(0.110)	0.059	0.268
171	14.25	0.90	0.327	(0.110)	0.059	0.268
172	14.33	0.87	0.315	(0.109)	0.057	0.258
173	14.42	0.87	0.315	(0.109)	0.057	0.258
174	14.50	0.87	0.315	(0.108)	0.057	0.258
175	14.58	0.87	0.315	(0.107)	0.057	0.258
176	14.67	0.87	0.315	(0.107)	0.057	0.258
177	14.75	0.87	0.315	(0.106)	0.057	0.258
178	14.83	0.83	0.303	(0.106)	0.055	0.249
179	14.92	0.83	0.303	(0.105)	0.055	0.249
180	15.00	0.83	0.303	(0.105)	0.055	0.249
181	15.08	0.80	0.291	(0.104)	0.052	0.239
182	15.17	0.80	0.291	(0.104)	0.052	0.239
183	15.25	0.80	0.291	(0.103)	0.052	0.239
184	15.33	0.77	0.279	(0.103)	0.050	0.229
185	15.42	0.77	0.279	(0.102)	0.050	0.229

186	15.50	0.77	0.279	(0.102)	0.050	0.229
187	15.58	0.63	0.230	(0.101)	0.041	0.189
188	15.67	0.63	0.230	(0.101)	0.041	0.189
189	15.75	0.63	0.230	(0.100)	0.041	0.189
190	15.83	0.63	0.230	(0.100)	0.041	0.189
191	15.92	0.63	0.230	(0.099)	0.041	0.189
192	16.00	0.63	0.230	(0.099)	0.041	0.189
193	16.08	0.13	0.048	(0.098)	0.009	0.040
194	16.17	0.13	0.048	(0.098)	0.009	0.040
195	16.25	0.13	0.048	(0.097)	0.009	0.040
196	16.33	0.13	0.048	(0.097)	0.009	0.040
197	16.42	0.13	0.048	(0.096)	0.009	0.040
198	16.50	0.13	0.048	(0.096)	0.009	0.040
199	16.58	0.10	0.036	(0.095)	0.007	0.030
200	16.67	0.10	0.036	(0.095)	0.007	0.030
201	16.75	0.10	0.036	(0.094)	0.007	0.030
202	16.83	0.10	0.036	(0.094)	0.007	0.030
203	16.92	0.10	0.036	(0.093)	0.007	0.030
204	17.00	0.10	0.036	(0.093)	0.007	0.030
205	17.08	0.17	0.061	(0.092)	0.011	0.050
206	17.17	0.17	0.061	(0.092)	0.011	0.050
207	17.25	0.17	0.061	(0.091)	0.011	0.050
208	17.33	0.17	0.061	(0.091)	0.011	0.050
209	17.42	0.17	0.061	(0.090)	0.011	0.050
210	17.50	0.17	0.061	(0.090)	0.011	0.050
211	17.58	0.17	0.061	(0.089)	0.011	0.050
212	17.67	0.17	0.061	(0.089)	0.011	0.050
213	17.75	0.17	0.061	(0.089)	0.011	0.050
214	17.83	0.13	0.048	(0.088)	0.009	0.040
215	17.92	0.13	0.048	(0.088)	0.009	0.040
216	18.00	0.13	0.048	(0.087)	0.009	0.040
217	18.08	0.13	0.048	(0.087)	0.009	0.040
218	18.17	0.13	0.048	(0.086)	0.009	0.040
219	18.25	0.13	0.048	(0.086)	0.009	0.040
220	18.33	0.13	0.048	(0.086)	0.009	0.040
221	18.42	0.13	0.048	(0.085)	0.009	0.040
222	18.50	0.13	0.048	(0.085)	0.009	0.040
223	18.58	0.10	0.036	(0.084)	0.007	0.030
224	18.67	0.10	0.036	(0.084)	0.007	0.030
225	18.75	0.10	0.036	(0.084)	0.007	0.030
226	18.83	0.07	0.024	(0.083)	0.004	0.020
227	18.92	0.07	0.024	(0.083)	0.004	0.020
228	19.00	0.07	0.024	(0.082)	0.004	0.020
229	19.08	0.10	0.036	(0.082)	0.007	0.030
230	19.17	0.10	0.036	(0.082)	0.007	0.030
231	19.25	0.10	0.036	(0.081)	0.007	0.030
232	19.33	0.13	0.048	(0.081)	0.009	0.040
233	19.42	0.13	0.048	(0.080)	0.009	0.040
234	19.50	0.13	0.048	(0.080)	0.009	0.040
235	19.58	0.10	0.036	(0.080)	0.007	0.030
236	19.67	0.10	0.036	(0.079)	0.007	0.030
237	19.75	0.10	0.036	(0.079)	0.007	0.030
238	19.83	0.07	0.024	(0.079)	0.004	0.020
239	19.92	0.07	0.024	(0.078)	0.004	0.020
240	20.00	0.07	0.024	(0.078)	0.004	0.020
241	20.08	0.10	0.036	(0.078)	0.007	0.030
242	20.17	0.10	0.036	(0.077)	0.007	0.030
243	20.25	0.10	0.036	(0.077)	0.007	0.030
244	20.33	0.10	0.036	(0.077)	0.007	0.030
245	20.42	0.10	0.036	(0.076)	0.007	0.030
246	20.50	0.10	0.036	(0.076)	0.007	0.030
247	20.58	0.10	0.036	(0.076)	0.007	0.030
248	20.67	0.10	0.036	(0.075)	0.007	0.030
249	20.75	0.10	0.036	(0.075)	0.007	0.030
250	20.83	0.07	0.024	(0.075)	0.004	0.020
251	20.92	0.07	0.024	(0.074)	0.004	0.020
252	21.00	0.07	0.024	(0.074)	0.004	0.020
253	21.08	0.10	0.036	(0.074)	0.007	0.030
254	21.17	0.10	0.036	(0.073)	0.007	0.030
255	21.25	0.10	0.036	(0.073)	0.007	0.030
256	21.33	0.07	0.024	(0.073)	0.004	0.020
257	21.42	0.07	0.024	(0.073)	0.004	0.020

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258  21.50     0.07      0.024       (  0.072)       0.004        0.020
259  21.58     0.10      0.036       (  0.072)       0.007        0.030
260  21.67     0.10      0.036       (  0.072)       0.007        0.030
261  21.75     0.10      0.036       (  0.072)       0.007        0.030
262  21.83     0.07      0.024       (  0.071)       0.004        0.020
263  21.92     0.07      0.024       (  0.071)       0.004        0.020
264  22.00     0.07      0.024       (  0.071)       0.004        0.020
265  22.08     0.10      0.036       (  0.071)       0.007        0.030
266  22.17     0.10      0.036       (  0.070)       0.007        0.030
267  22.25     0.10      0.036       (  0.070)       0.007        0.030
268  22.33     0.07      0.024       (  0.070)       0.004        0.020
269  22.42     0.07      0.024       (  0.070)       0.004        0.020
270  22.50     0.07      0.024       (  0.069)       0.004        0.020
271  22.58     0.07      0.024       (  0.069)       0.004        0.020
272  22.67     0.07      0.024       (  0.069)       0.004        0.020
273  22.75     0.07      0.024       (  0.069)       0.004        0.020
274  22.83     0.07      0.024       (  0.069)       0.004        0.020
275  22.92     0.07      0.024       (  0.069)       0.004        0.020
276  23.00     0.07      0.024       (  0.068)       0.004        0.020
277  23.08     0.07      0.024       (  0.068)       0.004        0.020
278  23.17     0.07      0.024       (  0.068)       0.004        0.020
279  23.25     0.07      0.024       (  0.068)       0.004        0.020
280  23.33     0.07      0.024       (  0.068)       0.004        0.020
281  23.42     0.07      0.024       (  0.068)       0.004        0.020
282  23.50     0.07      0.024       (  0.068)       0.004        0.020
283  23.58     0.07      0.024       (  0.067)       0.004        0.020
284  23.67     0.07      0.024       (  0.067)       0.004        0.020
285  23.75     0.07      0.024       (  0.067)       0.004        0.020
286  23.83     0.07      0.024       (  0.067)       0.004        0.020
287  23.92     0.07      0.024       (  0.067)       0.004        0.020
288  24.00     0.07      0.024       (  0.067)       0.004        0.020
              (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    29.8
       Flood volume = Effective rainfall      2.49(In)
        times area       5.3(Ac.)/[(In)/(Ft.)] =       1.1(Ac.Ft)
       Total soil loss =      0.55(In)
       Total soil loss =     0.241(Ac.Ft)
       Total rainfall =      3.03(In)
       Flood volume =       47900.2 Cubic Feet
       Total soil loss =       10514.7 Cubic Feet
       ---------------------------------------------------------------------
        Peak flow rate of this hydrograph =      1.810(CFS)
       ---------------------------------------------------------------------
       +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                           24 - H O U R    S T O R M
                       R u n o f f      H y d r o g r a p h
       ---------------------------------------------------------------------
                    Hydrograph in   5   Minute intervals ((CFS))

       ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0004      0.06  Q         |         |         |         |
   0+10       0.0011      0.10  Q         |         |         |         |
   0+15       0.0018      0.11  Q         |         |         |         |
   0+20       0.0028      0.14  Q         |         |         |         |
   0+25       0.0039      0.16  Q         |         |         |         |
   0+30       0.0050      0.16  Q         |         |         |         |
   0+35       0.0061      0.16  Q         |         |         |         |
   0+40       0.0072      0.16  Q         |         |         |         |
   0+45       0.0083      0.16  Q         |         |         |         |
   0+50       0.0096      0.19  Q         |         |         |         |
   0+55       0.0110      0.21  Q         |         |         |         |
   1+ 0       0.0125      0.21  Q         |         |         |         |
   1+ 5       0.0137      0.18  Q         |         |         |         |
   1+10       0.0149      0.16  Q         |         |         |         |
   1+15       0.0160      0.16  Q         |         |         |         |
   1+20       0.0171      0.16  Q         |         |         |         |
   1+25       0.0182      0.16  Q         |         |         |         |
   1+30       0.0193      0.16  Q         |         |         |         |
   1+35       0.0204      0.16  Q         |         |         |         |
   1+40       0.0215      0.16  Q         |         |         |         |
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1+45       0.0226      0.16  Q          |          |          |          |
1+50       0.0239      0.19  Q          |          |          |          |
1+55       0.0253      0.21  Q          |          |          |          |
2+ 0       0.0268      0.21  Q          |          |          |          |
2+ 5       0.0283      0.21  QV         |          |          |          |
2+10       0.0297      0.21  QV         |          |          |          |
2+15       0.0312      0.21  QV         |          |          |          |
2+20       0.0327      0.21  QV         |          |          |          |
2+25       0.0341      0.21  QV         |          |          |          |
2+30       0.0356      0.21  QV         |          |          |          |
2+35       0.0373      0.24  QV         |          |          |          |
2+40       0.0391      0.26  |Q         |          |          |          |
2+45       0.0409      0.27  |Q         |          |          |          |
2+50       0.0427      0.27  |Q         |          |          |          |
2+55       0.0446      0.27  |Q         |          |          |          |
3+ 0       0.0464      0.27  |Q         |          |          |          |
3+ 5       0.0482      0.27  |Q         |          |          |          |
3+10       0.0501      0.27  |Q         |          |          |          |
3+15       0.0519      0.27  |Q         |          |          |          |
3+20       0.0537      0.27  |Q         |          |          |          |
3+25       0.0556      0.27  |QV        |          |          |          |
3+30       0.0574      0.27  |QV        |          |          |          |
3+35       0.0592      0.27  |QV        |          |          |          |
3+40       0.0611      0.27  |QV        |          |          |          |
3+45       0.0629      0.27  |QV        |          |          |          |
3+50       0.0649      0.30  |QV        |          |          |          |
3+55       0.0671      0.32  |QV        |          |          |          |
4+ 0       0.0693      0.32  |QV        |          |          |          |
4+ 5       0.0715      0.32  |QV        |          |          |          |
4+10       0.0737      0.32  |QV        |          |          |          |
4+15       0.0759      0.32  |QV        |          |          |          |
4+20       0.0783      0.35  |QV        |          |          |          |
4+25       0.0809      0.37  |QV        |          |          |          |
4+30       0.0834      0.37  |Q V       |          |          |          |
4+35       0.0860      0.37  |Q V       |          |          |          |
4+40       0.0886      0.37  |Q V       |          |          |          |
4+45       0.0911      0.37  |Q V       |          |          |          |
4+50       0.0939      0.40  |Q V       |          |          |          |
4+55       0.0968      0.42  |Q V       |          |          |          |
5+ 0       0.0998      0.43  |Q V       |          |          |          |
5+ 5       0.1023      0.36  |Q V       |          |          |          |
5+10       0.1045      0.33  |Q V       |          |          |          |
5+15       0.1067      0.32  |Q V       |          |          |          |
5+20       0.1091      0.35  |Q V       |          |          |          |
5+25       0.1117      0.37  |Q  V      |          |          |          |
5+30       0.1142      0.37  |Q  V      |          |          |          |
5+35       0.1170      0.40  |Q  V      |          |          |          |
5+40       0.1199      0.42  |Q  V      |          |          |          |
5+45       0.1229      0.43  |Q  V      |          |          |          |
5+50       0.1258      0.43  |Q  V      |          |          |          |
5+55       0.1287      0.43  |Q  V      |          |          |          |
6+ 0       0.1317      0.43  |Q  V      |          |          |          |
6+ 5       0.1348      0.46  |Q  V      |          |          |          |
6+10       0.1381      0.48  |Q   V     |          |          |          |
6+15       0.1414      0.48  |Q   V     |          |          |          |
6+20       0.1447      0.48  |Q   V     |          |          |          |
6+25       0.1480      0.48  |Q   V     |          |          |          |
6+30       0.1513      0.48  |Q   V     |          |          |          |
6+35       0.1548      0.51  | Q  V     |          |          |          |
6+40       0.1584      0.53  | Q  V     |          |          |          |
6+45       0.1621      0.53  | Q  V     |          |          |          |
6+50       0.1658      0.53  | Q   V    |          |          |          |
6+55       0.1694      0.53  | Q   V    |          |          |          |
7+ 0       0.1731      0.53  | Q   V    |          |          |          |
7+ 5       0.1768      0.53  | Q   V    |          |          |          |
7+10       0.1804      0.53  | Q   V    |          |          |          |
7+15       0.1841      0.53  | Q   V    |          |          |          |
7+20       0.1880      0.56  | Q   V    |          |          |          |
7+25       0.1920      0.58  | Q   V    |          |          |          |
7+30       0.1960      0.59  | Q    V   |          |          |          |
7+35       0.2002      0.62  | Q    V   |          |          |          |
7+40       0.2046      0.64  | Q    V   |          |          |          |
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 7+45       0.2090      0.64   | Q    V  |          |          |          |
 7+50       0.2136      0.67   | Q    V  |          |          |          |
 7+55       0.2184      0.69   | Q    V  |          |          |          |
 8+ 0       0.2231      0.69   | Q     V |          |          |          |
 8+ 5       0.2283      0.75   |  Q    V |          |          |          |
 8+10       0.2338      0.79   |  Q    V |          |          |          |
 8+15       0.2393      0.80   |  Q    V |          |          |          |
 8+20       0.2448      0.80   |  Q    V |          |          |          |
 8+25       0.2503      0.80   |  Q     V|          |          |          |
 8+30       0.2558      0.80   |  Q     V|          |          |          |
 8+35       0.2615      0.83   |  Q     V|          |          |          |
 8+40       0.2673      0.85   |  Q     V|          |          |          |
 8+45       0.2732      0.85   |  Q     V|          |          |          |
 8+50       0.2793      0.88   |  Q      V          |          |          |
 8+55       0.2855      0.90   |  Q      V          |          |          |
 9+ 0       0.2917      0.90   |  Q      V          |          |          |
 9+ 5       0.2984      0.97   |  Q      V          |          |          |
 9+10       0.3053      1.01   |   Q     |V         |          |          |
 9+15       0.3123      1.01   |   Q     |V         |          |          |
 9+20       0.3194      1.04   |   Q     |V         |          |          |
 9+25       0.3267      1.06   |   Q     |V         |          |          |
 9+30       0.3341      1.06   |   Q     | V        |          |          |
 9+35       0.3416      1.10   |   Q     | V        |          |          |
 9+40       0.3493      1.11   |   Q     | V        |          |          |
 9+45       0.3570      1.12   |   Q     | V        |          |          |
 9+50       0.3649      1.15   |   Q     |  V       |          |          |
 9+55       0.3729      1.17   |   Q     |  V       |          |          |
10+ 0       0.3810      1.17   |   Q     |  V       |          |          |
10+ 5       0.3876      0.96   |  Q      |   V      |          |          |
10+10       0.3932      0.82   |  Q      |   V      |          |          |
10+15       0.3987      0.80   |  Q      |   V      |          |          |
10+20       0.4042      0.80   |  Q      |   V      |          |          |
10+25       0.4097      0.80   |  Q      |   V      |          |          |
10+30       0.4152      0.80   |  Q      |    V     |          |          |
10+35       0.4218      0.95   |  Q      |    V     |          |          |
10+40       0.4290      1.05   |   Q     |    V     |          |          |
10+45       0.4363      1.06   |   Q     |    V     |          |          |
10+50       0.4437      1.06   |   Q     |     V    |          |          |
10+55       0.4510      1.06   |   Q     |     V    |          |          |
11+ 0       0.4583      1.06   |   Q     |     V    |          |          |
11+ 5       0.4655      1.03   |   Q     |     V    |          |          |
11+10       0.4724      1.01   |   Q     |      V   |          |          |
11+15       0.4794      1.01   |   Q     |      V   |          |          |
11+20       0.4864      1.01   |   Q     |      V   |          |          |
11+25       0.4933      1.01   |   Q     |      V   |          |          |
11+30       0.5003      1.01   |   Q     |       V  |          |          |
11+35       0.5068      0.95   |  Q      |       V  |          |          |
11+40       0.5131      0.91   |  Q      |       V  |          |          |
11+45       0.5193      0.90   |  Q      |       V  |          |          |
11+50       0.5258      0.94   |  Q      |        V |          |          |
11+55       0.5324      0.95   |  Q      |        V |          |          |
12+ 0       0.5390      0.96   |  Q      |        V |          |          |
12+ 5       0.5470      1.17   |   Q     |        V |          |          |
12+10       0.5561      1.31   |    Q    |         V|          |          |
12+15       0.5652      1.33   |    Q    |         V|          |          |
12+20       0.5746      1.36   |    Q    |         V|          |          |
12+25       0.5841      1.38   |    Q    |          |V         |          |
12+30       0.5936      1.38   |    Q    |          |V         |          |
12+35       0.6036      1.45   |    Q    |          |V         |          |
12+40       0.6138      1.48   |    Q    |          | V        |          |
12+45       0.6241      1.49   |    Q    |          | V        |          |
12+50       0.6346      1.52   |     Q   |          |  V       |          |
12+55       0.6452      1.54   |     Q   |          |  V       |          |
13+ 0       0.6558      1.54   |     Q   |          |  V       |          |
13+ 5       0.6675      1.70   |     Q   |          |   V      |          |
13+10       0.6798      1.79   |      Q  |          |   V      |          |
13+15       0.6923      1.81   |      Q  |          |    V     |          |
13+20       0.7048      1.81   |      Q  |          |    V     |          |
13+25       0.7172      1.81   |      Q  |          |     V    |          |
13+30       0.7297      1.81   |      Q  |          |     V    |          |
13+35       0.7398      1.47   |    Q    |          |     V    |          |
13+40       0.7485      1.26   |    Q    |          |      V   |          |
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13+45       0.7569      1.22  |   Q     |          |       V  |          |
13+50       0.7653      1.22  |   Q     |          |       V  |          |
13+55       0.7738      1.22  |   Q     |          |        V |          |
14+ 0       0.7822      1.22  |   Q     |          |        V |          |
14+ 5       0.7915      1.35  |    Q    |          |        V |          |
14+10       0.8013      1.42  |    Q    |          |         V|          |
14+15       0.8112      1.44  |    Q    |          |         V|          |
14+20       0.8209      1.41  |    Q    |          |         V|          |
14+25       0.8304      1.39  |    Q    |          |          V          |
14+30       0.8400      1.38  |    Q    |          |          V          |
14+35       0.8495      1.38  |    Q    |          |          V          |
14+40       0.8590      1.38  |    Q    |          |          |V         |
14+45       0.8686      1.38  |    Q    |          |          |V         |
14+50       0.8779      1.35  |    Q    |          |          |V         |
14+55       0.8871      1.33  |    Q    |          |          | V        |
15+ 0       0.8962      1.33  |    Q    |          |          | V        |
15+ 5       0.9052      1.30  |    Q    |          |          | V        |
15+10       0.9140      1.28  |    Q    |          |          |  V       |
15+15       0.9228      1.28  |    Q    |          |          |  V       |
15+20       0.9314      1.25  |   Q     |          |          |  V       |
15+25       0.9398      1.23  |   Q     |          |          |   V      |
15+30       0.9483      1.22  |   Q     |          |          |   V      |
15+35       0.9558      1.10  |   Q     |          |          |   V      |
15+40       0.9629      1.02  |   Q     |          |          |    V     |
15+45       0.9698      1.01  |   Q     |          |          |    V     |
15+50       0.9768      1.01  |   Q     |          |          |    V     |
15+55       0.9838      1.01  |   Q     |          |          |    V     |
16+ 0       0.9907      1.01  |   Q     |          |          |     V    |
16+ 5       0.9945      0.55  | Q       |          |          |     V    |
16+10       0.9963      0.26  |Q        |          |          |     V    |
16+15       0.9978      0.21  Q         |          |          |     V    |
16+20       0.9992      0.21  Q         |          |          |     V    |
16+25       1.0007      0.21  Q         |          |          |     V    |
16+30       1.0022      0.21  Q         |          |          |     V    |
16+35       1.0034      0.18  Q         |          |          |     V    |
16+40       1.0045      0.16  Q         |          |          |     V    |
16+45       1.0056      0.16  Q         |          |          |     V    |
16+50       1.0067      0.16  Q         |          |          |     V    |
16+55       1.0078      0.16  Q         |          |          |     V    |
17+ 0       1.0089      0.16  Q         |          |          |     V    |
17+ 5       1.0105      0.22  Q         |          |          |     V    |
17+10       1.0123      0.26  |Q        |          |          |     V    |
17+15       1.0141      0.27  |Q        |          |          |     V    |
17+20       1.0159      0.27  |Q        |          |          |     V    |
17+25       1.0178      0.27  |Q        |          |          |      V   |
17+30       1.0196      0.27  |Q        |          |          |      V   |
17+35       1.0214      0.27  |Q        |          |          |      V   |
17+40       1.0233      0.27  |Q        |          |          |      V   |
17+45       1.0251      0.27  |Q        |          |          |      V   |
17+50       1.0267      0.24  Q         |          |          |      V   |
17+55       1.0282      0.22  Q         |          |          |      V   |
18+ 0       1.0297      0.21  Q         |          |          |      V   |
18+ 5       1.0311      0.21  Q         |          |          |      V   |
18+10       1.0326      0.21  Q         |          |          |      V   |
18+15       1.0341      0.21  Q         |          |          |      V   |
18+20       1.0355      0.21  Q         |          |          |      V   |
18+25       1.0370      0.21  Q         |          |          |      V   |
18+30       1.0385      0.21  Q         |          |          |      V   |
18+35       1.0397      0.18  Q         |          |          |      V   |
18+40       1.0408      0.16  Q         |          |          |      V   |
18+45       1.0419      0.16  Q         |          |          |      V   |
18+50       1.0428      0.13  Q         |          |          |      V   |
18+55       1.0436      0.11  Q         |          |          |      V   |
19+ 0       1.0443      0.11  Q         |          |          |      V   |
19+ 5       1.0452      0.14  Q         |          |          |       V  |
19+10       1.0463      0.16  Q         |          |          |       V  |
19+15       1.0474      0.16  Q         |          |          |       V  |
19+20       1.0487      0.19  Q         |          |          |       V  |
19+25       1.0502      0.21  Q         |          |          |       V  |
19+30       1.0517      0.21  Q         |          |          |       V  |
19+35       1.0529      0.18  Q         |          |          |       V  |
19+40       1.0540      0.16  Q         |          |          |       V  |
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  19+45       1.0551      0.16  Q          |           |           |        V |
  19+50       1.0560      0.13  Q          |           |           |        V |
  19+55       1.0568      0.11  Q          |           |           |        V |
  20+ 0       1.0575      0.11  Q          |           |           |        V |
  20+ 5       1.0584      0.14  Q          |           |           |        V |
  20+10       1.0595      0.16  Q          |           |           |        V |
  20+15       1.0606      0.16  Q          |           |           |        V |
  20+20       1.0617      0.16  Q          |           |           |        V |
  20+25       1.0628      0.16  Q          |           |           |        V |
  20+30       1.0639      0.16  Q          |           |           |        V |
  20+35       1.0650      0.16  Q          |           |           |        V |
  20+40       1.0661      0.16  Q          |           |           |        V |
  20+45       1.0672      0.16  Q          |           |           |        V |
  20+50       1.0681      0.13  Q          |           |           |        V |
  20+55       1.0689      0.11  Q          |           |           |        V |
  21+ 0       1.0696      0.11  Q          |           |           |        V |
  21+ 5       1.0705      0.14  Q          |           |           |        V |
  21+10       1.0716      0.16  Q          |           |           |        V |
  21+15       1.0727      0.16  Q          |           |           |         V|
  21+20       1.0736      0.13  Q          |           |           |         V|
  21+25       1.0744      0.11  Q          |           |           |         V|
  21+30       1.0751      0.11  Q          |           |           |         V|
  21+35       1.0760      0.14  Q          |           |           |         V|
  21+40       1.0771      0.16  Q          |           |           |         V|
  21+45       1.0782      0.16  Q          |           |           |         V|
  21+50       1.0791      0.13  Q          |           |           |         V|
  21+55       1.0799      0.11  Q          |           |           |         V|
  22+ 0       1.0806      0.11  Q          |           |           |         V|
  22+ 5       1.0815      0.14  Q          |           |           |         V|
  22+10       1.0826      0.16  Q          |           |           |         V|
  22+15       1.0837      0.16  Q          |           |           |         V|
  22+20       1.0846      0.13  Q          |           |           |         V|
  22+25       1.0854      0.11  Q          |           |           |         V|
  22+30       1.0861      0.11  Q          |           |           |         V|
  22+35       1.0868      0.11  Q          |           |           |         V|
  22+40       1.0876      0.11  Q          |           |           |         V|
  22+45       1.0883      0.11  Q          |           |           |         V|
  22+50       1.0890      0.11  Q          |           |           |         V|
  22+55       1.0898      0.11  Q          |           |           |         V|
  23+ 0       1.0905      0.11  Q          |           |           |         V|
  23+ 5       1.0912      0.11  Q          |           |           |         V|
  23+10       1.0920      0.11  Q          |           |           |         V|
  23+15       1.0927      0.11  Q          |           |           |         V|
  23+20       1.0934      0.11  Q          |           |           |         V|
  23+25       1.0942      0.11  Q          |           |           |         V|
  23+30       1.0949      0.11  Q          |           |           |         V|
  23+35       1.0956      0.11  Q          |           |           |         V|
  23+40       1.0964      0.11  Q          |           |           |         V|
  23+45       1.0971      0.11  Q          |           |           |         V|
  23+50       1.0978      0.11  Q          |           |           |         V|
  23+55       1.0986      0.11  Q          |           |           |         V|
  24+ 0       1.0993      0.11  Q          |           |           |         V|
  24+ 5       1.0996      0.04  Q          |           |           |         V|
  24+10       1.0996      0.01  Q          |           |           |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA0565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	1.20	6.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	3.00	15.93

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.622(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.622(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.097	(0.134)	0.018	0.080
2	0.17	0.60	0.117	(0.134)	0.021	0.096
3	0.25	0.60	0.117	(0.134)	0.021	0.096
4	0.33	0.60	0.117	(0.134)	0.021	0.096
5	0.42	0.60	0.117	(0.134)	0.021	0.096
6	0.50	0.70	0.136	(0.134)	0.025	0.112
7	0.58	0.70	0.136	(0.134)	0.025	0.112
8	0.67	0.70	0.136	(0.134)	0.025	0.112
9	0.75	0.70	0.136	(0.134)	0.025	0.112
10	0.83	0.70	0.136	(0.134)	0.025	0.112
11	0.92	0.70	0.136	(0.134)	0.025	0.112
12	1.00	0.80	0.156	(0.134)	0.028	0.128
13	1.08	0.80	0.156	(0.134)	0.028	0.128
14	1.17	0.80	0.156	(0.134)	0.028	0.128
15	1.25	0.80	0.156	(0.134)	0.028	0.128
16	1.33	0.80	0.156	(0.134)	0.028	0.128
17	1.42	0.80	0.156	(0.134)	0.028	0.128
18	1.50	0.80	0.156	(0.134)	0.028	0.128
19	1.58	0.80	0.156	(0.134)	0.028	0.128
20	1.67	0.80	0.156	(0.134)	0.028	0.128
21	1.75	0.80	0.156	(0.134)	0.028	0.128
22	1.83	0.80	0.156	(0.134)	0.028	0.128
23	1.92	0.80	0.156	(0.134)	0.028	0.128
24	2.00	0.90	0.175	(0.134)	0.032	0.144
25	2.08	0.80	0.156	(0.134)	0.028	0.128
26	2.17	0.90	0.175	(0.134)	0.032	0.144
27	2.25	0.90	0.175	(0.134)	0.032	0.144
28	2.33	0.90	0.175	(0.134)	0.032	0.144
29	2.42	0.90	0.175	(0.134)	0.032	0.144
30	2.50	0.90	0.175	(0.134)	0.032	0.144
31	2.58	0.90	0.175	(0.134)	0.032	0.144
32	2.67	0.90	0.175	(0.134)	0.032	0.144
33	2.75	1.00	0.195	(0.134)	0.035	0.160
34	2.83	1.00	0.195	(0.134)	0.035	0.160
35	2.92	1.00	0.195	(0.134)	0.035	0.160
36	3.00	1.00	0.195	(0.134)	0.035	0.160
37	3.08	1.00	0.195	(0.134)	0.035	0.160
38	3.17	1.10	0.214	(0.134)	0.039	0.176
39	3.25	1.10	0.214	(0.134)	0.039	0.176
40	3.33	1.10	0.214	(0.134)	0.039	0.176
41	3.42	1.20	0.234	(0.134)	0.042	0.191

42	3.50	1.30	0.253	(	0.134)	0.046	0.207
43	3.58	1.40	0.272	(	0.134)	0.049	0.223
44	3.67	1.40	0.272	(	0.134)	0.049	0.223
45	3.75	1.50	0.292	(	0.134)	0.053	0.239
46	3.83	1.50	0.292	(	0.134)	0.053	0.239
47	3.92	1.60	0.311	(	0.134)	0.056	0.255
48	4.00	1.60	0.311	(	0.134)	0.056	0.255
49	4.08	1.70	0.331	(	0.134)	0.060	0.271
50	4.17	1.80	0.350	(	0.134)	0.063	0.287
51	4.25	1.90	0.370	(	0.134)	0.067	0.303
52	4.33	2.00	0.389	(	0.134)	0.070	0.319
53	4.42	2.10	0.409	(	0.134)	0.074	0.335
54	4.50	2.10	0.409	(	0.134)	0.074	0.335
55	4.58	2.20	0.428	(	0.134)	0.077	0.351
56	4.67	2.30	0.448	(	0.134)	0.081	0.367
57	4.75	2.40	0.467	(	0.134)	0.084	0.383
58	4.83	2.40	0.467	(	0.134)	0.084	0.383
59	4.92	2.50	0.486	(	0.134)	0.088	0.399
60	5.00	2.60	0.506	(	0.134)	0.091	0.415
61	5.08	3.10	0.603	(	0.134)	0.109	0.495
62	5.17	3.60	0.701	(	0.134)	0.126	0.574
63	5.25	3.90	0.759		0.134	(0.137)	0.625
64	5.33	4.20	0.817		0.134	(0.147)	0.683
65	5.42	4.70	0.915		0.134	(0.165)	0.780
66	5.50	5.60	1.090		0.134	(0.196)	0.956
67	5.58	1.90	0.370	(	0.134)	0.067	0.303
68	5.67	0.90	0.175	(	0.134)	0.032	0.144
69	5.75	0.60	0.117	(	0.134)	0.021	0.096
70	5.83	0.50	0.097	(	0.134)	0.018	0.080
71	5.92	0.30	0.058	(	0.134)	0.011	0.048
72	6.00	0.20	0.039	(	0.134)	0.007	0.032

(Loss Rate Not Used)

Sum = 100.0 Sum = 16.1

Flood volume = Effective rainfall 1.34(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.28(In)
Total soil loss = 0.125(Ac.Ft)
Total rainfall = 1.62(In)
Flood volume = 25803.5 Cubic Feet
Total soil loss = 5452.8 Cubic Feet

Peak flow rate of this hydrograph = 4.691(CFS)

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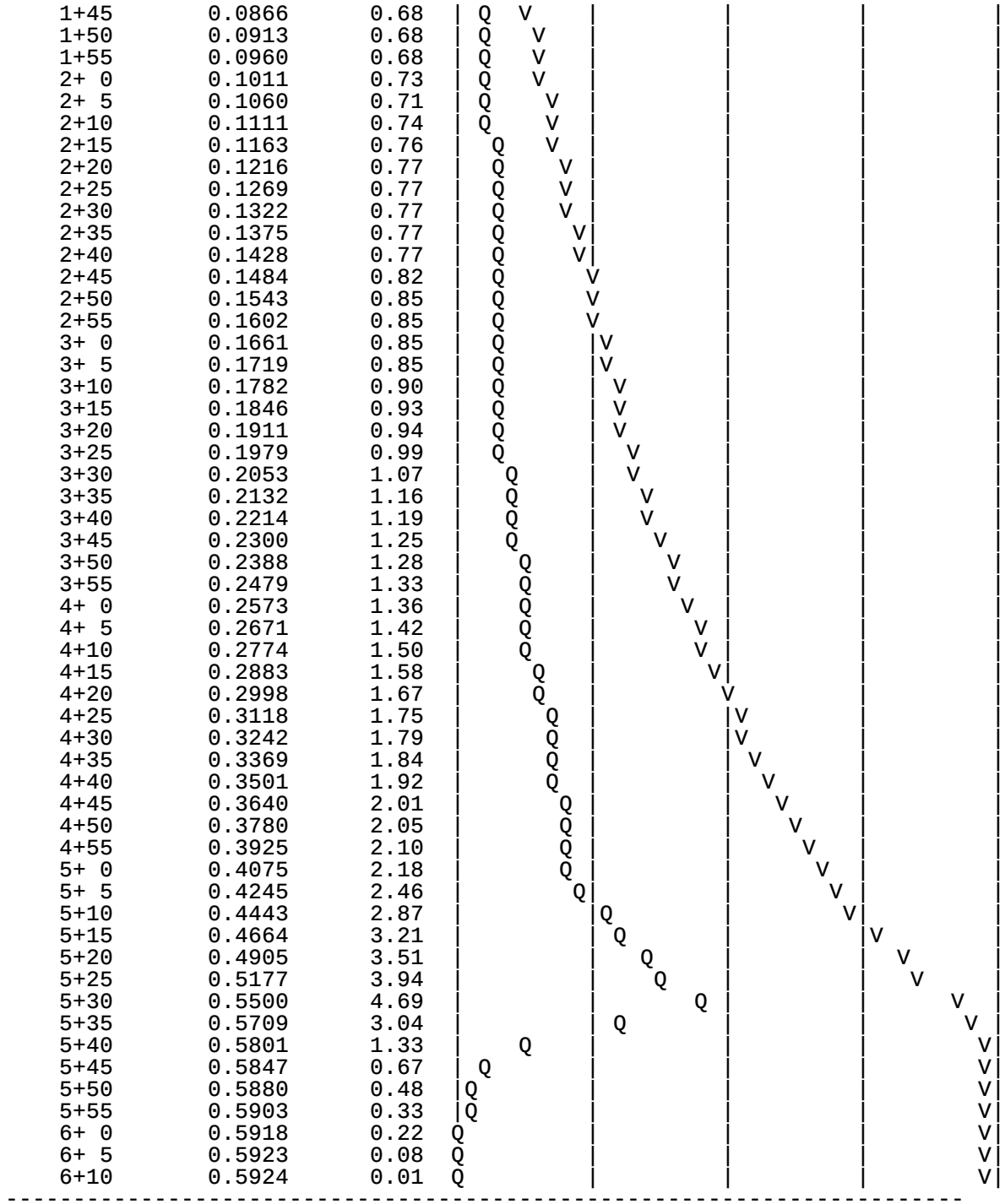
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0017	0.25	Q				
0+10	0.0048	0.45	VQ				
0+15	0.0083	0.51	V Q				
0+20	0.0118	0.51	V Q				
0+25	0.0154	0.51	|VQ				
0+30	0.0192	0.56	|VQ				
0+35	0.0233	0.59	|VQ				
0+40	0.0274	0.60	|VQ				
0+45	0.0316	0.60	| Q				
0+50	0.0357	0.60	| Q				
0+55	0.0398	0.60	| Q				
1+ 0	0.0443	0.65	| Q				
1+ 5	0.0489	0.68	| QV				
1+10	0.0536	0.68	| QV				
1+15	0.0584	0.68	| QV				
1+20	0.0631	0.68	| Q V				
1+25	0.0678	0.68	| Q V				
1+30	0.0725	0.68	| Q V				
1+35	0.0772	0.68	| Q V				
1+40	0.0819	0.68	| Q V				


1+45 0.0866 0.68
1+50 0.0913 0.68
1+55 0.0960 0.68
2+ 0 0.1011 0.73
2+ 5 0.1060 0.71
2+10 0.1111 0.74
2+15 0.1163 0.76
2+20 0.1216 0.77
2+25 0.1269 0.77
2+30 0.1322 0.77
2+35 0.1375 0.77
2+40 0.1428 0.77
2+45 0.1484 0.82
2+50 0.1543 0.85
2+55 0.1602 0.85
3+ 0 0.1661 0.85
3+ 5 0.1719 0.85
3+10 0.1782 0.90
3+15 0.1846 0.93
3+20 0.1911 0.94
3+25 0.1979 0.99
3+30 0.2053 1.07
3+35 0.2132 1.16
3+40 0.2214 1.19
3+45 0.2300 1.25
3+50 0.2388 1.28
3+55 0.2479 1.33
4+ 0 0.2573 1.36
4+ 5 0.2671 1.42
4+10 0.2774 1.50
4+15 0.2883 1.58
4+20 0.2998 1.67
4+25 0.3118 1.75
4+30 0.3242 1.79
4+35 0.3369 1.84
4+40 0.3501 1.92
4+45 0.3640 2.01
4+50 0.3780 2.05
4+55 0.3925 2.10
5+ 0 0.4075 2.18
5+ 5 0.4245 2.46
5+10 0.4443 2.87
5+15 0.4664 3.21
5+20 0.4905 3.51
5+25 0.5177 3.94
5+30 0.5500 4.69
5+35 0.5709 3.04
5+40 0.5801 1.33
5+45 0.5847 0.67
5+50 0.5880 0.48
5+55 0.5903 0.33
6+ 0 0.5918 0.22
6+ 5 0.5923 0.08
6+10 0.5924 0.01

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA0535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	0.90	4.78

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	2.35	12.48

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.240(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.240(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.193	(0.134)	0.035	0.159
2	0.17	1.30	0.193	(0.134)	0.035	0.159
3	0.25	1.10	0.164	(0.134)	0.029	0.134
4	0.33	1.50	0.223	(0.134)	0.040	0.183
5	0.42	1.50	0.223	(0.134)	0.040	0.183
6	0.50	1.80	0.268	(0.134)	0.048	0.220
7	0.58	1.50	0.223	(0.134)	0.040	0.183
8	0.67	1.80	0.268	(0.134)	0.048	0.220
9	0.75	1.80	0.268	(0.134)	0.048	0.220
10	0.83	1.50	0.223	(0.134)	0.040	0.183
11	0.92	1.60	0.238	(0.134)	0.043	0.195
12	1.00	1.80	0.268	(0.134)	0.048	0.220
13	1.08	2.20	0.327	(0.134)	0.059	0.268
14	1.17	2.20	0.327	(0.134)	0.059	0.268
15	1.25	2.20	0.327	(0.134)	0.059	0.268
16	1.33	2.00	0.298	(0.134)	0.054	0.244
17	1.42	2.60	0.387	(0.134)	0.070	0.317
18	1.50	2.70	0.402	(0.134)	0.072	0.329
19	1.58	2.40	0.357	(0.134)	0.064	0.293
20	1.67	2.70	0.402	(0.134)	0.072	0.329
21	1.75	3.30	0.491	(0.134)	0.088	0.403
22	1.83	3.10	0.461	(0.134)	0.083	0.378
23	1.92	2.90	0.431	(0.134)	0.078	0.354
24	2.00	3.00	0.446	(0.134)	0.080	0.366
25	2.08	3.10	0.461	(0.134)	0.083	0.378
26	2.17	4.20	0.625	(0.134)	0.112	0.512
27	2.25	5.00	0.744	(0.134)	0.134	0.610
28	2.33	3.50	0.521	(0.134)	0.094	0.427
29	2.42	6.80	1.012	0.134	(0.182)	0.877
30	2.50	7.30	1.086	0.134	(0.195)	0.952
31	2.58	8.20	1.220	0.134	(0.220)	1.086
32	2.67	5.90	0.878	0.134	(0.158)	0.743
33	2.75	2.00	0.298	(0.134)	0.054	0.244
34	2.83	1.80	0.268	(0.134)	0.048	0.220
35	2.92	1.80	0.268	(0.134)	0.048	0.220
36	3.00	0.60	0.089	(0.134)	0.016	0.073
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	12.4

Flood volume = Effective rainfall 1.03(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.20(In)

Total soil loss = 0.091(Ac.Ft)
Total rainfall = 1.24(In)
Flood volume = 19943.7 Cubic Feet
Total soil loss = 3949.9 Cubic Feet

Peak flow rate of this hydrograph = 5.488(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0034	0.49	VQ
0+10	0.0089	0.80	V Q
0+15	0.0142	0.77	V Q
0+20	0.0203	0.88	V Q
0+25	0.0269	0.96	VQ
0+30	0.0344	1.09	VQ
0+35	0.0417	1.05	VQ
0+40	0.0493	1.10	Q
0+45	0.0573	1.16	QV
0+50	0.0646	1.06	QV
0+55	0.0717	1.03	Q V
1+ 0	0.0794	1.12	Q V
1+ 5	0.0885	1.32	Q V
1+10	0.0983	1.42	Q V
1+15	0.1082	1.44	Q V
1+20	0.1175	1.36	Q V
1+25	0.1281	1.54	Q V
1+30	0.1399	1.71	Q V
1+35	0.1513	1.65	Q V
1+40	0.1629	1.69	Q V
1+45	0.1766	1.98	Q V
1+50	0.1907	2.06	Q V
1+55	0.2042	1.96	Q V
2+ 0	0.2176	1.94	Q V
2+ 5	0.2313	1.99	Q V
2+10	0.2481	2.44	Q V
2+15	0.2688	3.00	Q V
2+20	0.2871	2.67	Q V
2+25	0.3129	3.74	Q V
2+30	0.3459	4.79	Q V
2+35	0.3837	5.49	Q V
2+40	0.4161	4.71	Q V
2+45	0.4336	2.54	Q V
2+50	0.4431	1.38	Q V
2+55	0.4513	1.18	Q V
3+ 0	0.4562	0.72	Q V
3+ 5	0.4577	0.21	Q V
3+10	0.4578	0.02	Q V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA0515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	0.54	2.87

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	1.36	7.22

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.732(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.732(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
		Sum = 100.000	Sum=	5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.387	(0.134)	0.070	0.317
2	0.17	4.50	0.395	(0.134)	0.071	0.324
3	0.25	5.40	0.474	(0.134)	0.085	0.389
4	0.33	5.40	0.474	(0.134)	0.085	0.389
5	0.42	5.70	0.501	(0.134)	0.090	0.411
6	0.50	6.40	0.562	(0.134)	0.101	0.461
7	0.58	7.90	0.694	(0.134)	0.125	0.569
8	0.67	9.10	0.799	0.134	(0.144)	0.665
9	0.75	12.80	1.124	0.134	(0.202)	0.990
10	0.83	25.60	2.249	0.134	(0.405)	2.115
11	0.92	7.90	0.694	(0.134)	0.125	0.569
12	1.00	4.90	0.430	(0.134)	0.077	0.353
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.6

Flood volume = Effective rainfall 0.63(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.10(In)
Total soil loss = 0.045(Ac.Ft)
Total rainfall = 0.73(In)
Flood volume = 12130.3 Cubic Feet
Total soil loss = 1979.8 Cubic Feet

Peak flow rate of this hydrograph = 8.684(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0068	0.98	V Q				
0+10	0.0179	1.62	| V Q				
0+15	0.0313	1.93	| V Q				
0+20	0.0455	2.06	| V Q				
0+25	0.0603	2.15	| Q				
0+30	0.0764	2.35	| QV				

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   0+35       0.0956      2.79  |          |Q V       |          |          |
   0+40       0.1184      3.31  |          |  Q   V   |          |          |
   0+45       0.1497      4.54  |          |       Q  |V         |          |
   0+50       0.2095      8.68  |          |          |          V   Q      |
   0+55       0.2522      6.20  |          |          |    Q     |     V    |
   1+ 0       0.2718      2.85  |          |Q         |          |          V|
   1+ 5       0.2777      0.86  |  Q       |          |          |          V|
   1+10       0.2785      0.11  Q          |          |          |          V|
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	2.00	10.62

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	6.40	33.98

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.810(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.810(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.030	(0.172)	0.005	0.025
2	0.17	0.07	0.030	(0.171)	0.005	0.025
3	0.25	0.07	0.030	(0.171)	0.005	0.025
4	0.33	0.10	0.046	(0.170)	0.008	0.037
5	0.42	0.10	0.046	(0.169)	0.008	0.037
6	0.50	0.10	0.046	(0.169)	0.008	0.037
7	0.58	0.10	0.046	(0.168)	0.008	0.037
8	0.67	0.10	0.046	(0.167)	0.008	0.037
9	0.75	0.10	0.046	(0.167)	0.008	0.037
10	0.83	0.13	0.061	(0.166)	0.011	0.050
11	0.92	0.13	0.061	(0.165)	0.011	0.050
12	1.00	0.13	0.061	(0.165)	0.011	0.050
13	1.08	0.10	0.046	(0.164)	0.008	0.037
14	1.17	0.10	0.046	(0.163)	0.008	0.037
15	1.25	0.10	0.046	(0.163)	0.008	0.037
16	1.33	0.10	0.046	(0.162)	0.008	0.037
17	1.42	0.10	0.046	(0.162)	0.008	0.037
18	1.50	0.10	0.046	(0.161)	0.008	0.037
19	1.58	0.10	0.046	(0.160)	0.008	0.037
20	1.67	0.10	0.046	(0.160)	0.008	0.037
21	1.75	0.10	0.046	(0.159)	0.008	0.037
22	1.83	0.13	0.061	(0.158)	0.011	0.050
23	1.92	0.13	0.061	(0.158)	0.011	0.050
24	2.00	0.13	0.061	(0.157)	0.011	0.050
25	2.08	0.13	0.061	(0.156)	0.011	0.050
26	2.17	0.13	0.061	(0.156)	0.011	0.050
27	2.25	0.13	0.061	(0.155)	0.011	0.050
28	2.33	0.13	0.061	(0.155)	0.011	0.050
29	2.42	0.13	0.061	(0.154)	0.011	0.050
30	2.50	0.13	0.061	(0.153)	0.011	0.050
31	2.58	0.17	0.076	(0.153)	0.014	0.062
32	2.67	0.17	0.076	(0.152)	0.014	0.062
33	2.75	0.17	0.076	(0.151)	0.014	0.062
34	2.83	0.17	0.076	(0.151)	0.014	0.062
35	2.92	0.17	0.076	(0.150)	0.014	0.062
36	3.00	0.17	0.076	(0.150)	0.014	0.062
37	3.08	0.17	0.076	(0.149)	0.014	0.062
38	3.17	0.17	0.076	(0.148)	0.014	0.062
39	3.25	0.17	0.076	(0.148)	0.014	0.062
40	3.33	0.17	0.076	(0.147)	0.014	0.062
41	3.42	0.17	0.076	(0.146)	0.014	0.062

42	3.50	0.17	0.076	(0.146)	0.014	0.062
43	3.58	0.17	0.076	(0.145)	0.014	0.062
44	3.67	0.17	0.076	(0.145)	0.014	0.062
45	3.75	0.17	0.076	(0.144)	0.014	0.062
46	3.83	0.20	0.091	(0.143)	0.016	0.075
47	3.92	0.20	0.091	(0.143)	0.016	0.075
48	4.00	0.20	0.091	(0.142)	0.016	0.075
49	4.08	0.20	0.091	(0.142)	0.016	0.075
50	4.17	0.20	0.091	(0.141)	0.016	0.075
51	4.25	0.20	0.091	(0.140)	0.016	0.075
52	4.33	0.23	0.107	(0.140)	0.019	0.087
53	4.42	0.23	0.107	(0.139)	0.019	0.087
54	4.50	0.23	0.107	(0.139)	0.019	0.087
55	4.58	0.23	0.107	(0.138)	0.019	0.087
56	4.67	0.23	0.107	(0.137)	0.019	0.087
57	4.75	0.23	0.107	(0.137)	0.019	0.087
58	4.83	0.27	0.122	(0.136)	0.022	0.100
59	4.92	0.27	0.122	(0.136)	0.022	0.100
60	5.00	0.27	0.122	(0.135)	0.022	0.100
61	5.08	0.20	0.091	(0.134)	0.016	0.075
62	5.17	0.20	0.091	(0.134)	0.016	0.075
63	5.25	0.20	0.091	(0.133)	0.016	0.075
64	5.33	0.23	0.107	(0.133)	0.019	0.087
65	5.42	0.23	0.107	(0.132)	0.019	0.087
66	5.50	0.23	0.107	(0.132)	0.019	0.087
67	5.58	0.27	0.122	(0.131)	0.022	0.100
68	5.67	0.27	0.122	(0.130)	0.022	0.100
69	5.75	0.27	0.122	(0.130)	0.022	0.100
70	5.83	0.27	0.122	(0.129)	0.022	0.100
71	5.92	0.27	0.122	(0.129)	0.022	0.100
72	6.00	0.27	0.122	(0.128)	0.022	0.100
73	6.08	0.30	0.137	(0.128)	0.025	0.112
74	6.17	0.30	0.137	(0.127)	0.025	0.112
75	6.25	0.30	0.137	(0.126)	0.025	0.112
76	6.33	0.30	0.137	(0.126)	0.025	0.112
77	6.42	0.30	0.137	(0.125)	0.025	0.112
78	6.50	0.30	0.137	(0.125)	0.025	0.112
79	6.58	0.33	0.152	(0.124)	0.027	0.125
80	6.67	0.33	0.152	(0.124)	0.027	0.125
81	6.75	0.33	0.152	(0.123)	0.027	0.125
82	6.83	0.33	0.152	(0.122)	0.027	0.125
83	6.92	0.33	0.152	(0.122)	0.027	0.125
84	7.00	0.33	0.152	(0.121)	0.027	0.125
85	7.08	0.33	0.152	(0.121)	0.027	0.125
86	7.17	0.33	0.152	(0.120)	0.027	0.125
87	7.25	0.33	0.152	(0.120)	0.027	0.125
88	7.33	0.37	0.168	(0.119)	0.030	0.137
89	7.42	0.37	0.168	(0.119)	0.030	0.137
90	7.50	0.37	0.168	(0.118)	0.030	0.137
91	7.58	0.40	0.183	(0.118)	0.033	0.150
92	7.67	0.40	0.183	(0.117)	0.033	0.150
93	7.75	0.40	0.183	(0.116)	0.033	0.150
94	7.83	0.43	0.198	(0.116)	0.036	0.162
95	7.92	0.43	0.198	(0.115)	0.036	0.162
96	8.00	0.43	0.198	(0.115)	0.036	0.162
97	8.08	0.50	0.229	(0.114)	0.041	0.187
98	8.17	0.50	0.229	(0.114)	0.041	0.187
99	8.25	0.50	0.229	(0.113)	0.041	0.187
100	8.33	0.50	0.229	(0.113)	0.041	0.187
101	8.42	0.50	0.229	(0.112)	0.041	0.187
102	8.50	0.50	0.229	(0.112)	0.041	0.187
103	8.58	0.53	0.244	(0.111)	0.044	0.200
104	8.67	0.53	0.244	(0.111)	0.044	0.200
105	8.75	0.53	0.244	(0.110)	0.044	0.200
106	8.83	0.57	0.259	(0.110)	0.047	0.212
107	8.92	0.57	0.259	(0.109)	0.047	0.212
108	9.00	0.57	0.259	(0.109)	0.047	0.212
109	9.08	0.63	0.290	(0.108)	0.052	0.237
110	9.17	0.63	0.290	(0.108)	0.052	0.237
111	9.25	0.63	0.290	(0.107)	0.052	0.237
112	9.33	0.67	0.305	(0.107)	0.055	0.250
113	9.42	0.67	0.305	(0.106)	0.055	0.250

114	9.50	0.67	0.305	(0.105)	0.055	0.250
115	9.58	0.70	0.320	(0.105)	0.058	0.262
116	9.67	0.70	0.320	(0.104)	0.058	0.262
117	9.75	0.70	0.320	(0.104)	0.058	0.262
118	9.83	0.73	0.335	(0.103)	0.060	0.275
119	9.92	0.73	0.335	(0.103)	0.060	0.275
120	10.00	0.73	0.335	(0.102)	0.060	0.275
121	10.08	0.50	0.229	(0.102)	0.041	0.187
122	10.17	0.50	0.229	(0.101)	0.041	0.187
123	10.25	0.50	0.229	(0.101)	0.041	0.187
124	10.33	0.50	0.229	(0.101)	0.041	0.187
125	10.42	0.50	0.229	(0.100)	0.041	0.187
126	10.50	0.50	0.229	(0.100)	0.041	0.187
127	10.58	0.67	0.305	(0.099)	0.055	0.250
128	10.67	0.67	0.305	(0.099)	0.055	0.250
129	10.75	0.67	0.305	(0.098)	0.055	0.250
130	10.83	0.67	0.305	(0.098)	0.055	0.250
131	10.92	0.67	0.305	(0.097)	0.055	0.250
132	11.00	0.67	0.305	(0.097)	0.055	0.250
133	11.08	0.63	0.290	(0.096)	0.052	0.237
134	11.17	0.63	0.290	(0.096)	0.052	0.237
135	11.25	0.63	0.290	(0.095)	0.052	0.237
136	11.33	0.63	0.290	(0.095)	0.052	0.237
137	11.42	0.63	0.290	(0.094)	0.052	0.237
138	11.50	0.63	0.290	(0.094)	0.052	0.237
139	11.58	0.57	0.259	(0.093)	0.047	0.212
140	11.67	0.57	0.259	(0.093)	0.047	0.212
141	11.75	0.57	0.259	(0.092)	0.047	0.212
142	11.83	0.60	0.274	(0.092)	0.049	0.225
143	11.92	0.60	0.274	(0.092)	0.049	0.225
144	12.00	0.60	0.274	(0.091)	0.049	0.225
145	12.08	0.83	0.381	(0.091)	0.069	0.312
146	12.17	0.83	0.381	(0.090)	0.069	0.312
147	12.25	0.83	0.381	(0.090)	0.069	0.312
148	12.33	0.87	0.396	(0.089)	0.071	0.325
149	12.42	0.87	0.396	(0.089)	0.071	0.325
150	12.50	0.87	0.396	(0.088)	0.071	0.325
151	12.58	0.93	0.427	(0.088)	0.077	0.350
152	12.67	0.93	0.427	(0.087)	0.077	0.350
153	12.75	0.93	0.427	(0.087)	0.077	0.350
154	12.83	0.97	0.442	(0.087)	0.080	0.362
155	12.92	0.97	0.442	(0.086)	0.080	0.362
156	13.00	0.97	0.442	(0.086)	0.080	0.362
157	13.08	1.13	0.518	0.085	(0.093)	0.433
158	13.17	1.13	0.518	0.085	(0.093)	0.433
159	13.25	1.13	0.518	0.084	(0.093)	0.434
160	13.33	1.13	0.518	0.084	(0.093)	0.434
161	13.42	1.13	0.518	0.084	(0.093)	0.435
162	13.50	1.13	0.518	0.083	(0.093)	0.435
163	13.58	0.77	0.351	(0.083)	0.063	0.287
164	13.67	0.77	0.351	(0.082)	0.063	0.287
165	13.75	0.77	0.351	(0.082)	0.063	0.287
166	13.83	0.77	0.351	(0.081)	0.063	0.287
167	13.92	0.77	0.351	(0.081)	0.063	0.287
168	14.00	0.77	0.351	(0.081)	0.063	0.287
169	14.08	0.90	0.411	(0.080)	0.074	0.337
170	14.17	0.90	0.411	(0.080)	0.074	0.337
171	14.25	0.90	0.411	(0.079)	0.074	0.337
172	14.33	0.87	0.396	(0.079)	0.071	0.325
173	14.42	0.87	0.396	(0.079)	0.071	0.325
174	14.50	0.87	0.396	(0.078)	0.071	0.325
175	14.58	0.87	0.396	(0.078)	0.071	0.325
176	14.67	0.87	0.396	(0.077)	0.071	0.325
177	14.75	0.87	0.396	(0.077)	0.071	0.325
178	14.83	0.83	0.381	(0.077)	0.069	0.312
179	14.92	0.83	0.381	(0.076)	0.069	0.312
180	15.00	0.83	0.381	(0.076)	0.069	0.312
181	15.08	0.80	0.366	(0.075)	0.066	0.300
182	15.17	0.80	0.366	(0.075)	0.066	0.300
183	15.25	0.80	0.366	(0.075)	0.066	0.300
184	15.33	0.77	0.351	(0.074)	0.063	0.287
185	15.42	0.77	0.351	(0.074)	0.063	0.287

186	15.50	0.77	0.351	(0.073)	0.063	0.287
187	15.58	0.63	0.290	(0.073)	0.052	0.237
188	15.67	0.63	0.290	(0.073)	0.052	0.237
189	15.75	0.63	0.290	(0.072)	0.052	0.237
190	15.83	0.63	0.290	(0.072)	0.052	0.237
191	15.92	0.63	0.290	(0.072)	0.052	0.237
192	16.00	0.63	0.290	(0.071)	0.052	0.237
193	16.08	0.13	0.061	(0.071)	0.011	0.050
194	16.17	0.13	0.061	(0.071)	0.011	0.050
195	16.25	0.13	0.061	(0.070)	0.011	0.050
196	16.33	0.13	0.061	(0.070)	0.011	0.050
197	16.42	0.13	0.061	(0.069)	0.011	0.050
198	16.50	0.13	0.061	(0.069)	0.011	0.050
199	16.58	0.10	0.046	(0.069)	0.008	0.037
200	16.67	0.10	0.046	(0.068)	0.008	0.037
201	16.75	0.10	0.046	(0.068)	0.008	0.037
202	16.83	0.10	0.046	(0.068)	0.008	0.037
203	16.92	0.10	0.046	(0.067)	0.008	0.037
204	17.00	0.10	0.046	(0.067)	0.008	0.037
205	17.08	0.17	0.076	(0.067)	0.014	0.062
206	17.17	0.17	0.076	(0.066)	0.014	0.062
207	17.25	0.17	0.076	(0.066)	0.014	0.062
208	17.33	0.17	0.076	(0.066)	0.014	0.062
209	17.42	0.17	0.076	(0.065)	0.014	0.062
210	17.50	0.17	0.076	(0.065)	0.014	0.062
211	17.58	0.17	0.076	(0.065)	0.014	0.062
212	17.67	0.17	0.076	(0.064)	0.014	0.062
213	17.75	0.17	0.076	(0.064)	0.014	0.062
214	17.83	0.13	0.061	(0.064)	0.011	0.050
215	17.92	0.13	0.061	(0.063)	0.011	0.050
216	18.00	0.13	0.061	(0.063)	0.011	0.050
217	18.08	0.13	0.061	(0.063)	0.011	0.050
218	18.17	0.13	0.061	(0.063)	0.011	0.050
219	18.25	0.13	0.061	(0.062)	0.011	0.050
220	18.33	0.13	0.061	(0.062)	0.011	0.050
221	18.42	0.13	0.061	(0.062)	0.011	0.050
222	18.50	0.13	0.061	(0.061)	0.011	0.050
223	18.58	0.10	0.046	(0.061)	0.008	0.037
224	18.67	0.10	0.046	(0.061)	0.008	0.037
225	18.75	0.10	0.046	(0.060)	0.008	0.037
226	18.83	0.07	0.030	(0.060)	0.005	0.025
227	18.92	0.07	0.030	(0.060)	0.005	0.025
228	19.00	0.07	0.030	(0.060)	0.005	0.025
229	19.08	0.10	0.046	(0.059)	0.008	0.037
230	19.17	0.10	0.046	(0.059)	0.008	0.037
231	19.25	0.10	0.046	(0.059)	0.008	0.037
232	19.33	0.13	0.061	(0.058)	0.011	0.050
233	19.42	0.13	0.061	(0.058)	0.011	0.050
234	19.50	0.13	0.061	(0.058)	0.011	0.050
235	19.58	0.10	0.046	(0.058)	0.008	0.037
236	19.67	0.10	0.046	(0.057)	0.008	0.037
237	19.75	0.10	0.046	(0.057)	0.008	0.037
238	19.83	0.07	0.030	(0.057)	0.005	0.025
239	19.92	0.07	0.030	(0.057)	0.005	0.025
240	20.00	0.07	0.030	(0.056)	0.005	0.025
241	20.08	0.10	0.046	(0.056)	0.008	0.037
242	20.17	0.10	0.046	(0.056)	0.008	0.037
243	20.25	0.10	0.046	(0.056)	0.008	0.037
244	20.33	0.10	0.046	(0.055)	0.008	0.037
245	20.42	0.10	0.046	(0.055)	0.008	0.037
246	20.50	0.10	0.046	(0.055)	0.008	0.037
247	20.58	0.10	0.046	(0.055)	0.008	0.037
248	20.67	0.10	0.046	(0.054)	0.008	0.037
249	20.75	0.10	0.046	(0.054)	0.008	0.037
250	20.83	0.07	0.030	(0.054)	0.005	0.025
251	20.92	0.07	0.030	(0.054)	0.005	0.025
252	21.00	0.07	0.030	(0.054)	0.005	0.025
253	21.08	0.10	0.046	(0.053)	0.008	0.037
254	21.17	0.10	0.046	(0.053)	0.008	0.037
255	21.25	0.10	0.046	(0.053)	0.008	0.037
256	21.33	0.07	0.030	(0.053)	0.005	0.025
257	21.42	0.07	0.030	(0.053)	0.005	0.025

258	21.50	0.07	0.030	(0.052)	0.005	0.025
259	21.58	0.10	0.046	(0.052)	0.008	0.037
260	21.67	0.10	0.046	(0.052)	0.008	0.037
261	21.75	0.10	0.046	(0.052)	0.008	0.037
262	21.83	0.07	0.030	(0.052)	0.005	0.025
263	21.92	0.07	0.030	(0.051)	0.005	0.025
264	22.00	0.07	0.030	(0.051)	0.005	0.025
265	22.08	0.10	0.046	(0.051)	0.008	0.037
266	22.17	0.10	0.046	(0.051)	0.008	0.037
267	22.25	0.10	0.046	(0.051)	0.008	0.037
268	22.33	0.07	0.030	(0.051)	0.005	0.025
269	22.42	0.07	0.030	(0.050)	0.005	0.025
270	22.50	0.07	0.030	(0.050)	0.005	0.025
271	22.58	0.07	0.030	(0.050)	0.005	0.025
272	22.67	0.07	0.030	(0.050)	0.005	0.025
273	22.75	0.07	0.030	(0.050)	0.005	0.025
274	22.83	0.07	0.030	(0.050)	0.005	0.025
275	22.92	0.07	0.030	(0.050)	0.005	0.025
276	23.00	0.07	0.030	(0.049)	0.005	0.025
277	23.08	0.07	0.030	(0.049)	0.005	0.025
278	23.17	0.07	0.030	(0.049)	0.005	0.025
279	23.25	0.07	0.030	(0.049)	0.005	0.025
280	23.33	0.07	0.030	(0.049)	0.005	0.025
281	23.42	0.07	0.030	(0.049)	0.005	0.025
282	23.50	0.07	0.030	(0.049)	0.005	0.025
283	23.58	0.07	0.030	(0.049)	0.005	0.025
284	23.67	0.07	0.030	(0.049)	0.005	0.025
285	23.75	0.07	0.030	(0.049)	0.005	0.025
286	23.83	0.07	0.030	(0.049)	0.005	0.025
287	23.92	0.07	0.030	(0.049)	0.005	0.025
288	24.00	0.07	0.030	(0.049)	0.005	0.025

(Loss Rate Not Used)

Sum = 100.0 Sum = 37.5

Flood volume = Effective rainfall 3.13(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 1.4(Ac.Ft)
Total soil loss = 0.68(In)
Total soil loss = 0.301(Ac.Ft)
Total rainfall = 3.81(In)
Flood volume = 60309.8 Cubic Feet
Total soil loss = 13132.1 Cubic Feet

Peak flow rate of this hydrograph = 2.328(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0005	0.08	Q				
0+10	0.0014	0.13	Q				
0+15	0.0023	0.13	Q				
0+20	0.0035	0.17	Q				
0+25	0.0049	0.20	Q				
0+30	0.0063	0.20	Q				
0+35	0.0076	0.20	Q				
0+40	0.0090	0.20	Q				
0+45	0.0104	0.20	Q				
0+50	0.0120	0.24	Q				
0+55	0.0139	0.26	VQ				
1+ 0	0.0157	0.27	VQ				
1+ 5	0.0173	0.23	Q				
1+10	0.0187	0.20	Q				
1+15	0.0201	0.20	Q				
1+20	0.0215	0.20	Q				
1+25	0.0228	0.20	Q				
1+30	0.0242	0.20	Q				
1+35	0.0256	0.20	Q				
1+40	0.0270	0.20	Q				

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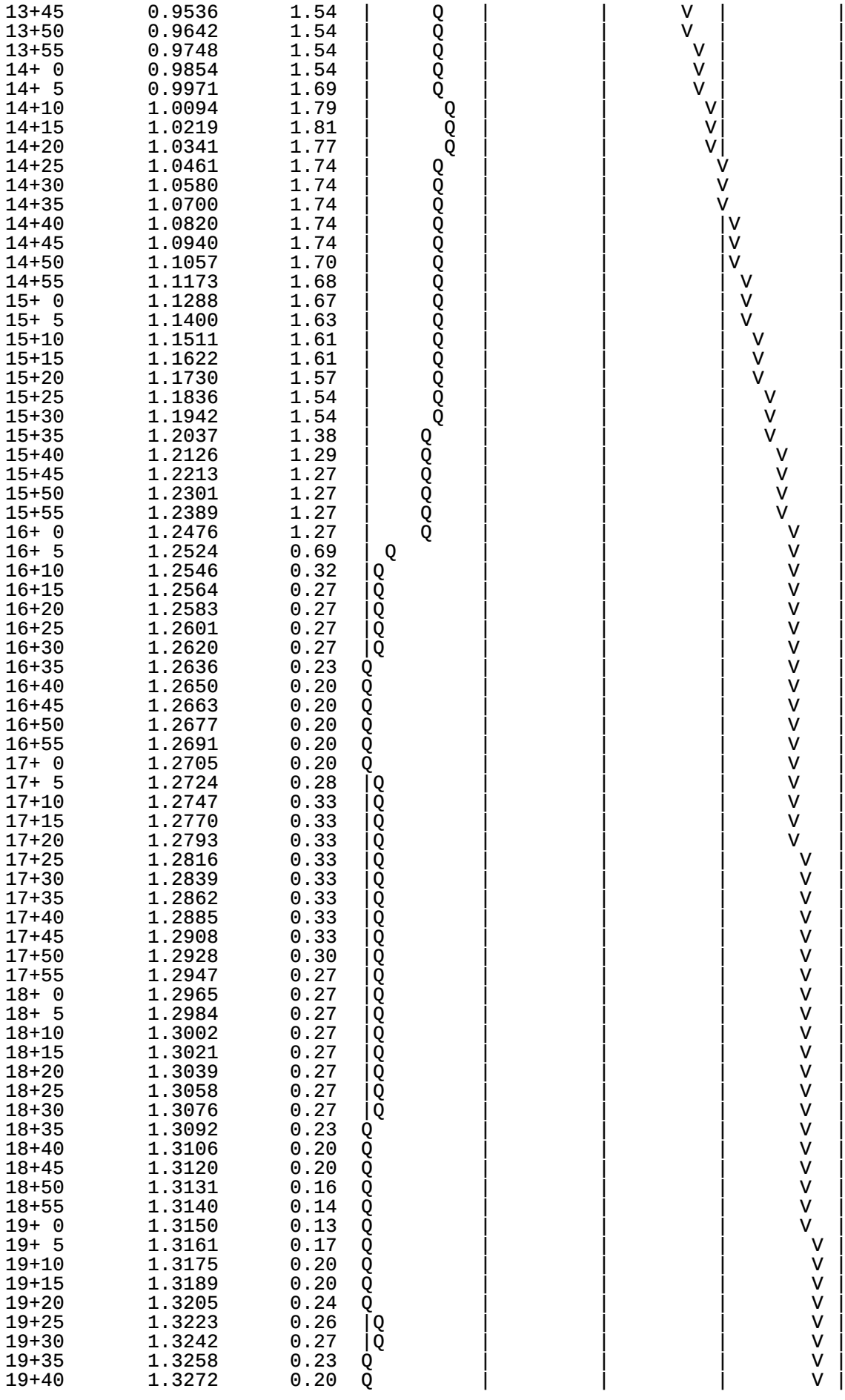
1+45       0.0284      0.20  Q         |          |          |          |
1+50       0.0300      0.24  Q         |          |          |          |
1+55       0.0318      0.26  VQ        |          |          |          |
2+ 0       0.0337      0.27  VQ        |          |          |          |
2+ 5       0.0355      0.27  |Q        |          |          |          |
2+10       0.0374      0.27  |Q        |          |          |          |
2+15       0.0392      0.27  |Q        |          |          |          |
2+20       0.0411      0.27  |Q        |          |          |          |
2+25       0.0429      0.27  |Q        |          |          |          |
2+30       0.0447      0.27  |Q        |          |          |          |
2+35       0.0469      0.31  |Q        |          |          |          |
2+40       0.0491      0.33  |Q        |          |          |          |
2+45       0.0514      0.33  |Q        |          |          |          |
2+50       0.0537      0.33  |Q        |          |          |          |
2+55       0.0560      0.33  |Q        |          |          |          |
3+ 0       0.0583      0.33  |Q        |          |          |          |
3+ 5       0.0606      0.33  |Q        |          |          |          |
3+10       0.0630      0.33  |Q        |          |          |          |
3+15       0.0653      0.33  |Q        |          |          |          |
3+20       0.0676      0.33  |Q        |          |          |          |
3+25       0.0699      0.33  |QV       |          |          |          |
3+30       0.0722      0.33  |QV       |          |          |          |
3+35       0.0745      0.33  |QV       |          |          |          |
3+40       0.0768      0.33  |QV       |          |          |          |
3+45       0.0791      0.33  |QV       |          |          |          |
3+50       0.0817      0.37  |QV       |          |          |          |
3+55       0.0844      0.40  |QV       |          |          |          |
4+ 0       0.0872      0.40  |QV       |          |          |          |
4+ 5       0.0899      0.40  |QV       |          |          |          |
4+10       0.0927      0.40  |QV       |          |          |          |
4+15       0.0955      0.40  |QV       |          |          |          |
4+20       0.0985      0.44  |QV       |          |          |          |
4+25       0.1017      0.46  |QV       |          |          |          |
4+30       0.1049      0.47  |Q V      |          |          |          |
4+35       0.1081      0.47  |Q V      |          |          |          |
4+40       0.1114      0.47  |Q V      |          |          |          |
4+45       0.1146      0.47  |Q V      |          |          |          |
4+50       0.1181      0.51  | QV      |          |          |          |
4+55       0.1217      0.53  | QV      |          |          |          |
5+ 0       0.1254      0.54  | QV      |          |          |          |
5+ 5       0.1286      0.46  |Q V      |          |          |          |
5+10       0.1314      0.41  |Q V      |          |          |          |
5+15       0.1342      0.40  |Q V      |          |          |          |
5+20       0.1372      0.44  |Q V      |          |          |          |
5+25       0.1404      0.46  |Q  V     |          |          |          |
5+30       0.1436      0.47  |Q  V     |          |          |          |
5+35       0.1471      0.51  | Q V     |          |          |          |
5+40       0.1508      0.53  | Q V     |          |          |          |
5+45       0.1545      0.54  | Q V     |          |          |          |
5+50       0.1581      0.54  | Q V     |          |          |          |
5+55       0.1618      0.54  | Q V     |          |          |          |
6+ 0       0.1655      0.54  | Q V     |          |          |          |
6+ 5       0.1695      0.57  | Q V     |          |          |          |
6+10       0.1736      0.60  | Q  V    |          |          |          |
6+15       0.1777      0.60  | Q  V    |          |          |          |
6+20       0.1819      0.60  | Q  V    |          |          |          |
6+25       0.1860      0.60  | Q  V    |          |          |          |
6+30       0.1902      0.60  | Q  V    |          |          |          |
6+35       0.1946      0.64  | Q  V    |          |          |          |
6+40       0.1992      0.67  | Q  V    |          |          |          |
6+45       0.2038      0.67  | Q  V    |          |          |          |
6+50       0.2084      0.67  | Q   V   |          |          |          |
6+55       0.2130      0.67  | Q   V   |          |          |          |
7+ 0       0.2176      0.67  | Q   V   |          |          |          |
7+ 5       0.2222      0.67  | Q   V   |          |          |          |
7+10       0.2268      0.67  | Q   V   |          |          |          |
7+15       0.2314      0.67  | Q   V   |          |          |          |
7+20       0.2363      0.71  | Q   V   |          |          |          |
7+25       0.2414      0.73  | Q   V   |          |          |          |
7+30       0.2464      0.74  | Q    V  |          |          |          |
7+35       0.2518      0.77  |  Q   V  |          |          |          |
7+40       0.2573      0.80  |  Q   V  |          |          |          |
```

7+45	0.2628	0.80	Q V				
7+50	0.2686	0.84	Q V				
7+55	0.2746	0.87	Q V				
8+ 0	0.2805	0.87	Q V				
8+ 5	0.2871	0.95	Q V				
8+10	0.2939	1.00	Q V				
8+15	0.3008	1.00	Q V				
8+20	0.3078	1.00	Q V				
8+25	0.3147	1.00	Q V				
8+30	0.3216	1.00	Q V				
8+35	0.3288	1.04	Q V				
8+40	0.3361	1.07	Q V				
8+45	0.3435	1.07	Q V				
8+50	0.3511	1.11	Q V				
8+55	0.3589	1.13	Q V				
9+ 0	0.3668	1.14	Q V				
9+ 5	0.3751	1.21	Q V				
9+10	0.3838	1.26	Q V				
9+15	0.3926	1.27	Q V				
9+20	0.4016	1.31	Q V				
9+25	0.4108	1.33	Q V				
9+30	0.4200	1.34	Q V				
9+35	0.4295	1.38	Q V				
9+40	0.4392	1.40	Q V				
9+45	0.4488	1.41	Q V				
9+50	0.4588	1.44	Q V				
9+55	0.4689	1.47	Q V				
10+ 0	0.4790	1.47	Q V				
10+ 5	0.4873	1.20	Q V				
10+10	0.4944	1.03	Q V				
10+15	0.5013	1.00	Q V				
10+20	0.5082	1.00	Q V				
10+25	0.5151	1.00	Q V				
10+30	0.5220	1.00	Q V				
10+35	0.5303	1.20	Q V				
10+40	0.5394	1.32	Q V				
10+45	0.5486	1.34	Q V				
10+50	0.5578	1.34	Q V				
10+55	0.5670	1.34	Q V				
11+ 0	0.5762	1.34	Q V				
11+ 5	0.5852	1.30	Q V				
11+10	0.5940	1.28	Q V				
11+15	0.6027	1.27	Q V				
11+20	0.6115	1.27	Q V				
11+25	0.6202	1.27	Q V				
11+30	0.6290	1.27	Q V				
11+35	0.6372	1.19	Q V				
11+40	0.6451	1.15	Q V				
11+45	0.6529	1.14	Q V				
11+50	0.6610	1.18	Q V				
11+55	0.6693	1.20	Q V				
12+ 0	0.6776	1.20	Q V				
12+ 5	0.6878	1.48	Q V				
12+10	0.6991	1.65	Q V				
12+15	0.7106	1.67	Q V				
12+20	0.7224	1.71	Q V				
12+25	0.7344	1.74	Q V				
12+30	0.7464	1.74	Q V				
12+35	0.7589	1.82	Q V				
12+40	0.7717	1.87	Q V				
12+45	0.7846	1.87	Q V				
12+50	0.7978	1.91	Q V				
12+55	0.8111	1.94	Q V				
13+ 0	0.8245	1.94	Q V				
13+ 5	0.8394	2.16	Q V				
13+10	0.8552	2.30	Q V				
13+15	0.8712	2.32	Q V				
13+20	0.8872	2.32	Q V				
13+25	0.9032	2.33	Q V				
13+30	0.9192	2.33	Q V				
13+35	0.9321	1.87	Q V				
13+40	0.9430	1.58	Q V				



13+45	0.9536	1.54	Q			V	
13+50	0.9642	1.54	Q			V	
13+55	0.9748	1.54	Q			V	
14+ 0	0.9854	1.54	Q			V	
14+ 5	0.9971	1.69	Q			V	
14+10	1.0094	1.79	Q			V	
14+15	1.0219	1.81	Q			V	
14+20	1.0341	1.77	Q			V	
14+25	1.0461	1.74	Q			V	
14+30	1.0580	1.74	Q			V	
14+35	1.0700	1.74	Q			V	
14+40	1.0820	1.74	Q			V	
14+45	1.0940	1.74	Q			V	
14+50	1.1057	1.70	Q			V	
14+55	1.1173	1.68	Q			V	
15+ 0	1.1288	1.67	Q			V	
15+ 5	1.1400	1.63	Q			V	
15+10	1.1511	1.61	Q			V	
15+15	1.1622	1.61	Q			V	
15+20	1.1730	1.57	Q			V	
15+25	1.1836	1.54	Q			V	
15+30	1.1942	1.54	Q			V	
15+35	1.2037	1.38	Q			V	
15+40	1.2126	1.29	Q			V	
15+45	1.2213	1.27	Q			V	
15+50	1.2301	1.27	Q			V	
15+55	1.2389	1.27	Q			V	
16+ 0	1.2476	1.27	Q			V	
16+ 5	1.2524	0.69	Q			V	
16+10	1.2546	0.32	Q			V	
16+15	1.2564	0.27	Q			V	
16+20	1.2583	0.27	Q			V	
16+25	1.2601	0.27	Q			V	
16+30	1.2620	0.27	Q			V	
16+35	1.2636	0.23	Q			V	
16+40	1.2650	0.20	Q			V	
16+45	1.2663	0.20	Q			V	
16+50	1.2677	0.20	Q			V	
16+55	1.2691	0.20	Q			V	
17+ 0	1.2705	0.20	Q			V	
17+ 5	1.2724	0.28	Q			V	
17+10	1.2747	0.33	Q			V	
17+15	1.2770	0.33	Q			V	
17+20	1.2793	0.33	Q			V	
17+25	1.2816	0.33	Q			V	
17+30	1.2839	0.33	Q			V	
17+35	1.2862	0.33	Q			V	
17+40	1.2885	0.33	Q			V	
17+45	1.2908	0.33	Q			V	
17+50	1.2928	0.30	Q			V	
17+55	1.2947	0.27	Q			V	
18+ 0	1.2965	0.27	Q			V	
18+ 5	1.2984	0.27	Q			V	
18+10	1.3002	0.27	Q			V	
18+15	1.3021	0.27	Q			V	
18+20	1.3039	0.27	Q			V	
18+25	1.3058	0.27	Q			V	
18+30	1.3076	0.27	Q			V	
18+35	1.3092	0.23	Q			V	
18+40	1.3106	0.20	Q			V	
18+45	1.3120	0.20	Q			V	
18+50	1.3131	0.16	Q			V	
18+55	1.3140	0.14	Q			V	
19+ 0	1.3150	0.13	Q			V	
19+ 5	1.3161	0.17	Q			V	
19+10	1.3175	0.20	Q			V	
19+15	1.3189	0.20	Q			V	
19+20	1.3205	0.24	Q			V	
19+25	1.3223	0.26	Q			V	
19+30	1.3242	0.27	Q			V	
19+35	1.3258	0.23	Q			V	
19+40	1.3272	0.20	Q			V	

19+45	1.3286	0.20	Q	|	|	|	V |
19+50	1.3297	0.16	Q	|	|	|	V |
19+55	1.3306	0.14	Q	|	|	|	V |
20+ 0	1.3315	0.13	Q	|	|	|	V |
20+ 5	1.3327	0.17	Q	|	|	|	V |
20+10	1.3341	0.20	Q	|	|	|	V |
20+15	1.3355	0.20	Q	|	|	|	V |
20+20	1.3369	0.20	Q	|	|	|	V |
20+25	1.3382	0.20	Q	|	|	|	V |
20+30	1.3396	0.20	Q	|	|	|	V |
20+35	1.3410	0.20	Q	|	|	|	V |
20+40	1.3424	0.20	Q	|	|	|	V |
20+45	1.3438	0.20	Q	|	|	|	V |
20+50	1.3449	0.16	Q	|	|	|	V |
20+55	1.3458	0.14	Q	|	|	|	V |
21+ 0	1.3468	0.13	Q	|	|	|	V |
21+ 5	1.3479	0.17	Q	|	|	|	V |
21+10	1.3493	0.20	Q	|	|	|	V |
21+15	1.3507	0.20	Q	|	|	|	V|
21+20	1.3518	0.16	Q	|	|	|	V|
21+25	1.3527	0.14	Q	|	|	|	V|
21+30	1.3537	0.13	Q	|	|	|	V|
21+35	1.3549	0.17	Q	|	|	|	V|
21+40	1.3562	0.20	Q	|	|	|	V|
21+45	1.3576	0.20	Q	|	|	|	V|
21+50	1.3587	0.16	Q	|	|	|	V|
21+55	1.3597	0.14	Q	|	|	|	V|
22+ 0	1.3606	0.13	Q	|	|	|	V|
22+ 5	1.3618	0.17	Q	|	|	|	V|
22+10	1.3631	0.20	Q	|	|	|	V|
22+15	1.3645	0.20	Q	|	|	|	V|
22+20	1.3656	0.16	Q	|	|	|	V|
22+25	1.3666	0.14	Q	|	|	|	V|
22+30	1.3675	0.13	Q	|	|	|	V|
22+35	1.3684	0.13	Q	|	|	|	V|
22+40	1.3693	0.13	Q	|	|	|	V|
22+45	1.3703	0.13	Q	|	|	|	V|
22+50	1.3712	0.13	Q	|	|	|	V|
22+55	1.3721	0.13	Q	|	|	|	V|
23+ 0	1.3730	0.13	Q	|	|	|	V|
23+ 5	1.3739	0.13	Q	|	|	|	V|
23+10	1.3749	0.13	Q	|	|	|	V|
23+15	1.3758	0.13	Q	|	|	|	V|
23+20	1.3767	0.13	Q	|	|	|	V|
23+25	1.3776	0.13	Q	|	|	|	V|
23+30	1.3786	0.13	Q	|	|	|	V|
23+35	1.3795	0.13	Q	|	|	|	V|
23+40	1.3804	0.13	Q	|	|	|	V|
23+45	1.3813	0.13	Q	|	|	|	V|
23+50	1.3822	0.13	Q	|	|	|	V|
23+55	1.3832	0.13	Q	|	|	|	V|
24+ 0	1.3841	0.13	Q	|	|	|	V|
24+ 5	1.3845	0.06	Q	|	|	|	V|
24+10	1.3845	0.01	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA10610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	1.20	6.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	3.00	15.93

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.941(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.940(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.116	(0.097)	0.021	0.095
2	0.17	0.60	0.140	(0.097)	0.025	0.115
3	0.25	0.60	0.140	(0.097)	0.025	0.115
4	0.33	0.60	0.140	(0.097)	0.025	0.115
5	0.42	0.60	0.140	(0.097)	0.025	0.115
6	0.50	0.70	0.163	(0.097)	0.029	0.134
7	0.58	0.70	0.163	(0.097)	0.029	0.134
8	0.67	0.70	0.163	(0.097)	0.029	0.134
9	0.75	0.70	0.163	(0.097)	0.029	0.134
10	0.83	0.70	0.163	(0.097)	0.029	0.134
11	0.92	0.70	0.163	(0.097)	0.029	0.134
12	1.00	0.80	0.186	(0.097)	0.034	0.153
13	1.08	0.80	0.186	(0.097)	0.034	0.153
14	1.17	0.80	0.186	(0.097)	0.034	0.153
15	1.25	0.80	0.186	(0.097)	0.034	0.153
16	1.33	0.80	0.186	(0.097)	0.034	0.153
17	1.42	0.80	0.186	(0.097)	0.034	0.153
18	1.50	0.80	0.186	(0.097)	0.034	0.153
19	1.58	0.80	0.186	(0.097)	0.034	0.153
20	1.67	0.80	0.186	(0.097)	0.034	0.153
21	1.75	0.80	0.186	(0.097)	0.034	0.153
22	1.83	0.80	0.186	(0.097)	0.034	0.153
23	1.92	0.80	0.186	(0.097)	0.034	0.153
24	2.00	0.90	0.210	(0.097)	0.038	0.172
25	2.08	0.80	0.186	(0.097)	0.034	0.153
26	2.17	0.90	0.210	(0.097)	0.038	0.172
27	2.25	0.90	0.210	(0.097)	0.038	0.172
28	2.33	0.90	0.210	(0.097)	0.038	0.172
29	2.42	0.90	0.210	(0.097)	0.038	0.172
30	2.50	0.90	0.210	(0.097)	0.038	0.172
31	2.58	0.90	0.210	(0.097)	0.038	0.172
32	2.67	0.90	0.210	(0.097)	0.038	0.172
33	2.75	1.00	0.233	(0.097)	0.042	0.191
34	2.83	1.00	0.233	(0.097)	0.042	0.191
35	2.92	1.00	0.233	(0.097)	0.042	0.191
36	3.00	1.00	0.233	(0.097)	0.042	0.191
37	3.08	1.00	0.233	(0.097)	0.042	0.191
38	3.17	1.10	0.256	(0.097)	0.046	0.210
39	3.25	1.10	0.256	(0.097)	0.046	0.210
40	3.33	1.10	0.256	(0.097)	0.046	0.210
41	3.42	1.20	0.279	(0.097)	0.050	0.229

42	3.50	1.30	0.303	(	0.097)	0.054		0.248
43	3.58	1.40	0.326	(	0.097)	0.059		0.267
44	3.67	1.40	0.326	(	0.097)	0.059		0.267
45	3.75	1.50	0.349	(	0.097)	0.063		0.286
46	3.83	1.50	0.349	(	0.097)	0.063		0.286
47	3.92	1.60	0.373	(	0.097)	0.067		0.306
48	4.00	1.60	0.373	(	0.097)	0.067		0.306
49	4.08	1.70	0.396	(	0.097)	0.071		0.325
50	4.17	1.80	0.419	(	0.097)	0.075		0.344
51	4.25	1.90	0.442	(	0.097)	0.080		0.363
52	4.33	2.00	0.466	(	0.097)	0.084		0.382
53	4.42	2.10	0.489	(	0.097)	0.088		0.401
54	4.50	2.10	0.489	(	0.097)	0.088		0.401
55	4.58	2.20	0.512	(	0.097)	0.092		0.420
56	4.67	2.30	0.536	(	0.097)	0.096		0.439
57	4.75	2.40	0.559		0.097	(0.101)		0.462
58	4.83	2.40	0.559		0.097	(0.101)		0.462
59	4.92	2.50	0.582		0.097	(0.105)		0.485
60	5.00	2.60	0.605		0.097	(0.109)		0.508
61	5.08	3.10	0.722		0.097	(0.130)		0.625
62	5.17	3.60	0.838		0.097	(0.151)		0.741
63	5.25	3.90	0.908		0.097	(0.163)		0.811
64	5.33	4.20	0.978		0.097	(0.176)		0.881
65	5.42	4.70	1.094		0.097	(0.197)		0.997
66	5.50	5.60	1.304		0.097	(0.235)		1.207
67	5.58	1.90	0.442	(	0.097)	0.080		0.363
68	5.67	0.90	0.210	(	0.097)	0.038		0.172
69	5.75	0.60	0.140	(	0.097)	0.025		0.115
70	5.83	0.50	0.116	(	0.097)	0.021		0.095
71	5.92	0.30	0.070	(	0.097)	0.013		0.057
72	6.00	0.20	0.047	(	0.097)	0.008		0.038

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.6

Flood volume = Effective rainfall 1.63(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.7(Ac.Ft)
Total soil loss = 0.31(In)
Total soil loss = 0.136(Ac.Ft)
Total rainfall = 1.94(In)
Flood volume = 31468.5 Cubic Feet
Total soil loss = 5935.2 Cubic Feet

Peak flow rate of this hydrograph = 5.954(CFS)

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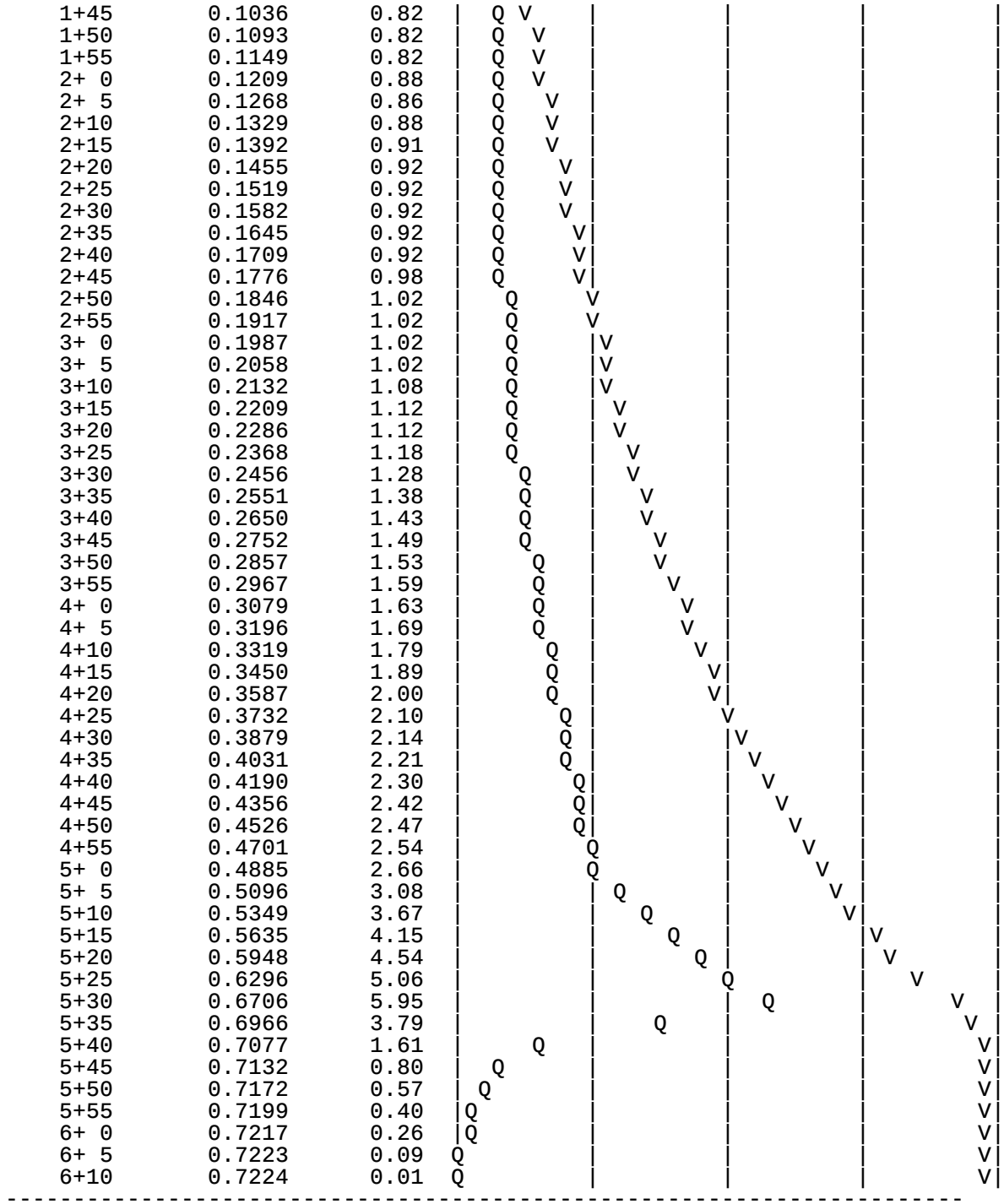
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0020	0.30	VQ				
0+10	0.0058	0.54	V Q				
0+15	0.0099	0.61	V Q				
0+20	0.0142	0.61	V Q				
0+25	0.0184	0.61	|VQ				
0+30	0.0230	0.67	|VQ				
0+35	0.0279	0.71	|VQ				
0+40	0.0328	0.72	|VQ				
0+45	0.0378	0.72	| Q				
0+50	0.0427	0.72	| Q				
0+55	0.0476	0.72	| Q				
1+ 0	0.0530	0.77	| VQ				
1+ 5	0.0586	0.81	| Q				
1+10	0.0642	0.82	| Q				
1+15	0.0698	0.82	| Q				
1+20	0.0755	0.82	| QV				
1+25	0.0811	0.82	| QV				
1+30	0.0867	0.82	| QV				
1+35	0.0924	0.82	| Q V				
1+40	0.0980	0.82	| Q V				


1+45 0.1036 0.82
1+50 0.1093 0.82
1+55 0.1149 0.82
2+ 0 0.1209 0.88
2+ 5 0.1268 0.86
2+10 0.1329 0.88
2+15 0.1392 0.91
2+20 0.1455 0.92
2+25 0.1519 0.92
2+30 0.1582 0.92
2+35 0.1645 0.92
2+40 0.1709 0.92
2+45 0.1776 0.98
2+50 0.1846 1.02
2+55 0.1917 1.02
3+ 0 0.1987 1.02
3+ 5 0.2058 1.02
3+10 0.2132 1.08
3+15 0.2209 1.12
3+20 0.2286 1.12
3+25 0.2368 1.18
3+30 0.2456 1.28
3+35 0.2551 1.38
3+40 0.2650 1.43
3+45 0.2752 1.49
3+50 0.2857 1.53
3+55 0.2967 1.59
4+ 0 0.3079 1.63
4+ 5 0.3196 1.69
4+10 0.3319 1.79
4+15 0.3450 1.89
4+20 0.3587 2.00
4+25 0.3732 2.10
4+30 0.3879 2.14
4+35 0.4031 2.21
4+40 0.4190 2.30
4+45 0.4356 2.42
4+50 0.4526 2.47
4+55 0.4701 2.54
5+ 0 0.4885 2.66
5+ 5 0.5096 3.08
5+10 0.5349 3.67
5+15 0.5635 4.15
5+20 0.5948 4.54
5+25 0.6296 5.06
5+30 0.6706 5.95
5+35 0.6966 3.79
5+40 0.7077 1.61
5+45 0.7132 0.80
5+50 0.7172 0.57
5+55 0.7199 0.40
6+ 0 0.7217 0.26
6+ 5 0.7223 0.09
6+10 0.7224 0.01

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA10310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	0.90	4.78

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	2.35	12.48

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.497(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.497(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
			Sum = 100.000	Sum= 5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	1.30	0.233	(0.097)		0.042	0.191
2	0.17	1.30	0.233	(0.097)		0.042	0.191
3	0.25	1.10	0.198	(0.097)		0.036	0.162
4	0.33	1.50	0.269	(0.097)		0.048	0.221
5	0.42	1.50	0.269	(0.097)		0.048	0.221
6	0.50	1.80	0.323	(0.097)		0.058	0.265
7	0.58	1.50	0.269	(0.097)		0.048	0.221
8	0.67	1.80	0.323	(0.097)		0.058	0.265
9	0.75	1.80	0.323	(0.097)		0.058	0.265
10	0.83	1.50	0.269	(0.097)		0.048	0.221
11	0.92	1.60	0.287	(0.097)		0.052	0.236
12	1.00	1.80	0.323	(0.097)		0.058	0.265
13	1.08	2.20	0.395	(0.097)		0.071	0.324
14	1.17	2.20	0.395	(0.097)		0.071	0.324
15	1.25	2.20	0.395	(0.097)		0.071	0.324
16	1.33	2.00	0.359	(0.097)		0.065	0.295
17	1.42	2.60	0.467	(0.097)		0.084	0.383
18	1.50	2.70	0.485	(0.097)		0.087	0.398
19	1.58	2.40	0.431	(0.097)		0.078	0.353
20	1.67	2.70	0.485	(0.097)		0.087	0.398
21	1.75	3.30	0.593	0.097	(	0.107)	0.496
22	1.83	3.10	0.557	0.097	(	0.100)	0.460
23	1.92	2.90	0.521	(0.097)		0.094	0.427
24	2.00	3.00	0.539	(0.097)		0.097	0.442
25	2.08	3.10	0.557	0.097	(	0.100)	0.460
26	2.17	4.20	0.754	0.097	(	0.136)	0.657
27	2.25	5.00	0.898	0.097	(	0.162)	0.801
28	2.33	3.50	0.629	0.097	(	0.113)	0.531
29	2.42	6.80	1.221	0.097	(	0.220)	1.124
30	2.50	7.30	1.311	0.097	(	0.236)	1.214
31	2.58	8.20	1.473	0.097	(	0.265)	1.376
32	2.67	5.90	1.060	0.097	(	0.191)	0.962
33	2.75	2.00	0.359	(0.097)		0.065	0.295
34	2.83	1.80	0.323	(0.097)		0.058	0.265
35	2.92	1.80	0.323	(0.097)		0.058	0.265
36	3.00	0.60	0.108	(0.097)		0.019	0.088
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	15.4

Flood volume = Effective rainfall 1.28(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.21(In)

Total soil loss = 0.095(Ac.Ft)
Total rainfall = 1.50(In)
Flood volume = 24711.4 Cubic Feet
Total soil loss = 4134.3 Cubic Feet

Peak flow rate of this hydrograph = 6.973(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0041	0.59	V Q
0+10	0.0107	0.97	V Q
0+15	0.0172	0.93	V Q
0+20	0.0245	1.06	V Q
0+25	0.0325	1.16	V Q
0+30	0.0416	1.32	V Q
0+35	0.0503	1.27	V Q
0+40	0.0595	1.33	VQ
0+45	0.0692	1.41	VQ
0+50	0.0780	1.28	Q
0+55	0.0866	1.24	Q V
1+ 0	0.0958	1.35	QV
1+ 5	0.1068	1.59	QV
1+10	0.1186	1.72	Q V
1+15	0.1306	1.73	Q V
1+20	0.1419	1.64	Q V
1+25	0.1547	1.86	Q V
1+30	0.1689	2.07	Q V
1+35	0.1826	1.99	Q V
1+40	0.1967	2.04	Q V
1+45	0.2134	2.42	Q V
1+50	0.2307	2.51	Q V
1+55	0.2470	2.37	Q V
2+ 0	0.2631	2.34	Q V
2+ 5	0.2798	2.42	Q V
2+10	0.3009	3.07	Q V
2+15	0.3278	3.90	Q V
2+20	0.3513	3.41	Q V
2+25	0.3841	4.76	Q V
2+30	0.4262	6.12	Q V
2+35	0.4742	6.97	Q V
2+40	0.5158	6.04	Q V
2+45	0.5379	3.21	Q V
2+50	0.5495	1.69	Q V
2+55	0.5594	1.43	Q V
3+ 0	0.5654	0.87	Q V
3+ 5	0.5671	0.25	Q V
3+10	0.5673	0.03	Q V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PA10110.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 5.31(Ac.) = 0.008 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 5.31(Ac.) = 0.008 Sq. Mi.
Length along longest watercourse = 699.00(Ft.)
Length along longest watercourse measured to centroid = 450.00(Ft.)
Length along longest watercourse = 0.132 Mi.
Length along longest watercourse measured to centroid = 0.085 Mi.
Difference in elevation = 14.70(Ft.)
Slope along watercourse = 111.0386 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.027 Hr.
Lag time = 1.61 Min.
25% of lag time = 0.40 Min.
40% of lag time = 0.64 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	0.54	2.87

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
5.31	1.36	7.22

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.877(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.877(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
5.310	56.00	0.900

Total Area Entered = 5.31(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	311.341	57.815	3.094
2	0.167	622.682	36.513	1.954
3	0.250	934.022	5.672	0.304
		Sum = 100.000	Sum=	5.351

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.463	(0.097)	0.083	0.380
2	0.17	4.50	0.474	(0.097)	0.085	0.388
3	0.25	5.40	0.568	0.097	(0.102)	0.471
4	0.33	5.40	0.568	0.097	(0.102)	0.471
5	0.42	5.70	0.600	0.097	(0.108)	0.503
6	0.50	6.40	0.674	0.097	(0.121)	0.577
7	0.58	7.90	0.832	0.097	(0.150)	0.735
8	0.67	9.10	0.958	0.097	(0.172)	0.861
9	0.75	12.80	1.348	0.097	(0.243)	1.250
10	0.83	25.60	2.695	0.097	(0.485)	2.598
11	0.92	7.90	0.832	0.097	(0.150)	0.735
12	1.00	4.90	0.516	(0.097)	0.093	0.423
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	9.4

Flood volume = Effective rainfall 0.78(In)
times area 5.3(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.09(In)
Total soil loss = 0.042(Ac.Ft)
Total rainfall = 0.88(In)
Flood volume = 15087.4 Cubic Feet
Total soil loss = 1823.1 Cubic Feet

Peak flow rate of this hydrograph = 10.749(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0081	1.18	V Q				
0+10	0.0215	1.95	| VQ				
0+15	0.0376	2.33	| Q				
0+20	0.0548	2.50	| Q V				
0+25	0.0728	2.62	| Q V				
0+30	0.0929	2.91	| Q V				

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   0+35       0.1174      3.55  |      Q  |  V      |          |          |
   0+40       0.1468      4.28  |       Q |     V   |          |          |
   0+45       0.1866      5.78  |         |Q        |V         |          |
   0+50       0.2606     10.75  |         |         |Q         V          |
   0+55       0.3139      7.73  |         |    Q    |          |     V    |
   1+ 0       0.3382      3.53  |      Q  |         |          |          V|
   1+ 5       0.3455      1.05  | Q       |         |          |          V|
   1+10       0.3464      0.13  Q         |         |          |          V|
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB02242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	2.00	0.26

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	6.40	0.83

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
			Sum = 100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(0.238)	0.003	0.013
2	0.17	0.07	0.016	(0.237)	0.003	0.013
3	0.25	0.07	0.016	(0.236)	0.003	0.013
4	0.33	0.10	0.024	(0.235)	0.004	0.020
5	0.42	0.10	0.024	(0.234)	0.004	0.020
6	0.50	0.10	0.024	(0.233)	0.004	0.020
7	0.58	0.10	0.024	(0.232)	0.004	0.020
8	0.67	0.10	0.024	(0.231)	0.004	0.020
9	0.75	0.10	0.024	(0.230)	0.004	0.020
10	0.83	0.13	0.032	(0.230)	0.006	0.026
11	0.92	0.13	0.032	(0.229)	0.006	0.026
12	1.00	0.13	0.032	(0.228)	0.006	0.026
13	1.08	0.10	0.024	(0.227)	0.004	0.020
14	1.17	0.10	0.024	(0.226)	0.004	0.020
15	1.25	0.10	0.024	(0.225)	0.004	0.020
16	1.33	0.10	0.024	(0.224)	0.004	0.020
17	1.42	0.10	0.024	(0.223)	0.004	0.020
18	1.50	0.10	0.024	(0.222)	0.004	0.020
19	1.58	0.10	0.024	(0.222)	0.004	0.020
20	1.67	0.10	0.024	(0.221)	0.004	0.020
21	1.75	0.10	0.024	(0.220)	0.004	0.020
22	1.83	0.13	0.032	(0.219)	0.006	0.026
23	1.92	0.13	0.032	(0.218)	0.006	0.026
24	2.00	0.13	0.032	(0.217)	0.006	0.026
25	2.08	0.13	0.032	(0.216)	0.006	0.026
26	2.17	0.13	0.032	(0.215)	0.006	0.026
27	2.25	0.13	0.032	(0.214)	0.006	0.026
28	2.33	0.13	0.032	(0.214)	0.006	0.026
29	2.42	0.13	0.032	(0.213)	0.006	0.026
30	2.50	0.13	0.032	(0.212)	0.006	0.026
31	2.58	0.17	0.040	(0.211)	0.007	0.033
32	2.67	0.17	0.040	(0.210)	0.007	0.033
33	2.75	0.17	0.040	(0.209)	0.007	0.033
34	2.83	0.17	0.040	(0.208)	0.007	0.033
35	2.92	0.17	0.040	(0.208)	0.007	0.033
36	3.00	0.17	0.040	(0.207)	0.007	0.033
37	3.08	0.17	0.040	(0.206)	0.007	0.033
38	3.17	0.17	0.040	(0.205)	0.007	0.033
39	3.25	0.17	0.040	(0.204)	0.007	0.033
40	3.33	0.17	0.040	(0.203)	0.007	0.033
41	3.42	0.17	0.040	(0.202)	0.007	0.033
42	3.50	0.17	0.040	(0.202)	0.007	0.033
43	3.58	0.17	0.040	(0.201)	0.007	0.033

44	3.67	0.17	0.040	(0.200)	0.007	0.033
45	3.75	0.17	0.040	(0.199)	0.007	0.033
46	3.83	0.20	0.048	(0.198)	0.009	0.039
47	3.92	0.20	0.048	(0.197)	0.009	0.039
48	4.00	0.20	0.048	(0.197)	0.009	0.039
49	4.08	0.20	0.048	(0.196)	0.009	0.039
50	4.17	0.20	0.048	(0.195)	0.009	0.039
51	4.25	0.20	0.048	(0.194)	0.009	0.039
52	4.33	0.23	0.056	(0.193)	0.010	0.046
53	4.42	0.23	0.056	(0.192)	0.010	0.046
54	4.50	0.23	0.056	(0.192)	0.010	0.046
55	4.58	0.23	0.056	(0.191)	0.010	0.046
56	4.67	0.23	0.056	(0.190)	0.010	0.046
57	4.75	0.23	0.056	(0.189)	0.010	0.046
58	4.83	0.27	0.064	(0.188)	0.012	0.052
59	4.92	0.27	0.064	(0.187)	0.012	0.052
60	5.00	0.27	0.064	(0.187)	0.012	0.052
61	5.08	0.20	0.048	(0.186)	0.009	0.039
62	5.17	0.20	0.048	(0.185)	0.009	0.039
63	5.25	0.20	0.048	(0.184)	0.009	0.039
64	5.33	0.23	0.056	(0.183)	0.010	0.046
65	5.42	0.23	0.056	(0.183)	0.010	0.046
66	5.50	0.23	0.056	(0.182)	0.010	0.046
67	5.58	0.27	0.064	(0.181)	0.012	0.052
68	5.67	0.27	0.064	(0.180)	0.012	0.052
69	5.75	0.27	0.064	(0.179)	0.012	0.052
70	5.83	0.27	0.064	(0.179)	0.012	0.052
71	5.92	0.27	0.064	(0.178)	0.012	0.052
72	6.00	0.27	0.064	(0.177)	0.012	0.052
73	6.08	0.30	0.072	(0.176)	0.013	0.059
74	6.17	0.30	0.072	(0.175)	0.013	0.059
75	6.25	0.30	0.072	(0.175)	0.013	0.059
76	6.33	0.30	0.072	(0.174)	0.013	0.059
77	6.42	0.30	0.072	(0.173)	0.013	0.059
78	6.50	0.30	0.072	(0.172)	0.013	0.059
79	6.58	0.33	0.080	(0.172)	0.014	0.066
80	6.67	0.33	0.080	(0.171)	0.014	0.066
81	6.75	0.33	0.080	(0.170)	0.014	0.066
82	6.83	0.33	0.080	(0.169)	0.014	0.066
83	6.92	0.33	0.080	(0.169)	0.014	0.066
84	7.00	0.33	0.080	(0.168)	0.014	0.066
85	7.08	0.33	0.080	(0.167)	0.014	0.066
86	7.17	0.33	0.080	(0.166)	0.014	0.066
87	7.25	0.33	0.080	(0.165)	0.014	0.066
88	7.33	0.37	0.088	(0.165)	0.016	0.072
89	7.42	0.37	0.088	(0.164)	0.016	0.072
90	7.50	0.37	0.088	(0.163)	0.016	0.072
91	7.58	0.40	0.096	(0.162)	0.017	0.079
92	7.67	0.40	0.096	(0.162)	0.017	0.079
93	7.75	0.40	0.096	(0.161)	0.017	0.079
94	7.83	0.43	0.104	(0.160)	0.019	0.085
95	7.92	0.43	0.104	(0.159)	0.019	0.085
96	8.00	0.43	0.104	(0.159)	0.019	0.085
97	8.08	0.50	0.120	(0.158)	0.022	0.098
98	8.17	0.50	0.120	(0.157)	0.022	0.098
99	8.25	0.50	0.120	(0.157)	0.022	0.098
100	8.33	0.50	0.120	(0.156)	0.022	0.098
101	8.42	0.50	0.120	(0.155)	0.022	0.098
102	8.50	0.50	0.120	(0.154)	0.022	0.098
103	8.58	0.53	0.128	(0.154)	0.023	0.105
104	8.67	0.53	0.128	(0.153)	0.023	0.105
105	8.75	0.53	0.128	(0.152)	0.023	0.105
106	8.83	0.57	0.136	(0.151)	0.024	0.112
107	8.92	0.57	0.136	(0.151)	0.024	0.112
108	9.00	0.57	0.136	(0.150)	0.024	0.112
109	9.08	0.63	0.152	(0.149)	0.027	0.125
110	9.17	0.63	0.152	(0.149)	0.027	0.125
111	9.25	0.63	0.152	(0.148)	0.027	0.125
112	9.33	0.67	0.160	(0.147)	0.029	0.131
113	9.42	0.67	0.160	(0.147)	0.029	0.131
114	9.50	0.67	0.160	(0.146)	0.029	0.131
115	9.58	0.70	0.168	(0.145)	0.030	0.138

116	9.67	0.70	0.168	(0.144)	0.030	0.138
117	9.75	0.70	0.168	(0.144)	0.030	0.138
118	9.83	0.73	0.176	(0.143)	0.032	0.144
119	9.92	0.73	0.176	(0.142)	0.032	0.144
120	10.00	0.73	0.176	(0.142)	0.032	0.144
121	10.08	0.50	0.120	(0.141)	0.022	0.098
122	10.17	0.50	0.120	(0.140)	0.022	0.098
123	10.25	0.50	0.120	(0.140)	0.022	0.098
124	10.33	0.50	0.120	(0.139)	0.022	0.098
125	10.42	0.50	0.120	(0.138)	0.022	0.098
126	10.50	0.50	0.120	(0.138)	0.022	0.098
127	10.58	0.67	0.160	(0.137)	0.029	0.131
128	10.67	0.67	0.160	(0.136)	0.029	0.131
129	10.75	0.67	0.160	(0.136)	0.029	0.131
130	10.83	0.67	0.160	(0.135)	0.029	0.131
131	10.92	0.67	0.160	(0.134)	0.029	0.131
132	11.00	0.67	0.160	(0.134)	0.029	0.131
133	11.08	0.63	0.152	(0.133)	0.027	0.125
134	11.17	0.63	0.152	(0.132)	0.027	0.125
135	11.25	0.63	0.152	(0.132)	0.027	0.125
136	11.33	0.63	0.152	(0.131)	0.027	0.125
137	11.42	0.63	0.152	(0.130)	0.027	0.125
138	11.50	0.63	0.152	(0.130)	0.027	0.125
139	11.58	0.57	0.136	(0.129)	0.024	0.112
140	11.67	0.57	0.136	(0.128)	0.024	0.112
141	11.75	0.57	0.136	(0.128)	0.024	0.112
142	11.83	0.60	0.144	(0.127)	0.026	0.118
143	11.92	0.60	0.144	(0.126)	0.026	0.118
144	12.00	0.60	0.144	(0.126)	0.026	0.118
145	12.08	0.83	0.200	(0.125)	0.036	0.164
146	12.17	0.83	0.200	(0.125)	0.036	0.164
147	12.25	0.83	0.200	(0.124)	0.036	0.164
148	12.33	0.87	0.208	(0.123)	0.037	0.171
149	12.42	0.87	0.208	(0.123)	0.037	0.171
150	12.50	0.87	0.208	(0.122)	0.037	0.171
151	12.58	0.93	0.224	(0.121)	0.040	0.184
152	12.67	0.93	0.224	(0.121)	0.040	0.184
153	12.75	0.93	0.224	(0.120)	0.040	0.184
154	12.83	0.97	0.232	(0.120)	0.042	0.190
155	12.92	0.97	0.232	(0.119)	0.042	0.190
156	13.00	0.97	0.232	(0.118)	0.042	0.190
157	13.08	1.13	0.272	(0.118)	0.049	0.223
158	13.17	1.13	0.272	(0.117)	0.049	0.223
159	13.25	1.13	0.272	(0.117)	0.049	0.223
160	13.33	1.13	0.272	(0.116)	0.049	0.223
161	13.42	1.13	0.272	(0.115)	0.049	0.223
162	13.50	1.13	0.272	(0.115)	0.049	0.223
163	13.58	0.77	0.184	(0.114)	0.033	0.151
164	13.67	0.77	0.184	(0.114)	0.033	0.151
165	13.75	0.77	0.184	(0.113)	0.033	0.151
166	13.83	0.77	0.184	(0.113)	0.033	0.151
167	13.92	0.77	0.184	(0.112)	0.033	0.151
168	14.00	0.77	0.184	(0.111)	0.033	0.151
169	14.08	0.90	0.216	(0.111)	0.039	0.177
170	14.17	0.90	0.216	(0.110)	0.039	0.177
171	14.25	0.90	0.216	(0.110)	0.039	0.177
172	14.33	0.87	0.208	(0.109)	0.037	0.171
173	14.42	0.87	0.208	(0.109)	0.037	0.171
174	14.50	0.87	0.208	(0.108)	0.037	0.171
175	14.58	0.87	0.208	(0.107)	0.037	0.171
176	14.67	0.87	0.208	(0.107)	0.037	0.171
177	14.75	0.87	0.208	(0.106)	0.037	0.171
178	14.83	0.83	0.200	(0.106)	0.036	0.164
179	14.92	0.83	0.200	(0.105)	0.036	0.164
180	15.00	0.83	0.200	(0.105)	0.036	0.164
181	15.08	0.80	0.192	(0.104)	0.035	0.157
182	15.17	0.80	0.192	(0.104)	0.035	0.157
183	15.25	0.80	0.192	(0.103)	0.035	0.157
184	15.33	0.77	0.184	(0.103)	0.033	0.151
185	15.42	0.77	0.184	(0.102)	0.033	0.151
186	15.50	0.77	0.184	(0.102)	0.033	0.151
187	15.58	0.63	0.152	(0.101)	0.027	0.125

188	15.67	0.63	0.152	(0.101)	0.027	0.125
189	15.75	0.63	0.152	(0.100)	0.027	0.125
190	15.83	0.63	0.152	(0.100)	0.027	0.125
191	15.92	0.63	0.152	(0.099)	0.027	0.125
192	16.00	0.63	0.152	(0.099)	0.027	0.125
193	16.08	0.13	0.032	(0.098)	0.006	0.026
194	16.17	0.13	0.032	(0.098)	0.006	0.026
195	16.25	0.13	0.032	(0.097)	0.006	0.026
196	16.33	0.13	0.032	(0.097)	0.006	0.026
197	16.42	0.13	0.032	(0.096)	0.006	0.026
198	16.50	0.13	0.032	(0.096)	0.006	0.026
199	16.58	0.10	0.024	(0.095)	0.004	0.020
200	16.67	0.10	0.024	(0.095)	0.004	0.020
201	16.75	0.10	0.024	(0.094)	0.004	0.020
202	16.83	0.10	0.024	(0.094)	0.004	0.020
203	16.92	0.10	0.024	(0.093)	0.004	0.020
204	17.00	0.10	0.024	(0.093)	0.004	0.020
205	17.08	0.17	0.040	(0.092)	0.007	0.033
206	17.17	0.17	0.040	(0.092)	0.007	0.033
207	17.25	0.17	0.040	(0.091)	0.007	0.033
208	17.33	0.17	0.040	(0.091)	0.007	0.033
209	17.42	0.17	0.040	(0.090)	0.007	0.033
210	17.50	0.17	0.040	(0.090)	0.007	0.033
211	17.58	0.17	0.040	(0.089)	0.007	0.033
212	17.67	0.17	0.040	(0.089)	0.007	0.033
213	17.75	0.17	0.040	(0.089)	0.007	0.033
214	17.83	0.13	0.032	(0.088)	0.006	0.026
215	17.92	0.13	0.032	(0.088)	0.006	0.026
216	18.00	0.13	0.032	(0.087)	0.006	0.026
217	18.08	0.13	0.032	(0.087)	0.006	0.026
218	18.17	0.13	0.032	(0.086)	0.006	0.026
219	18.25	0.13	0.032	(0.086)	0.006	0.026
220	18.33	0.13	0.032	(0.086)	0.006	0.026
221	18.42	0.13	0.032	(0.085)	0.006	0.026
222	18.50	0.13	0.032	(0.085)	0.006	0.026
223	18.58	0.10	0.024	(0.084)	0.004	0.020
224	18.67	0.10	0.024	(0.084)	0.004	0.020
225	18.75	0.10	0.024	(0.084)	0.004	0.020
226	18.83	0.07	0.016	(0.083)	0.003	0.013
227	18.92	0.07	0.016	(0.083)	0.003	0.013
228	19.00	0.07	0.016	(0.082)	0.003	0.013
229	19.08	0.10	0.024	(0.082)	0.004	0.020
230	19.17	0.10	0.024	(0.082)	0.004	0.020
231	19.25	0.10	0.024	(0.081)	0.004	0.020
232	19.33	0.13	0.032	(0.081)	0.006	0.026
233	19.42	0.13	0.032	(0.080)	0.006	0.026
234	19.50	0.13	0.032	(0.080)	0.006	0.026
235	19.58	0.10	0.024	(0.080)	0.004	0.020
236	19.67	0.10	0.024	(0.079)	0.004	0.020
237	19.75	0.10	0.024	(0.079)	0.004	0.020
238	19.83	0.07	0.016	(0.079)	0.003	0.013
239	19.92	0.07	0.016	(0.078)	0.003	0.013
240	20.00	0.07	0.016	(0.078)	0.003	0.013
241	20.08	0.10	0.024	(0.078)	0.004	0.020
242	20.17	0.10	0.024	(0.077)	0.004	0.020
243	20.25	0.10	0.024	(0.077)	0.004	0.020
244	20.33	0.10	0.024	(0.077)	0.004	0.020
245	20.42	0.10	0.024	(0.076)	0.004	0.020
246	20.50	0.10	0.024	(0.076)	0.004	0.020
247	20.58	0.10	0.024	(0.076)	0.004	0.020
248	20.67	0.10	0.024	(0.075)	0.004	0.020
249	20.75	0.10	0.024	(0.075)	0.004	0.020
250	20.83	0.07	0.016	(0.075)	0.003	0.013
251	20.92	0.07	0.016	(0.074)	0.003	0.013
252	21.00	0.07	0.016	(0.074)	0.003	0.013
253	21.08	0.10	0.024	(0.074)	0.004	0.020
254	21.17	0.10	0.024	(0.073)	0.004	0.020
255	21.25	0.10	0.024	(0.073)	0.004	0.020
256	21.33	0.07	0.016	(0.073)	0.003	0.013
257	21.42	0.07	0.016	(0.073)	0.003	0.013
258	21.50	0.07	0.016	(0.072)	0.003	0.013
259	21.58	0.10	0.024	(0.072)	0.004	0.020

260	21.67	0.10	0.024	(0.072)	0.004	0.020
261	21.75	0.10	0.024	(0.072)	0.004	0.020
262	21.83	0.07	0.016	(0.071)	0.003	0.013
263	21.92	0.07	0.016	(0.071)	0.003	0.013
264	22.00	0.07	0.016	(0.071)	0.003	0.013
265	22.08	0.10	0.024	(0.071)	0.004	0.020
266	22.17	0.10	0.024	(0.070)	0.004	0.020
267	22.25	0.10	0.024	(0.070)	0.004	0.020
268	22.33	0.07	0.016	(0.070)	0.003	0.013
269	22.42	0.07	0.016	(0.070)	0.003	0.013
270	22.50	0.07	0.016	(0.069)	0.003	0.013
271	22.58	0.07	0.016	(0.069)	0.003	0.013
272	22.67	0.07	0.016	(0.069)	0.003	0.013
273	22.75	0.07	0.016	(0.069)	0.003	0.013
274	22.83	0.07	0.016	(0.069)	0.003	0.013
275	22.92	0.07	0.016	(0.069)	0.003	0.013
276	23.00	0.07	0.016	(0.068)	0.003	0.013
277	23.08	0.07	0.016	(0.068)	0.003	0.013
278	23.17	0.07	0.016	(0.068)	0.003	0.013
279	23.25	0.07	0.016	(0.068)	0.003	0.013
280	23.33	0.07	0.016	(0.068)	0.003	0.013
281	23.42	0.07	0.016	(0.068)	0.003	0.013
282	23.50	0.07	0.016	(0.068)	0.003	0.013
283	23.58	0.07	0.016	(0.067)	0.003	0.013
284	23.67	0.07	0.016	(0.067)	0.003	0.013
285	23.75	0.07	0.016	(0.067)	0.003	0.013
286	23.83	0.07	0.016	(0.067)	0.003	0.013
287	23.92	0.07	0.016	(0.067)	0.003	0.013
288	24.00	0.07	0.016	(0.067)	0.003	0.013

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.7

Flood volume = Effective rainfall 1.64(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.36(In)
Total soil loss = 0.004(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 773.9 Cubic Feet
Total soil loss = 169.9 Cubic Feet

Peak flow rate of this hydrograph = 0.029(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q	|	|	|	|
0+10	0.0000	0.00	Q	|	|	|	|
0+15	0.0000	0.00	Q	|	|	|	|
0+20	0.0001	0.00	Q	|	|	|	|
0+25	0.0001	0.00	Q	|	|	|	|
0+30	0.0001	0.00	Q	|	|	|	|
0+35	0.0001	0.00	Q	|	|	|	|
0+40	0.0001	0.00	Q	|	|	|	|
0+45	0.0001	0.00	Q	|	|	|	|
0+50	0.0002	0.00	Q	|	|	|	|
0+55	0.0002	0.00	Q	|	|	|	|
1+ 0	0.0002	0.00	Q	|	|	|	|
1+ 5	0.0002	0.00	Q	|	|	|	|
1+10	0.0002	0.00	Q	|	|	|	|
1+15	0.0003	0.00	Q	|	|	|	|
1+20	0.0003	0.00	Q	|	|	|	|
1+25	0.0003	0.00	Q	|	|	|	|
1+30	0.0003	0.00	Q	|	|	|	|
1+35	0.0003	0.00	Q	|	|	|	|
1+40	0.0004	0.00	Q	|	|	|	|
1+45	0.0004	0.00	Q	|	|	|	|
1+50	0.0004	0.00	Q	|	|	|	|

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1+55       0.0004      0.00  Q          |          |          |          |
2+ 0       0.0004      0.00  QV         |          |          |          |
2+ 5       0.0005      0.00  QV         |          |          |          |
2+10       0.0005      0.00  QV         |          |          |          |
2+15       0.0005      0.00  QV         |          |          |          |
2+20       0.0005      0.00  QV         |          |          |          |
2+25       0.0006      0.00  QV         |          |          |          |
2+30       0.0006      0.00  QV         |          |          |          |
2+35       0.0006      0.00  QV         |          |          |          |
2+40       0.0006      0.00  QV         |          |          |          |
2+45       0.0007      0.00  QV         |          |          |          |
2+50       0.0007      0.00  QV         |          |          |          |
2+55       0.0007      0.00  QV         |          |          |          |
3+ 0       0.0008      0.00  QV         |          |          |          |
3+ 5       0.0008      0.00  QV         |          |          |          |
3+10       0.0008      0.00  QV         |          |          |          |
3+15       0.0009      0.00  QV         |          |          |          |
3+20       0.0009      0.00  QV         |          |          |          |
3+25       0.0009      0.00  Q V        |          |          |          |
3+30       0.0009      0.00  Q V        |          |          |          |
3+35       0.0010      0.00  Q V        |          |          |          |
3+40       0.0010      0.00  Q V        |          |          |          |
3+45       0.0010      0.00  Q V        |          |          |          |
3+50       0.0011      0.01  Q V        |          |          |          |
3+55       0.0011      0.01  Q V        |          |          |          |
4+ 0       0.0011      0.01  Q V        |          |          |          |
4+ 5       0.0012      0.01  Q V        |          |          |          |
4+10       0.0012      0.01  Q V        |          |          |          |
4+15       0.0012      0.01  Q V        |          |          |          |
4+20       0.0013      0.01  Q V        |          |          |          |
4+25       0.0013      0.01  Q V        |          |          |          |
4+30       0.0014      0.01  Q  V       |          |          |          |
4+35       0.0014      0.01  Q  V       |          |          |          |
4+40       0.0015      0.01  Q  V       |          |          |          |
4+45       0.0015      0.01  Q  V       |          |          |          |
4+50       0.0015      0.01  Q  V       |          |          |          |
4+55       0.0016      0.01  Q  V       |          |          |          |
5+ 0       0.0016      0.01  Q  V       |          |          |          |
5+ 5       0.0017      0.01  Q  V       |          |          |          |
5+10       0.0017      0.01  Q  V       |          |          |          |
5+15       0.0017      0.01  Q  V       |          |          |          |
5+20       0.0018      0.01  Q   V      |          |          |          |
5+25       0.0018      0.01  Q   V      |          |          |          |
5+30       0.0019      0.01  Q   V      |          |          |          |
5+35       0.0019      0.01  Q   V      |          |          |          |
5+40       0.0020      0.01  Q   V      |          |          |          |
5+45       0.0020      0.01  Q   V      |          |          |          |
5+50       0.0021      0.01  Q   V      |          |          |          |
5+55       0.0021      0.01  Q   V      |          |          |          |
6+ 0       0.0021      0.01  Q   V      |          |          |          |
6+ 5       0.0022      0.01  Q   V      |          |          |          |
6+10       0.0023      0.01  Q    V     |          |          |          |
6+15       0.0023      0.01  Q    V     |          |          |          |
6+20       0.0024      0.01  Q    V     |          |          |          |
6+25       0.0024      0.01  Q    V     |          |          |          |
6+30       0.0025      0.01  Q    V     |          |          |          |
6+35       0.0025      0.01  Q    V     |          |          |          |
6+40       0.0026      0.01  Q    V     |          |          |          |
6+45       0.0026      0.01  Q    V     |          |          |          |
6+50       0.0027      0.01  Q     V    |          |          |          |
6+55       0.0028      0.01  Q     V    |          |          |          |
7+ 0       0.0028      0.01  Q     V    |          |          |          |
7+ 5       0.0029      0.01  Q     V    |          |          |          |
7+10       0.0029      0.01  Q     V    |          |          |          |
7+15       0.0030      0.01  Q     V    |          |          |          |
7+20       0.0031      0.01  Q     V    |          |          |          |
7+25       0.0031      0.01  Q      V   |          |          |          |
7+30       0.0032      0.01  Q      V   |          |          |          |
7+35       0.0033      0.01  Q      V   |          |          |          |
7+40       0.0033      0.01  Q      V   |          |          |          |
7+45       0.0034      0.01  Q      V   |          |          |          |
7+50       0.0035      0.01  Q      V   |          |          |          |
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 7+55       0.0036      0.01  Q       V |          |          |          |
 8+ 0       0.0036      0.01  Q       V |          |          |          |
 8+ 5       0.0037      0.01  Q       V |          |          |          |
 8+10       0.0038      0.01  Q       V |          |          |          |
 8+15       0.0039      0.01  Q       V |          |          |          |
 8+20       0.0040      0.01  Q        V|          |          |          |
 8+25       0.0041      0.01  Q        V|          |          |          |
 8+30       0.0042      0.01  Q        V|          |          |          |
 8+35       0.0043      0.01  Q        V|          |          |          |
 8+40       0.0044      0.01  Q        V|          |          |          |
 8+45       0.0045      0.01  Q         V          |          |          |
 8+50       0.0046      0.01  Q         V          |          |          |
 8+55       0.0047      0.01  Q         V          |          |          |
 9+ 0       0.0048      0.01  Q         V          |          |          |
 9+ 5       0.0049      0.02  Q         V          |          |          |
 9+10       0.0050      0.02  Q          |V         |          |          |
 9+15       0.0051      0.02  Q          |V         |          |          |
 9+20       0.0052      0.02  Q          |V         |          |          |
 9+25       0.0053      0.02  Q          | V        |          |          |
 9+30       0.0055      0.02  Q          | V        |          |          |
 9+35       0.0056      0.02  Q          | V        |          |          |
 9+40       0.0057      0.02  Q          | V        |          |          |
 9+45       0.0058      0.02  Q          |  V       |          |          |
 9+50       0.0060      0.02  Q          |  V       |          |          |
 9+55       0.0061      0.02  Q          |  V       |          |          |
10+ 0       0.0062      0.02  Q          |   V      |          |          |
10+ 5       0.0063      0.01  Q          |   V      |          |          |
10+10       0.0064      0.01  Q          |   V      |          |          |
10+15       0.0065      0.01  Q          |   V      |          |          |
10+20       0.0066      0.01  Q          |   V      |          |          |
10+25       0.0067      0.01  Q          |    V     |          |          |
10+30       0.0068      0.01  Q          |    V     |          |          |
10+35       0.0069      0.02  Q          |    V     |          |          |
10+40       0.0070      0.02  Q          |    V     |          |          |
10+45       0.0071      0.02  Q          |     V    |          |          |
10+50       0.0072      0.02  Q          |     V    |          |          |
10+55       0.0073      0.02  Q          |     V    |          |          |
11+ 0       0.0075      0.02  Q          |     V    |          |          |
11+ 5       0.0076      0.02  Q          |      V   |          |          |
11+10       0.0077      0.02  Q          |      V   |          |          |
11+15       0.0078      0.02  Q          |      V   |          |          |
11+20       0.0079      0.02  Q          |      V   |          |          |
11+25       0.0080      0.02  Q          |       V  |          |          |
11+30       0.0081      0.02  Q          |       V  |          |          |
11+35       0.0082      0.01  Q          |       V  |          |          |
11+40       0.0083      0.01  Q          |       V  |          |          |
11+45       0.0084      0.01  Q          |        V |          |          |
11+50       0.0085      0.02  Q          |        V |          |          |
11+55       0.0087      0.02  Q          |        V |          |          |
12+ 0       0.0088      0.02  Q          |        V |          |          |
12+ 5       0.0089      0.02  Q          |         V          |          |
12+10       0.0091      0.02  Q          |         V          |          |
12+15       0.0092      0.02  Q          |         V          |          |
12+20       0.0094      0.02  Q          |          |V        |          |
12+25       0.0095      0.02  Q          |          |V        |          |
12+30       0.0097      0.02  Q          |          |V        |          |
12+35       0.0098      0.02  Q          |          | V       |          |
12+40       0.0100      0.02  Q          |          | V       |          |
12+45       0.0102      0.02  Q          |          | V       |          |
12+50       0.0103      0.02  Q          |          |  V      |          |
12+55       0.0105      0.02  Q          |          |  V      |          |
13+ 0       0.0107      0.02  Q          |          |   V     |          |
13+ 5       0.0109      0.03  Q          |          |   V     |          |
13+10       0.0111      0.03  Q          |          |   V     |          |
13+15       0.0113      0.03  Q          |          |    V    |          |
13+20       0.0115      0.03  Q          |          |    V    |          |
13+25       0.0117      0.03  Q          |          |     V   |          |
13+30       0.0119      0.03  Q          |          |     V   |          |
13+35       0.0120      0.02  Q          |          |      V  |          |
13+40       0.0122      0.02  Q          |          |      V  |          |
13+45       0.0123      0.02  Q          |          |      V  |          |
13+50       0.0124      0.02  Q          |          |      V  |          |
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13+55       0.0126      0.02  Q          |           |        V |          |
14+ 0       0.0127      0.02  Q          |           |        V |          |
14+ 5       0.0129      0.02  Q          |           |        V |          |
14+10       0.0130      0.02  Q          |           |         V|          |
14+15       0.0132      0.02  Q          |           |         V|          |
14+20       0.0133      0.02  Q          |           |          V          |
14+25       0.0135      0.02  Q          |           |          V          |
14+30       0.0136      0.02  Q          |           |          V          |
14+35       0.0138      0.02  Q          |           |          |V         |
14+40       0.0140      0.02  Q          |           |          |V         |
14+45       0.0141      0.02  Q          |           |          |V         |
14+50       0.0143      0.02  Q          |           |          | V        |
14+55       0.0144      0.02  Q          |           |          | V        |
15+ 0       0.0146      0.02  Q          |           |          | V        |
15+ 5       0.0147      0.02  Q          |           |          |  V       |
15+10       0.0148      0.02  Q          |           |          |  V       |
15+15       0.0150      0.02  Q          |           |          |  V       |
15+20       0.0151      0.02  Q          |           |          |   V      |
15+25       0.0152      0.02  Q          |           |          |   V      |
15+30       0.0154      0.02  Q          |           |          |   V      |
15+35       0.0155      0.02  Q          |           |          |   V      |
15+40       0.0156      0.02  Q          |           |          |    V     |
15+45       0.0157      0.02  Q          |           |          |    V     |
15+50       0.0158      0.02  Q          |           |          |    V     |
15+55       0.0159      0.02  Q          |           |          |    V     |
16+ 0       0.0161      0.02  Q          |           |          |     V    |
16+ 5       0.0161      0.00  Q          |           |          |     V    |
16+10       0.0161      0.00  Q          |           |          |     V    |
16+15       0.0161      0.00  Q          |           |          |     V    |
16+20       0.0162      0.00  Q          |           |          |     V    |
16+25       0.0162      0.00  Q          |           |          |     V    |
16+30       0.0162      0.00  Q          |           |          |     V    |
16+35       0.0162      0.00  Q          |           |          |     V    |
16+40       0.0162      0.00  Q          |           |          |     V    |
16+45       0.0163      0.00  Q          |           |          |     V    |
16+50       0.0163      0.00  Q          |           |          |     V    |
16+55       0.0163      0.00  Q          |           |          |     V    |
17+ 0       0.0163      0.00  Q          |           |          |     V    |
17+ 5       0.0163      0.00  Q          |           |          |     V    |
17+10       0.0164      0.00  Q          |           |          |     V    |
17+15       0.0164      0.00  Q          |           |          |     V    |
17+20       0.0164      0.00  Q          |           |          |     V    |
17+25       0.0165      0.00  Q          |           |          |      V   |
17+30       0.0165      0.00  Q          |           |          |      V   |
17+35       0.0165      0.00  Q          |           |          |      V   |
17+40       0.0165      0.00  Q          |           |          |      V   |
17+45       0.0166      0.00  Q          |           |          |      V   |
17+50       0.0166      0.00  Q          |           |          |      V   |
17+55       0.0166      0.00  Q          |           |          |      V   |
18+ 0       0.0166      0.00  Q          |           |          |      V   |
18+ 5       0.0167      0.00  Q          |           |          |      V   |
18+10       0.0167      0.00  Q          |           |          |      V   |
18+15       0.0167      0.00  Q          |           |          |      V   |
18+20       0.0167      0.00  Q          |           |          |      V   |
18+25       0.0168      0.00  Q          |           |          |      V   |
18+30       0.0168      0.00  Q          |           |          |      V   |
18+35       0.0168      0.00  Q          |           |          |      V   |
18+40       0.0168      0.00  Q          |           |          |      V   |
18+45       0.0168      0.00  Q          |           |          |      V   |
18+50       0.0169      0.00  Q          |           |          |      V   |
18+55       0.0169      0.00  Q          |           |          |      V   |
19+ 0       0.0169      0.00  Q          |           |          |       V  |
19+ 5       0.0169      0.00  Q          |           |          |       V  |
19+10       0.0169      0.00  Q          |           |          |       V  |
19+15       0.0169      0.00  Q          |           |          |       V  |
19+20       0.0170      0.00  Q          |           |          |       V  |
19+25       0.0170      0.00  Q          |           |          |       V  |
19+30       0.0170      0.00  Q          |           |          |       V  |
19+35       0.0170      0.00  Q          |           |          |       V  |
19+40       0.0170      0.00  Q          |           |          |       V  |
19+45       0.0171      0.00  Q          |           |          |       V  |
19+50       0.0171      0.00  Q          |           |          |       V  |
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  19+55       0.0171      0.00  Q          |          |          |        V |
  20+ 0       0.0171      0.00  Q          |          |          |        V |
  20+ 5       0.0171      0.00  Q          |          |          |        V |
  20+10       0.0171      0.00  Q          |          |          |        V |
  20+15       0.0171      0.00  Q          |          |          |        V |
  20+20       0.0172      0.00  Q          |          |          |        V |
  20+25       0.0172      0.00  Q          |          |          |        V |
  20+30       0.0172      0.00  Q          |          |          |        V |
  20+35       0.0172      0.00  Q          |          |          |        V |
  20+40       0.0172      0.00  Q          |          |          |        V |
  20+45       0.0173      0.00  Q          |          |          |        V |
  20+50       0.0173      0.00  Q          |          |          |        V |
  20+55       0.0173      0.00  Q          |          |          |        V |
  21+ 0       0.0173      0.00  Q          |          |          |        V |
  21+ 5       0.0173      0.00  Q          |          |          |        V |
  21+10       0.0173      0.00  Q          |          |          |         V|
  21+15       0.0173      0.00  Q          |          |          |         V|
  21+20       0.0174      0.00  Q          |          |          |         V|
  21+25       0.0174      0.00  Q          |          |          |         V|
  21+30       0.0174      0.00  Q          |          |          |         V|
  21+35       0.0174      0.00  Q          |          |          |         V|
  21+40       0.0174      0.00  Q          |          |          |         V|
  21+45       0.0174      0.00  Q          |          |          |         V|
  21+50       0.0174      0.00  Q          |          |          |         V|
  21+55       0.0175      0.00  Q          |          |          |         V|
  22+ 0       0.0175      0.00  Q          |          |          |         V|
  22+ 5       0.0175      0.00  Q          |          |          |         V|
  22+10       0.0175      0.00  Q          |          |          |         V|
  22+15       0.0175      0.00  Q          |          |          |         V|
  22+20       0.0175      0.00  Q          |          |          |         V|
  22+25       0.0175      0.00  Q          |          |          |         V|
  22+30       0.0176      0.00  Q          |          |          |         V|
  22+35       0.0176      0.00  Q          |          |          |         V|
  22+40       0.0176      0.00  Q          |          |          |         V|
  22+45       0.0176      0.00  Q          |          |          |         V|
  22+50       0.0176      0.00  Q          |          |          |         V|
  22+55       0.0176      0.00  Q          |          |          |         V|
  23+ 0       0.0176      0.00  Q          |          |          |         V|
  23+ 5       0.0176      0.00  Q          |          |          |         V|
  23+10       0.0176      0.00  Q          |          |          |         V|
  23+15       0.0177      0.00  Q          |          |          |         V|
  23+20       0.0177      0.00  Q          |          |          |         V|
  23+25       0.0177      0.00  Q          |          |          |         V|
  23+30       0.0177      0.00  Q          |          |          |         V|
  23+35       0.0177      0.00  Q          |          |          |         V|
  23+40       0.0177      0.00  Q          |          |          |         V|
  23+45       0.0177      0.00  Q          |          |          |         V|
  23+50       0.0177      0.00  Q          |          |          |         V|
  23+55       0.0178      0.00  Q          |          |          |         V|
  24+ 0       0.0178      0.00  Q          |          |          |          V
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB0262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	1.20	0.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	3.00	0.39

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.200(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

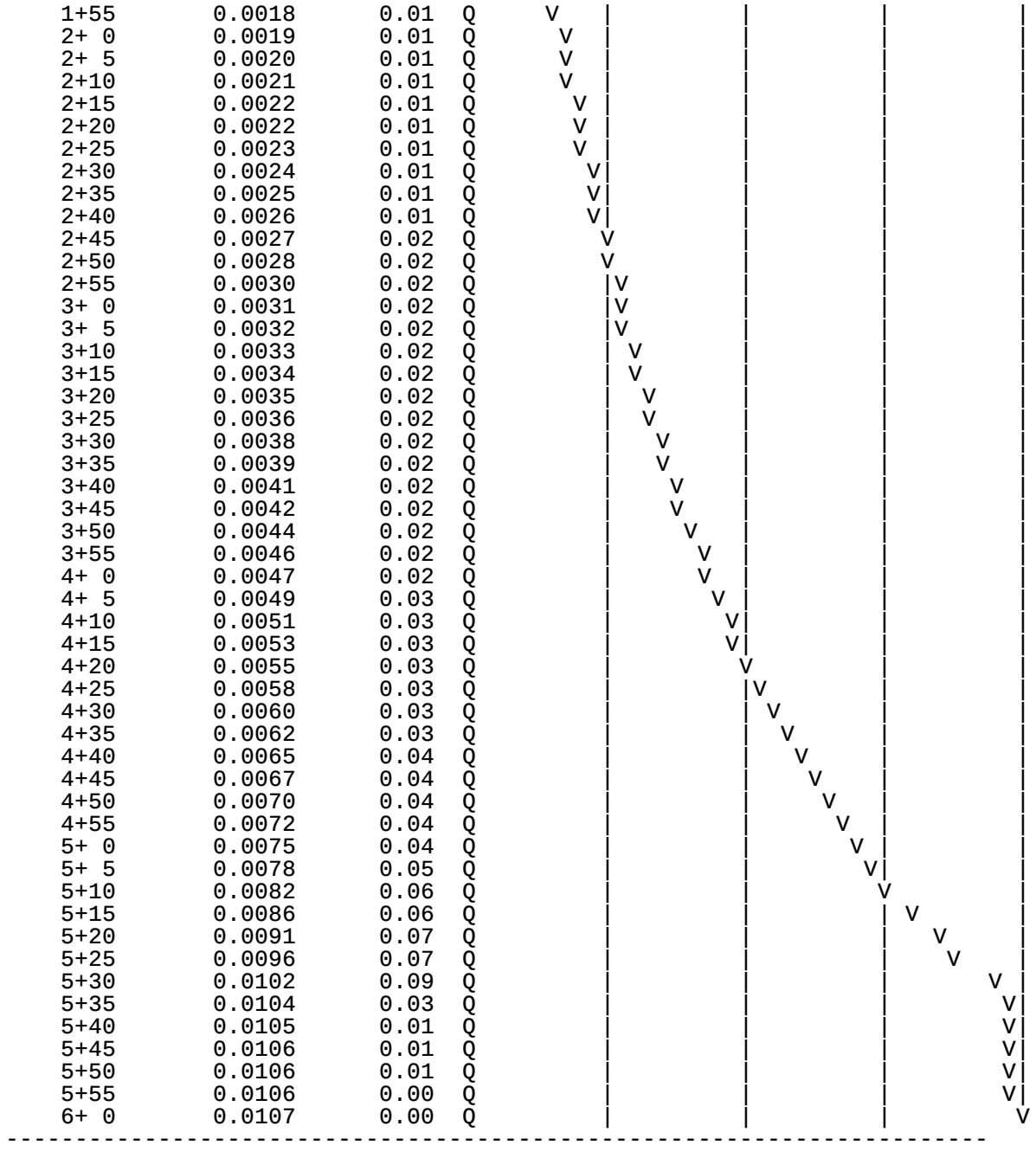
Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
			Sum = 100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.072	(0.134)	0.013	0.059
2	0.17	0.60	0.086	(0.134)	0.016	0.071
3	0.25	0.60	0.086	(0.134)	0.016	0.071
4	0.33	0.60	0.086	(0.134)	0.016	0.071
5	0.42	0.60	0.086	(0.134)	0.016	0.071
6	0.50	0.70	0.101	(0.134)	0.018	0.083
7	0.58	0.70	0.101	(0.134)	0.018	0.083
8	0.67	0.70	0.101	(0.134)	0.018	0.083
9	0.75	0.70	0.101	(0.134)	0.018	0.083
10	0.83	0.70	0.101	(0.134)	0.018	0.083
11	0.92	0.70	0.101	(0.134)	0.018	0.083
12	1.00	0.80	0.115	(0.134)	0.021	0.094
13	1.08	0.80	0.115	(0.134)	0.021	0.094
14	1.17	0.80	0.115	(0.134)	0.021	0.094
15	1.25	0.80	0.115	(0.134)	0.021	0.094
16	1.33	0.80	0.115	(0.134)	0.021	0.094
17	1.42	0.80	0.115	(0.134)	0.021	0.094
18	1.50	0.80	0.115	(0.134)	0.021	0.094
19	1.58	0.80	0.115	(0.134)	0.021	0.094
20	1.67	0.80	0.115	(0.134)	0.021	0.094
21	1.75	0.80	0.115	(0.134)	0.021	0.094
22	1.83	0.80	0.115	(0.134)	0.021	0.094
23	1.92	0.80	0.115	(0.134)	0.021	0.094
24	2.00	0.90	0.130	(0.134)	0.023	0.106
25	2.08	0.80	0.115	(0.134)	0.021	0.094
26	2.17	0.90	0.130	(0.134)	0.023	0.106
27	2.25	0.90	0.130	(0.134)	0.023	0.106
28	2.33	0.90	0.130	(0.134)	0.023	0.106
29	2.42	0.90	0.130	(0.134)	0.023	0.106
30	2.50	0.90	0.130	(0.134)	0.023	0.106
31	2.58	0.90	0.130	(0.134)	0.023	0.106
32	2.67	0.90	0.130	(0.134)	0.023	0.106
33	2.75	1.00	0.144	(0.134)	0.026	0.118
34	2.83	1.00	0.144	(0.134)	0.026	0.118
35	2.92	1.00	0.144	(0.134)	0.026	0.118
36	3.00	1.00	0.144	(0.134)	0.026	0.118
37	3.08	1.00	0.144	(0.134)	0.026	0.118
38	3.17	1.10	0.158	(0.134)	0.029	0.130
39	3.25	1.10	0.158	(0.134)	0.029	0.130
40	3.33	1.10	0.158	(0.134)	0.029	0.130
41	3.42	1.20	0.173	(0.134)	0.031	0.142
42	3.50	1.30	0.187	(0.134)	0.034	0.154
43	3.58	1.40	0.202	(0.134)	0.036	0.165

```
44   3.67     1.40      0.202       (  0.134)       0.036        0.165
45   3.75     1.50      0.216       (  0.134)       0.039        0.177
46   3.83     1.50      0.216       (  0.134)       0.039        0.177
47   3.92     1.60      0.230       (  0.134)       0.041        0.189
48   4.00     1.60      0.230       (  0.134)       0.041        0.189
49   4.08     1.70      0.245       (  0.134)       0.044        0.201
50   4.17     1.80      0.259       (  0.134)       0.047        0.213
51   4.25     1.90      0.274       (  0.134)       0.049        0.224
52   4.33     2.00      0.288       (  0.134)       0.052        0.236
53   4.42     2.10      0.302       (  0.134)       0.054        0.248
54   4.50     2.10      0.302       (  0.134)       0.054        0.248
55   4.58     2.20      0.317       (  0.134)       0.057        0.260
56   4.67     2.30      0.331       (  0.134)       0.060        0.272
57   4.75     2.40      0.346       (  0.134)       0.062        0.283
58   4.83     2.40      0.346       (  0.134)       0.062        0.283
59   4.92     2.50      0.360       (  0.134)       0.065        0.295
60   5.00     2.60      0.374       (  0.134)       0.067        0.307
61   5.08     3.10      0.446       (  0.134)       0.080        0.366
62   5.17     3.60      0.518       (  0.134)       0.093        0.425
63   5.25     3.90      0.562       (  0.134)       0.101        0.461
64   5.33     4.20      0.605       (  0.134)       0.109        0.496
65   5.42     4.70      0.677       (  0.134)       0.122        0.555
66   5.50     5.60      0.806          0.134    (   0.145)       0.672
67   5.58     1.90      0.274       (  0.134)       0.049        0.224
68   5.67     0.90      0.130       (  0.134)       0.023        0.106
69   5.75     0.60      0.086       (  0.134)       0.016        0.071
70   5.83     0.50      0.072       (  0.134)       0.013        0.059
71   5.92     0.30      0.043       (  0.134)       0.008        0.035
72   6.00     0.20      0.029       (  0.134)       0.005        0.024
              (Loss Rate Not Used)
   Sum =     100.0                                   Sum =    11.8
      Flood volume = Effective rainfall      0.98(In)
       times area       0.1(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
      Total soil loss =      0.22(In)
      Total soil loss =     0.002(Ac.Ft)
      Total rainfall =      1.20(In)
      Flood volume =         464.8 Cubic Feet
      Total soil loss =         101.5 Cubic Feet
      ---------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.088(CFS)
      ---------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0001      0.01  Q         |         |         |         |
  0+10       0.0001      0.01  Q         |         |         |         |
  0+15       0.0002      0.01  Q         |         |         |         |
  0+20       0.0002      0.01  Q         |         |         |         |
  0+25       0.0003      0.01  QV        |         |         |         |
  0+30       0.0004      0.01  QV        |         |         |         |
  0+35       0.0005      0.01  QV        |         |         |         |
  0+40       0.0005      0.01  QV        |         |         |         |
  0+45       0.0006      0.01  Q V       |         |         |         |
  0+50       0.0007      0.01  Q V       |         |         |         |
  0+55       0.0008      0.01  Q V       |         |         |         |
  1+ 0       0.0008      0.01  Q  V      |         |         |         |
  1+ 5       0.0009      0.01  Q  V      |         |         |         |
  1+10       0.0010      0.01  Q  V      |         |         |         |
  1+15       0.0011      0.01  Q   V     |         |         |         |
  1+20       0.0012      0.01  Q   V     |         |         |         |
  1+25       0.0013      0.01  Q   V     |         |         |         |
  1+30       0.0014      0.01  Q    V    |         |         |         |
  1+35       0.0014      0.01  Q    V    |         |         |         |
  1+40       0.0015      0.01  Q    V    |         |         |         |
  1+45       0.0016      0.01  Q     V   |         |         |         |
  1+50       0.0017      0.01  Q     V   |         |         |         |
```


1+55 0.0018 0.01 Q
2+ 0 0.0019 0.01 Q
2+ 5 0.0020 0.01 Q
2+10 0.0021 0.01 Q
2+15 0.0022 0.01 Q
2+20 0.0022 0.01 Q
2+25 0.0023 0.01 Q
2+30 0.0024 0.01 Q
2+35 0.0025 0.01 Q
2+40 0.0026 0.01 Q
2+45 0.0027 0.02 Q
2+50 0.0028 0.02 Q
2+55 0.0030 0.02 Q
3+ 0 0.0031 0.02 Q
3+ 5 0.0032 0.02 Q
3+10 0.0033 0.02 Q
3+15 0.0034 0.02 Q
3+20 0.0035 0.02 Q
3+25 0.0036 0.02 Q
3+30 0.0038 0.02 Q
3+35 0.0039 0.02 Q
3+40 0.0041 0.02 Q
3+45 0.0042 0.02 Q
3+50 0.0044 0.02 Q
3+55 0.0046 0.02 Q
4+ 0 0.0047 0.02 Q
4+ 5 0.0049 0.03 Q
4+10 0.0051 0.03 Q
4+15 0.0053 0.03 Q
4+20 0.0055 0.03 Q
4+25 0.0058 0.03 Q
4+30 0.0060 0.03 Q
4+35 0.0062 0.03 Q
4+40 0.0065 0.04 Q
4+45 0.0067 0.04 Q
4+50 0.0070 0.04 Q
4+55 0.0072 0.04 Q
5+ 0 0.0075 0.04 Q
5+ 5 0.0078 0.05 Q
5+10 0.0082 0.06 Q
5+15 0.0086 0.06 Q
5+20 0.0091 0.07 Q
5+25 0.0096 0.07 Q
5+30 0.0102 0.09 Q
5+35 0.0104 0.03 Q
5+40 0.0105 0.01 Q
5+45 0.0106 0.01 Q
5+50 0.0106 0.01 Q
5+55 0.0106 0.00 Q
6+ 0 0.0107 0.00 Q

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB0232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	0.90	0.12

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	2.35	0.31

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 0.900(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.900(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
		Sum =	100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.140	(0.134)	0.025	0.115
2	0.17	1.30	0.140	(0.134)	0.025	0.115
3	0.25	1.10	0.119	(0.134)	0.021	0.097
4	0.33	1.50	0.162	(0.134)	0.029	0.133
5	0.42	1.50	0.162	(0.134)	0.029	0.133
6	0.50	1.80	0.194	(0.134)	0.035	0.159
7	0.58	1.50	0.162	(0.134)	0.029	0.133
8	0.67	1.80	0.194	(0.134)	0.035	0.159
9	0.75	1.80	0.194	(0.134)	0.035	0.159
10	0.83	1.50	0.162	(0.134)	0.029	0.133
11	0.92	1.60	0.173	(0.134)	0.031	0.142
12	1.00	1.80	0.194	(0.134)	0.035	0.159
13	1.08	2.20	0.238	(0.134)	0.043	0.195
14	1.17	2.20	0.238	(0.134)	0.043	0.195
15	1.25	2.20	0.238	(0.134)	0.043	0.195
16	1.33	2.00	0.216	(0.134)	0.039	0.177
17	1.42	2.60	0.281	(0.134)	0.051	0.230
18	1.50	2.70	0.292	(0.134)	0.052	0.239
19	1.58	2.40	0.259	(0.134)	0.047	0.213
20	1.67	2.70	0.292	(0.134)	0.052	0.239
21	1.75	3.30	0.356	(0.134)	0.064	0.292
22	1.83	3.10	0.335	(0.134)	0.060	0.275
23	1.92	2.90	0.313	(0.134)	0.056	0.257
24	2.00	3.00	0.324	(0.134)	0.058	0.266
25	2.08	3.10	0.335	(0.134)	0.060	0.275
26	2.17	4.20	0.454	(0.134)	0.082	0.372
27	2.25	5.00	0.540	(0.134)	0.097	0.443
28	2.33	3.50	0.378	(0.134)	0.068	0.310
29	2.42	6.80	0.734	(0.134)	0.132	0.602
30	2.50	7.30	0.788	0.134	(0.142)	0.654
31	2.58	8.20	0.886	0.134	(0.159)	0.751
32	2.67	5.90	0.637	(0.134)	0.115	0.523
33	2.75	2.00	0.216	(0.134)	0.039	0.177
34	2.83	1.80	0.194	(0.134)	0.035	0.159
35	2.92	1.80	0.194	(0.134)	0.035	0.159
36	3.00	0.60	0.065	(0.134)	0.012	0.053
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.9

Flood volume = Effective rainfall 0.74(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.16(In)
Total soil loss = 0.002(Ac.Ft)
Total rainfall = 0.90(In)

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      Flood volume =         349.6 Cubic Feet
      Total soil loss =          75.1 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.099(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ----------------------------------------------------------------------------
   0+ 5       0.0001      0.02  Q         |         |         |         |
   0+10       0.0002      0.02  QV        |         |         |         |
   0+15       0.0003      0.01  QV        |         |         |         |
   0+20       0.0004      0.02  Q V       |         |         |         |
   0+25       0.0005      0.02  Q V       |         |         |         |
   0+30       0.0007      0.02  Q  V      |         |         |         |
   0+35       0.0008      0.02  Q  V      |         |         |         |
   0+40       0.0009      0.02  Q   V     |         |         |         |
   0+45       0.0011      0.02  Q    V    |         |         |         |
   0+50       0.0012      0.02  Q     V   |         |         |         |
   0+55       0.0013      0.02  Q     V   |         |         |         |
   1+ 0       0.0015      0.02  Q      V  |         |         |         |
   1+ 5       0.0017      0.03  Q       V |         |         |         |
   1+10       0.0018      0.03  Q        V|         |         |         |
   1+15       0.0020      0.03  Q         V         |         |         |
   1+20       0.0022      0.02  Q         V         |         |         |
   1+25       0.0024      0.03  Q         |V        |         |         |
   1+30       0.0026      0.03  Q         | V       |         |         |
   1+35       0.0028      0.03  Q         |  V      |         |         |
   1+40       0.0030      0.03  Q         |   V     |         |         |
   1+45       0.0033      0.04  Q         |     V   |         |         |
   1+50       0.0035      0.04  Q         |      V  |         |         |
   1+55       0.0037      0.03  Q         |       V |         |         |
   2+ 0       0.0040      0.03  Q         |        V|         |         |
   2+ 5       0.0042      0.04  Q         |         |V        |         |
   2+10       0.0046      0.05  Q         |         | V       |         |
   2+15       0.0050      0.06  Q         |         |   V     |         |
   2+20       0.0052      0.04  Q         |         |     V   |         |
   2+25       0.0058      0.08  Q         |         |       V |         |
   2+30       0.0064      0.09  Q         |         |         |V        |
   2+35       0.0071      0.10  Q         |         |         |    V    |
   2+40       0.0075      0.07  Q         |         |         |      V  |
   2+45       0.0077      0.02  Q         |         |         |       V |
   2+50       0.0078      0.02  Q         |         |         |        V|
   2+55       0.0080      0.02  Q         |         |         |         V|
   3+ 0       0.0080      0.01  Q         |         |         |          V
----------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB0212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	0.54	0.07

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	1.36	0.18

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.540(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.540(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
		Sum =	100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.285	(0.134)	0.051	0.234
2	0.17	4.50	0.292	(0.134)	0.052	0.239
3	0.25	5.40	0.350	(0.134)	0.063	0.287
4	0.33	5.40	0.350	(0.134)	0.063	0.287
5	0.42	5.70	0.369	(0.134)	0.066	0.303
6	0.50	6.40	0.415	(0.134)	0.075	0.340
7	0.58	7.90	0.512	(0.134)	0.092	0.420
8	0.67	9.10	0.590	(0.134)	0.106	0.484
9	0.75	12.80	0.829	0.134	(0.149)	0.695
10	0.83	25.60	1.659	0.134	(0.299)	1.525
11	0.92	7.90	0.512	(0.134)	0.092	0.420
12	1.00	4.90	0.318	(0.134)	0.057	0.260
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.5

Flood volume = Effective rainfall 0.46(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.08(In)
Total soil loss = 0.001(Ac.Ft)
Total rainfall = 0.54(In)
Flood volume = 216.0 Cubic Feet
Total soil loss = 38.8 Cubic Feet

Peak flow rate of this hydrograph = 0.200(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0002	0.03	QV				
0+10	0.0004	0.03	Q V				
0+15	0.0007	0.04	Q V				
0+20	0.0009	0.04	Q V				
0+25	0.0012	0.04	Q V				
0+30	0.0015	0.04	Q V				
0+35	0.0019	0.06	Q V				
0+40	0.0023	0.06	Q V				

```
   0+45       0.0030      0.09  Q          |          |  V      |          |
   0+50       0.0043      0.20  Q          |          |         |    V     |
   0+55       0.0047      0.06  Q          |          |         |       V  |
   1+ 0       0.0050      0.03  Q          |          |         |          V
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB05245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	2.00	0.26

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	6.40	0.83

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.031(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.031(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
			Sum = 100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.024	(0.238)	0.004	0.020
2	0.17	0.07	0.024	(0.237)	0.004	0.020
3	0.25	0.07	0.024	(0.236)	0.004	0.020
4	0.33	0.10	0.036	(0.235)	0.007	0.030
5	0.42	0.10	0.036	(0.234)	0.007	0.030
6	0.50	0.10	0.036	(0.233)	0.007	0.030
7	0.58	0.10	0.036	(0.232)	0.007	0.030
8	0.67	0.10	0.036	(0.231)	0.007	0.030
9	0.75	0.10	0.036	(0.230)	0.007	0.030
10	0.83	0.13	0.048	(0.230)	0.009	0.040
11	0.92	0.13	0.048	(0.229)	0.009	0.040
12	1.00	0.13	0.048	(0.228)	0.009	0.040
13	1.08	0.10	0.036	(0.227)	0.007	0.030
14	1.17	0.10	0.036	(0.226)	0.007	0.030
15	1.25	0.10	0.036	(0.225)	0.007	0.030
16	1.33	0.10	0.036	(0.224)	0.007	0.030
17	1.42	0.10	0.036	(0.223)	0.007	0.030
18	1.50	0.10	0.036	(0.222)	0.007	0.030
19	1.58	0.10	0.036	(0.222)	0.007	0.030
20	1.67	0.10	0.036	(0.221)	0.007	0.030
21	1.75	0.10	0.036	(0.220)	0.007	0.030
22	1.83	0.13	0.048	(0.219)	0.009	0.040
23	1.92	0.13	0.048	(0.218)	0.009	0.040
24	2.00	0.13	0.048	(0.217)	0.009	0.040
25	2.08	0.13	0.048	(0.216)	0.009	0.040
26	2.17	0.13	0.048	(0.215)	0.009	0.040
27	2.25	0.13	0.048	(0.214)	0.009	0.040
28	2.33	0.13	0.048	(0.214)	0.009	0.040
29	2.42	0.13	0.048	(0.213)	0.009	0.040
30	2.50	0.13	0.048	(0.212)	0.009	0.040
31	2.58	0.17	0.061	(0.211)	0.011	0.050
32	2.67	0.17	0.061	(0.210)	0.011	0.050
33	2.75	0.17	0.061	(0.209)	0.011	0.050
34	2.83	0.17	0.061	(0.208)	0.011	0.050
35	2.92	0.17	0.061	(0.208)	0.011	0.050
36	3.00	0.17	0.061	(0.207)	0.011	0.050
37	3.08	0.17	0.061	(0.206)	0.011	0.050
38	3.17	0.17	0.061	(0.205)	0.011	0.050
39	3.25	0.17	0.061	(0.204)	0.011	0.050
40	3.33	0.17	0.061	(0.203)	0.011	0.050
41	3.42	0.17	0.061	(0.202)	0.011	0.050
42	3.50	0.17	0.061	(0.202)	0.011	0.050
43	3.58	0.17	0.061	(0.201)	0.011	0.050

44	3.67	0.17	0.061	(0.200)	0.011	0.050
45	3.75	0.17	0.061	(0.199)	0.011	0.050
46	3.83	0.20	0.073	(0.198)	0.013	0.060
47	3.92	0.20	0.073	(0.197)	0.013	0.060
48	4.00	0.20	0.073	(0.197)	0.013	0.060
49	4.08	0.20	0.073	(0.196)	0.013	0.060
50	4.17	0.20	0.073	(0.195)	0.013	0.060
51	4.25	0.20	0.073	(0.194)	0.013	0.060
52	4.33	0.23	0.085	(0.193)	0.015	0.070
53	4.42	0.23	0.085	(0.192)	0.015	0.070
54	4.50	0.23	0.085	(0.192)	0.015	0.070
55	4.58	0.23	0.085	(0.191)	0.015	0.070
56	4.67	0.23	0.085	(0.190)	0.015	0.070
57	4.75	0.23	0.085	(0.189)	0.015	0.070
58	4.83	0.27	0.097	(0.188)	0.017	0.080
59	4.92	0.27	0.097	(0.187)	0.017	0.080
60	5.00	0.27	0.097	(0.187)	0.017	0.080
61	5.08	0.20	0.073	(0.186)	0.013	0.060
62	5.17	0.20	0.073	(0.185)	0.013	0.060
63	5.25	0.20	0.073	(0.184)	0.013	0.060
64	5.33	0.23	0.085	(0.183)	0.015	0.070
65	5.42	0.23	0.085	(0.183)	0.015	0.070
66	5.50	0.23	0.085	(0.182)	0.015	0.070
67	5.58	0.27	0.097	(0.181)	0.017	0.080
68	5.67	0.27	0.097	(0.180)	0.017	0.080
69	5.75	0.27	0.097	(0.179)	0.017	0.080
70	5.83	0.27	0.097	(0.179)	0.017	0.080
71	5.92	0.27	0.097	(0.178)	0.017	0.080
72	6.00	0.27	0.097	(0.177)	0.017	0.080
73	6.08	0.30	0.109	(0.176)	0.020	0.089
74	6.17	0.30	0.109	(0.175)	0.020	0.089
75	6.25	0.30	0.109	(0.175)	0.020	0.089
76	6.33	0.30	0.109	(0.174)	0.020	0.089
77	6.42	0.30	0.109	(0.173)	0.020	0.089
78	6.50	0.30	0.109	(0.172)	0.020	0.089
79	6.58	0.33	0.121	(0.172)	0.022	0.099
80	6.67	0.33	0.121	(0.171)	0.022	0.099
81	6.75	0.33	0.121	(0.170)	0.022	0.099
82	6.83	0.33	0.121	(0.169)	0.022	0.099
83	6.92	0.33	0.121	(0.169)	0.022	0.099
84	7.00	0.33	0.121	(0.168)	0.022	0.099
85	7.08	0.33	0.121	(0.167)	0.022	0.099
86	7.17	0.33	0.121	(0.166)	0.022	0.099
87	7.25	0.33	0.121	(0.165)	0.022	0.099
88	7.33	0.37	0.133	(0.165)	0.024	0.109
89	7.42	0.37	0.133	(0.164)	0.024	0.109
90	7.50	0.37	0.133	(0.163)	0.024	0.109
91	7.58	0.40	0.145	(0.162)	0.026	0.119
92	7.67	0.40	0.145	(0.162)	0.026	0.119
93	7.75	0.40	0.145	(0.161)	0.026	0.119
94	7.83	0.43	0.158	(0.160)	0.028	0.129
95	7.92	0.43	0.158	(0.159)	0.028	0.129
96	8.00	0.43	0.158	(0.159)	0.028	0.129
97	8.08	0.50	0.182	(0.158)	0.033	0.149
98	8.17	0.50	0.182	(0.157)	0.033	0.149
99	8.25	0.50	0.182	(0.157)	0.033	0.149
100	8.33	0.50	0.182	(0.156)	0.033	0.149
101	8.42	0.50	0.182	(0.155)	0.033	0.149
102	8.50	0.50	0.182	(0.154)	0.033	0.149
103	8.58	0.53	0.194	(0.154)	0.035	0.159
104	8.67	0.53	0.194	(0.153)	0.035	0.159
105	8.75	0.53	0.194	(0.152)	0.035	0.159
106	8.83	0.57	0.206	(0.151)	0.037	0.169
107	8.92	0.57	0.206	(0.151)	0.037	0.169
108	9.00	0.57	0.206	(0.150)	0.037	0.169
109	9.08	0.63	0.230	(0.149)	0.041	0.189
110	9.17	0.63	0.230	(0.149)	0.041	0.189
111	9.25	0.63	0.230	(0.148)	0.041	0.189
112	9.33	0.67	0.242	(0.147)	0.044	0.199
113	9.42	0.67	0.242	(0.147)	0.044	0.199
114	9.50	0.67	0.242	(0.146)	0.044	0.199
115	9.58	0.70	0.255	(0.145)	0.046	0.209

116	9.67	0.70	0.255	(0.144)	0.046	0.209
117	9.75	0.70	0.255	(0.144)	0.046	0.209
118	9.83	0.73	0.267	(0.143)	0.048	0.219
119	9.92	0.73	0.267	(0.142)	0.048	0.219
120	10.00	0.73	0.267	(0.142)	0.048	0.219
121	10.08	0.50	0.182	(0.141)	0.033	0.149
122	10.17	0.50	0.182	(0.140)	0.033	0.149
123	10.25	0.50	0.182	(0.140)	0.033	0.149
124	10.33	0.50	0.182	(0.139)	0.033	0.149
125	10.42	0.50	0.182	(0.138)	0.033	0.149
126	10.50	0.50	0.182	(0.138)	0.033	0.149
127	10.58	0.67	0.242	(0.137)	0.044	0.199
128	10.67	0.67	0.242	(0.136)	0.044	0.199
129	10.75	0.67	0.242	(0.136)	0.044	0.199
130	10.83	0.67	0.242	(0.135)	0.044	0.199
131	10.92	0.67	0.242	(0.134)	0.044	0.199
132	11.00	0.67	0.242	(0.134)	0.044	0.199
133	11.08	0.63	0.230	(0.133)	0.041	0.189
134	11.17	0.63	0.230	(0.132)	0.041	0.189
135	11.25	0.63	0.230	(0.132)	0.041	0.189
136	11.33	0.63	0.230	(0.131)	0.041	0.189
137	11.42	0.63	0.230	(0.130)	0.041	0.189
138	11.50	0.63	0.230	(0.130)	0.041	0.189
139	11.58	0.57	0.206	(0.129)	0.037	0.169
140	11.67	0.57	0.206	(0.128)	0.037	0.169
141	11.75	0.57	0.206	(0.128)	0.037	0.169
142	11.83	0.60	0.218	(0.127)	0.039	0.179
143	11.92	0.60	0.218	(0.126)	0.039	0.179
144	12.00	0.60	0.218	(0.126)	0.039	0.179
145	12.08	0.83	0.303	(0.125)	0.055	0.249
146	12.17	0.83	0.303	(0.125)	0.055	0.249
147	12.25	0.83	0.303	(0.124)	0.055	0.249
148	12.33	0.87	0.315	(0.123)	0.057	0.258
149	12.42	0.87	0.315	(0.123)	0.057	0.258
150	12.50	0.87	0.315	(0.122)	0.057	0.258
151	12.58	0.93	0.339	(0.121)	0.061	0.278
152	12.67	0.93	0.339	(0.121)	0.061	0.278
153	12.75	0.93	0.339	(0.120)	0.061	0.278
154	12.83	0.97	0.352	(0.120)	0.063	0.288
155	12.92	0.97	0.352	(0.119)	0.063	0.288
156	13.00	0.97	0.352	(0.118)	0.063	0.288
157	13.08	1.13	0.412	(0.118)	0.074	0.338
158	13.17	1.13	0.412	(0.117)	0.074	0.338
159	13.25	1.13	0.412	(0.117)	0.074	0.338
160	13.33	1.13	0.412	(0.116)	0.074	0.338
161	13.42	1.13	0.412	(0.115)	0.074	0.338
162	13.50	1.13	0.412	(0.115)	0.074	0.338
163	13.58	0.77	0.279	(0.114)	0.050	0.229
164	13.67	0.77	0.279	(0.114)	0.050	0.229
165	13.75	0.77	0.279	(0.113)	0.050	0.229
166	13.83	0.77	0.279	(0.113)	0.050	0.229
167	13.92	0.77	0.279	(0.112)	0.050	0.229
168	14.00	0.77	0.279	(0.111)	0.050	0.229
169	14.08	0.90	0.327	(0.111)	0.059	0.268
170	14.17	0.90	0.327	(0.110)	0.059	0.268
171	14.25	0.90	0.327	(0.110)	0.059	0.268
172	14.33	0.87	0.315	(0.109)	0.057	0.258
173	14.42	0.87	0.315	(0.109)	0.057	0.258
174	14.50	0.87	0.315	(0.108)	0.057	0.258
175	14.58	0.87	0.315	(0.107)	0.057	0.258
176	14.67	0.87	0.315	(0.107)	0.057	0.258
177	14.75	0.87	0.315	(0.106)	0.057	0.258
178	14.83	0.83	0.303	(0.106)	0.055	0.249
179	14.92	0.83	0.303	(0.105)	0.055	0.249
180	15.00	0.83	0.303	(0.105)	0.055	0.249
181	15.08	0.80	0.291	(0.104)	0.052	0.239
182	15.17	0.80	0.291	(0.104)	0.052	0.239
183	15.25	0.80	0.291	(0.103)	0.052	0.239
184	15.33	0.77	0.279	(0.103)	0.050	0.229
185	15.42	0.77	0.279	(0.102)	0.050	0.229
186	15.50	0.77	0.279	(0.102)	0.050	0.229
187	15.58	0.63	0.230	(0.101)	0.041	0.189

188	15.67	0.63	0.230	(0.101)	0.041	0.189
189	15.75	0.63	0.230	(0.100)	0.041	0.189
190	15.83	0.63	0.230	(0.100)	0.041	0.189
191	15.92	0.63	0.230	(0.099)	0.041	0.189
192	16.00	0.63	0.230	(0.099)	0.041	0.189
193	16.08	0.13	0.048	(0.098)	0.009	0.040
194	16.17	0.13	0.048	(0.098)	0.009	0.040
195	16.25	0.13	0.048	(0.097)	0.009	0.040
196	16.33	0.13	0.048	(0.097)	0.009	0.040
197	16.42	0.13	0.048	(0.096)	0.009	0.040
198	16.50	0.13	0.048	(0.096)	0.009	0.040
199	16.58	0.10	0.036	(0.095)	0.007	0.030
200	16.67	0.10	0.036	(0.095)	0.007	0.030
201	16.75	0.10	0.036	(0.094)	0.007	0.030
202	16.83	0.10	0.036	(0.094)	0.007	0.030
203	16.92	0.10	0.036	(0.093)	0.007	0.030
204	17.00	0.10	0.036	(0.093)	0.007	0.030
205	17.08	0.17	0.061	(0.092)	0.011	0.050
206	17.17	0.17	0.061	(0.092)	0.011	0.050
207	17.25	0.17	0.061	(0.091)	0.011	0.050
208	17.33	0.17	0.061	(0.091)	0.011	0.050
209	17.42	0.17	0.061	(0.090)	0.011	0.050
210	17.50	0.17	0.061	(0.090)	0.011	0.050
211	17.58	0.17	0.061	(0.089)	0.011	0.050
212	17.67	0.17	0.061	(0.089)	0.011	0.050
213	17.75	0.17	0.061	(0.089)	0.011	0.050
214	17.83	0.13	0.048	(0.088)	0.009	0.040
215	17.92	0.13	0.048	(0.088)	0.009	0.040
216	18.00	0.13	0.048	(0.087)	0.009	0.040
217	18.08	0.13	0.048	(0.087)	0.009	0.040
218	18.17	0.13	0.048	(0.086)	0.009	0.040
219	18.25	0.13	0.048	(0.086)	0.009	0.040
220	18.33	0.13	0.048	(0.086)	0.009	0.040
221	18.42	0.13	0.048	(0.085)	0.009	0.040
222	18.50	0.13	0.048	(0.085)	0.009	0.040
223	18.58	0.10	0.036	(0.084)	0.007	0.030
224	18.67	0.10	0.036	(0.084)	0.007	0.030
225	18.75	0.10	0.036	(0.084)	0.007	0.030
226	18.83	0.07	0.024	(0.083)	0.004	0.020
227	18.92	0.07	0.024	(0.083)	0.004	0.020
228	19.00	0.07	0.024	(0.082)	0.004	0.020
229	19.08	0.10	0.036	(0.082)	0.007	0.030
230	19.17	0.10	0.036	(0.082)	0.007	0.030
231	19.25	0.10	0.036	(0.081)	0.007	0.030
232	19.33	0.13	0.048	(0.081)	0.009	0.040
233	19.42	0.13	0.048	(0.080)	0.009	0.040
234	19.50	0.13	0.048	(0.080)	0.009	0.040
235	19.58	0.10	0.036	(0.080)	0.007	0.030
236	19.67	0.10	0.036	(0.079)	0.007	0.030
237	19.75	0.10	0.036	(0.079)	0.007	0.030
238	19.83	0.07	0.024	(0.079)	0.004	0.020
239	19.92	0.07	0.024	(0.078)	0.004	0.020
240	20.00	0.07	0.024	(0.078)	0.004	0.020
241	20.08	0.10	0.036	(0.078)	0.007	0.030
242	20.17	0.10	0.036	(0.077)	0.007	0.030
243	20.25	0.10	0.036	(0.077)	0.007	0.030
244	20.33	0.10	0.036	(0.077)	0.007	0.030
245	20.42	0.10	0.036	(0.076)	0.007	0.030
246	20.50	0.10	0.036	(0.076)	0.007	0.030
247	20.58	0.10	0.036	(0.076)	0.007	0.030
248	20.67	0.10	0.036	(0.075)	0.007	0.030
249	20.75	0.10	0.036	(0.075)	0.007	0.030
250	20.83	0.07	0.024	(0.075)	0.004	0.020
251	20.92	0.07	0.024	(0.074)	0.004	0.020
252	21.00	0.07	0.024	(0.074)	0.004	0.020
253	21.08	0.10	0.036	(0.074)	0.007	0.030
254	21.17	0.10	0.036	(0.073)	0.007	0.030
255	21.25	0.10	0.036	(0.073)	0.007	0.030
256	21.33	0.07	0.024	(0.073)	0.004	0.020
257	21.42	0.07	0.024	(0.073)	0.004	0.020
258	21.50	0.07	0.024	(0.072)	0.004	0.020
259	21.58	0.10	0.036	(0.072)	0.007	0.030

260	21.67	0.10	0.036	(0.072)	0.007	0.030
261	21.75	0.10	0.036	(0.072)	0.007	0.030
262	21.83	0.07	0.024	(0.071)	0.004	0.020
263	21.92	0.07	0.024	(0.071)	0.004	0.020
264	22.00	0.07	0.024	(0.071)	0.004	0.020
265	22.08	0.10	0.036	(0.071)	0.007	0.030
266	22.17	0.10	0.036	(0.070)	0.007	0.030
267	22.25	0.10	0.036	(0.070)	0.007	0.030
268	22.33	0.07	0.024	(0.070)	0.004	0.020
269	22.42	0.07	0.024	(0.070)	0.004	0.020
270	22.50	0.07	0.024	(0.069)	0.004	0.020
271	22.58	0.07	0.024	(0.069)	0.004	0.020
272	22.67	0.07	0.024	(0.069)	0.004	0.020
273	22.75	0.07	0.024	(0.069)	0.004	0.020
274	22.83	0.07	0.024	(0.069)	0.004	0.020
275	22.92	0.07	0.024	(0.069)	0.004	0.020
276	23.00	0.07	0.024	(0.068)	0.004	0.020
277	23.08	0.07	0.024	(0.068)	0.004	0.020
278	23.17	0.07	0.024	(0.068)	0.004	0.020
279	23.25	0.07	0.024	(0.068)	0.004	0.020
280	23.33	0.07	0.024	(0.068)	0.004	0.020
281	23.42	0.07	0.024	(0.068)	0.004	0.020
282	23.50	0.07	0.024	(0.068)	0.004	0.020
283	23.58	0.07	0.024	(0.067)	0.004	0.020
284	23.67	0.07	0.024	(0.067)	0.004	0.020
285	23.75	0.07	0.024	(0.067)	0.004	0.020
286	23.83	0.07	0.024	(0.067)	0.004	0.020
287	23.92	0.07	0.024	(0.067)	0.004	0.020
288	24.00	0.07	0.024	(0.067)	0.004	0.020

(Loss Rate Not Used)

Sum = 100.0 Sum = 29.8

Flood volume = Effective rainfall 2.49(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.55(In)
Total soil loss = 0.006(Ac.Ft)
Total rainfall = 3.03(In)
Flood volume = 1172.7 Cubic Feet
Total soil loss = 257.4 Cubic Feet

Peak flow rate of this hydrograph = 0.044(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q				
0+10	0.0000	0.00	Q				
0+15	0.0001	0.00	Q				
0+20	0.0001	0.00	Q				
0+25	0.0001	0.00	Q				
0+30	0.0001	0.00	Q				
0+35	0.0002	0.00	Q				
0+40	0.0002	0.00	Q				
0+45	0.0002	0.00	Q				
0+50	0.0003	0.01	Q				
0+55	0.0003	0.01	Q				
1+ 0	0.0003	0.01	Q				
1+ 5	0.0003	0.00	Q				
1+10	0.0004	0.00	Q				
1+15	0.0004	0.00	Q				
1+20	0.0004	0.00	Q				
1+25	0.0005	0.00	Q				
1+30	0.0005	0.00	Q				
1+35	0.0005	0.00	Q				
1+40	0.0005	0.00	Q				
1+45	0.0006	0.00	Q				
1+50	0.0006	0.01	Q				

1+55	0.0006	0.01	Q	|	|	|	|
2+ 0	0.0007	0.01	Q	|	|	|	|
2+ 5	0.0007	0.01	QV	|	|	|	|
2+10	0.0007	0.01	QV	|	|	|	|
2+15	0.0008	0.01	QV	|	|	|	|
2+20	0.0008	0.01	QV	|	|	|	|
2+25	0.0009	0.01	QV	|	|	|	|
2+30	0.0009	0.01	QV	|	|	|	|
2+35	0.0009	0.01	QV	|	|	|	|
2+40	0.0010	0.01	QV	|	|	|	|
2+45	0.0010	0.01	QV	|	|	|	|
2+50	0.0011	0.01	QV	|	|	|	|
2+55	0.0011	0.01	QV	|	|	|	|
3+ 0	0.0012	0.01	QV	|	|	|	|
3+ 5	0.0012	0.01	QV	|	|	|	|
3+10	0.0012	0.01	QV	|	|	|	|
3+15	0.0013	0.01	QV	|	|	|	|
3+20	0.0013	0.01	QV	|	|	|	|
3+25	0.0014	0.01	Q V	|	|	|	|
3+30	0.0014	0.01	Q V	|	|	|	|
3+35	0.0015	0.01	Q V	|	|	|	|
3+40	0.0015	0.01	Q V	|	|	|	|
3+45	0.0016	0.01	Q V	|	|	|	|
3+50	0.0016	0.01	Q V	|	|	|	|
3+55	0.0017	0.01	Q V	|	|	|	|
4+ 0	0.0017	0.01	Q V	|	|	|	|
4+ 5	0.0018	0.01	Q V	|	|	|	|
4+10	0.0018	0.01	Q V	|	|	|	|
4+15	0.0019	0.01	Q V	|	|	|	|
4+20	0.0019	0.01	Q V	|	|	|	|
4+25	0.0020	0.01	Q V	|	|	|	|
4+30	0.0021	0.01	Q V	|	|	|	|
4+35	0.0021	0.01	Q V	|	|	|	|
4+40	0.0022	0.01	Q V	|	|	|	|
4+45	0.0023	0.01	Q V	|	|	|	|
4+50	0.0023	0.01	Q V	|	|	|	|
4+55	0.0024	0.01	Q V	|	|	|	|
5+ 0	0.0025	0.01	Q V	|	|	|	|
5+ 5	0.0025	0.01	Q V	|	|	|	|
5+10	0.0026	0.01	Q V	|	|	|	|
5+15	0.0026	0.01	Q V	|	|	|	|
5+20	0.0027	0.01	Q V	|	|	|	|
5+25	0.0028	0.01	Q V	|	|	|	|
5+30	0.0028	0.01	Q V	|	|	|	|
5+35	0.0029	0.01	Q V	|	|	|	|
5+40	0.0030	0.01	Q V	|	|	|	|
5+45	0.0030	0.01	Q V	|	|	|	|
5+50	0.0031	0.01	Q V	|	|	|	|
5+55	0.0032	0.01	Q V	|	|	|	|
6+ 0	0.0033	0.01	Q V	|	|	|	|
6+ 5	0.0033	0.01	Q V	|	|	|	|
6+10	0.0034	0.01	Q V	|	|	|	|
6+15	0.0035	0.01	Q V	|	|	|	|
6+20	0.0036	0.01	Q V	|	|	|	|
6+25	0.0037	0.01	Q V	|	|	|	|
6+30	0.0037	0.01	Q V	|	|	|	|
6+35	0.0038	0.01	Q V	|	|	|	|
6+40	0.0039	0.01	Q V	|	|	|	|
6+45	0.0040	0.01	Q V	|	|	|	|
6+50	0.0041	0.01	Q V	|	|	|	|
6+55	0.0042	0.01	Q V	|	|	|	|
7+ 0	0.0043	0.01	Q V	|	|	|	|
7+ 5	0.0044	0.01	Q V	|	|	|	|
7+10	0.0045	0.01	Q V	|	|	|	|
7+15	0.0045	0.01	Q V	|	|	|	|
7+20	0.0046	0.01	Q V	|	|	|	|
7+25	0.0047	0.01	Q V	|	|	|	|
7+30	0.0048	0.01	Q V	|	|	|	|
7+35	0.0050	0.02	Q V	|	|	|	|
7+40	0.0051	0.02	Q V	|	|	|	|
7+45	0.0052	0.02	Q V	|	|	|	|
7+50	0.0053	0.02	Q V	|	|	|	|

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 7+55       0.0054      0.02  Q       V |          |          |          |
 8+ 0       0.0055      0.02  Q       V |          |          |          |
 8+ 5       0.0057      0.02  Q       V |          |          |          |
 8+10       0.0058      0.02  Q       V |          |          |          |
 8+15       0.0059      0.02  Q       V |          |          |          |
 8+20       0.0061      0.02  Q       V |          |          |          |
 8+25       0.0062      0.02  Q        V|          |          |          |
 8+30       0.0063      0.02  Q        V|          |          |          |
 8+35       0.0065      0.02  Q        V|          |          |          |
 8+40       0.0066      0.02  Q        V|          |          |          |
 8+45       0.0068      0.02  Q         V          |          |          |
 8+50       0.0069      0.02  Q         V          |          |          |
 8+55       0.0071      0.02  Q         V          |          |          |
 9+ 0       0.0072      0.02  Q         V          |          |          |
 9+ 5       0.0074      0.02  Q         V          |          |          |
 9+10       0.0076      0.02  Q          |V         |          |          |
 9+15       0.0077      0.02  Q          |V         |          |          |
 9+20       0.0079      0.03  Q          |V         |          |          |
 9+25       0.0081      0.03  Q          | V        |          |          |
 9+30       0.0083      0.03  Q          | V        |          |          |
 9+35       0.0085      0.03  Q          | V        |          |          |
 9+40       0.0086      0.03  Q          | V        |          |          |
 9+45       0.0088      0.03  Q          |  V       |          |          |
 9+50       0.0090      0.03  Q          |  V       |          |          |
 9+55       0.0092      0.03  Q          |  V       |          |          |
10+ 0       0.0094      0.03  Q          |  V       |          |          |
10+ 5       0.0096      0.02  Q          |   V      |          |          |
10+10       0.0097      0.02  Q          |   V      |          |          |
10+15       0.0098      0.02  Q          |   V      |          |          |
10+20       0.0100      0.02  Q          |   V      |          |          |
10+25       0.0101      0.02  Q          |   V      |          |          |
10+30       0.0102      0.02  Q          |    V     |          |          |
10+35       0.0104      0.03  Q          |    V     |          |          |
10+40       0.0106      0.03  Q          |    V     |          |          |
10+45       0.0108      0.03  Q          |    V     |          |          |
10+50       0.0109      0.03  Q          |     V    |          |          |
10+55       0.0111      0.03  Q          |     V    |          |          |
11+ 0       0.0113      0.03  Q          |     V    |          |          |
11+ 5       0.0115      0.02  Q          |      V   |          |          |
11+10       0.0116      0.02  Q          |      V   |          |          |
11+15       0.0118      0.02  Q          |      V   |          |          |
11+20       0.0120      0.02  Q          |      V   |          |          |
11+25       0.0122      0.02  Q          |       V  |          |          |
11+30       0.0123      0.02  Q          |       V  |          |          |
11+35       0.0125      0.02  Q          |       V  |          |          |
11+40       0.0126      0.02  Q          |       V  |          |          |
11+45       0.0128      0.02  Q          |       V  |          |          |
11+50       0.0129      0.02  Q          |        V |          |          |
11+55       0.0131      0.02  Q          |        V |          |          |
12+ 0       0.0133      0.02  Q          |        V |          |          |
12+ 5       0.0135      0.03  Q          |         V          |          |
12+10       0.0137      0.03  Q          |         V          |          |
12+15       0.0139      0.03  Q          |         V          |          |
12+20       0.0142      0.03  Q          |          |V        |          |
12+25       0.0144      0.03  Q          |          |V        |          |
12+30       0.0146      0.03  Q          |          |V        |          |
12+35       0.0149      0.04  Q          |          | V       |          |
12+40       0.0151      0.04  Q          |          | V       |          |
12+45       0.0154      0.04  Q          |          | V       |          |
12+50       0.0157      0.04  Q          |          |  V      |          |
12+55       0.0159      0.04  Q          |          |  V      |          |
13+ 0       0.0162      0.04  Q          |          |   V     |          |
13+ 5       0.0165      0.04  Q          |          |   V     |          |
13+10       0.0168      0.04  Q          |          |   V     |          |
13+15       0.0171      0.04  Q          |          |    V    |          |
13+20       0.0174      0.04  Q          |          |    V    |          |
13+25       0.0177      0.04  Q          |          |     V   |          |
13+30       0.0180      0.04  Q          |          |     V   |          |
13+35       0.0182      0.03  Q          |          |      V  |          |
13+40       0.0184      0.03  Q          |          |      V  |          |
13+45       0.0186      0.03  Q          |          |      V  |          |
13+50       0.0188      0.03  Q          |          |      V  |          |
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13+55       0.0190      0.03  Q          |           |         V |           |
14+ 0       0.0192      0.03  Q          |           |         V |           |
14+ 5       0.0195      0.04  Q          |           |         V |           |
14+10       0.0197      0.04  Q          |           |          V|           |
14+15       0.0200      0.04  Q          |           |          V|           |
14+20       0.0202      0.03  Q          |           |           V           |
14+25       0.0204      0.03  Q          |           |           V           |
14+30       0.0207      0.03  Q          |           |           V           |
14+35       0.0209      0.03  Q          |           |           |V          |
14+40       0.0211      0.03  Q          |           |           |V          |
14+45       0.0214      0.03  Q          |           |           |V          |
14+50       0.0216      0.03  Q          |           |           | V         |
14+55       0.0218      0.03  Q          |           |           | V         |
15+ 0       0.0220      0.03  Q          |           |           | V         |
15+ 5       0.0223      0.03  Q          |           |           |  V        |
15+10       0.0225      0.03  Q          |           |           |  V        |
15+15       0.0227      0.03  Q          |           |           |  V        |
15+20       0.0229      0.03  Q          |           |           |   V       |
15+25       0.0231      0.03  Q          |           |           |   V       |
15+30       0.0233      0.03  Q          |           |           |   V       |
15+35       0.0235      0.02  Q          |           |           |   V       |
15+40       0.0237      0.02  Q          |           |           |    V      |
15+45       0.0238      0.02  Q          |           |           |    V      |
15+50       0.0240      0.02  Q          |           |           |    V      |
15+55       0.0242      0.02  Q          |           |           |    V      |
16+ 0       0.0243      0.02  Q          |           |           |     V     |
16+ 5       0.0244      0.01  Q          |           |           |     V     |
16+10       0.0244      0.01  Q          |           |           |     V     |
16+15       0.0244      0.01  Q          |           |           |     V     |
16+20       0.0245      0.01  Q          |           |           |     V     |
16+25       0.0245      0.01  Q          |           |           |     V     |
16+30       0.0246      0.01  Q          |           |           |     V     |
16+35       0.0246      0.00  Q          |           |           |     V     |
16+40       0.0246      0.00  Q          |           |           |     V     |
16+45       0.0246      0.00  Q          |           |           |     V     |
16+50       0.0247      0.00  Q          |           |           |     V     |
16+55       0.0247      0.00  Q          |           |           |     V     |
17+ 0       0.0247      0.00  Q          |           |           |     V     |
17+ 5       0.0248      0.01  Q          |           |           |     V     |
17+10       0.0248      0.01  Q          |           |           |     V     |
17+15       0.0248      0.01  Q          |           |           |     V     |
17+20       0.0249      0.01  Q          |           |           |     V     |
17+25       0.0249      0.01  Q          |           |           |      V    |
17+30       0.0250      0.01  Q          |           |           |      V    |
17+35       0.0250      0.01  Q          |           |           |      V    |
17+40       0.0251      0.01  Q          |           |           |      V    |
17+45       0.0251      0.01  Q          |           |           |      V    |
17+50       0.0252      0.01  Q          |           |           |      V    |
17+55       0.0252      0.01  Q          |           |           |      V    |
18+ 0       0.0252      0.01  Q          |           |           |      V    |
18+ 5       0.0253      0.01  Q          |           |           |      V    |
18+10       0.0253      0.01  Q          |           |           |      V    |
18+15       0.0253      0.01  Q          |           |           |      V    |
18+20       0.0254      0.01  Q          |           |           |      V    |
18+25       0.0254      0.01  Q          |           |           |      V    |
18+30       0.0254      0.01  Q          |           |           |      V    |
18+35       0.0255      0.00  Q          |           |           |      V    |
18+40       0.0255      0.00  Q          |           |           |      V    |
18+45       0.0255      0.00  Q          |           |           |      V    |
18+50       0.0255      0.00  Q          |           |           |      V    |
18+55       0.0256      0.00  Q          |           |           |      V    |
19+ 0       0.0256      0.00  Q          |           |           |      V    |
19+ 5       0.0256      0.00  Q          |           |           |       V   |
19+10       0.0256      0.00  Q          |           |           |       V   |
19+15       0.0257      0.00  Q          |           |           |       V   |
19+20       0.0257      0.01  Q          |           |           |       V   |
19+25       0.0257      0.01  Q          |           |           |       V   |
19+30       0.0258      0.01  Q          |           |           |       V   |
19+35       0.0258      0.00  Q          |           |           |       V   |
19+40       0.0258      0.00  Q          |           |           |       V   |
19+45       0.0258      0.00  Q          |           |           |       V   |
19+50       0.0259      0.00  Q          |           |           |       V   |
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19+55	0.0259	0.00	Q	|	|	|	V |
20+ 0	0.0259	0.00	Q	|	|	|	V |
20+ 5	0.0259	0.00	Q	|	|	|	V |
20+10	0.0260	0.00	Q	|	|	|	V |
20+15	0.0260	0.00	Q	|	|	|	V |
20+20	0.0260	0.00	Q	|	|	|	V |
20+25	0.0260	0.00	Q	|	|	|	V |
20+30	0.0261	0.00	Q	|	|	|	V |
20+35	0.0261	0.00	Q	|	|	|	V |
20+40	0.0261	0.00	Q	|	|	|	V |
20+45	0.0261	0.00	Q	|	|	|	V |
20+50	0.0262	0.00	Q	|	|	|	V |
20+55	0.0262	0.00	Q	|	|	|	V |
21+ 0	0.0262	0.00	Q	|	|	|	V |
21+ 5	0.0262	0.00	Q	|	|	|	V |
21+10	0.0262	0.00	Q	|	|	|	V |
21+15	0.0263	0.00	Q	|	|	|	V|
21+20	0.0263	0.00	Q	|	|	|	V|
21+25	0.0263	0.00	Q	|	|	|	V|
21+30	0.0263	0.00	Q	|	|	|	V|
21+35	0.0264	0.00	Q	|	|	|	V|
21+40	0.0264	0.00	Q	|	|	|	V|
21+45	0.0264	0.00	Q	|	|	|	V|
21+50	0.0264	0.00	Q	|	|	|	V|
21+55	0.0264	0.00	Q	|	|	|	V|
22+ 0	0.0265	0.00	Q	|	|	|	V|
22+ 5	0.0265	0.00	Q	|	|	|	V|
22+10	0.0265	0.00	Q	|	|	|	V|
22+15	0.0265	0.00	Q	|	|	|	V|
22+20	0.0266	0.00	Q	|	|	|	V|
22+25	0.0266	0.00	Q	|	|	|	V|
22+30	0.0266	0.00	Q	|	|	|	V|
22+35	0.0266	0.00	Q	|	|	|	V|
22+40	0.0266	0.00	Q	|	|	|	V|
22+45	0.0267	0.00	Q	|	|	|	V|
22+50	0.0267	0.00	Q	|	|	|	V|
22+55	0.0267	0.00	Q	|	|	|	V|
23+ 0	0.0267	0.00	Q	|	|	|	V|
23+ 5	0.0267	0.00	Q	|	|	|	V|
23+10	0.0267	0.00	Q	|	|	|	V|
23+15	0.0268	0.00	Q	|	|	|	V|
23+20	0.0268	0.00	Q	|	|	|	V|
23+25	0.0268	0.00	Q	|	|	|	V|
23+30	0.0268	0.00	Q	|	|	|	V|
23+35	0.0268	0.00	Q	|	|	|	V|
23+40	0.0268	0.00	Q	|	|	|	V|
23+45	0.0269	0.00	Q	|	|	|	V|
23+50	0.0269	0.00	Q	|	|	|	V|
23+55	0.0269	0.00	Q	|	|	|	V|
24+ 0	0.0269	0.00	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB0565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	1.20	0.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	3.00	0.39

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.622(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.622(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

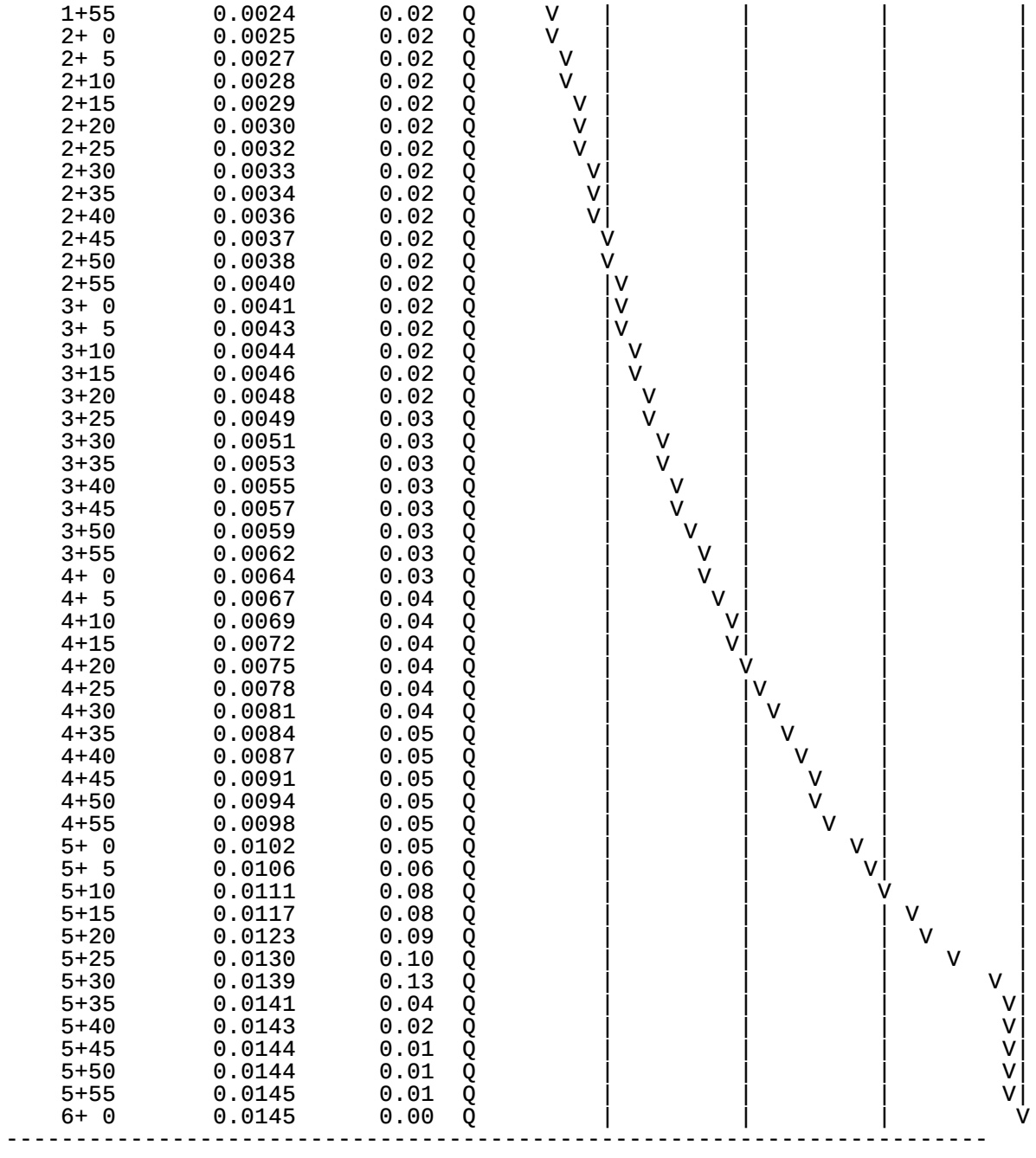
Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
			Sum = 100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.097	(0.134)	0.018	0.080
2	0.17	0.60	0.117	(0.134)	0.021	0.096
3	0.25	0.60	0.117	(0.134)	0.021	0.096
4	0.33	0.60	0.117	(0.134)	0.021	0.096
5	0.42	0.60	0.117	(0.134)	0.021	0.096
6	0.50	0.70	0.136	(0.134)	0.025	0.112
7	0.58	0.70	0.136	(0.134)	0.025	0.112
8	0.67	0.70	0.136	(0.134)	0.025	0.112
9	0.75	0.70	0.136	(0.134)	0.025	0.112
10	0.83	0.70	0.136	(0.134)	0.025	0.112
11	0.92	0.70	0.136	(0.134)	0.025	0.112
12	1.00	0.80	0.156	(0.134)	0.028	0.128
13	1.08	0.80	0.156	(0.134)	0.028	0.128
14	1.17	0.80	0.156	(0.134)	0.028	0.128
15	1.25	0.80	0.156	(0.134)	0.028	0.128
16	1.33	0.80	0.156	(0.134)	0.028	0.128
17	1.42	0.80	0.156	(0.134)	0.028	0.128
18	1.50	0.80	0.156	(0.134)	0.028	0.128
19	1.58	0.80	0.156	(0.134)	0.028	0.128
20	1.67	0.80	0.156	(0.134)	0.028	0.128
21	1.75	0.80	0.156	(0.134)	0.028	0.128
22	1.83	0.80	0.156	(0.134)	0.028	0.128
23	1.92	0.80	0.156	(0.134)	0.028	0.128
24	2.00	0.90	0.175	(0.134)	0.032	0.144
25	2.08	0.80	0.156	(0.134)	0.028	0.128
26	2.17	0.90	0.175	(0.134)	0.032	0.144
27	2.25	0.90	0.175	(0.134)	0.032	0.144
28	2.33	0.90	0.175	(0.134)	0.032	0.144
29	2.42	0.90	0.175	(0.134)	0.032	0.144
30	2.50	0.90	0.175	(0.134)	0.032	0.144
31	2.58	0.90	0.175	(0.134)	0.032	0.144
32	2.67	0.90	0.175	(0.134)	0.032	0.144
33	2.75	1.00	0.195	(0.134)	0.035	0.160
34	2.83	1.00	0.195	(0.134)	0.035	0.160
35	2.92	1.00	0.195	(0.134)	0.035	0.160
36	3.00	1.00	0.195	(0.134)	0.035	0.160
37	3.08	1.00	0.195	(0.134)	0.035	0.160
38	3.17	1.10	0.214	(0.134)	0.039	0.176
39	3.25	1.10	0.214	(0.134)	0.039	0.176
40	3.33	1.10	0.214	(0.134)	0.039	0.176
41	3.42	1.20	0.234	(0.134)	0.042	0.191
42	3.50	1.30	0.253	(0.134)	0.046	0.207
43	3.58	1.40	0.272	(0.134)	0.049	0.223

```
44   3.67     1.40      0.272       (  0.134)       0.049        0.223
45   3.75     1.50      0.292       (  0.134)       0.053        0.239
46   3.83     1.50      0.292       (  0.134)       0.053        0.239
47   3.92     1.60      0.311       (  0.134)       0.056        0.255
48   4.00     1.60      0.311       (  0.134)       0.056        0.255
49   4.08     1.70      0.331       (  0.134)       0.060        0.271
50   4.17     1.80      0.350       (  0.134)       0.063        0.287
51   4.25     1.90      0.370       (  0.134)       0.067        0.303
52   4.33     2.00      0.389       (  0.134)       0.070        0.319
53   4.42     2.10      0.409       (  0.134)       0.074        0.335
54   4.50     2.10      0.409       (  0.134)       0.074        0.335
55   4.58     2.20      0.428       (  0.134)       0.077        0.351
56   4.67     2.30      0.448       (  0.134)       0.081        0.367
57   4.75     2.40      0.467       (  0.134)       0.084        0.383
58   4.83     2.40      0.467       (  0.134)       0.084        0.383
59   4.92     2.50      0.486       (  0.134)       0.088        0.399
60   5.00     2.60      0.506       (  0.134)       0.091        0.415
61   5.08     3.10      0.603       (  0.134)       0.109        0.495
62   5.17     3.60      0.701       (  0.134)       0.126        0.574
63   5.25     3.90      0.759          0.134    (  0.137)       0.625
64   5.33     4.20      0.817          0.134    (  0.147)       0.683
65   5.42     4.70      0.915          0.134    (  0.165)       0.780
66   5.50     5.60      1.090          0.134    (  0.196)       0.956
67   5.58     1.90      0.370       (  0.134)       0.067        0.303
68   5.67     0.90      0.175       (  0.134)       0.032        0.144
69   5.75     0.60      0.117       (  0.134)       0.021        0.096
70   5.83     0.50      0.097       (  0.134)       0.018        0.080
71   5.92     0.30      0.058       (  0.134)       0.011        0.048
72   6.00     0.20      0.039       (  0.134)       0.007        0.032
              (Loss Rate Not Used)
   Sum =     100.0                                   Sum =    16.1
      Flood volume = Effective rainfall      1.34(In)
       times area       0.1(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
      Total soil loss =      0.28(In)
      Total soil loss =     0.003(Ac.Ft)
      Total rainfall =      1.62(In)
      Flood volume =         631.7 Cubic Feet
      Total soil loss =         133.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.125(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0001      0.01  Q         |         |         |         |
  0+10       0.0002      0.01  Q         |         |         |         |
  0+15       0.0002      0.01  Q         |         |         |         |
  0+20       0.0003      0.01  Q         |         |         |         |
  0+25       0.0004      0.01  QV        |         |         |         |
  0+30       0.0005      0.01  QV        |         |         |         |
  0+35       0.0006      0.01  QV        |         |         |         |
  0+40       0.0007      0.01  QV        |         |         |         |
  0+45       0.0008      0.01  Q V       |         |         |         |
  0+50       0.0009      0.01  Q V       |         |         |         |
  0+55       0.0010      0.01  Q V       |         |         |         |
  1+ 0       0.0011      0.02  Q  V      |         |         |         |
  1+ 5       0.0013      0.02  Q  V      |         |         |         |
  1+10       0.0014      0.02  Q  V      |         |         |         |
  1+15       0.0015      0.02  Q   V     |         |         |         |
  1+20       0.0016      0.02  Q   V     |         |         |         |
  1+25       0.0017      0.02  Q   V     |         |         |         |
  1+30       0.0018      0.02  Q    V    |         |         |         |
  1+35       0.0019      0.02  Q    V    |         |         |         |
  1+40       0.0021      0.02  Q    V    |         |         |         |
  1+45       0.0022      0.02  Q    V    |         |         |         |
  1+50       0.0023      0.02  Q     V   |         |         |         |
```


1+55 0.0024 0.02 Q
2+ 0 0.0025 0.02 Q
2+ 5 0.0027 0.02 Q
2+10 0.0028 0.02 Q
2+15 0.0029 0.02 Q
2+20 0.0030 0.02 Q
2+25 0.0032 0.02 Q
2+30 0.0033 0.02 Q
2+35 0.0034 0.02 Q
2+40 0.0036 0.02 Q
2+45 0.0037 0.02 Q
2+50 0.0038 0.02 Q
2+55 0.0040 0.02 Q
3+ 0 0.0041 0.02 Q
3+ 5 0.0043 0.02 Q
3+10 0.0044 0.02 Q
3+15 0.0046 0.02 Q
3+20 0.0048 0.02 Q
3+25 0.0049 0.03 Q
3+30 0.0051 0.03 Q
3+35 0.0053 0.03 Q
3+40 0.0055 0.03 Q
3+45 0.0057 0.03 Q
3+50 0.0059 0.03 Q
3+55 0.0062 0.03 Q
4+ 0 0.0064 0.03 Q
4+ 5 0.0067 0.04 Q
4+10 0.0069 0.04 Q
4+15 0.0072 0.04 Q
4+20 0.0075 0.04 Q
4+25 0.0078 0.04 Q
4+30 0.0081 0.04 Q
4+35 0.0084 0.05 Q
4+40 0.0087 0.05 Q
4+45 0.0091 0.05 Q
4+50 0.0094 0.05 Q
4+55 0.0098 0.05 Q
5+ 0 0.0102 0.05 Q
5+ 5 0.0106 0.06 Q
5+10 0.0111 0.08 Q
5+15 0.0117 0.08 Q
5+20 0.0123 0.09 Q
5+25 0.0130 0.10 Q
5+30 0.0139 0.13 Q
5+35 0.0141 0.04 Q
5+40 0.0143 0.02 Q
5+45 0.0144 0.01 Q
5+50 0.0144 0.01 Q
5+55 0.0145 0.01 Q
6+ 0 0.0145 0.00 Q

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB0535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	0.90	0.12

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	2.35	0.31

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.240(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.240(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
		Sum =	100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.193	(0.134)	0.035	0.159
2	0.17	1.30	0.193	(0.134)	0.035	0.159
3	0.25	1.10	0.164	(0.134)	0.029	0.134
4	0.33	1.50	0.223	(0.134)	0.040	0.183
5	0.42	1.50	0.223	(0.134)	0.040	0.183
6	0.50	1.80	0.268	(0.134)	0.048	0.220
7	0.58	1.50	0.223	(0.134)	0.040	0.183
8	0.67	1.80	0.268	(0.134)	0.048	0.220
9	0.75	1.80	0.268	(0.134)	0.048	0.220
10	0.83	1.50	0.223	(0.134)	0.040	0.183
11	0.92	1.60	0.238	(0.134)	0.043	0.195
12	1.00	1.80	0.268	(0.134)	0.048	0.220
13	1.08	2.20	0.327	(0.134)	0.059	0.268
14	1.17	2.20	0.327	(0.134)	0.059	0.268
15	1.25	2.20	0.327	(0.134)	0.059	0.268
16	1.33	2.00	0.298	(0.134)	0.054	0.244
17	1.42	2.60	0.387	(0.134)	0.070	0.317
18	1.50	2.70	0.402	(0.134)	0.072	0.329
19	1.58	2.40	0.357	(0.134)	0.064	0.293
20	1.67	2.70	0.402	(0.134)	0.072	0.329
21	1.75	3.30	0.491	(0.134)	0.088	0.403
22	1.83	3.10	0.461	(0.134)	0.083	0.378
23	1.92	2.90	0.431	(0.134)	0.078	0.354
24	2.00	3.00	0.446	(0.134)	0.080	0.366
25	2.08	3.10	0.461	(0.134)	0.083	0.378
26	2.17	4.20	0.625	(0.134)	0.112	0.512
27	2.25	5.00	0.744	(0.134)	0.134	0.610
28	2.33	3.50	0.521	(0.134)	0.094	0.427
29	2.42	6.80	1.012	0.134	(0.182)	0.877
30	2.50	7.30	1.086	0.134	(0.195)	0.952
31	2.58	8.20	1.220	0.134	(0.220)	1.086
32	2.67	5.90	0.878	0.134	(0.158)	0.744
33	2.75	2.00	0.298	(0.134)	0.054	0.244
34	2.83	1.80	0.268	(0.134)	0.048	0.220
35	2.92	1.80	0.268	(0.134)	0.048	0.220
36	3.00	0.60	0.089	(0.134)	0.016	0.073
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	12.4

Flood volume = Effective rainfall 1.03(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.002(Ac.Ft)
Total rainfall = 1.24(In)

```
      Flood volume =         488.3 Cubic Feet
      Total soil loss =          96.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.142(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ---------------------------------------------------------------------------
   0+ 5       0.0001      0.02  Q         |         |         |         |
   0+10       0.0003      0.02  QV        |         |         |         |
   0+15       0.0004      0.02  QV        |         |         |         |
   0+20       0.0006      0.02  Q V       |         |         |         |
   0+25       0.0007      0.02  Q V       |         |         |         |
   0+30       0.0009      0.03  Q  V      |         |         |         |
   0+35       0.0011      0.02  Q  V      |         |         |         |
   0+40       0.0013      0.03  Q   V     |         |         |         |
   0+45       0.0015      0.03  Q    V    |         |         |         |
   0+50       0.0017      0.02  Q    V    |         |         |         |
   0+55       0.0018      0.03  Q     V   |         |         |         |
   1+ 0       0.0020      0.03  Q      V  |         |         |         |
   1+ 5       0.0023      0.04  Q       V |         |         |         |
   1+10       0.0025      0.04  Q       V |         |         |         |
   1+15       0.0028      0.04  Q        V|         |         |         |
   1+20       0.0030      0.03  Q         V         |         |         |
   1+25       0.0033      0.04  Q         |V        |         |         |
   1+30       0.0036      0.04  Q         | V       |         |         |
   1+35       0.0038      0.04  Q         |  V      |         |         |
   1+40       0.0041      0.04  Q         |   V     |         |         |
   1+45       0.0045      0.05  Q         |     V   |         |         |
   1+50       0.0048      0.05  Q         |      V  |         |         |
   1+55       0.0052      0.05  Q         |       V |         |         |
   2+ 0       0.0055      0.05  Q         |        V|         |         |
   2+ 5       0.0058      0.05  Q         |         V         |         |
   2+10       0.0063      0.07  Q         |          V        |         |
   2+15       0.0068      0.08  Q         |           V       |         |
   2+20       0.0072      0.06  Q         |            V      |         |
   2+25       0.0080      0.12  Q         |             V     |         |
   2+30       0.0089      0.12  Q         |              V    |         |
   2+35       0.0099      0.14  Q         |               V   |         |
   2+40       0.0105      0.10  Q         |                V  |         |
   2+45       0.0107      0.03  Q         |                 V |         |
   2+50       0.0109      0.03  Q         |                  V|         |
   2+55       0.0111      0.03  Q         |                  V|         |
   3+ 0       0.0112      0.01  Q         |                  V|         |
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB0515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	0.54	0.07

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	1.36	0.18

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.732(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.732(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	100.000	0.131
	2289.994	Sum = 100.000	Sum= 0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.387	(0.134)	0.070	0.317
2	0.17	4.50	0.395	(0.134)	0.071	0.324
3	0.25	5.40	0.474	(0.134)	0.085	0.389
4	0.33	5.40	0.474	(0.134)	0.085	0.389
5	0.42	5.70	0.501	(0.134)	0.090	0.411
6	0.50	6.40	0.562	(0.134)	0.101	0.461
7	0.58	7.90	0.694	(0.134)	0.125	0.569
8	0.67	9.10	0.799	0.134	(0.144)	0.665
9	0.75	12.80	1.124	0.134	(0.202)	0.990
10	0.83	25.60	2.249	0.134	(0.405)	2.115
11	0.92	7.90	0.694	(0.134)	0.125	0.569
12	1.00	4.90	0.430	(0.134)	0.077	0.353
	(Loss Rate Not Used)					
Sum =	100.0				Sum =	7.6

Flood volume = Effective rainfall 0.63(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.10(In)
Total soil loss = 0.001(Ac.Ft)
Total rainfall = 0.73(In)
Flood volume = 297.0 Cubic Feet
Total soil loss = 48.5 Cubic Feet

Peak flow rate of this hydrograph = 0.277(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0003	0.04	QV				
0+10	0.0006	0.04	Q V				
0+15	0.0009	0.05	Q V				
0+20	0.0013	0.05	Q V				
0+25	0.0017	0.05	Q V				
0+30	0.0021	0.06	Q V				
0+35	0.0026	0.07	Q V				
0+40	0.0032	0.09	Q V				

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    0+45       0.0041      0.13  Q          |          |  V      |          |
    0+50       0.0060      0.28  |Q         |          |         |    V     |
    0+55       0.0065      0.07  Q          |          |         |       V  |
    1+ 0       0.0068      0.05  Q          |          |         |        V |
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	2.00	0.26

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	6.40	0.83

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.810(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.810(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
			Sum = 100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.030	(0.172)	0.005	0.025
2	0.17	0.07	0.030	(0.171)	0.005	0.025
3	0.25	0.07	0.030	(0.171)	0.005	0.025
4	0.33	0.10	0.046	(0.170)	0.008	0.037
5	0.42	0.10	0.046	(0.169)	0.008	0.037
6	0.50	0.10	0.046	(0.169)	0.008	0.037
7	0.58	0.10	0.046	(0.168)	0.008	0.037
8	0.67	0.10	0.046	(0.167)	0.008	0.037
9	0.75	0.10	0.046	(0.167)	0.008	0.037
10	0.83	0.13	0.061	(0.166)	0.011	0.050
11	0.92	0.13	0.061	(0.165)	0.011	0.050
12	1.00	0.13	0.061	(0.165)	0.011	0.050
13	1.08	0.10	0.046	(0.164)	0.008	0.037
14	1.17	0.10	0.046	(0.163)	0.008	0.037
15	1.25	0.10	0.046	(0.163)	0.008	0.037
16	1.33	0.10	0.046	(0.162)	0.008	0.037
17	1.42	0.10	0.046	(0.162)	0.008	0.037
18	1.50	0.10	0.046	(0.161)	0.008	0.037
19	1.58	0.10	0.046	(0.160)	0.008	0.037
20	1.67	0.10	0.046	(0.160)	0.008	0.037
21	1.75	0.10	0.046	(0.159)	0.008	0.037
22	1.83	0.13	0.061	(0.158)	0.011	0.050
23	1.92	0.13	0.061	(0.158)	0.011	0.050
24	2.00	0.13	0.061	(0.157)	0.011	0.050
25	2.08	0.13	0.061	(0.156)	0.011	0.050
26	2.17	0.13	0.061	(0.156)	0.011	0.050
27	2.25	0.13	0.061	(0.155)	0.011	0.050
28	2.33	0.13	0.061	(0.155)	0.011	0.050
29	2.42	0.13	0.061	(0.154)	0.011	0.050
30	2.50	0.13	0.061	(0.153)	0.011	0.050
31	2.58	0.17	0.076	(0.153)	0.014	0.062
32	2.67	0.17	0.076	(0.152)	0.014	0.062
33	2.75	0.17	0.076	(0.151)	0.014	0.062
34	2.83	0.17	0.076	(0.151)	0.014	0.062
35	2.92	0.17	0.076	(0.150)	0.014	0.062
36	3.00	0.17	0.076	(0.150)	0.014	0.062
37	3.08	0.17	0.076	(0.149)	0.014	0.062
38	3.17	0.17	0.076	(0.148)	0.014	0.062
39	3.25	0.17	0.076	(0.148)	0.014	0.062
40	3.33	0.17	0.076	(0.147)	0.014	0.062
41	3.42	0.17	0.076	(0.146)	0.014	0.062
42	3.50	0.17	0.076	(0.146)	0.014	0.062
43	3.58	0.17	0.076	(0.145)	0.014	0.062

44	3.67	0.17	0.076	(0.145)	0.014	0.062
45	3.75	0.17	0.076	(0.144)	0.014	0.062
46	3.83	0.20	0.091	(0.143)	0.016	0.075
47	3.92	0.20	0.091	(0.143)	0.016	0.075
48	4.00	0.20	0.091	(0.142)	0.016	0.075
49	4.08	0.20	0.091	(0.142)	0.016	0.075
50	4.17	0.20	0.091	(0.141)	0.016	0.075
51	4.25	0.20	0.091	(0.140)	0.016	0.075
52	4.33	0.23	0.107	(0.140)	0.019	0.087
53	4.42	0.23	0.107	(0.139)	0.019	0.087
54	4.50	0.23	0.107	(0.139)	0.019	0.087
55	4.58	0.23	0.107	(0.138)	0.019	0.087
56	4.67	0.23	0.107	(0.137)	0.019	0.087
57	4.75	0.23	0.107	(0.137)	0.019	0.087
58	4.83	0.27	0.122	(0.136)	0.022	0.100
59	4.92	0.27	0.122	(0.136)	0.022	0.100
60	5.00	0.27	0.122	(0.135)	0.022	0.100
61	5.08	0.20	0.091	(0.134)	0.016	0.075
62	5.17	0.20	0.091	(0.134)	0.016	0.075
63	5.25	0.20	0.091	(0.133)	0.016	0.075
64	5.33	0.23	0.107	(0.133)	0.019	0.087
65	5.42	0.23	0.107	(0.132)	0.019	0.087
66	5.50	0.23	0.107	(0.132)	0.019	0.087
67	5.58	0.27	0.122	(0.131)	0.022	0.100
68	5.67	0.27	0.122	(0.130)	0.022	0.100
69	5.75	0.27	0.122	(0.130)	0.022	0.100
70	5.83	0.27	0.122	(0.129)	0.022	0.100
71	5.92	0.27	0.122	(0.129)	0.022	0.100
72	6.00	0.27	0.122	(0.128)	0.022	0.100
73	6.08	0.30	0.137	(0.128)	0.025	0.112
74	6.17	0.30	0.137	(0.127)	0.025	0.112
75	6.25	0.30	0.137	(0.126)	0.025	0.112
76	6.33	0.30	0.137	(0.126)	0.025	0.112
77	6.42	0.30	0.137	(0.125)	0.025	0.112
78	6.50	0.30	0.137	(0.125)	0.025	0.112
79	6.58	0.33	0.152	(0.124)	0.027	0.125
80	6.67	0.33	0.152	(0.124)	0.027	0.125
81	6.75	0.33	0.152	(0.123)	0.027	0.125
82	6.83	0.33	0.152	(0.122)	0.027	0.125
83	6.92	0.33	0.152	(0.122)	0.027	0.125
84	7.00	0.33	0.152	(0.121)	0.027	0.125
85	7.08	0.33	0.152	(0.121)	0.027	0.125
86	7.17	0.33	0.152	(0.120)	0.027	0.125
87	7.25	0.33	0.152	(0.120)	0.027	0.125
88	7.33	0.37	0.168	(0.119)	0.030	0.137
89	7.42	0.37	0.168	(0.119)	0.030	0.137
90	7.50	0.37	0.168	(0.118)	0.030	0.137
91	7.58	0.40	0.183	(0.118)	0.033	0.150
92	7.67	0.40	0.183	(0.117)	0.033	0.150
93	7.75	0.40	0.183	(0.116)	0.033	0.150
94	7.83	0.43	0.198	(0.116)	0.036	0.162
95	7.92	0.43	0.198	(0.115)	0.036	0.162
96	8.00	0.43	0.198	(0.115)	0.036	0.162
97	8.08	0.50	0.229	(0.114)	0.041	0.187
98	8.17	0.50	0.229	(0.114)	0.041	0.187
99	8.25	0.50	0.229	(0.113)	0.041	0.187
100	8.33	0.50	0.229	(0.113)	0.041	0.187
101	8.42	0.50	0.229	(0.112)	0.041	0.187
102	8.50	0.50	0.229	(0.112)	0.041	0.187
103	8.58	0.53	0.244	(0.111)	0.044	0.200
104	8.67	0.53	0.244	(0.111)	0.044	0.200
105	8.75	0.53	0.244	(0.110)	0.044	0.200
106	8.83	0.57	0.259	(0.110)	0.047	0.212
107	8.92	0.57	0.259	(0.109)	0.047	0.212
108	9.00	0.57	0.259	(0.109)	0.047	0.212
109	9.08	0.63	0.290	(0.108)	0.052	0.237
110	9.17	0.63	0.290	(0.108)	0.052	0.237
111	9.25	0.63	0.290	(0.107)	0.052	0.237
112	9.33	0.67	0.305	(0.107)	0.055	0.250
113	9.42	0.67	0.305	(0.106)	0.055	0.250
114	9.50	0.67	0.305	(0.105)	0.055	0.250
115	9.58	0.70	0.320	(0.105)	0.058	0.262

116	9.67	0.70	0.320	(0.104)	0.058	0.262
117	9.75	0.70	0.320	(0.104)	0.058	0.262
118	9.83	0.73	0.335	(0.103)	0.060	0.275
119	9.92	0.73	0.335	(0.103)	0.060	0.275
120	10.00	0.73	0.335	(0.102)	0.060	0.275
121	10.08	0.50	0.229	(0.102)	0.041	0.187
122	10.17	0.50	0.229	(0.101)	0.041	0.187
123	10.25	0.50	0.229	(0.101)	0.041	0.187
124	10.33	0.50	0.229	(0.101)	0.041	0.187
125	10.42	0.50	0.229	(0.100)	0.041	0.187
126	10.50	0.50	0.229	(0.100)	0.041	0.187
127	10.58	0.67	0.305	(0.099)	0.055	0.250
128	10.67	0.67	0.305	(0.099)	0.055	0.250
129	10.75	0.67	0.305	(0.098)	0.055	0.250
130	10.83	0.67	0.305	(0.098)	0.055	0.250
131	10.92	0.67	0.305	(0.097)	0.055	0.250
132	11.00	0.67	0.305	(0.097)	0.055	0.250
133	11.08	0.63	0.290	(0.096)	0.052	0.237
134	11.17	0.63	0.290	(0.096)	0.052	0.237
135	11.25	0.63	0.290	(0.095)	0.052	0.237
136	11.33	0.63	0.290	(0.095)	0.052	0.237
137	11.42	0.63	0.290	(0.094)	0.052	0.237
138	11.50	0.63	0.290	(0.094)	0.052	0.237
139	11.58	0.57	0.259	(0.093)	0.047	0.212
140	11.67	0.57	0.259	(0.093)	0.047	0.212
141	11.75	0.57	0.259	(0.092)	0.047	0.212
142	11.83	0.60	0.274	(0.092)	0.049	0.225
143	11.92	0.60	0.274	(0.092)	0.049	0.225
144	12.00	0.60	0.274	(0.091)	0.049	0.225
145	12.08	0.83	0.381	(0.091)	0.069	0.312
146	12.17	0.83	0.381	(0.090)	0.069	0.312
147	12.25	0.83	0.381	(0.090)	0.069	0.312
148	12.33	0.87	0.396	(0.089)	0.071	0.325
149	12.42	0.87	0.396	(0.089)	0.071	0.325
150	12.50	0.87	0.396	(0.088)	0.071	0.325
151	12.58	0.93	0.427	(0.088)	0.077	0.350
152	12.67	0.93	0.427	(0.087)	0.077	0.350
153	12.75	0.93	0.427	(0.087)	0.077	0.350
154	12.83	0.97	0.442	(0.087)	0.080	0.362
155	12.92	0.97	0.442	(0.086)	0.080	0.362
156	13.00	0.97	0.442	(0.086)	0.080	0.362
157	13.08	1.13	0.518	0.085	(0.093)	0.433
158	13.17	1.13	0.518	0.085	(0.093)	0.433
159	13.25	1.13	0.518	0.084	(0.093)	0.434
160	13.33	1.13	0.518	0.084	(0.093)	0.434
161	13.42	1.13	0.518	0.084	(0.093)	0.435
162	13.50	1.13	0.518	0.083	(0.093)	0.435
163	13.58	0.77	0.351	(0.083)	0.063	0.287
164	13.67	0.77	0.351	(0.082)	0.063	0.287
165	13.75	0.77	0.351	(0.082)	0.063	0.287
166	13.83	0.77	0.351	(0.081)	0.063	0.287
167	13.92	0.77	0.351	(0.081)	0.063	0.287
168	14.00	0.77	0.351	(0.081)	0.063	0.287
169	14.08	0.90	0.412	(0.080)	0.074	0.337
170	14.17	0.90	0.412	(0.080)	0.074	0.337
171	14.25	0.90	0.412	(0.079)	0.074	0.337
172	14.33	0.87	0.396	(0.079)	0.071	0.325
173	14.42	0.87	0.396	(0.079)	0.071	0.325
174	14.50	0.87	0.396	(0.078)	0.071	0.325
175	14.58	0.87	0.396	(0.078)	0.071	0.325
176	14.67	0.87	0.396	(0.077)	0.071	0.325
177	14.75	0.87	0.396	(0.077)	0.071	0.325
178	14.83	0.83	0.381	(0.077)	0.069	0.312
179	14.92	0.83	0.381	(0.076)	0.069	0.312
180	15.00	0.83	0.381	(0.076)	0.069	0.312
181	15.08	0.80	0.366	(0.075)	0.066	0.300
182	15.17	0.80	0.366	(0.075)	0.066	0.300
183	15.25	0.80	0.366	(0.075)	0.066	0.300
184	15.33	0.77	0.351	(0.074)	0.063	0.287
185	15.42	0.77	0.351	(0.074)	0.063	0.287
186	15.50	0.77	0.351	(0.073)	0.063	0.287
187	15.58	0.63	0.290	(0.073)	0.052	0.237

188	15.67	0.63	0.290	(0.073)	0.052	0.237
189	15.75	0.63	0.290	(0.072)	0.052	0.237
190	15.83	0.63	0.290	(0.072)	0.052	0.237
191	15.92	0.63	0.290	(0.072)	0.052	0.237
192	16.00	0.63	0.290	(0.071)	0.052	0.237
193	16.08	0.13	0.061	(0.071)	0.011	0.050
194	16.17	0.13	0.061	(0.071)	0.011	0.050
195	16.25	0.13	0.061	(0.070)	0.011	0.050
196	16.33	0.13	0.061	(0.070)	0.011	0.050
197	16.42	0.13	0.061	(0.069)	0.011	0.050
198	16.50	0.13	0.061	(0.069)	0.011	0.050
199	16.58	0.10	0.046	(0.069)	0.008	0.037
200	16.67	0.10	0.046	(0.068)	0.008	0.037
201	16.75	0.10	0.046	(0.068)	0.008	0.037
202	16.83	0.10	0.046	(0.068)	0.008	0.037
203	16.92	0.10	0.046	(0.067)	0.008	0.037
204	17.00	0.10	0.046	(0.067)	0.008	0.037
205	17.08	0.17	0.076	(0.067)	0.014	0.062
206	17.17	0.17	0.076	(0.066)	0.014	0.062
207	17.25	0.17	0.076	(0.066)	0.014	0.062
208	17.33	0.17	0.076	(0.066)	0.014	0.062
209	17.42	0.17	0.076	(0.065)	0.014	0.062
210	17.50	0.17	0.076	(0.065)	0.014	0.062
211	17.58	0.17	0.076	(0.065)	0.014	0.062
212	17.67	0.17	0.076	(0.064)	0.014	0.062
213	17.75	0.17	0.076	(0.064)	0.014	0.062
214	17.83	0.13	0.061	(0.064)	0.011	0.050
215	17.92	0.13	0.061	(0.063)	0.011	0.050
216	18.00	0.13	0.061	(0.063)	0.011	0.050
217	18.08	0.13	0.061	(0.063)	0.011	0.050
218	18.17	0.13	0.061	(0.063)	0.011	0.050
219	18.25	0.13	0.061	(0.062)	0.011	0.050
220	18.33	0.13	0.061	(0.062)	0.011	0.050
221	18.42	0.13	0.061	(0.062)	0.011	0.050
222	18.50	0.13	0.061	(0.061)	0.011	0.050
223	18.58	0.10	0.046	(0.061)	0.008	0.037
224	18.67	0.10	0.046	(0.061)	0.008	0.037
225	18.75	0.10	0.046	(0.060)	0.008	0.037
226	18.83	0.07	0.030	(0.060)	0.005	0.025
227	18.92	0.07	0.030	(0.060)	0.005	0.025
228	19.00	0.07	0.030	(0.060)	0.005	0.025
229	19.08	0.10	0.046	(0.059)	0.008	0.037
230	19.17	0.10	0.046	(0.059)	0.008	0.037
231	19.25	0.10	0.046	(0.059)	0.008	0.037
232	19.33	0.13	0.061	(0.058)	0.011	0.050
233	19.42	0.13	0.061	(0.058)	0.011	0.050
234	19.50	0.13	0.061	(0.058)	0.011	0.050
235	19.58	0.10	0.046	(0.058)	0.008	0.037
236	19.67	0.10	0.046	(0.057)	0.008	0.037
237	19.75	0.10	0.046	(0.057)	0.008	0.037
238	19.83	0.07	0.030	(0.057)	0.005	0.025
239	19.92	0.07	0.030	(0.057)	0.005	0.025
240	20.00	0.07	0.030	(0.056)	0.005	0.025
241	20.08	0.10	0.046	(0.056)	0.008	0.037
242	20.17	0.10	0.046	(0.056)	0.008	0.037
243	20.25	0.10	0.046	(0.056)	0.008	0.037
244	20.33	0.10	0.046	(0.055)	0.008	0.037
245	20.42	0.10	0.046	(0.055)	0.008	0.037
246	20.50	0.10	0.046	(0.055)	0.008	0.037
247	20.58	0.10	0.046	(0.055)	0.008	0.037
248	20.67	0.10	0.046	(0.054)	0.008	0.037
249	20.75	0.10	0.046	(0.054)	0.008	0.037
250	20.83	0.07	0.030	(0.054)	0.005	0.025
251	20.92	0.07	0.030	(0.054)	0.005	0.025
252	21.00	0.07	0.030	(0.054)	0.005	0.025
253	21.08	0.10	0.046	(0.053)	0.008	0.037
254	21.17	0.10	0.046	(0.053)	0.008	0.037
255	21.25	0.10	0.046	(0.053)	0.008	0.037
256	21.33	0.07	0.030	(0.053)	0.005	0.025
257	21.42	0.07	0.030	(0.053)	0.005	0.025
258	21.50	0.07	0.030	(0.052)	0.005	0.025
259	21.58	0.10	0.046	(0.052)	0.008	0.037

260	21.67	0.10	0.046	(0.052)	0.008	0.037
261	21.75	0.10	0.046	(0.052)	0.008	0.037
262	21.83	0.07	0.030	(0.052)	0.005	0.025
263	21.92	0.07	0.030	(0.051)	0.005	0.025
264	22.00	0.07	0.030	(0.051)	0.005	0.025
265	22.08	0.10	0.046	(0.051)	0.008	0.037
266	22.17	0.10	0.046	(0.051)	0.008	0.037
267	22.25	0.10	0.046	(0.051)	0.008	0.037
268	22.33	0.07	0.030	(0.051)	0.005	0.025
269	22.42	0.07	0.030	(0.050)	0.005	0.025
270	22.50	0.07	0.030	(0.050)	0.005	0.025
271	22.58	0.07	0.030	(0.050)	0.005	0.025
272	22.67	0.07	0.030	(0.050)	0.005	0.025
273	22.75	0.07	0.030	(0.050)	0.005	0.025
274	22.83	0.07	0.030	(0.050)	0.005	0.025
275	22.92	0.07	0.030	(0.050)	0.005	0.025
276	23.00	0.07	0.030	(0.049)	0.005	0.025
277	23.08	0.07	0.030	(0.049)	0.005	0.025
278	23.17	0.07	0.030	(0.049)	0.005	0.025
279	23.25	0.07	0.030	(0.049)	0.005	0.025
280	23.33	0.07	0.030	(0.049)	0.005	0.025
281	23.42	0.07	0.030	(0.049)	0.005	0.025
282	23.50	0.07	0.030	(0.049)	0.005	0.025
283	23.58	0.07	0.030	(0.049)	0.005	0.025
284	23.67	0.07	0.030	(0.049)	0.005	0.025
285	23.75	0.07	0.030	(0.049)	0.005	0.025
286	23.83	0.07	0.030	(0.049)	0.005	0.025
287	23.92	0.07	0.030	(0.049)	0.005	0.025
288	24.00	0.07	0.030	(0.049)	0.005	0.025

(Loss Rate Not Used)

Sum = 100.0 Sum = 37.5

Flood volume = Effective rainfall 3.13(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.68(In)
Total soil loss = 0.007(Ac.Ft)
Total rainfall = 3.81(In)
Flood volume = 1476.5 Cubic Feet
Total soil loss = 321.5 Cubic Feet

Peak flow rate of this hydrograph = 0.057(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q	|	|	|	|
0+10	0.0000	0.00	Q	|	|	|	|
0+15	0.0001	0.00	Q	|	|	|	|
0+20	0.0001	0.00	Q	|	|	|	|
0+25	0.0001	0.00	Q	|	|	|	|
0+30	0.0002	0.00	Q	|	|	|	|
0+35	0.0002	0.00	Q	|	|	|	|
0+40	0.0002	0.00	Q	|	|	|	|
0+45	0.0003	0.00	Q	|	|	|	|
0+50	0.0003	0.01	Q	|	|	|	|
0+55	0.0004	0.01	Q	|	|	|	|
1+ 0	0.0004	0.01	Q	|	|	|	|
1+ 5	0.0004	0.00	Q	|	|	|	|
1+10	0.0005	0.00	Q	|	|	|	|
1+15	0.0005	0.00	Q	|	|	|	|
1+20	0.0005	0.00	Q	|	|	|	|
1+25	0.0006	0.00	Q	|	|	|	|
1+30	0.0006	0.00	Q	|	|	|	|
1+35	0.0006	0.00	Q	|	|	|	|
1+40	0.0007	0.00	Q	|	|	|	|
1+45	0.0007	0.00	Q	|	|	|	|
1+50	0.0008	0.01	Q	|	|	|	|

1+55	0.0008	0.01	Q	|	|	|	|
2+ 0	0.0008	0.01	Q	|	|	|	|
2+ 5	0.0009	0.01	QV	|	|	|	|
2+10	0.0009	0.01	QV	|	|	|	|
2+15	0.0010	0.01	QV	|	|	|	|
2+20	0.0010	0.01	QV	|	|	|	|
2+25	0.0011	0.01	QV	|	|	|	|
2+30	0.0011	0.01	QV	|	|	|	|
2+35	0.0012	0.01	QV	|	|	|	|
2+40	0.0012	0.01	QV	|	|	|	|
2+45	0.0013	0.01	QV	|	|	|	|
2+50	0.0013	0.01	QV	|	|	|	|
2+55	0.0014	0.01	QV	|	|	|	|
3+ 0	0.0015	0.01	QV	|	|	|	|
3+ 5	0.0015	0.01	QV	|	|	|	|
3+10	0.0016	0.01	QV	|	|	|	|
3+15	0.0016	0.01	QV	|	|	|	|
3+20	0.0017	0.01	QV	|	|	|	|
3+25	0.0017	0.01	Q V	|	|	|	|
3+30	0.0018	0.01	Q V	|	|	|	|
3+35	0.0019	0.01	Q V	|	|	|	|
3+40	0.0019	0.01	Q V	|	|	|	|
3+45	0.0020	0.01	Q V	|	|	|	|
3+50	0.0020	0.01	Q V	|	|	|	|
3+55	0.0021	0.01	Q V	|	|	|	|
4+ 0	0.0022	0.01	Q V	|	|	|	|
4+ 5	0.0022	0.01	Q V	|	|	|	|
4+10	0.0023	0.01	Q V	|	|	|	|
4+15	0.0024	0.01	Q V	|	|	|	|
4+20	0.0024	0.01	Q V	|	|	|	|
4+25	0.0025	0.01	Q V	|	|	|	|
4+30	0.0026	0.01	Q V	|	|	|	|
4+35	0.0027	0.01	Q V	|	|	|	|
4+40	0.0028	0.01	Q V	|	|	|	|
4+45	0.0028	0.01	Q V	|	|	|	|
4+50	0.0029	0.01	Q V	|	|	|	|
4+55	0.0030	0.01	Q V	|	|	|	|
5+ 0	0.0031	0.01	Q V	|	|	|	|
5+ 5	0.0032	0.01	Q V	|	|	|	|
5+10	0.0032	0.01	Q V	|	|	|	|
5+15	0.0033	0.01	Q V	|	|	|	|
5+20	0.0034	0.01	Q V	|	|	|	|
5+25	0.0035	0.01	Q V	|	|	|	|
5+30	0.0036	0.01	Q V	|	|	|	|
5+35	0.0036	0.01	Q V	|	|	|	|
5+40	0.0037	0.01	Q V	|	|	|	|
5+45	0.0038	0.01	Q V	|	|	|	|
5+50	0.0039	0.01	Q V	|	|	|	|
5+55	0.0040	0.01	Q V	|	|	|	|
6+ 0	0.0041	0.01	Q V	|	|	|	|
6+ 5	0.0042	0.01	Q V	|	|	|	|
6+10	0.0043	0.01	Q V	|	|	|	|
6+15	0.0044	0.01	Q V	|	|	|	|
6+20	0.0045	0.01	Q V	|	|	|	|
6+25	0.0046	0.01	Q V	|	|	|	|
6+30	0.0047	0.01	Q V	|	|	|	|
6+35	0.0048	0.02	Q V	|	|	|	|
6+40	0.0049	0.02	Q V	|	|	|	|
6+45	0.0050	0.02	Q V	|	|	|	|
6+50	0.0052	0.02	Q V	|	|	|	|
6+55	0.0053	0.02	Q V	|	|	|	|
7+ 0	0.0054	0.02	Q V	|	|	|	|
7+ 5	0.0055	0.02	Q V	|	|	|	|
7+10	0.0056	0.02	Q V	|	|	|	|
7+15	0.0057	0.02	Q V	|	|	|	|
7+20	0.0058	0.02	Q V	|	|	|	|
7+25	0.0060	0.02	Q V	|	|	|	|
7+30	0.0061	0.02	Q V	|	|	|	|
7+35	0.0062	0.02	Q V	|	|	|	|
7+40	0.0064	0.02	Q V	|	|	|	|
7+45	0.0065	0.02	Q V	|	|	|	|
7+50	0.0066	0.02	Q V	|	|	|	|

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 7+55       0.0068      0.02  Q       V |          |          |          |
 8+ 0       0.0069      0.02  Q       V |          |          |          |
 8+ 5       0.0071      0.02  Q       V |          |          |          |
 8+10       0.0073      0.02  Q       V |          |          |          |
 8+15       0.0074      0.02  Q       V |          |          |          |
 8+20       0.0076      0.02  Q       V |          |          |          |
 8+25       0.0078      0.02  Q        V|          |          |          |
 8+30       0.0080      0.02  Q        V|          |          |          |
 8+35       0.0081      0.03  Q        V|          |          |          |
 8+40       0.0083      0.03  Q        V|          |          |          |
 8+45       0.0085      0.03  Q         V          |          |          |
 8+50       0.0087      0.03  Q         V          |          |          |
 8+55       0.0089      0.03  Q         V          |          |          |
 9+ 0       0.0091      0.03  Q         V          |          |          |
 9+ 5       0.0093      0.03  Q         V          |          |          |
 9+10       0.0095      0.03  Q          |V         |          |          |
 9+15       0.0097      0.03  Q          |V         |          |          |
 9+20       0.0099      0.03  Q          |V         |          |          |
 9+25       0.0102      0.03  Q          |V         |          |          |
 9+30       0.0104      0.03  Q          | V        |          |          |
 9+35       0.0106      0.03  Q          | V        |          |          |
 9+40       0.0109      0.03  Q          | V        |          |          |
 9+45       0.0111      0.03  Q          |  V       |          |          |
 9+50       0.0114      0.04  Q          |  V       |          |          |
 9+55       0.0116      0.04  Q          |  V       |          |          |
10+ 0       0.0118      0.04  Q          |  V       |          |          |
10+ 5       0.0120      0.02  Q          |   V      |          |          |
10+10       0.0122      0.02  Q          |   V      |          |          |
10+15       0.0124      0.02  Q          |   V      |          |          |
10+20       0.0125      0.02  Q          |   V      |          |          |
10+25       0.0127      0.02  Q          |   V      |          |          |
10+30       0.0129      0.02  Q          |    V     |          |          |
10+35       0.0131      0.03  Q          |    V     |          |          |
10+40       0.0133      0.03  Q          |    V     |          |          |
10+45       0.0135      0.03  Q          |    V     |          |          |
10+50       0.0138      0.03  Q          |     V    |          |          |
10+55       0.0140      0.03  Q          |     V    |          |          |
11+ 0       0.0142      0.03  Q          |     V    |          |          |
11+ 5       0.0144      0.03  Q          |      V   |          |          |
11+10       0.0146      0.03  Q          |      V   |          |          |
11+15       0.0149      0.03  Q          |      V   |          |          |
11+20       0.0151      0.03  Q          |      V   |          |          |
11+25       0.0153      0.03  Q          |       V  |          |          |
11+30       0.0155      0.03  Q          |       V  |          |          |
11+35       0.0157      0.03  Q          |       V  |          |          |
11+40       0.0159      0.03  Q          |       V  |          |          |
11+45       0.0161      0.03  Q          |       V  |          |          |
11+50       0.0163      0.03  Q          |        V |          |          |
11+55       0.0165      0.03  Q          |        V |          |          |
12+ 0       0.0167      0.03  Q          |        V |          |          |
12+ 5       0.0170      0.04  Q          |         V          |          |
12+10       0.0173      0.04  Q          |         V          |          |
12+15       0.0175      0.04  Q          |         V          |          |
12+20       0.0178      0.04  Q          |          |V        |          |
12+25       0.0181      0.04  Q          |          |V        |          |
12+30       0.0184      0.04  Q          |          |V        |          |
12+35       0.0187      0.05  Q          |          | V       |          |
12+40       0.0190      0.05  Q          |          | V       |          |
12+45       0.0194      0.05  Q          |          | V       |          |
12+50       0.0197      0.05  Q          |          |  V      |          |
12+55       0.0200      0.05  Q          |          |  V      |          |
13+ 0       0.0203      0.05  Q          |          |   V     |          |
13+ 5       0.0207      0.06  Q          |          |   V     |          |
13+10       0.0211      0.06  Q          |          |   V     |          |
13+15       0.0215      0.06  Q          |          |    V    |          |
13+20       0.0219      0.06  Q          |          |    V    |          |
13+25       0.0223      0.06  Q          |          |     V   |          |
13+30       0.0227      0.06  Q          |          |     V   |          |
13+35       0.0230      0.04  Q          |          |      V  |          |
13+40       0.0232      0.04  Q          |          |      V  |          |
13+45       0.0235      0.04  Q          |          |      V  |          |
13+50       0.0237      0.04  Q          |          |       V |          |
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13+55       0.0240      0.04  Q          |           |         V |           |
14+ 0       0.0242      0.04  Q          |           |         V |           |
14+ 5       0.0246      0.04  Q          |           |         V |           |
14+10       0.0249      0.04  Q          |           |          V|           |
14+15       0.0252      0.04  Q          |           |          V|           |
14+20       0.0255      0.04  Q          |           |           V           |
14+25       0.0258      0.04  Q          |           |           V           |
14+30       0.0260      0.04  Q          |           |           V           |
14+35       0.0263      0.04  Q          |           |           |V          |
14+40       0.0266      0.04  Q          |           |           |V          |
14+45       0.0269      0.04  Q          |           |           |V          |
14+50       0.0272      0.04  Q          |           |           | V         |
14+55       0.0275      0.04  Q          |           |           | V         |
15+ 0       0.0278      0.04  Q          |           |           | V         |
15+ 5       0.0280      0.04  Q          |           |           |  V        |
15+10       0.0283      0.04  Q          |           |           |  V        |
15+15       0.0286      0.04  Q          |           |           |  V        |
15+20       0.0288      0.04  Q          |           |           |   V       |
15+25       0.0291      0.04  Q          |           |           |   V       |
15+30       0.0294      0.04  Q          |           |           |   V       |
15+35       0.0296      0.03  Q          |           |           |   V       |
15+40       0.0298      0.03  Q          |           |           |    V      |
15+45       0.0300      0.03  Q          |           |           |    V      |
15+50       0.0302      0.03  Q          |           |           |    V      |
15+55       0.0304      0.03  Q          |           |           |    V      |
16+ 0       0.0306      0.03  Q          |           |           |     V     |
16+ 5       0.0307      0.01  Q          |           |           |     V     |
16+10       0.0307      0.01  Q          |           |           |     V     |
16+15       0.0308      0.01  Q          |           |           |     V     |
16+20       0.0308      0.01  Q          |           |           |     V     |
16+25       0.0309      0.01  Q          |           |           |     V     |
16+30       0.0309      0.01  Q          |           |           |     V     |
16+35       0.0310      0.00  Q          |           |           |     V     |
16+40       0.0310      0.00  Q          |           |           |     V     |
16+45       0.0310      0.00  Q          |           |           |     V     |
16+50       0.0311      0.00  Q          |           |           |     V     |
16+55       0.0311      0.00  Q          |           |           |     V     |
17+ 0       0.0311      0.00  Q          |           |           |     V     |
17+ 5       0.0312      0.01  Q          |           |           |     V     |
17+10       0.0312      0.01  Q          |           |           |     V     |
17+15       0.0313      0.01  Q          |           |           |     V     |
17+20       0.0313      0.01  Q          |           |           |     V     |
17+25       0.0314      0.01  Q          |           |           |      V    |
17+30       0.0315      0.01  Q          |           |           |      V    |
17+35       0.0315      0.01  Q          |           |           |      V    |
17+40       0.0316      0.01  Q          |           |           |      V    |
17+45       0.0316      0.01  Q          |           |           |      V    |
17+50       0.0317      0.01  Q          |           |           |      V    |
17+55       0.0317      0.01  Q          |           |           |      V    |
18+ 0       0.0318      0.01  Q          |           |           |      V    |
18+ 5       0.0318      0.01  Q          |           |           |      V    |
18+10       0.0319      0.01  Q          |           |           |      V    |
18+15       0.0319      0.01  Q          |           |           |      V    |
18+20       0.0319      0.01  Q          |           |           |      V    |
18+25       0.0320      0.01  Q          |           |           |      V    |
18+30       0.0320      0.01  Q          |           |           |      V    |
18+35       0.0321      0.00  Q          |           |           |      V    |
18+40       0.0321      0.00  Q          |           |           |      V    |
18+45       0.0321      0.00  Q          |           |           |      V    |
18+50       0.0322      0.00  Q          |           |           |      V    |
18+55       0.0322      0.00  Q          |           |           |      V    |
19+ 0       0.0322      0.00  Q          |           |           |       V   |
19+ 5       0.0322      0.00  Q          |           |           |       V   |
19+10       0.0323      0.00  Q          |           |           |       V   |
19+15       0.0323      0.00  Q          |           |           |       V   |
19+20       0.0324      0.01  Q          |           |           |       V   |
19+25       0.0324      0.01  Q          |           |           |       V   |
19+30       0.0324      0.01  Q          |           |           |       V   |
19+35       0.0325      0.00  Q          |           |           |       V   |
19+40       0.0325      0.00  Q          |           |           |       V   |
19+45       0.0325      0.00  Q          |           |           |       V   |
19+50       0.0326      0.00  Q          |           |           |       V   |
```

19+55	0.0326	0.00	Q	|	|	|	V |
20+ 0	0.0326	0.00	Q	|	|	|	V |
20+ 5	0.0326	0.00	Q	|	|	|	V |
20+10	0.0327	0.00	Q	|	|	|	V |
20+15	0.0327	0.00	Q	|	|	|	V |
20+20	0.0327	0.00	Q	|	|	|	V |
20+25	0.0328	0.00	Q	|	|	|	V |
20+30	0.0328	0.00	Q	|	|	|	V |
20+35	0.0328	0.00	Q	|	|	|	V |
20+40	0.0329	0.00	Q	|	|	|	V |
20+45	0.0329	0.00	Q	|	|	|	V |
20+50	0.0329	0.00	Q	|	|	|	V |
20+55	0.0330	0.00	Q	|	|	|	V |
21+ 0	0.0330	0.00	Q	|	|	|	V |
21+ 5	0.0330	0.00	Q	|	|	|	V |
21+10	0.0331	0.00	Q	|	|	|	V|
21+15	0.0331	0.00	Q	|	|	|	V|
21+20	0.0331	0.00	Q	|	|	|	V|
21+25	0.0331	0.00	Q	|	|	|	V|
21+30	0.0332	0.00	Q	|	|	|	V|
21+35	0.0332	0.00	Q	|	|	|	V|
21+40	0.0332	0.00	Q	|	|	|	V|
21+45	0.0333	0.00	Q	|	|	|	V|
21+50	0.0333	0.00	Q	|	|	|	V|
21+55	0.0333	0.00	Q	|	|	|	V|
22+ 0	0.0333	0.00	Q	|	|	|	V|
22+ 5	0.0334	0.00	Q	|	|	|	V|
22+10	0.0334	0.00	Q	|	|	|	V|
22+15	0.0334	0.00	Q	|	|	|	V|
22+20	0.0334	0.00	Q	|	|	|	V|
22+25	0.0335	0.00	Q	|	|	|	V|
22+30	0.0335	0.00	Q	|	|	|	V|
22+35	0.0335	0.00	Q	|	|	|	V|
22+40	0.0335	0.00	Q	|	|	|	V|
22+45	0.0336	0.00	Q	|	|	|	V|
22+50	0.0336	0.00	Q	|	|	|	V|
22+55	0.0336	0.00	Q	|	|	|	V|
23+ 0	0.0336	0.00	Q	|	|	|	V|
23+ 5	0.0336	0.00	Q	|	|	|	V|
23+10	0.0337	0.00	Q	|	|	|	V|
23+15	0.0337	0.00	Q	|	|	|	V|
23+20	0.0337	0.00	Q	|	|	|	V|
23+25	0.0337	0.00	Q	|	|	|	V|
23+30	0.0338	0.00	Q	|	|	|	V|
23+35	0.0338	0.00	Q	|	|	|	V|
23+40	0.0338	0.00	Q	|	|	|	V|
23+45	0.0338	0.00	Q	|	|	|	V|
23+50	0.0339	0.00	Q	|	|	|	V|
23+55	0.0339	0.00	Q	|	|	|	V|
24+ 0	0.0339	0.00	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB10610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	1.20	0.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	3.00	0.39

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.941(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.941(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
			Sum = 100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.116	(0.097)	0.021	0.095
2	0.17	0.60	0.140	(0.097)	0.025	0.115
3	0.25	0.60	0.140	(0.097)	0.025	0.115
4	0.33	0.60	0.140	(0.097)	0.025	0.115
5	0.42	0.60	0.140	(0.097)	0.025	0.115
6	0.50	0.70	0.163	(0.097)	0.029	0.134
7	0.58	0.70	0.163	(0.097)	0.029	0.134
8	0.67	0.70	0.163	(0.097)	0.029	0.134
9	0.75	0.70	0.163	(0.097)	0.029	0.134
10	0.83	0.70	0.163	(0.097)	0.029	0.134
11	0.92	0.70	0.163	(0.097)	0.029	0.134
12	1.00	0.80	0.186	(0.097)	0.034	0.153
13	1.08	0.80	0.186	(0.097)	0.034	0.153
14	1.17	0.80	0.186	(0.097)	0.034	0.153
15	1.25	0.80	0.186	(0.097)	0.034	0.153
16	1.33	0.80	0.186	(0.097)	0.034	0.153
17	1.42	0.80	0.186	(0.097)	0.034	0.153
18	1.50	0.80	0.186	(0.097)	0.034	0.153
19	1.58	0.80	0.186	(0.097)	0.034	0.153
20	1.67	0.80	0.186	(0.097)	0.034	0.153
21	1.75	0.80	0.186	(0.097)	0.034	0.153
22	1.83	0.80	0.186	(0.097)	0.034	0.153
23	1.92	0.80	0.186	(0.097)	0.034	0.153
24	2.00	0.90	0.210	(0.097)	0.038	0.172
25	2.08	0.80	0.186	(0.097)	0.034	0.153
26	2.17	0.90	0.210	(0.097)	0.038	0.172
27	2.25	0.90	0.210	(0.097)	0.038	0.172
28	2.33	0.90	0.210	(0.097)	0.038	0.172
29	2.42	0.90	0.210	(0.097)	0.038	0.172
30	2.50	0.90	0.210	(0.097)	0.038	0.172
31	2.58	0.90	0.210	(0.097)	0.038	0.172
32	2.67	0.90	0.210	(0.097)	0.038	0.172
33	2.75	1.00	0.233	(0.097)	0.042	0.191
34	2.83	1.00	0.233	(0.097)	0.042	0.191
35	2.92	1.00	0.233	(0.097)	0.042	0.191
36	3.00	1.00	0.233	(0.097)	0.042	0.191
37	3.08	1.00	0.233	(0.097)	0.042	0.191
38	3.17	1.10	0.256	(0.097)	0.046	0.210
39	3.25	1.10	0.256	(0.097)	0.046	0.210
40	3.33	1.10	0.256	(0.097)	0.046	0.210
41	3.42	1.20	0.279	(0.097)	0.050	0.229
42	3.50	1.30	0.303	(0.097)	0.054	0.248
43	3.58	1.40	0.326	(0.097)	0.059	0.267

44	3.67	1.40	0.326	(	0.097)	0.059	0.267
45	3.75	1.50	0.349	(	0.097)	0.063	0.286
46	3.83	1.50	0.349	(	0.097)	0.063	0.286
47	3.92	1.60	0.373	(	0.097)	0.067	0.306
48	4.00	1.60	0.373	(	0.097)	0.067	0.306
49	4.08	1.70	0.396	(	0.097)	0.071	0.325
50	4.17	1.80	0.419	(	0.097)	0.075	0.344
51	4.25	1.90	0.442	(	0.097)	0.080	0.363
52	4.33	2.00	0.466	(	0.097)	0.084	0.382
53	4.42	2.10	0.489	(	0.097)	0.088	0.401
54	4.50	2.10	0.489	(	0.097)	0.088	0.401
55	4.58	2.20	0.512	(	0.097)	0.092	0.420
56	4.67	2.30	0.536	(	0.097)	0.096	0.439
57	4.75	2.40	0.559		0.097	(0.101)	0.462
58	4.83	2.40	0.559		0.097	(0.101)	0.462
59	4.92	2.50	0.582		0.097	(0.105)	0.485
60	5.00	2.60	0.605		0.097	(0.109)	0.508
61	5.08	3.10	0.722		0.097	(0.130)	0.625
62	5.17	3.60	0.838		0.097	(0.151)	0.741
63	5.25	3.90	0.908		0.097	(0.163)	0.811
64	5.33	4.20	0.978		0.097	(0.176)	0.881
65	5.42	4.70	1.094		0.097	(0.197)	0.997
66	5.50	5.60	1.304		0.097	(0.235)	1.207
67	5.58	1.90	0.442	(	0.097)	0.080	0.363
68	5.67	0.90	0.210	(	0.097)	0.038	0.172
69	5.75	0.60	0.140	(	0.097)	0.025	0.115
70	5.83	0.50	0.116	(	0.097)	0.021	0.095
71	5.92	0.30	0.070	(	0.097)	0.013	0.057
72	6.00	0.20	0.047	(	0.097)	0.008	0.038

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.6

Flood volume = Effective rainfall 1.63(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.31(In)
Total soil loss = 0.003(Ac.Ft)
Total rainfall = 1.94(In)
Flood volume = 770.4 Cubic Feet
Total soil loss = 145.3 Cubic Feet

Peak flow rate of this hydrograph = 0.158(CFS)

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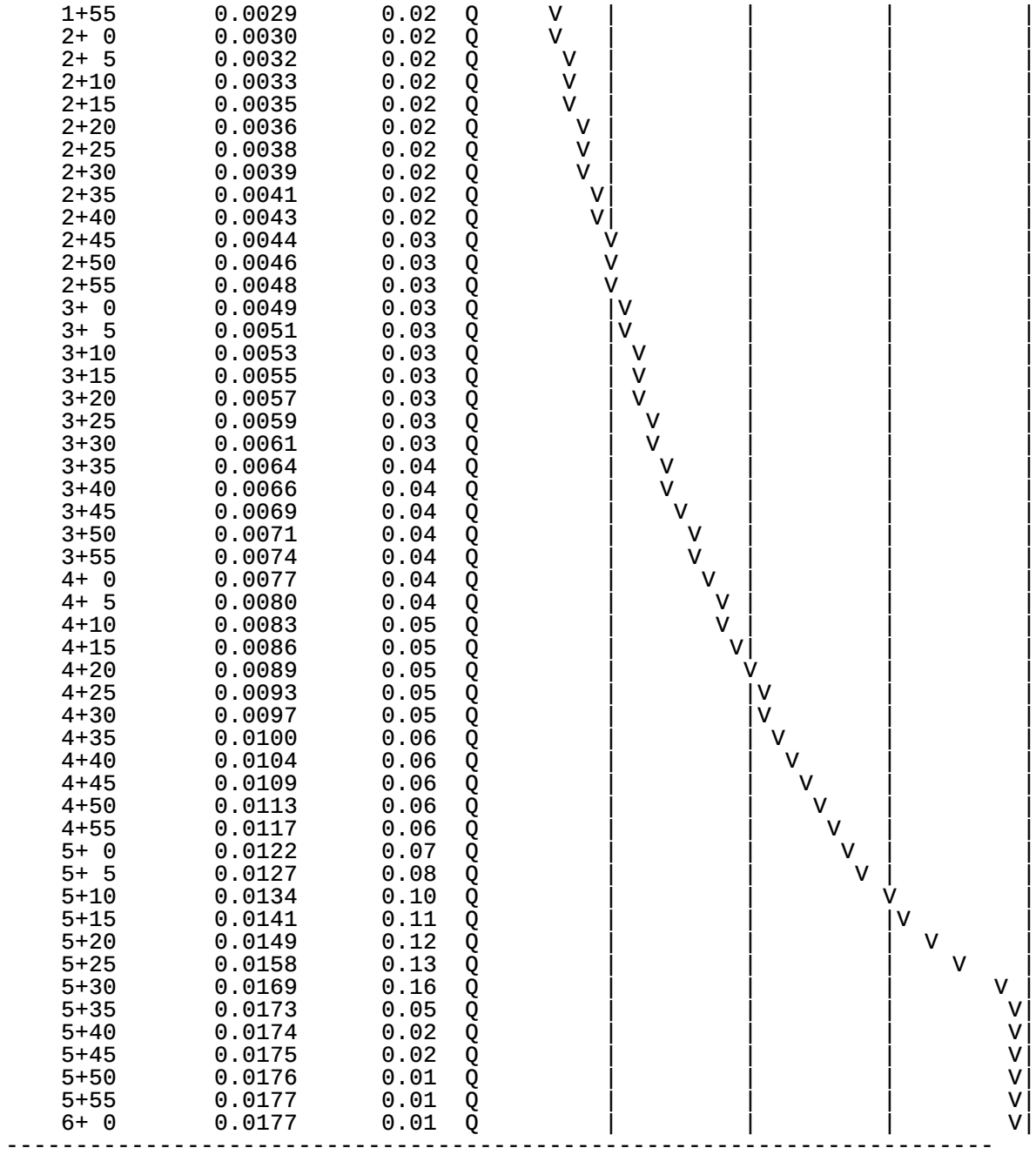
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q				
0+10	0.0002	0.02	Q				
0+15	0.0003	0.02	Q				
0+20	0.0004	0.02	Q				
0+25	0.0005	0.02	QV				
0+30	0.0006	0.02	QV				
0+35	0.0007	0.02	QV				
0+40	0.0009	0.02	QV				
0+45	0.0010	0.02	Q V				
0+50	0.0011	0.02	Q V				
0+55	0.0012	0.02	Q V				
1+ 0	0.0014	0.02	Q V				
1+ 5	0.0015	0.02	Q V				
1+10	0.0016	0.02	Q V				
1+15	0.0018	0.02	Q V				
1+20	0.0019	0.02	Q V				
1+25	0.0021	0.02	Q V				
1+30	0.0022	0.02	Q V				
1+35	0.0023	0.02	Q V				
1+40	0.0025	0.02	Q V				
1+45	0.0026	0.02	Q V				
1+50	0.0027	0.02	Q V				


1+55 0.0029 0.02 Q
2+ 0 0.0030 0.02 Q
2+ 5 0.0032 0.02 Q
2+10 0.0033 0.02 Q
2+15 0.0035 0.02 Q
2+20 0.0036 0.02 Q
2+25 0.0038 0.02 Q
2+30 0.0039 0.02 Q
2+35 0.0041 0.02 Q
2+40 0.0043 0.02 Q
2+45 0.0044 0.03 Q
2+50 0.0046 0.03 Q
2+55 0.0048 0.03 Q
3+ 0 0.0049 0.03 Q
3+ 5 0.0051 0.03 Q
3+10 0.0053 0.03 Q
3+15 0.0055 0.03 Q
3+20 0.0057 0.03 Q
3+25 0.0059 0.03 Q
3+30 0.0061 0.03 Q
3+35 0.0064 0.04 Q
3+40 0.0066 0.04 Q
3+45 0.0069 0.04 Q
3+50 0.0071 0.04 Q
3+55 0.0074 0.04 Q
4+ 0 0.0077 0.04 Q
4+ 5 0.0080 0.04 Q
4+10 0.0083 0.05 Q
4+15 0.0086 0.05 Q
4+20 0.0089 0.05 Q
4+25 0.0093 0.05 Q
4+30 0.0097 0.05 Q
4+35 0.0100 0.06 Q
4+40 0.0104 0.06 Q
4+45 0.0109 0.06 Q
4+50 0.0113 0.06 Q
4+55 0.0117 0.06 Q
5+ 0 0.0122 0.07 Q
5+ 5 0.0127 0.08 Q
5+10 0.0134 0.10 Q
5+15 0.0141 0.11 Q
5+20 0.0149 0.12 Q
5+25 0.0158 0.13 Q
5+30 0.0169 0.16 Q
5+35 0.0173 0.05 Q
5+40 0.0174 0.02 Q
5+45 0.0175 0.02 Q
5+50 0.0176 0.01 Q
5+55 0.0177 0.01 Q
6+ 0 0.0177 0.01 Q

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB10310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	0.90	0.12

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	2.35	0.31

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.497(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.497(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	2289.994	100.000	0.131
		Sum =	100.000 Sum=	0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.233	(0.097)	0.042	0.191
2	0.17	1.30	0.233	(0.097)	0.042	0.191
3	0.25	1.10	0.198	(0.097)	0.036	0.162
4	0.33	1.50	0.269	(0.097)	0.048	0.221
5	0.42	1.50	0.269	(0.097)	0.048	0.221
6	0.50	1.80	0.323	(0.097)	0.058	0.265
7	0.58	1.50	0.269	(0.097)	0.048	0.221
8	0.67	1.80	0.323	(0.097)	0.058	0.265
9	0.75	1.80	0.323	(0.097)	0.058	0.265
10	0.83	1.50	0.269	(0.097)	0.048	0.221
11	0.92	1.60	0.287	(0.097)	0.052	0.236
12	1.00	1.80	0.323	(0.097)	0.058	0.265
13	1.08	2.20	0.395	(0.097)	0.071	0.324
14	1.17	2.20	0.395	(0.097)	0.071	0.324
15	1.25	2.20	0.395	(0.097)	0.071	0.324
16	1.33	2.00	0.359	(0.097)	0.065	0.295
17	1.42	2.60	0.467	(0.097)	0.084	0.383
18	1.50	2.70	0.485	(0.097)	0.087	0.398
19	1.58	2.40	0.431	(0.097)	0.078	0.353
20	1.67	2.70	0.485	(0.097)	0.087	0.398
21	1.75	3.30	0.593	0.097	(0.107)	0.496
22	1.83	3.10	0.557	0.097	(0.100)	0.460
23	1.92	2.90	0.521	(0.097)	0.094	0.427
24	2.00	3.00	0.539	(0.097)	0.097	0.442
25	2.08	3.10	0.557	0.097	(0.100)	0.460
26	2.17	4.20	0.754	0.097	(0.136)	0.657
27	2.25	5.00	0.898	0.097	(0.162)	0.801
28	2.33	3.50	0.629	0.097	(0.113)	0.531
29	2.42	6.80	1.221	0.097	(0.220)	1.124
30	2.50	7.30	1.311	0.097	(0.236)	1.214
31	2.58	8.20	1.473	0.097	(0.265)	1.376
32	2.67	5.90	1.060	0.097	(0.191)	0.962
33	2.75	2.00	0.359	(0.097)	0.065	0.295
34	2.83	1.80	0.323	(0.097)	0.058	0.265
35	2.92	1.80	0.323	(0.097)	0.058	0.265
36	3.00	0.60	0.108	(0.097)	0.019	0.088
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	15.4

Flood volume = Effective rainfall 1.28(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.002(Ac.Ft)
Total rainfall = 1.50(In)

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      Flood volume =         605.0 Cubic Feet
      Total soil loss =         101.2 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.180(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ----------------------------------------------------------------------------
   0+ 5       0.0002      0.03  Q         |         |         |         |
   0+10       0.0003      0.03  Q         |         |         |         |
   0+15       0.0005      0.02  QV        |         |         |         |
   0+20       0.0007      0.03  QV        |         |         |         |
   0+25       0.0009      0.03  Q V       |         |         |         |
   0+30       0.0011      0.03  Q  V      |         |         |         |
   0+35       0.0013      0.03  Q  V      |         |         |         |
   0+40       0.0016      0.03  Q   V     |         |         |         |
   0+45       0.0018      0.03  Q    V    |         |         |         |
   0+50       0.0020      0.03  Q    V    |         |         |         |
   0+55       0.0022      0.03  Q     V   |         |         |         |
   1+ 0       0.0025      0.03  Q      V  |         |         |         |
   1+ 5       0.0028      0.04  Q      V  |         |         |         |
   1+10       0.0030      0.04  Q       V |         |         |         |
   1+15       0.0033      0.04  Q        V|         |         |         |
   1+20       0.0036      0.04  Q         V         |         |         |
   1+25       0.0039      0.05  Q         |V        |         |         |
   1+30       0.0043      0.05  Q         | V       |         |         |
   1+35       0.0046      0.05  Q         |  V      |         |         |
   1+40       0.0050      0.05  Q         |   V     |         |         |
   1+45       0.0054      0.06  Q         |    V    |         |         |
   1+50       0.0058      0.06  Q         |     V   |         |         |
   1+55       0.0062      0.06  Q         |      V  |         |         |
   2+ 0       0.0066      0.06  Q         |       V |         |         |
   2+ 5       0.0070      0.06  Q         |        V|         |         |
   2+10       0.0076      0.09  Q         |         | V       |         |
   2+15       0.0084      0.10  Q         |         |  V      |         |
   2+20       0.0088      0.07  Q         |         |   V     |         |
   2+25       0.0099      0.15  Q         |         |    V    |         |
   2+30       0.0110      0.16  Q         |         |     V   |         |
   2+35       0.0122      0.18  Q         |         |      V  |         |
   2+40       0.0131      0.13  Q         |         |       V |         |
   2+45       0.0133      0.04  Q         |         |        V|         |
   2+50       0.0136      0.03  Q         |         |         V|        |
   2+55       0.0138      0.03  Q         |         |         V|        |
   3+ 0       0.0139      0.01  Q         |         |          V        |
----------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PB10110.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 132
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.13(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.13(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 81.00(Ft.)
Length along longest watercourse measured to centroid = 30.00(Ft.)
Length along longest watercourse = 0.015 Mi.
Length along longest watercourse measured to centroid = 0.006 Mi.
Difference in elevation = 3.70(Ft.)
Slope along watercourse = 241.1852 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.004 Hr.
Lag time = 0.22 Min.
25% of lag time = 0.05 Min.
40% of lag time = 0.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	0.54	0.07

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.13	1.36	0.18

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.877(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.877(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.130	56.00	0.900

Total Area Entered = 0.13(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	100.000	0.131
	2289.994	Sum = 100.000	Sum= 0.131

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.463	(0.097) 0.083	0.380
2	0.17	4.50	0.474	(0.097) 0.085	0.388
3	0.25	5.40	0.569	0.097 (0.102)	0.471
4	0.33	5.40	0.569	0.097 (0.102)	0.471
5	0.42	5.70	0.600	0.097 (0.108)	0.503
6	0.50	6.40	0.674	0.097 (0.121)	0.577
7	0.58	7.90	0.832	0.097 (0.150)	0.735
8	0.67	9.10	0.958	0.097 (0.172)	0.861
9	0.75	12.80	1.348	0.097 (0.243)	1.251
10	0.83	25.60	2.695	0.097 (0.485)	2.598
11	0.92	7.90	0.832	0.097 (0.150)	0.735
12	1.00	4.90	0.516	(0.097) 0.093	0.423
	(Loss Rate Not Used)				
Sum =	100.0			Sum =	9.4

Flood volume = Effective rainfall 0.78(In)
times area 0.1(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.09(In)
Total soil loss = 0.001(Ac.Ft)
Total rainfall = 0.88(In)
Flood volume = 369.4 Cubic Feet
Total soil loss = 44.6 Cubic Feet

Peak flow rate of this hydrograph = 0.341(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0003	0.05	QV				
0+10	0.0007	0.05	Q V				
0+15	0.0011	0.06	Q V				
0+20	0.0015	0.06	Q V				
0+25	0.0020	0.07	Q V				
0+30	0.0025	0.08	Q V				
0+35	0.0032	0.10	Q V				
0+40	0.0040	0.11	Q V				

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    0+45       0.0051      0.16  Q          |          |   V     |          |
    0+50       0.0074      0.34  |Q         |          |         |    V     |
    0+55       0.0081      0.10  Q          |          |         |       V  |
    1+ 0       0.0085      0.06  Q          |          |         |          V
-------------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC02242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	2.00	0.58

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	6.40	1.86

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
			Sum = 100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(0.238)	0.003	0.013
2	0.17	0.07	0.016	(0.237)	0.003	0.013
3	0.25	0.07	0.016	(0.236)	0.003	0.013
4	0.33	0.10	0.024	(0.235)	0.004	0.020
5	0.42	0.10	0.024	(0.234)	0.004	0.020
6	0.50	0.10	0.024	(0.233)	0.004	0.020
7	0.58	0.10	0.024	(0.232)	0.004	0.020
8	0.67	0.10	0.024	(0.231)	0.004	0.020
9	0.75	0.10	0.024	(0.230)	0.004	0.020
10	0.83	0.13	0.032	(0.230)	0.006	0.026
11	0.92	0.13	0.032	(0.229)	0.006	0.026
12	1.00	0.13	0.032	(0.228)	0.006	0.026
13	1.08	0.10	0.024	(0.227)	0.004	0.020
14	1.17	0.10	0.024	(0.226)	0.004	0.020
15	1.25	0.10	0.024	(0.225)	0.004	0.020
16	1.33	0.10	0.024	(0.224)	0.004	0.020
17	1.42	0.10	0.024	(0.223)	0.004	0.020
18	1.50	0.10	0.024	(0.222)	0.004	0.020
19	1.58	0.10	0.024	(0.222)	0.004	0.020
20	1.67	0.10	0.024	(0.221)	0.004	0.020
21	1.75	0.10	0.024	(0.220)	0.004	0.020
22	1.83	0.13	0.032	(0.219)	0.006	0.026
23	1.92	0.13	0.032	(0.218)	0.006	0.026
24	2.00	0.13	0.032	(0.217)	0.006	0.026
25	2.08	0.13	0.032	(0.216)	0.006	0.026
26	2.17	0.13	0.032	(0.215)	0.006	0.026
27	2.25	0.13	0.032	(0.214)	0.006	0.026
28	2.33	0.13	0.032	(0.214)	0.006	0.026
29	2.42	0.13	0.032	(0.213)	0.006	0.026
30	2.50	0.13	0.032	(0.212)	0.006	0.026
31	2.58	0.17	0.040	(0.211)	0.007	0.033
32	2.67	0.17	0.040	(0.210)	0.007	0.033
33	2.75	0.17	0.040	(0.209)	0.007	0.033
34	2.83	0.17	0.040	(0.208)	0.007	0.033
35	2.92	0.17	0.040	(0.208)	0.007	0.033
36	3.00	0.17	0.040	(0.207)	0.007	0.033
37	3.08	0.17	0.040	(0.206)	0.007	0.033
38	3.17	0.17	0.040	(0.205)	0.007	0.033
39	3.25	0.17	0.040	(0.204)	0.007	0.033
40	3.33	0.17	0.040	(0.203)	0.007	0.033
41	3.42	0.17	0.040	(0.202)	0.007	0.033
42	3.50	0.17	0.040	(0.202)	0.007	0.033
43	3.58	0.17	0.040	(0.201)	0.007	0.033

44	3.67	0.17	0.040	(0.200)	0.007	0.033
45	3.75	0.17	0.040	(0.199)	0.007	0.033
46	3.83	0.20	0.048	(0.198)	0.009	0.039
47	3.92	0.20	0.048	(0.197)	0.009	0.039
48	4.00	0.20	0.048	(0.197)	0.009	0.039
49	4.08	0.20	0.048	(0.196)	0.009	0.039
50	4.17	0.20	0.048	(0.195)	0.009	0.039
51	4.25	0.20	0.048	(0.194)	0.009	0.039
52	4.33	0.23	0.056	(0.193)	0.010	0.046
53	4.42	0.23	0.056	(0.192)	0.010	0.046
54	4.50	0.23	0.056	(0.192)	0.010	0.046
55	4.58	0.23	0.056	(0.191)	0.010	0.046
56	4.67	0.23	0.056	(0.190)	0.010	0.046
57	4.75	0.23	0.056	(0.189)	0.010	0.046
58	4.83	0.27	0.064	(0.188)	0.012	0.052
59	4.92	0.27	0.064	(0.187)	0.012	0.052
60	5.00	0.27	0.064	(0.187)	0.012	0.052
61	5.08	0.20	0.048	(0.186)	0.009	0.039
62	5.17	0.20	0.048	(0.185)	0.009	0.039
63	5.25	0.20	0.048	(0.184)	0.009	0.039
64	5.33	0.23	0.056	(0.183)	0.010	0.046
65	5.42	0.23	0.056	(0.183)	0.010	0.046
66	5.50	0.23	0.056	(0.182)	0.010	0.046
67	5.58	0.27	0.064	(0.181)	0.012	0.052
68	5.67	0.27	0.064	(0.180)	0.012	0.052
69	5.75	0.27	0.064	(0.179)	0.012	0.052
70	5.83	0.27	0.064	(0.179)	0.012	0.052
71	5.92	0.27	0.064	(0.178)	0.012	0.052
72	6.00	0.27	0.064	(0.177)	0.012	0.052
73	6.08	0.30	0.072	(0.176)	0.013	0.059
74	6.17	0.30	0.072	(0.175)	0.013	0.059
75	6.25	0.30	0.072	(0.175)	0.013	0.059
76	6.33	0.30	0.072	(0.174)	0.013	0.059
77	6.42	0.30	0.072	(0.173)	0.013	0.059
78	6.50	0.30	0.072	(0.172)	0.013	0.059
79	6.58	0.33	0.080	(0.172)	0.014	0.066
80	6.67	0.33	0.080	(0.171)	0.014	0.066
81	6.75	0.33	0.080	(0.170)	0.014	0.066
82	6.83	0.33	0.080	(0.169)	0.014	0.066
83	6.92	0.33	0.080	(0.169)	0.014	0.066
84	7.00	0.33	0.080	(0.168)	0.014	0.066
85	7.08	0.33	0.080	(0.167)	0.014	0.066
86	7.17	0.33	0.080	(0.166)	0.014	0.066
87	7.25	0.33	0.080	(0.165)	0.014	0.066
88	7.33	0.37	0.088	(0.165)	0.016	0.072
89	7.42	0.37	0.088	(0.164)	0.016	0.072
90	7.50	0.37	0.088	(0.163)	0.016	0.072
91	7.58	0.40	0.096	(0.162)	0.017	0.079
92	7.67	0.40	0.096	(0.162)	0.017	0.079
93	7.75	0.40	0.096	(0.161)	0.017	0.079
94	7.83	0.43	0.104	(0.160)	0.019	0.085
95	7.92	0.43	0.104	(0.159)	0.019	0.085
96	8.00	0.43	0.104	(0.159)	0.019	0.085
97	8.08	0.50	0.120	(0.158)	0.022	0.098
98	8.17	0.50	0.120	(0.157)	0.022	0.098
99	8.25	0.50	0.120	(0.157)	0.022	0.098
100	8.33	0.50	0.120	(0.156)	0.022	0.098
101	8.42	0.50	0.120	(0.155)	0.022	0.098
102	8.50	0.50	0.120	(0.154)	0.022	0.098
103	8.58	0.53	0.128	(0.154)	0.023	0.105
104	8.67	0.53	0.128	(0.153)	0.023	0.105
105	8.75	0.53	0.128	(0.152)	0.023	0.105
106	8.83	0.57	0.136	(0.151)	0.024	0.112
107	8.92	0.57	0.136	(0.151)	0.024	0.112
108	9.00	0.57	0.136	(0.150)	0.024	0.112
109	9.08	0.63	0.152	(0.149)	0.027	0.125
110	9.17	0.63	0.152	(0.149)	0.027	0.125
111	9.25	0.63	0.152	(0.148)	0.027	0.125
112	9.33	0.67	0.160	(0.147)	0.029	0.131
113	9.42	0.67	0.160	(0.147)	0.029	0.131
114	9.50	0.67	0.160	(0.146)	0.029	0.131
115	9.58	0.70	0.168	(0.145)	0.030	0.138

116	9.67	0.70	0.168	(0.144)	0.030	0.138
117	9.75	0.70	0.168	(0.144)	0.030	0.138
118	9.83	0.73	0.176	(0.143)	0.032	0.144
119	9.92	0.73	0.176	(0.142)	0.032	0.144
120	10.00	0.73	0.176	(0.142)	0.032	0.144
121	10.08	0.50	0.120	(0.141)	0.022	0.098
122	10.17	0.50	0.120	(0.140)	0.022	0.098
123	10.25	0.50	0.120	(0.140)	0.022	0.098
124	10.33	0.50	0.120	(0.139)	0.022	0.098
125	10.42	0.50	0.120	(0.138)	0.022	0.098
126	10.50	0.50	0.120	(0.138)	0.022	0.098
127	10.58	0.67	0.160	(0.137)	0.029	0.131
128	10.67	0.67	0.160	(0.136)	0.029	0.131
129	10.75	0.67	0.160	(0.136)	0.029	0.131
130	10.83	0.67	0.160	(0.135)	0.029	0.131
131	10.92	0.67	0.160	(0.134)	0.029	0.131
132	11.00	0.67	0.160	(0.134)	0.029	0.131
133	11.08	0.63	0.152	(0.133)	0.027	0.125
134	11.17	0.63	0.152	(0.132)	0.027	0.125
135	11.25	0.63	0.152	(0.132)	0.027	0.125
136	11.33	0.63	0.152	(0.131)	0.027	0.125
137	11.42	0.63	0.152	(0.130)	0.027	0.125
138	11.50	0.63	0.152	(0.130)	0.027	0.125
139	11.58	0.57	0.136	(0.129)	0.024	0.112
140	11.67	0.57	0.136	(0.128)	0.024	0.112
141	11.75	0.57	0.136	(0.128)	0.024	0.112
142	11.83	0.60	0.144	(0.127)	0.026	0.118
143	11.92	0.60	0.144	(0.126)	0.026	0.118
144	12.00	0.60	0.144	(0.126)	0.026	0.118
145	12.08	0.83	0.200	(0.125)	0.036	0.164
146	12.17	0.83	0.200	(0.125)	0.036	0.164
147	12.25	0.83	0.200	(0.124)	0.036	0.164
148	12.33	0.87	0.208	(0.123)	0.037	0.171
149	12.42	0.87	0.208	(0.123)	0.037	0.171
150	12.50	0.87	0.208	(0.122)	0.037	0.171
151	12.58	0.93	0.224	(0.121)	0.040	0.184
152	12.67	0.93	0.224	(0.121)	0.040	0.184
153	12.75	0.93	0.224	(0.120)	0.040	0.184
154	12.83	0.97	0.232	(0.120)	0.042	0.190
155	12.92	0.97	0.232	(0.119)	0.042	0.190
156	13.00	0.97	0.232	(0.118)	0.042	0.190
157	13.08	1.13	0.272	(0.118)	0.049	0.223
158	13.17	1.13	0.272	(0.117)	0.049	0.223
159	13.25	1.13	0.272	(0.117)	0.049	0.223
160	13.33	1.13	0.272	(0.116)	0.049	0.223
161	13.42	1.13	0.272	(0.115)	0.049	0.223
162	13.50	1.13	0.272	(0.115)	0.049	0.223
163	13.58	0.77	0.184	(0.114)	0.033	0.151
164	13.67	0.77	0.184	(0.114)	0.033	0.151
165	13.75	0.77	0.184	(0.113)	0.033	0.151
166	13.83	0.77	0.184	(0.113)	0.033	0.151
167	13.92	0.77	0.184	(0.112)	0.033	0.151
168	14.00	0.77	0.184	(0.111)	0.033	0.151
169	14.08	0.90	0.216	(0.111)	0.039	0.177
170	14.17	0.90	0.216	(0.110)	0.039	0.177
171	14.25	0.90	0.216	(0.110)	0.039	0.177
172	14.33	0.87	0.208	(0.109)	0.037	0.171
173	14.42	0.87	0.208	(0.109)	0.037	0.171
174	14.50	0.87	0.208	(0.108)	0.037	0.171
175	14.58	0.87	0.208	(0.107)	0.037	0.171
176	14.67	0.87	0.208	(0.107)	0.037	0.171
177	14.75	0.87	0.208	(0.106)	0.037	0.171
178	14.83	0.83	0.200	(0.106)	0.036	0.164
179	14.92	0.83	0.200	(0.105)	0.036	0.164
180	15.00	0.83	0.200	(0.105)	0.036	0.164
181	15.08	0.80	0.192	(0.104)	0.035	0.157
182	15.17	0.80	0.192	(0.104)	0.035	0.157
183	15.25	0.80	0.192	(0.103)	0.035	0.157
184	15.33	0.77	0.184	(0.103)	0.033	0.151
185	15.42	0.77	0.184	(0.102)	0.033	0.151
186	15.50	0.77	0.184	(0.102)	0.033	0.151
187	15.58	0.63	0.152	(0.101)	0.027	0.125

188	15.67	0.63	0.152	(0.101)	0.027	0.125
189	15.75	0.63	0.152	(0.100)	0.027	0.125
190	15.83	0.63	0.152	(0.100)	0.027	0.125
191	15.92	0.63	0.152	(0.099)	0.027	0.125
192	16.00	0.63	0.152	(0.099)	0.027	0.125
193	16.08	0.13	0.032	(0.098)	0.006	0.026
194	16.17	0.13	0.032	(0.098)	0.006	0.026
195	16.25	0.13	0.032	(0.097)	0.006	0.026
196	16.33	0.13	0.032	(0.097)	0.006	0.026
197	16.42	0.13	0.032	(0.096)	0.006	0.026
198	16.50	0.13	0.032	(0.096)	0.006	0.026
199	16.58	0.10	0.024	(0.095)	0.004	0.020
200	16.67	0.10	0.024	(0.095)	0.004	0.020
201	16.75	0.10	0.024	(0.094)	0.004	0.020
202	16.83	0.10	0.024	(0.094)	0.004	0.020
203	16.92	0.10	0.024	(0.093)	0.004	0.020
204	17.00	0.10	0.024	(0.093)	0.004	0.020
205	17.08	0.17	0.040	(0.092)	0.007	0.033
206	17.17	0.17	0.040	(0.092)	0.007	0.033
207	17.25	0.17	0.040	(0.091)	0.007	0.033
208	17.33	0.17	0.040	(0.091)	0.007	0.033
209	17.42	0.17	0.040	(0.090)	0.007	0.033
210	17.50	0.17	0.040	(0.090)	0.007	0.033
211	17.58	0.17	0.040	(0.089)	0.007	0.033
212	17.67	0.17	0.040	(0.089)	0.007	0.033
213	17.75	0.17	0.040	(0.089)	0.007	0.033
214	17.83	0.13	0.032	(0.088)	0.006	0.026
215	17.92	0.13	0.032	(0.088)	0.006	0.026
216	18.00	0.13	0.032	(0.087)	0.006	0.026
217	18.08	0.13	0.032	(0.087)	0.006	0.026
218	18.17	0.13	0.032	(0.086)	0.006	0.026
219	18.25	0.13	0.032	(0.086)	0.006	0.026
220	18.33	0.13	0.032	(0.086)	0.006	0.026
221	18.42	0.13	0.032	(0.085)	0.006	0.026
222	18.50	0.13	0.032	(0.085)	0.006	0.026
223	18.58	0.10	0.024	(0.084)	0.004	0.020
224	18.67	0.10	0.024	(0.084)	0.004	0.020
225	18.75	0.10	0.024	(0.084)	0.004	0.020
226	18.83	0.07	0.016	(0.083)	0.003	0.013
227	18.92	0.07	0.016	(0.083)	0.003	0.013
228	19.00	0.07	0.016	(0.082)	0.003	0.013
229	19.08	0.10	0.024	(0.082)	0.004	0.020
230	19.17	0.10	0.024	(0.082)	0.004	0.020
231	19.25	0.10	0.024	(0.081)	0.004	0.020
232	19.33	0.13	0.032	(0.081)	0.006	0.026
233	19.42	0.13	0.032	(0.080)	0.006	0.026
234	19.50	0.13	0.032	(0.080)	0.006	0.026
235	19.58	0.10	0.024	(0.080)	0.004	0.020
236	19.67	0.10	0.024	(0.079)	0.004	0.020
237	19.75	0.10	0.024	(0.079)	0.004	0.020
238	19.83	0.07	0.016	(0.079)	0.003	0.013
239	19.92	0.07	0.016	(0.078)	0.003	0.013
240	20.00	0.07	0.016	(0.078)	0.003	0.013
241	20.08	0.10	0.024	(0.078)	0.004	0.020
242	20.17	0.10	0.024	(0.077)	0.004	0.020
243	20.25	0.10	0.024	(0.077)	0.004	0.020
244	20.33	0.10	0.024	(0.077)	0.004	0.020
245	20.42	0.10	0.024	(0.076)	0.004	0.020
246	20.50	0.10	0.024	(0.076)	0.004	0.020
247	20.58	0.10	0.024	(0.076)	0.004	0.020
248	20.67	0.10	0.024	(0.075)	0.004	0.020
249	20.75	0.10	0.024	(0.075)	0.004	0.020
250	20.83	0.07	0.016	(0.075)	0.003	0.013
251	20.92	0.07	0.016	(0.074)	0.003	0.013
252	21.00	0.07	0.016	(0.074)	0.003	0.013
253	21.08	0.10	0.024	(0.074)	0.004	0.020
254	21.17	0.10	0.024	(0.073)	0.004	0.020
255	21.25	0.10	0.024	(0.073)	0.004	0.020
256	21.33	0.07	0.016	(0.073)	0.003	0.013
257	21.42	0.07	0.016	(0.073)	0.003	0.013
258	21.50	0.07	0.016	(0.072)	0.003	0.013
259	21.58	0.10	0.024	(0.072)	0.004	0.020

260	21.67	0.10	0.024	(0.072)	0.004	0.020
261	21.75	0.10	0.024	(0.072)	0.004	0.020
262	21.83	0.07	0.016	(0.071)	0.003	0.013
263	21.92	0.07	0.016	(0.071)	0.003	0.013
264	22.00	0.07	0.016	(0.071)	0.003	0.013
265	22.08	0.10	0.024	(0.071)	0.004	0.020
266	22.17	0.10	0.024	(0.070)	0.004	0.020
267	22.25	0.10	0.024	(0.070)	0.004	0.020
268	22.33	0.07	0.016	(0.070)	0.003	0.013
269	22.42	0.07	0.016	(0.070)	0.003	0.013
270	22.50	0.07	0.016	(0.069)	0.003	0.013
271	22.58	0.07	0.016	(0.069)	0.003	0.013
272	22.67	0.07	0.016	(0.069)	0.003	0.013
273	22.75	0.07	0.016	(0.069)	0.003	0.013
274	22.83	0.07	0.016	(0.069)	0.003	0.013
275	22.92	0.07	0.016	(0.069)	0.003	0.013
276	23.00	0.07	0.016	(0.068)	0.003	0.013
277	23.08	0.07	0.016	(0.068)	0.003	0.013
278	23.17	0.07	0.016	(0.068)	0.003	0.013
279	23.25	0.07	0.016	(0.068)	0.003	0.013
280	23.33	0.07	0.016	(0.068)	0.003	0.013
281	23.42	0.07	0.016	(0.068)	0.003	0.013
282	23.50	0.07	0.016	(0.068)	0.003	0.013
283	23.58	0.07	0.016	(0.067)	0.003	0.013
284	23.67	0.07	0.016	(0.067)	0.003	0.013
285	23.75	0.07	0.016	(0.067)	0.003	0.013
286	23.83	0.07	0.016	(0.067)	0.003	0.013
287	23.92	0.07	0.016	(0.067)	0.003	0.013
288	24.00	0.07	0.016	(0.067)	0.003	0.013

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.7

Flood volume = Effective rainfall 1.64(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.36(In)
Total soil loss = 0.009(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 1726.4 Cubic Feet
Total soil loss = 379.0 Cubic Feet

Peak flow rate of this hydrograph = 0.065(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q	|	|	|	|
0+10	0.0001	0.00	Q	|	|	|	|
0+15	0.0001	0.00	Q	|	|	|	|
0+20	0.0001	0.01	Q	|	|	|	|
0+25	0.0002	0.01	Q	|	|	|	|
0+30	0.0002	0.01	Q	|	|	|	|
0+35	0.0002	0.01	Q	|	|	|	|
0+40	0.0003	0.01	Q	|	|	|	|
0+45	0.0003	0.01	Q	|	|	|	|
0+50	0.0004	0.01	Q	|	|	|	|
0+55	0.0004	0.01	Q	|	|	|	|
1+ 0	0.0005	0.01	Q	|	|	|	|
1+ 5	0.0005	0.01	Q	|	|	|	|
1+10	0.0006	0.01	Q	|	|	|	|
1+15	0.0006	0.01	Q	|	|	|	|
1+20	0.0006	0.01	Q	|	|	|	|
1+25	0.0007	0.01	Q	|	|	|	|
1+30	0.0007	0.01	Q	|	|	|	|
1+35	0.0008	0.01	Q	|	|	|	|
1+40	0.0008	0.01	Q	|	|	|	|
1+45	0.0008	0.01	Q	|	|	|	|
1+50	0.0009	0.01	Q	|	|	|	|

1+55	0.0009	0.01	Q	|	|	|	|
2+ 0	0.0010	0.01	Q	|	|	|	|
2+ 5	0.0010	0.01	QV	|	|	|	|
2+10	0.0011	0.01	QV	|	|	|	|
2+15	0.0011	0.01	QV	|	|	|	|
2+20	0.0012	0.01	QV	|	|	|	|
2+25	0.0013	0.01	QV	|	|	|	|
2+30	0.0013	0.01	QV	|	|	|	|
2+35	0.0014	0.01	QV	|	|	|	|
2+40	0.0014	0.01	QV	|	|	|	|
2+45	0.0015	0.01	QV	|	|	|	|
2+50	0.0016	0.01	QV	|	|	|	|
2+55	0.0016	0.01	QV	|	|	|	|
3+ 0	0.0017	0.01	QV	|	|	|	|
3+ 5	0.0018	0.01	QV	|	|	|	|
3+10	0.0018	0.01	QV	|	|	|	|
3+15	0.0019	0.01	QV	|	|	|	|
3+20	0.0020	0.01	QV	|	|	|	|
3+25	0.0020	0.01	Q V	|	|	|	|
3+30	0.0021	0.01	Q V	|	|	|	|
3+35	0.0022	0.01	Q V	|	|	|	|
3+40	0.0022	0.01	Q V	|	|	|	|
3+45	0.0023	0.01	Q V	|	|	|	|
3+50	0.0024	0.01	Q V	|	|	|	|
3+55	0.0025	0.01	Q V	|	|	|	|
4+ 0	0.0025	0.01	Q V	|	|	|	|
4+ 5	0.0026	0.01	Q V	|	|	|	|
4+10	0.0027	0.01	Q V	|	|	|	|
4+15	0.0028	0.01	Q V	|	|	|	|
4+20	0.0029	0.01	Q V	|	|	|	|
4+25	0.0030	0.01	Q V	|	|	|	|
4+30	0.0031	0.01	Q V	|	|	|	|
4+35	0.0031	0.01	Q V	|	|	|	|
4+40	0.0032	0.01	Q V	|	|	|	|
4+45	0.0033	0.01	Q V	|	|	|	|
4+50	0.0034	0.02	Q V	|	|	|	|
4+55	0.0035	0.02	Q V	|	|	|	|
5+ 0	0.0036	0.02	Q V	|	|	|	|
5+ 5	0.0037	0.01	Q V	|	|	|	|
5+10	0.0038	0.01	Q V	|	|	|	|
5+15	0.0039	0.01	Q V	|	|	|	|
5+20	0.0040	0.01	Q V	|	|	|	|
5+25	0.0041	0.01	Q V	|	|	|	|
5+30	0.0042	0.01	Q V	|	|	|	|
5+35	0.0043	0.02	Q V	|	|	|	|
5+40	0.0044	0.02	Q V	|	|	|	|
5+45	0.0045	0.02	Q V	|	|	|	|
5+50	0.0046	0.02	Q V	|	|	|	|
5+55	0.0047	0.02	Q V	|	|	|	|
6+ 0	0.0048	0.02	Q V	|	|	|	|
6+ 5	0.0049	0.02	Q V	|	|	|	|
6+10	0.0050	0.02	Q V	|	|	|	|
6+15	0.0052	0.02	Q V	|	|	|	|
6+20	0.0053	0.02	Q V	|	|	|	|
6+25	0.0054	0.02	Q V	|	|	|	|
6+30	0.0055	0.02	Q V	|	|	|	|
6+35	0.0056	0.02	Q V	|	|	|	|
6+40	0.0058	0.02	Q V	|	|	|	|
6+45	0.0059	0.02	Q V	|	|	|	|
6+50	0.0060	0.02	Q V	|	|	|	|
6+55	0.0062	0.02	Q V	|	|	|	|
7+ 0	0.0063	0.02	Q V	|	|	|	|
7+ 5	0.0064	0.02	Q V	|	|	|	|
7+10	0.0066	0.02	Q V	|	|	|	|
7+15	0.0067	0.02	Q V	|	|	|	|
7+20	0.0068	0.02	Q V	|	|	|	|
7+25	0.0070	0.02	Q V	|	|	|	|
7+30	0.0071	0.02	Q V	|	|	|	|
7+35	0.0073	0.02	Q V	|	|	|	|
7+40	0.0075	0.02	Q V	|	|	|	|
7+45	0.0076	0.02	Q V	|	|	|	|
7+50	0.0078	0.02	Q V	|	|	|	|

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 7+55       0.0080      0.02  Q       V |          |          |          |
 8+ 0       0.0081      0.02  Q       V |          |          |          |
 8+ 5       0.0083      0.03  Q       V |          |          |          |
 8+10       0.0085      0.03  Q       V |          |          |          |
 8+15       0.0087      0.03  Q       V |          |          |          |
 8+20       0.0089      0.03  Q       V |          |          |          |
 8+25       0.0091      0.03  Q        V|          |          |          |
 8+30       0.0093      0.03  Q        V|          |          |          |
 8+35       0.0095      0.03  Q        V|          |          |          |
 8+40       0.0097      0.03  Q        V|          |          |          |
 8+45       0.0099      0.03  Q         V          |          |          |
 8+50       0.0102      0.03  Q         V          |          |          |
 8+55       0.0104      0.03  Q         V          |          |          |
 9+ 0       0.0106      0.03  Q         V          |          |          |
 9+ 5       0.0109      0.04  Q         V          |          |          |
 9+10       0.0111      0.04  Q          |V         |          |          |
 9+15       0.0114      0.04  Q          |V         |          |          |
 9+20       0.0116      0.04  Q          |V         |          |          |
 9+25       0.0119      0.04  Q          | V        |          |          |
 9+30       0.0122      0.04  Q          | V        |          |          |
 9+35       0.0124      0.04  Q          | V        |          |          |
 9+40       0.0127      0.04  Q          | V        |          |          |
 9+45       0.0130      0.04  Q          |  V       |          |          |
 9+50       0.0133      0.04  Q          |  V       |          |          |
 9+55       0.0136      0.04  Q          |  V       |          |          |
10+ 0       0.0139      0.04  Q          |  V       |          |          |
10+ 5       0.0141      0.03  Q          |   V      |          |          |
10+10       0.0143      0.03  Q          |   V      |          |          |
10+15       0.0145      0.03  Q          |   V      |          |          |
10+20       0.0147      0.03  Q          |   V      |          |          |
10+25       0.0149      0.03  Q          |   V      |          |          |
10+30       0.0151      0.03  Q          |    V     |          |          |
10+35       0.0153      0.04  Q          |    V     |          |          |
10+40       0.0156      0.04  Q          |    V     |          |          |
10+45       0.0159      0.04  Q          |    V     |          |          |
10+50       0.0161      0.04  Q          |     V    |          |          |
10+55       0.0164      0.04  Q          |     V    |          |          |
11+ 0       0.0166      0.04  Q          |     V    |          |          |
11+ 5       0.0169      0.04  Q          |      V   |          |          |
11+10       0.0171      0.04  Q          |      V   |          |          |
11+15       0.0174      0.04  Q          |      V   |          |          |
11+20       0.0177      0.04  Q          |      V   |          |          |
11+25       0.0179      0.04  Q          |       V  |          |          |
11+30       0.0182      0.04  Q          |       V  |          |          |
11+35       0.0184      0.03  Q          |       V  |          |          |
11+40       0.0186      0.03  Q          |       V  |          |          |
11+45       0.0188      0.03  Q          |       V  |          |          |
11+50       0.0191      0.03  Q          |        V |          |          |
11+55       0.0193      0.03  Q          |        V |          |          |
12+ 0       0.0195      0.03  Q          |        V |          |          |
12+ 5       0.0199      0.05  Q          |         V          |          |
12+10       0.0202      0.05  Q          |         V          |          |
12+15       0.0205      0.05  Q          |         V          |          |
12+20       0.0209      0.05  Q          |          |V        |          |
12+25       0.0212      0.05  Q          |          |V        |          |
12+30       0.0216      0.05  Q          |          |V        |          |
12+35       0.0219      0.05  Q          |          | V       |          |
12+40       0.0223      0.05  Q          |          | V       |          |
12+45       0.0227      0.05  Q          |          | V       |          |
12+50       0.0231      0.06  Q          |          |  V      |          |
12+55       0.0234      0.06  Q          |          |  V      |          |
13+ 0       0.0238      0.06  Q          |          |   V     |          |
13+ 5       0.0243      0.07  Q          |          |   V     |          |
13+10       0.0247      0.07  Q          |          |   V     |          |
13+15       0.0252      0.07  Q          |          |    V    |          |
13+20       0.0256      0.07  Q          |          |    V    |          |
13+25       0.0261      0.07  Q          |          |     V   |          |
13+30       0.0265      0.07  Q          |          |     V   |          |
13+35       0.0268      0.04  Q          |          |      V  |          |
13+40       0.0271      0.04  Q          |          |      V  |          |
13+45       0.0274      0.04  Q          |          |      V  |          |
13+50       0.0277      0.04  Q          |          |      V  |          |
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13+55       0.0280      0.04  Q          |           |         V |           |
14+ 0       0.0283      0.04  Q          |           |         V |           |
14+ 5       0.0287      0.05  Q          |           |         V |           |
14+10       0.0291      0.05  Q          |           |          V|           |
14+15       0.0294      0.05  Q          |           |          V|           |
14+20       0.0298      0.05  Q          |           |           V           |
14+25       0.0301      0.05  Q          |           |           V           |
14+30       0.0304      0.05  Q          |           |           V           |
14+35       0.0308      0.05  Q          |           |           |V          |
14+40       0.0311      0.05  Q          |           |           |V          |
14+45       0.0315      0.05  Q          |           |           |V          |
14+50       0.0318      0.05  Q          |           |           | V         |
14+55       0.0321      0.05  Q          |           |           | V         |
15+ 0       0.0325      0.05  Q          |           |           | V         |
15+ 5       0.0328      0.05  Q          |           |           |  V        |
15+10       0.0331      0.05  Q          |           |           |  V        |
15+15       0.0334      0.05  Q          |           |           |  V        |
15+20       0.0337      0.04  Q          |           |           |   V       |
15+25       0.0340      0.04  Q          |           |           |   V       |
15+30       0.0343      0.04  Q          |           |           |   V       |
15+35       0.0346      0.04  Q          |           |           |   V       |
15+40       0.0348      0.04  Q          |           |           |    V      |
15+45       0.0351      0.04  Q          |           |           |    V      |
15+50       0.0353      0.04  Q          |           |           |    V      |
15+55       0.0356      0.04  Q          |           |           |    V      |
16+ 0       0.0358      0.04  Q          |           |           |     V     |
16+ 5       0.0359      0.01  Q          |           |           |     V     |
16+10       0.0359      0.01  Q          |           |           |     V     |
16+15       0.0360      0.01  Q          |           |           |     V     |
16+20       0.0360      0.01  Q          |           |           |     V     |
16+25       0.0361      0.01  Q          |           |           |     V     |
16+30       0.0361      0.01  Q          |           |           |     V     |
16+35       0.0362      0.01  Q          |           |           |     V     |
16+40       0.0362      0.01  Q          |           |           |     V     |
16+45       0.0363      0.01  Q          |           |           |     V     |
16+50       0.0363      0.01  Q          |           |           |     V     |
16+55       0.0363      0.01  Q          |           |           |     V     |
17+ 0       0.0364      0.01  Q          |           |           |     V     |
17+ 5       0.0364      0.01  Q          |           |           |     V     |
17+10       0.0365      0.01  Q          |           |           |     V     |
17+15       0.0366      0.01  Q          |           |           |     V     |
17+20       0.0366      0.01  Q          |           |           |     V     |
17+25       0.0367      0.01  Q          |           |           |      V    |
17+30       0.0368      0.01  Q          |           |           |      V    |
17+35       0.0368      0.01  Q          |           |           |      V    |
17+40       0.0369      0.01  Q          |           |           |      V    |
17+45       0.0370      0.01  Q          |           |           |      V    |
17+50       0.0370      0.01  Q          |           |           |      V    |
17+55       0.0371      0.01  Q          |           |           |      V    |
18+ 0       0.0371      0.01  Q          |           |           |      V    |
18+ 5       0.0372      0.01  Q          |           |           |      V    |
18+10       0.0372      0.01  Q          |           |           |      V    |
18+15       0.0373      0.01  Q          |           |           |      V    |
18+20       0.0373      0.01  Q          |           |           |      V    |
18+25       0.0374      0.01  Q          |           |           |      V    |
18+30       0.0375      0.01  Q          |           |           |      V    |
18+35       0.0375      0.01  Q          |           |           |      V    |
18+40       0.0375      0.01  Q          |           |           |      V    |
18+45       0.0376      0.01  Q          |           |           |      V    |
18+50       0.0376      0.00  Q          |           |           |      V    |
18+55       0.0376      0.00  Q          |           |           |      V    |
19+ 0       0.0377      0.00  Q          |           |           |      V    |
19+ 5       0.0377      0.01  Q          |           |           |       V   |
19+10       0.0377      0.01  Q          |           |           |       V   |
19+15       0.0378      0.01  Q          |           |           |       V   |
19+20       0.0378      0.01  Q          |           |           |       V   |
19+25       0.0379      0.01  Q          |           |           |       V   |
19+30       0.0379      0.01  Q          |           |           |       V   |
19+35       0.0380      0.01  Q          |           |           |       V   |
19+40       0.0380      0.01  Q          |           |           |       V   |
19+45       0.0380      0.01  Q          |           |           |       V   |
19+50       0.0381      0.00  Q          |           |           |       V   |
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  19+55       0.0381      0.00  Q          |          |          |        V |
  20+ 0       0.0381      0.00  Q          |          |          |        V |
  20+ 5       0.0382      0.01  Q          |          |          |        V |
  20+10       0.0382      0.01  Q          |          |          |        V |
  20+15       0.0382      0.01  Q          |          |          |        V |
  20+20       0.0383      0.01  Q          |          |          |        V |
  20+25       0.0383      0.01  Q          |          |          |        V |
  20+30       0.0384      0.01  Q          |          |          |        V |
  20+35       0.0384      0.01  Q          |          |          |        V |
  20+40       0.0384      0.01  Q          |          |          |        V |
  20+45       0.0385      0.01  Q          |          |          |        V |
  20+50       0.0385      0.00  Q          |          |          |        V |
  20+55       0.0385      0.00  Q          |          |          |        V |
  21+ 0       0.0386      0.00  Q          |          |          |        V |
  21+ 5       0.0386      0.01  Q          |          |          |        V |
  21+10       0.0386      0.01  Q          |          |          |        V |
  21+15       0.0387      0.01  Q          |          |          |         V|
  21+20       0.0387      0.00  Q          |          |          |         V|
  21+25       0.0387      0.00  Q          |          |          |         V|
  21+30       0.0388      0.00  Q          |          |          |         V|
  21+35       0.0388      0.01  Q          |          |          |         V|
  21+40       0.0388      0.01  Q          |          |          |         V|
  21+45       0.0389      0.01  Q          |          |          |         V|
  21+50       0.0389      0.00  Q          |          |          |         V|
  21+55       0.0389      0.00  Q          |          |          |         V|
  22+ 0       0.0390      0.00  Q          |          |          |         V|
  22+ 5       0.0390      0.01  Q          |          |          |         V|
  22+10       0.0390      0.01  Q          |          |          |         V|
  22+15       0.0391      0.01  Q          |          |          |         V|
  22+20       0.0391      0.00  Q          |          |          |         V|
  22+25       0.0391      0.00  Q          |          |          |         V|
  22+30       0.0392      0.00  Q          |          |          |         V|
  22+35       0.0392      0.00  Q          |          |          |         V|
  22+40       0.0392      0.00  Q          |          |          |         V|
  22+45       0.0392      0.00  Q          |          |          |         V|
  22+50       0.0393      0.00  Q          |          |          |         V|
  22+55       0.0393      0.00  Q          |          |          |         V|
  23+ 0       0.0393      0.00  Q          |          |          |         V|
  23+ 5       0.0393      0.00  Q          |          |          |         V|
  23+10       0.0394      0.00  Q          |          |          |         V|
  23+15       0.0394      0.00  Q          |          |          |         V|
  23+20       0.0394      0.00  Q          |          |          |         V|
  23+25       0.0394      0.00  Q          |          |          |         V|
  23+30       0.0395      0.00  Q          |          |          |         V|
  23+35       0.0395      0.00  Q          |          |          |         V|
  23+40       0.0395      0.00  Q          |          |          |         V|
  23+45       0.0396      0.00  Q          |          |          |         V|
  23+50       0.0396      0.00  Q          |          |          |         V|
  23+55       0.0396      0.00  Q          |          |          |         V|
  24+ 0       0.0396      0.00  Q          |          |          |         V|
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC0262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	1.20	0.35

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	3.00	0.87

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.200(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
			Sum = 100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.072	(0.134)	0.013	0.059
2	0.17	0.60	0.086	(0.134)	0.016	0.071
3	0.25	0.60	0.086	(0.134)	0.016	0.071
4	0.33	0.60	0.086	(0.134)	0.016	0.071
5	0.42	0.60	0.086	(0.134)	0.016	0.071
6	0.50	0.70	0.101	(0.134)	0.018	0.083
7	0.58	0.70	0.101	(0.134)	0.018	0.083
8	0.67	0.70	0.101	(0.134)	0.018	0.083
9	0.75	0.70	0.101	(0.134)	0.018	0.083
10	0.83	0.70	0.101	(0.134)	0.018	0.083
11	0.92	0.70	0.101	(0.134)	0.018	0.083
12	1.00	0.80	0.115	(0.134)	0.021	0.094
13	1.08	0.80	0.115	(0.134)	0.021	0.094
14	1.17	0.80	0.115	(0.134)	0.021	0.094
15	1.25	0.80	0.115	(0.134)	0.021	0.094
16	1.33	0.80	0.115	(0.134)	0.021	0.094
17	1.42	0.80	0.115	(0.134)	0.021	0.094
18	1.50	0.80	0.115	(0.134)	0.021	0.094
19	1.58	0.80	0.115	(0.134)	0.021	0.094
20	1.67	0.80	0.115	(0.134)	0.021	0.094
21	1.75	0.80	0.115	(0.134)	0.021	0.094
22	1.83	0.80	0.115	(0.134)	0.021	0.094
23	1.92	0.80	0.115	(0.134)	0.021	0.094
24	2.00	0.90	0.130	(0.134)	0.023	0.106
25	2.08	0.80	0.115	(0.134)	0.021	0.094
26	2.17	0.90	0.130	(0.134)	0.023	0.106
27	2.25	0.90	0.130	(0.134)	0.023	0.106
28	2.33	0.90	0.130	(0.134)	0.023	0.106
29	2.42	0.90	0.130	(0.134)	0.023	0.106
30	2.50	0.90	0.130	(0.134)	0.023	0.106
31	2.58	0.90	0.130	(0.134)	0.023	0.106
32	2.67	0.90	0.130	(0.134)	0.023	0.106
33	2.75	1.00	0.144	(0.134)	0.026	0.118
34	2.83	1.00	0.144	(0.134)	0.026	0.118
35	2.92	1.00	0.144	(0.134)	0.026	0.118
36	3.00	1.00	0.144	(0.134)	0.026	0.118
37	3.08	1.00	0.144	(0.134)	0.026	0.118
38	3.17	1.10	0.158	(0.134)	0.029	0.130
39	3.25	1.10	0.158	(0.134)	0.029	0.130
40	3.33	1.10	0.158	(0.134)	0.029	0.130
41	3.42	1.20	0.173	(0.134)	0.031	0.142
42	3.50	1.30	0.187	(0.134)	0.034	0.154
43	3.58	1.40	0.202	(0.134)	0.036	0.165

44	3.67	1.40	0.202	(	0.134)	0.036	0.165
45	3.75	1.50	0.216	(	0.134)	0.039	0.177
46	3.83	1.50	0.216	(	0.134)	0.039	0.177
47	3.92	1.60	0.230	(	0.134)	0.041	0.189
48	4.00	1.60	0.230	(	0.134)	0.041	0.189
49	4.08	1.70	0.245	(	0.134)	0.044	0.201
50	4.17	1.80	0.259	(	0.134)	0.047	0.213
51	4.25	1.90	0.274	(	0.134)	0.049	0.224
52	4.33	2.00	0.288	(	0.134)	0.052	0.236
53	4.42	2.10	0.302	(	0.134)	0.054	0.248
54	4.50	2.10	0.302	(	0.134)	0.054	0.248
55	4.58	2.20	0.317	(	0.134)	0.057	0.260
56	4.67	2.30	0.331	(	0.134)	0.060	0.272
57	4.75	2.40	0.346	(	0.134)	0.062	0.283
58	4.83	2.40	0.346	(	0.134)	0.062	0.283
59	4.92	2.50	0.360	(	0.134)	0.065	0.295
60	5.00	2.60	0.374	(	0.134)	0.067	0.307
61	5.08	3.10	0.446	(	0.134)	0.080	0.366
62	5.17	3.60	0.518	(	0.134)	0.093	0.425
63	5.25	3.90	0.562	(	0.134)	0.101	0.461
64	5.33	4.20	0.605	(	0.134)	0.109	0.496
65	5.42	4.70	0.677	(	0.134)	0.122	0.555
66	5.50	5.60	0.806		0.134	(0.145)	0.672
67	5.58	1.90	0.274	(	0.134)	0.049	0.224
68	5.67	0.90	0.130	(	0.134)	0.023	0.106
69	5.75	0.60	0.086	(	0.134)	0.016	0.071
70	5.83	0.50	0.072	(	0.134)	0.013	0.059
71	5.92	0.30	0.043	(	0.134)	0.008	0.035
72	6.00	0.20	0.029	(	0.134)	0.005	0.024

(Loss Rate Not Used)

Sum = 100.0 Sum = 11.8

Flood volume = Effective rainfall 0.98(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.22(In)
Total soil loss = 0.005(Ac.Ft)
Total rainfall = 1.20(In)
Flood volume = 1036.8 Cubic Feet
Total soil loss = 226.4 Cubic Feet

Peak flow rate of this hydrograph = 0.197(CFS)

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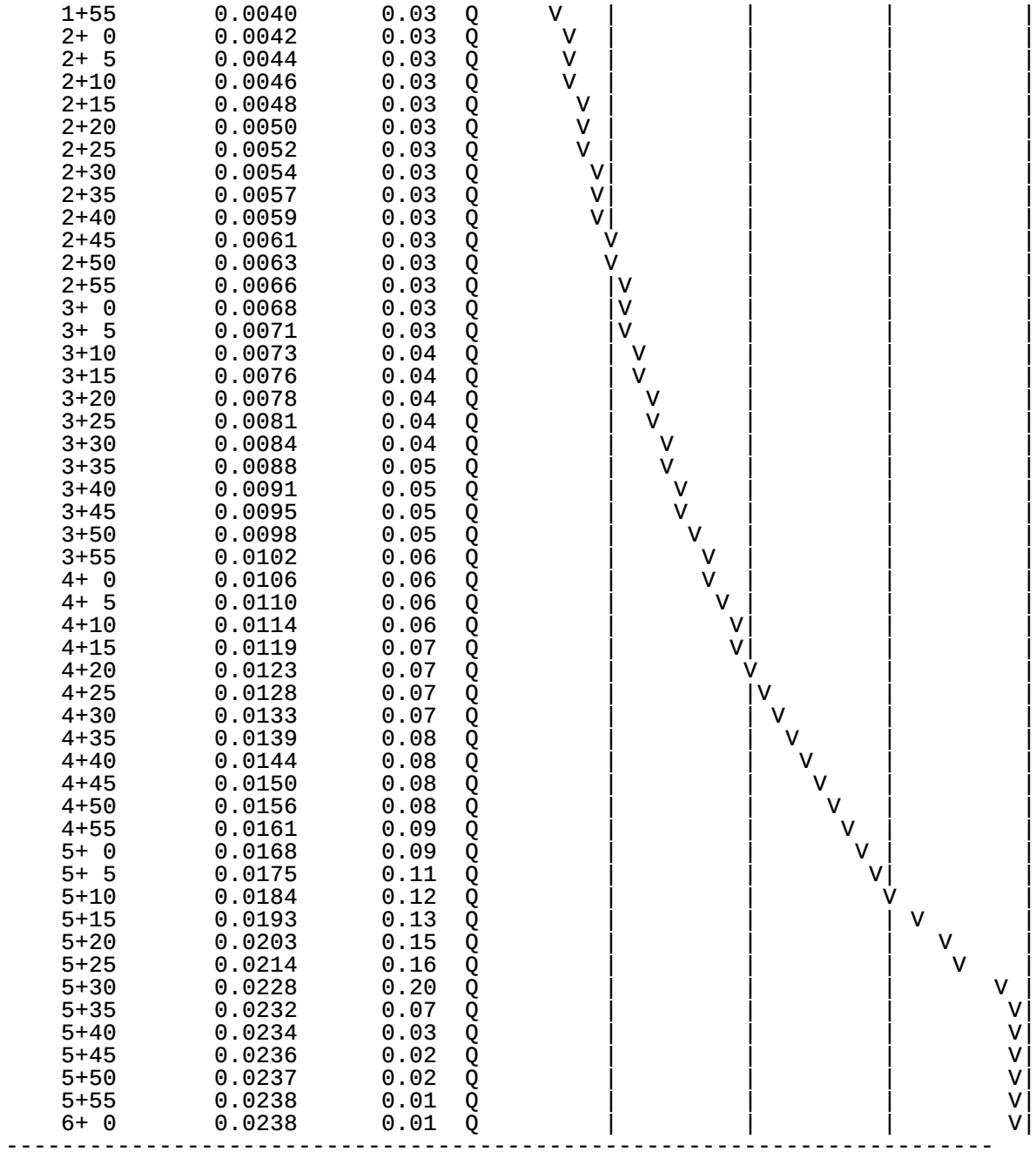
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q				
0+10	0.0003	0.02	Q				
0+15	0.0004	0.02	Q				
0+20	0.0005	0.02	Q				
0+25	0.0007	0.02	QV				
0+30	0.0009	0.02	QV				
0+35	0.0010	0.02	QV				
0+40	0.0012	0.02	QV				
0+45	0.0014	0.02	Q V				
0+50	0.0015	0.02	Q V				
0+55	0.0017	0.02	Q V				
1+ 0	0.0019	0.03	Q V				
1+ 5	0.0021	0.03	Q V				
1+10	0.0023	0.03	Q V				
1+15	0.0024	0.03	Q V				
1+20	0.0026	0.03	Q V				
1+25	0.0028	0.03	Q V				
1+30	0.0030	0.03	Q V				
1+35	0.0032	0.03	Q V				
1+40	0.0034	0.03	Q V				
1+45	0.0036	0.03	Q V				
1+50	0.0038	0.03	Q V				


1+55 0.0040 0.03 Q
2+ 0 0.0042 0.03 Q
2+ 5 0.0044 0.03 Q
2+10 0.0046 0.03 Q
2+15 0.0048 0.03 Q
2+20 0.0050 0.03 Q
2+25 0.0052 0.03 Q
2+30 0.0054 0.03 Q
2+35 0.0057 0.03 Q
2+40 0.0059 0.03 Q
2+45 0.0061 0.03 Q
2+50 0.0063 0.03 Q
2+55 0.0066 0.03 Q
3+ 0 0.0068 0.03 Q
3+ 5 0.0071 0.03 Q
3+10 0.0073 0.04 Q
3+15 0.0076 0.04 Q
3+20 0.0078 0.04 Q
3+25 0.0081 0.04 Q
3+30 0.0084 0.04 Q
3+35 0.0088 0.05 Q
3+40 0.0091 0.05 Q
3+45 0.0095 0.05 Q
3+50 0.0098 0.05 Q
3+55 0.0102 0.06 Q
4+ 0 0.0106 0.06 Q
4+ 5 0.0110 0.06 Q
4+10 0.0114 0.06 Q
4+15 0.0119 0.07 Q
4+20 0.0123 0.07 Q
4+25 0.0128 0.07 Q
4+30 0.0133 0.07 Q
4+35 0.0139 0.08 Q
4+40 0.0144 0.08 Q
4+45 0.0150 0.08 Q
4+50 0.0156 0.08 Q
4+55 0.0161 0.09 Q
5+ 0 0.0168 0.09 Q
5+ 5 0.0175 0.11 Q
5+10 0.0184 0.12 Q
5+15 0.0193 0.13 Q
5+20 0.0203 0.15 Q
5+25 0.0214 0.16 Q
5+30 0.0228 0.20 Q
5+35 0.0232 0.07 Q
5+40 0.0234 0.03 Q
5+45 0.0236 0.02 Q
5+50 0.0237 0.02 Q
5+55 0.0238 0.01 Q
6+ 0 0.0238 0.01 Q

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC0232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	0.90	0.26

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	2.35	0.68

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 0.900(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.900(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
		Sum = 100.000	Sum= 0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.140	(0.134)	0.025	0.115
2	0.17	1.30	0.140	(0.134)	0.025	0.115
3	0.25	1.10	0.119	(0.134)	0.021	0.097
4	0.33	1.50	0.162	(0.134)	0.029	0.133
5	0.42	1.50	0.162	(0.134)	0.029	0.133
6	0.50	1.80	0.194	(0.134)	0.035	0.159
7	0.58	1.50	0.162	(0.134)	0.029	0.133
8	0.67	1.80	0.194	(0.134)	0.035	0.159
9	0.75	1.80	0.194	(0.134)	0.035	0.159
10	0.83	1.50	0.162	(0.134)	0.029	0.133
11	0.92	1.60	0.173	(0.134)	0.031	0.142
12	1.00	1.80	0.194	(0.134)	0.035	0.159
13	1.08	2.20	0.238	(0.134)	0.043	0.195
14	1.17	2.20	0.238	(0.134)	0.043	0.195
15	1.25	2.20	0.238	(0.134)	0.043	0.195
16	1.33	2.00	0.216	(0.134)	0.039	0.177
17	1.42	2.60	0.281	(0.134)	0.051	0.230
18	1.50	2.70	0.292	(0.134)	0.052	0.239
19	1.58	2.40	0.259	(0.134)	0.047	0.213
20	1.67	2.70	0.292	(0.134)	0.052	0.239
21	1.75	3.30	0.356	(0.134)	0.064	0.292
22	1.83	3.10	0.335	(0.134)	0.060	0.275
23	1.92	2.90	0.313	(0.134)	0.056	0.257
24	2.00	3.00	0.324	(0.134)	0.058	0.266
25	2.08	3.10	0.335	(0.134)	0.060	0.275
26	2.17	4.20	0.454	(0.134)	0.082	0.372
27	2.25	5.00	0.540	(0.134)	0.097	0.443
28	2.33	3.50	0.378	(0.134)	0.068	0.310
29	2.42	6.80	0.734	(0.134)	0.132	0.602
30	2.50	7.30	0.788	0.134	(0.142)	0.654
31	2.58	8.20	0.886	0.134	(0.159)	0.751
32	2.67	5.90	0.637	(0.134)	0.115	0.523
33	2.75	2.00	0.216	(0.134)	0.039	0.177
34	2.83	1.80	0.194	(0.134)	0.035	0.159
35	2.92	1.80	0.194	(0.134)	0.035	0.159
36	3.00	0.60	0.065	(0.134)	0.012	0.053
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.9

Flood volume = Effective rainfall 0.74(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.16(In)
Total soil loss = 0.004(Ac.Ft)
Total rainfall = 0.90(In)

```
      Flood volume =         779.8 Cubic Feet
      Total soil loss =         167.6 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.220(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ----------------------------------------------------------------------------
   0+ 5       0.0002      0.03  Q         |         |         |         |
   0+10       0.0005      0.03  QV        |         |         |         |
   0+15       0.0007      0.03  QV        |         |         |         |
   0+20       0.0009      0.04  Q V       |         |         |         |
   0+25       0.0012      0.04  Q V       |         |         |         |
   0+30       0.0015      0.05  Q  V      |         |         |         |
   0+35       0.0018      0.04  Q  V      |         |         |         |
   0+40       0.0021      0.05  Q   V     |         |         |         |
   0+45       0.0024      0.05  Q    V    |         |         |         |
   0+50       0.0027      0.04  Q     V   |         |         |         |
   0+55       0.0030      0.04  Q     V   |         |         |         |
   1+ 0       0.0033      0.05  Q      V  |         |         |         |
   1+ 5       0.0037      0.06  Q       V |         |         |         |
   1+10       0.0041      0.06  Q        V|         |         |         |
   1+15       0.0045      0.06  Q         V         |         |         |
   1+20       0.0048      0.05  Q         V         |         |         |
   1+25       0.0053      0.07  Q         |V        |         |         |
   1+30       0.0058      0.07  Q         | V       |         |         |
   1+35       0.0062      0.06  Q         |  V      |         |         |
   1+40       0.0067      0.07  Q         |   V     |         |         |
   1+45       0.0073      0.09  Q         |     V   |         |         |
   1+50       0.0078      0.08  Q         |      V  |         |         |
   1+55       0.0083      0.08  Q         |       V |         |         |
   2+ 0       0.0089      0.08  Q         |        V|         |         |
   2+ 5       0.0094      0.08  Q         |         |V        |         |
   2+10       0.0102      0.11  Q         |         | V       |         |
   2+15       0.0111      0.13  Q         |         |   V     |         |
   2+20       0.0117      0.09  Q         |         |     V   |         |
   2+25       0.0129      0.18  Q         |         |       V |         |
   2+30       0.0142      0.19  Q         |         |         |V        |
   2+35       0.0157      0.22  Q         |         |         |    V    |
   2+40       0.0168      0.15  Q         |         |         |      V  |
   2+45       0.0172      0.05  Q         |         |         |       V |
   2+50       0.0175      0.05  Q         |         |         |        V|
   2+55       0.0178      0.05  Q         |         |         |         V|
   3+ 0       0.0179      0.02  Q         |         |         |          V
----------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC0212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	0.54	0.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	1.36	0.39

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.540(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.540(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	100.000	0.292
	1529.917	Sum = 100.000	Sum= 0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.285	(0.134)	0.051	0.234
2	0.17	4.50	0.292	(0.134)	0.052	0.239
3	0.25	5.40	0.350	(0.134)	0.063	0.287
4	0.33	5.40	0.350	(0.134)	0.063	0.287
5	0.42	5.70	0.369	(0.134)	0.066	0.303
6	0.50	6.40	0.415	(0.134)	0.075	0.340
7	0.58	7.90	0.512	(0.134)	0.092	0.420
8	0.67	9.10	0.590	(0.134)	0.106	0.484
9	0.75	12.80	0.829	0.134	(0.149)	0.695
10	0.83	25.60	1.659	0.134	(0.299)	1.525
11	0.92	7.90	0.512	(0.134)	0.092	0.420
12	1.00	4.90	0.318	(0.134)	0.057	0.260
	(Loss Rate Not Used)					
Sum =	100.0				Sum =	5.5

Flood volume = Effective rainfall 0.46(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.08(In)
Total soil loss = 0.002(Ac.Ft)
Total rainfall = 0.54(In)
Flood volume = 481.9 Cubic Feet
Total soil loss = 86.6 Cubic Feet

Peak flow rate of this hydrograph = 0.446(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0005	0.07	QV				
0+10	0.0010	0.07	Q V				
0+15	0.0015	0.08	Q V				
0+20	0.0021	0.08	Q V				
0+25	0.0027	0.09	Q V				
0+30	0.0034	0.10	Q V				
0+35	0.0042	0.12	Q V				
0+40	0.0052	0.14	Q V				

```
   0+45       0.0066      0.20  Q          |          |  V      |          |
   0+50       0.0097      0.45  |Q         |          |         |    V     |
   0+55       0.0105      0.12  Q          |          |         |       V  |
   1+ 0       0.0111      0.08  Q          |          |         |          V
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC05245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	2.00	0.58

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	6.40	1.86

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.031(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.031(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
			Sum = 100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.024	(0.238)	0.004	0.020
2	0.17	0.07	0.024	(0.237)	0.004	0.020
3	0.25	0.07	0.024	(0.236)	0.004	0.020
4	0.33	0.10	0.036	(0.235)	0.007	0.030
5	0.42	0.10	0.036	(0.234)	0.007	0.030
6	0.50	0.10	0.036	(0.233)	0.007	0.030
7	0.58	0.10	0.036	(0.232)	0.007	0.030
8	0.67	0.10	0.036	(0.231)	0.007	0.030
9	0.75	0.10	0.036	(0.230)	0.007	0.030
10	0.83	0.13	0.048	(0.230)	0.009	0.040
11	0.92	0.13	0.048	(0.229)	0.009	0.040
12	1.00	0.13	0.048	(0.228)	0.009	0.040
13	1.08	0.10	0.036	(0.227)	0.007	0.030
14	1.17	0.10	0.036	(0.226)	0.007	0.030
15	1.25	0.10	0.036	(0.225)	0.007	0.030
16	1.33	0.10	0.036	(0.224)	0.007	0.030
17	1.42	0.10	0.036	(0.223)	0.007	0.030
18	1.50	0.10	0.036	(0.222)	0.007	0.030
19	1.58	0.10	0.036	(0.222)	0.007	0.030
20	1.67	0.10	0.036	(0.221)	0.007	0.030
21	1.75	0.10	0.036	(0.220)	0.007	0.030
22	1.83	0.13	0.048	(0.219)	0.009	0.040
23	1.92	0.13	0.048	(0.218)	0.009	0.040
24	2.00	0.13	0.048	(0.217)	0.009	0.040
25	2.08	0.13	0.048	(0.216)	0.009	0.040
26	2.17	0.13	0.048	(0.215)	0.009	0.040
27	2.25	0.13	0.048	(0.214)	0.009	0.040
28	2.33	0.13	0.048	(0.214)	0.009	0.040
29	2.42	0.13	0.048	(0.213)	0.009	0.040
30	2.50	0.13	0.048	(0.212)	0.009	0.040
31	2.58	0.17	0.061	(0.211)	0.011	0.050
32	2.67	0.17	0.061	(0.210)	0.011	0.050
33	2.75	0.17	0.061	(0.209)	0.011	0.050
34	2.83	0.17	0.061	(0.208)	0.011	0.050
35	2.92	0.17	0.061	(0.208)	0.011	0.050
36	3.00	0.17	0.061	(0.207)	0.011	0.050
37	3.08	0.17	0.061	(0.206)	0.011	0.050
38	3.17	0.17	0.061	(0.205)	0.011	0.050
39	3.25	0.17	0.061	(0.204)	0.011	0.050
40	3.33	0.17	0.061	(0.203)	0.011	0.050
41	3.42	0.17	0.061	(0.202)	0.011	0.050
42	3.50	0.17	0.061	(0.202)	0.011	0.050
43	3.58	0.17	0.061	(0.201)	0.011	0.050

44	3.67	0.17	0.061	(0.200)	0.011	0.050
45	3.75	0.17	0.061	(0.199)	0.011	0.050
46	3.83	0.20	0.073	(0.198)	0.013	0.060
47	3.92	0.20	0.073	(0.197)	0.013	0.060
48	4.00	0.20	0.073	(0.197)	0.013	0.060
49	4.08	0.20	0.073	(0.196)	0.013	0.060
50	4.17	0.20	0.073	(0.195)	0.013	0.060
51	4.25	0.20	0.073	(0.194)	0.013	0.060
52	4.33	0.23	0.085	(0.193)	0.015	0.070
53	4.42	0.23	0.085	(0.192)	0.015	0.070
54	4.50	0.23	0.085	(0.192)	0.015	0.070
55	4.58	0.23	0.085	(0.191)	0.015	0.070
56	4.67	0.23	0.085	(0.190)	0.015	0.070
57	4.75	0.23	0.085	(0.189)	0.015	0.070
58	4.83	0.27	0.097	(0.188)	0.017	0.080
59	4.92	0.27	0.097	(0.187)	0.017	0.080
60	5.00	0.27	0.097	(0.187)	0.017	0.080
61	5.08	0.20	0.073	(0.186)	0.013	0.060
62	5.17	0.20	0.073	(0.185)	0.013	0.060
63	5.25	0.20	0.073	(0.184)	0.013	0.060
64	5.33	0.23	0.085	(0.183)	0.015	0.070
65	5.42	0.23	0.085	(0.183)	0.015	0.070
66	5.50	0.23	0.085	(0.182)	0.015	0.070
67	5.58	0.27	0.097	(0.181)	0.017	0.080
68	5.67	0.27	0.097	(0.180)	0.017	0.080
69	5.75	0.27	0.097	(0.179)	0.017	0.080
70	5.83	0.27	0.097	(0.179)	0.017	0.080
71	5.92	0.27	0.097	(0.178)	0.017	0.080
72	6.00	0.27	0.097	(0.177)	0.017	0.080
73	6.08	0.30	0.109	(0.176)	0.020	0.089
74	6.17	0.30	0.109	(0.175)	0.020	0.089
75	6.25	0.30	0.109	(0.175)	0.020	0.089
76	6.33	0.30	0.109	(0.174)	0.020	0.089
77	6.42	0.30	0.109	(0.173)	0.020	0.089
78	6.50	0.30	0.109	(0.172)	0.020	0.089
79	6.58	0.33	0.121	(0.172)	0.022	0.099
80	6.67	0.33	0.121	(0.171)	0.022	0.099
81	6.75	0.33	0.121	(0.170)	0.022	0.099
82	6.83	0.33	0.121	(0.169)	0.022	0.099
83	6.92	0.33	0.121	(0.169)	0.022	0.099
84	7.00	0.33	0.121	(0.168)	0.022	0.099
85	7.08	0.33	0.121	(0.167)	0.022	0.099
86	7.17	0.33	0.121	(0.166)	0.022	0.099
87	7.25	0.33	0.121	(0.165)	0.022	0.099
88	7.33	0.37	0.133	(0.165)	0.024	0.109
89	7.42	0.37	0.133	(0.164)	0.024	0.109
90	7.50	0.37	0.133	(0.163)	0.024	0.109
91	7.58	0.40	0.145	(0.162)	0.026	0.119
92	7.67	0.40	0.145	(0.162)	0.026	0.119
93	7.75	0.40	0.145	(0.161)	0.026	0.119
94	7.83	0.43	0.158	(0.160)	0.028	0.129
95	7.92	0.43	0.158	(0.159)	0.028	0.129
96	8.00	0.43	0.158	(0.159)	0.028	0.129
97	8.08	0.50	0.182	(0.158)	0.033	0.149
98	8.17	0.50	0.182	(0.157)	0.033	0.149
99	8.25	0.50	0.182	(0.157)	0.033	0.149
100	8.33	0.50	0.182	(0.156)	0.033	0.149
101	8.42	0.50	0.182	(0.155)	0.033	0.149
102	8.50	0.50	0.182	(0.154)	0.033	0.149
103	8.58	0.53	0.194	(0.154)	0.035	0.159
104	8.67	0.53	0.194	(0.153)	0.035	0.159
105	8.75	0.53	0.194	(0.152)	0.035	0.159
106	8.83	0.57	0.206	(0.151)	0.037	0.169
107	8.92	0.57	0.206	(0.151)	0.037	0.169
108	9.00	0.57	0.206	(0.150)	0.037	0.169
109	9.08	0.63	0.230	(0.149)	0.041	0.189
110	9.17	0.63	0.230	(0.149)	0.041	0.189
111	9.25	0.63	0.230	(0.148)	0.041	0.189
112	9.33	0.67	0.242	(0.147)	0.044	0.199
113	9.42	0.67	0.242	(0.147)	0.044	0.199
114	9.50	0.67	0.242	(0.146)	0.044	0.199
115	9.58	0.70	0.255	(0.145)	0.046	0.209

116	9.67	0.70	0.255	(0.144)	0.046	0.209
117	9.75	0.70	0.255	(0.144)	0.046	0.209
118	9.83	0.73	0.267	(0.143)	0.048	0.219
119	9.92	0.73	0.267	(0.142)	0.048	0.219
120	10.00	0.73	0.267	(0.142)	0.048	0.219
121	10.08	0.50	0.182	(0.141)	0.033	0.149
122	10.17	0.50	0.182	(0.140)	0.033	0.149
123	10.25	0.50	0.182	(0.140)	0.033	0.149
124	10.33	0.50	0.182	(0.139)	0.033	0.149
125	10.42	0.50	0.182	(0.138)	0.033	0.149
126	10.50	0.50	0.182	(0.138)	0.033	0.149
127	10.58	0.67	0.242	(0.137)	0.044	0.199
128	10.67	0.67	0.242	(0.136)	0.044	0.199
129	10.75	0.67	0.242	(0.136)	0.044	0.199
130	10.83	0.67	0.242	(0.135)	0.044	0.199
131	10.92	0.67	0.242	(0.134)	0.044	0.199
132	11.00	0.67	0.242	(0.134)	0.044	0.199
133	11.08	0.63	0.230	(0.133)	0.041	0.189
134	11.17	0.63	0.230	(0.132)	0.041	0.189
135	11.25	0.63	0.230	(0.132)	0.041	0.189
136	11.33	0.63	0.230	(0.131)	0.041	0.189
137	11.42	0.63	0.230	(0.130)	0.041	0.189
138	11.50	0.63	0.230	(0.130)	0.041	0.189
139	11.58	0.57	0.206	(0.129)	0.037	0.169
140	11.67	0.57	0.206	(0.128)	0.037	0.169
141	11.75	0.57	0.206	(0.128)	0.037	0.169
142	11.83	0.60	0.218	(0.127)	0.039	0.179
143	11.92	0.60	0.218	(0.126)	0.039	0.179
144	12.00	0.60	0.218	(0.126)	0.039	0.179
145	12.08	0.83	0.303	(0.125)	0.055	0.249
146	12.17	0.83	0.303	(0.125)	0.055	0.249
147	12.25	0.83	0.303	(0.124)	0.055	0.249
148	12.33	0.87	0.315	(0.123)	0.057	0.258
149	12.42	0.87	0.315	(0.123)	0.057	0.258
150	12.50	0.87	0.315	(0.122)	0.057	0.258
151	12.58	0.93	0.339	(0.121)	0.061	0.278
152	12.67	0.93	0.339	(0.121)	0.061	0.278
153	12.75	0.93	0.339	(0.120)	0.061	0.278
154	12.83	0.97	0.352	(0.120)	0.063	0.288
155	12.92	0.97	0.352	(0.119)	0.063	0.288
156	13.00	0.97	0.352	(0.118)	0.063	0.288
157	13.08	1.13	0.412	(0.118)	0.074	0.338
158	13.17	1.13	0.412	(0.117)	0.074	0.338
159	13.25	1.13	0.412	(0.117)	0.074	0.338
160	13.33	1.13	0.412	(0.116)	0.074	0.338
161	13.42	1.13	0.412	(0.115)	0.074	0.338
162	13.50	1.13	0.412	(0.115)	0.074	0.338
163	13.58	0.77	0.279	(0.114)	0.050	0.229
164	13.67	0.77	0.279	(0.114)	0.050	0.229
165	13.75	0.77	0.279	(0.113)	0.050	0.229
166	13.83	0.77	0.279	(0.113)	0.050	0.229
167	13.92	0.77	0.279	(0.112)	0.050	0.229
168	14.00	0.77	0.279	(0.111)	0.050	0.229
169	14.08	0.90	0.327	(0.111)	0.059	0.268
170	14.17	0.90	0.327	(0.110)	0.059	0.268
171	14.25	0.90	0.327	(0.110)	0.059	0.268
172	14.33	0.87	0.315	(0.109)	0.057	0.258
173	14.42	0.87	0.315	(0.109)	0.057	0.258
174	14.50	0.87	0.315	(0.108)	0.057	0.258
175	14.58	0.87	0.315	(0.107)	0.057	0.258
176	14.67	0.87	0.315	(0.107)	0.057	0.258
177	14.75	0.87	0.315	(0.106)	0.057	0.258
178	14.83	0.83	0.303	(0.106)	0.055	0.249
179	14.92	0.83	0.303	(0.105)	0.055	0.249
180	15.00	0.83	0.303	(0.105)	0.055	0.249
181	15.08	0.80	0.291	(0.104)	0.052	0.239
182	15.17	0.80	0.291	(0.104)	0.052	0.239
183	15.25	0.80	0.291	(0.103)	0.052	0.239
184	15.33	0.77	0.279	(0.103)	0.050	0.229
185	15.42	0.77	0.279	(0.102)	0.050	0.229
186	15.50	0.77	0.279	(0.102)	0.050	0.229
187	15.58	0.63	0.230	(0.101)	0.041	0.189

188	15.67	0.63	0.230	(0.101)	0.041	0.189
189	15.75	0.63	0.230	(0.100)	0.041	0.189
190	15.83	0.63	0.230	(0.100)	0.041	0.189
191	15.92	0.63	0.230	(0.099)	0.041	0.189
192	16.00	0.63	0.230	(0.099)	0.041	0.189
193	16.08	0.13	0.048	(0.098)	0.009	0.040
194	16.17	0.13	0.048	(0.098)	0.009	0.040
195	16.25	0.13	0.048	(0.097)	0.009	0.040
196	16.33	0.13	0.048	(0.097)	0.009	0.040
197	16.42	0.13	0.048	(0.096)	0.009	0.040
198	16.50	0.13	0.048	(0.096)	0.009	0.040
199	16.58	0.10	0.036	(0.095)	0.007	0.030
200	16.67	0.10	0.036	(0.095)	0.007	0.030
201	16.75	0.10	0.036	(0.094)	0.007	0.030
202	16.83	0.10	0.036	(0.094)	0.007	0.030
203	16.92	0.10	0.036	(0.093)	0.007	0.030
204	17.00	0.10	0.036	(0.093)	0.007	0.030
205	17.08	0.17	0.061	(0.092)	0.011	0.050
206	17.17	0.17	0.061	(0.092)	0.011	0.050
207	17.25	0.17	0.061	(0.091)	0.011	0.050
208	17.33	0.17	0.061	(0.091)	0.011	0.050
209	17.42	0.17	0.061	(0.090)	0.011	0.050
210	17.50	0.17	0.061	(0.090)	0.011	0.050
211	17.58	0.17	0.061	(0.089)	0.011	0.050
212	17.67	0.17	0.061	(0.089)	0.011	0.050
213	17.75	0.17	0.061	(0.089)	0.011	0.050
214	17.83	0.13	0.048	(0.088)	0.009	0.040
215	17.92	0.13	0.048	(0.088)	0.009	0.040
216	18.00	0.13	0.048	(0.087)	0.009	0.040
217	18.08	0.13	0.048	(0.087)	0.009	0.040
218	18.17	0.13	0.048	(0.086)	0.009	0.040
219	18.25	0.13	0.048	(0.086)	0.009	0.040
220	18.33	0.13	0.048	(0.086)	0.009	0.040
221	18.42	0.13	0.048	(0.085)	0.009	0.040
222	18.50	0.13	0.048	(0.085)	0.009	0.040
223	18.58	0.10	0.036	(0.084)	0.007	0.030
224	18.67	0.10	0.036	(0.084)	0.007	0.030
225	18.75	0.10	0.036	(0.084)	0.007	0.030
226	18.83	0.07	0.024	(0.083)	0.004	0.020
227	18.92	0.07	0.024	(0.083)	0.004	0.020
228	19.00	0.07	0.024	(0.082)	0.004	0.020
229	19.08	0.10	0.036	(0.082)	0.007	0.030
230	19.17	0.10	0.036	(0.082)	0.007	0.030
231	19.25	0.10	0.036	(0.081)	0.007	0.030
232	19.33	0.13	0.048	(0.081)	0.009	0.040
233	19.42	0.13	0.048	(0.080)	0.009	0.040
234	19.50	0.13	0.048	(0.080)	0.009	0.040
235	19.58	0.10	0.036	(0.080)	0.007	0.030
236	19.67	0.10	0.036	(0.079)	0.007	0.030
237	19.75	0.10	0.036	(0.079)	0.007	0.030
238	19.83	0.07	0.024	(0.079)	0.004	0.020
239	19.92	0.07	0.024	(0.078)	0.004	0.020
240	20.00	0.07	0.024	(0.078)	0.004	0.020
241	20.08	0.10	0.036	(0.078)	0.007	0.030
242	20.17	0.10	0.036	(0.077)	0.007	0.030
243	20.25	0.10	0.036	(0.077)	0.007	0.030
244	20.33	0.10	0.036	(0.077)	0.007	0.030
245	20.42	0.10	0.036	(0.076)	0.007	0.030
246	20.50	0.10	0.036	(0.076)	0.007	0.030
247	20.58	0.10	0.036	(0.076)	0.007	0.030
248	20.67	0.10	0.036	(0.075)	0.007	0.030
249	20.75	0.10	0.036	(0.075)	0.007	0.030
250	20.83	0.07	0.024	(0.075)	0.004	0.020
251	20.92	0.07	0.024	(0.074)	0.004	0.020
252	21.00	0.07	0.024	(0.074)	0.004	0.020
253	21.08	0.10	0.036	(0.074)	0.007	0.030
254	21.17	0.10	0.036	(0.073)	0.007	0.030
255	21.25	0.10	0.036	(0.073)	0.007	0.030
256	21.33	0.07	0.024	(0.073)	0.004	0.020
257	21.42	0.07	0.024	(0.073)	0.004	0.020
258	21.50	0.07	0.024	(0.072)	0.004	0.020
259	21.58	0.10	0.036	(0.072)	0.007	0.030

260	21.67	0.10	0.036	(0.072)	0.007	0.030
261	21.75	0.10	0.036	(0.072)	0.007	0.030
262	21.83	0.07	0.024	(0.071)	0.004	0.020
263	21.92	0.07	0.024	(0.071)	0.004	0.020
264	22.00	0.07	0.024	(0.071)	0.004	0.020
265	22.08	0.10	0.036	(0.071)	0.007	0.030
266	22.17	0.10	0.036	(0.070)	0.007	0.030
267	22.25	0.10	0.036	(0.070)	0.007	0.030
268	22.33	0.07	0.024	(0.070)	0.004	0.020
269	22.42	0.07	0.024	(0.070)	0.004	0.020
270	22.50	0.07	0.024	(0.069)	0.004	0.020
271	22.58	0.07	0.024	(0.069)	0.004	0.020
272	22.67	0.07	0.024	(0.069)	0.004	0.020
273	22.75	0.07	0.024	(0.069)	0.004	0.020
274	22.83	0.07	0.024	(0.069)	0.004	0.020
275	22.92	0.07	0.024	(0.069)	0.004	0.020
276	23.00	0.07	0.024	(0.068)	0.004	0.020
277	23.08	0.07	0.024	(0.068)	0.004	0.020
278	23.17	0.07	0.024	(0.068)	0.004	0.020
279	23.25	0.07	0.024	(0.068)	0.004	0.020
280	23.33	0.07	0.024	(0.068)	0.004	0.020
281	23.42	0.07	0.024	(0.068)	0.004	0.020
282	23.50	0.07	0.024	(0.068)	0.004	0.020
283	23.58	0.07	0.024	(0.067)	0.004	0.020
284	23.67	0.07	0.024	(0.067)	0.004	0.020
285	23.75	0.07	0.024	(0.067)	0.004	0.020
286	23.83	0.07	0.024	(0.067)	0.004	0.020
287	23.92	0.07	0.024	(0.067)	0.004	0.020
288	24.00	0.07	0.024	(0.067)	0.004	0.020

(Loss Rate Not Used)

Sum = 100.0 Sum = 29.8

Flood volume = Effective rainfall 2.49(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.55(In)
Total soil loss = 0.013(Ac.Ft)
Total rainfall = 3.03(In)
Flood volume = 2616.0 Cubic Feet
Total soil loss = 574.3 Cubic Feet

Peak flow rate of this hydrograph = 0.099(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.01	Q	|	|	|	|
0+10	0.0001	0.01	Q	|	|	|	|
0+15	0.0001	0.01	Q	|	|	|	|
0+20	0.0002	0.01	Q	|	|	|	|
0+25	0.0002	0.01	Q	|	|	|	|
0+30	0.0003	0.01	Q	|	|	|	|
0+35	0.0004	0.01	Q	|	|	|	|
0+40	0.0004	0.01	Q	|	|	|	|
0+45	0.0005	0.01	Q	|	|	|	|
0+50	0.0006	0.01	Q	|	|	|	|
0+55	0.0006	0.01	Q	|	|	|	|
1+ 0	0.0007	0.01	Q	|	|	|	|
1+ 5	0.0008	0.01	Q	|	|	|	|
1+10	0.0008	0.01	Q	|	|	|	|
1+15	0.0009	0.01	Q	|	|	|	|
1+20	0.0010	0.01	Q	|	|	|	|
1+25	0.0010	0.01	Q	|	|	|	|
1+30	0.0011	0.01	Q	|	|	|	|
1+35	0.0011	0.01	Q	|	|	|	|
1+40	0.0012	0.01	Q	|	|	|	|
1+45	0.0013	0.01	Q	|	|	|	|
1+50	0.0013	0.01	Q	|	|	|	|

1+55	0.0014	0.01	Q	|	|	|	|
2+ 0	0.0015	0.01	QV	|	|	|	|
2+ 5	0.0016	0.01	QV	|	|	|	|
2+10	0.0017	0.01	QV	|	|	|	|
2+15	0.0017	0.01	QV	|	|	|	|
2+20	0.0018	0.01	QV	|	|	|	|
2+25	0.0019	0.01	QV	|	|	|	|
2+30	0.0020	0.01	QV	|	|	|	|
2+35	0.0021	0.01	QV	|	|	|	|
2+40	0.0022	0.01	QV	|	|	|	|
2+45	0.0023	0.01	QV	|	|	|	|
2+50	0.0024	0.01	QV	|	|	|	|
2+55	0.0025	0.01	QV	|	|	|	|
3+ 0	0.0026	0.01	QV	|	|	|	|
3+ 5	0.0027	0.01	QV	|	|	|	|
3+10	0.0028	0.01	QV	|	|	|	|
3+15	0.0029	0.01	QV	|	|	|	|
3+20	0.0030	0.01	QV	|	|	|	|
3+25	0.0031	0.01	Q V	|	|	|	|
3+30	0.0032	0.01	Q V	|	|	|	|
3+35	0.0033	0.01	Q V	|	|	|	|
3+40	0.0034	0.01	Q V	|	|	|	|
3+45	0.0035	0.01	Q V	|	|	|	|
3+50	0.0036	0.02	Q V	|	|	|	|
3+55	0.0037	0.02	Q V	|	|	|	|
4+ 0	0.0038	0.02	Q V	|	|	|	|
4+ 5	0.0040	0.02	Q V	|	|	|	|
4+10	0.0041	0.02	Q V	|	|	|	|
4+15	0.0042	0.02	Q V	|	|	|	|
4+20	0.0043	0.02	Q V	|	|	|	|
4+25	0.0045	0.02	Q V	|	|	|	|
4+30	0.0046	0.02	Q V	|	|	|	|
4+35	0.0048	0.02	Q V	|	|	|	|
4+40	0.0049	0.02	Q V	|	|	|	|
4+45	0.0050	0.02	Q V	|	|	|	|
4+50	0.0052	0.02	Q V	|	|	|	|
4+55	0.0054	0.02	Q V	|	|	|	|
5+ 0	0.0055	0.02	Q V	|	|	|	|
5+ 5	0.0056	0.02	Q V	|	|	|	|
5+10	0.0058	0.02	Q V	|	|	|	|
5+15	0.0059	0.02	Q V	|	|	|	|
5+20	0.0060	0.02	Q V	|	|	|	|
5+25	0.0062	0.02	Q V	|	|	|	|
5+30	0.0063	0.02	Q V	|	|	|	|
5+35	0.0065	0.02	Q V	|	|	|	|
5+40	0.0066	0.02	Q V	|	|	|	|
5+45	0.0068	0.02	Q V	|	|	|	|
5+50	0.0069	0.02	Q V	|	|	|	|
5+55	0.0071	0.02	Q V	|	|	|	|
6+ 0	0.0073	0.02	Q V	|	|	|	|
6+ 5	0.0074	0.03	Q V	|	|	|	|
6+10	0.0076	0.03	Q V	|	|	|	|
6+15	0.0078	0.03	Q V	|	|	|	|
6+20	0.0080	0.03	Q V	|	|	|	|
6+25	0.0082	0.03	Q V	|	|	|	|
6+30	0.0083	0.03	Q V	|	|	|	|
6+35	0.0085	0.03	Q V	|	|	|	|
6+40	0.0087	0.03	Q V	|	|	|	|
6+45	0.0089	0.03	Q V	|	|	|	|
6+50	0.0091	0.03	Q V	|	|	|	|
6+55	0.0093	0.03	Q V	|	|	|	|
7+ 0	0.0095	0.03	Q V	|	|	|	|
7+ 5	0.0097	0.03	Q V	|	|	|	|
7+10	0.0099	0.03	Q V	|	|	|	|
7+15	0.0101	0.03	Q V	|	|	|	|
7+20	0.0104	0.03	Q V	|	|	|	|
7+25	0.0106	0.03	Q V	|	|	|	|
7+30	0.0108	0.03	Q V	|	|	|	|
7+35	0.0111	0.03	Q V	|	|	|	|
7+40	0.0113	0.03	Q V	|	|	|	|
7+45	0.0115	0.03	Q V	|	|	|	|
7+50	0.0118	0.04	Q V	|	|	|	|

7+55	0.0121	0.04	Q	V | | | |
8+ 0	0.0123	0.04	Q	V | | | |
8+ 5	0.0126	0.04	Q	V | | | |
8+10	0.0129	0.04	Q	V | | | |
8+15	0.0132	0.04	Q	V | | | |
8+20	0.0135	0.04	Q	V| | | |
8+25	0.0138	0.04	Q	V| | | |
8+30	0.0141	0.04	Q	V| | | |
8+35	0.0144	0.05	Q	V| | | |
8+40	0.0148	0.05	Q	V| | | |
8+45	0.0151	0.05	Q	V | | |
8+50	0.0154	0.05	Q	V | | |
8+55	0.0158	0.05	Q	V | | |
9+ 0	0.0161	0.05	Q	V | | |
9+ 5	0.0165	0.06	Q	V | | |
9+10	0.0169	0.06	Q	|V | | |
9+15	0.0172	0.06	Q	|V | | |
9+20	0.0176	0.06	Q	|V | | |
9+25	0.0180	0.06	Q	| V | | |
9+30	0.0184	0.06	Q	| V | | |
9+35	0.0189	0.06	Q	| V | | |
9+40	0.0193	0.06	Q	| V | | |
9+45	0.0197	0.06	Q	| V | | |
9+50	0.0201	0.06	Q	| V | | |
9+55	0.0206	0.06	Q	| V | | |
10+ 0	0.0210	0.06	Q	| V | | |
10+ 5	0.0213	0.04	Q	| V | | |
10+10	0.0216	0.04	Q	| V | | |
10+15	0.0219	0.04	Q	| V | | |
10+20	0.0222	0.04	Q	| V | | |
10+25	0.0225	0.04	Q	| V | | |
10+30	0.0228	0.04	Q	| V | | |
10+35	0.0232	0.06	Q	| V | | |
10+40	0.0236	0.06	Q	| V | | |
10+45	0.0240	0.06	Q	| V | | |
10+50	0.0244	0.06	Q	| V | | |
10+55	0.0248	0.06	Q	| V | | |
11+ 0	0.0252	0.06	Q	| V | | |
11+ 5	0.0256	0.06	Q	| V | | |
11+10	0.0260	0.06	Q	| V | | |
11+15	0.0264	0.06	Q	| V | | |
11+20	0.0267	0.06	Q	| V | | |
11+25	0.0271	0.06	Q	| V | | |
11+30	0.0275	0.06	Q	| V | | |
11+35	0.0278	0.05	Q	| V | | |
11+40	0.0282	0.05	Q	| V | | |
11+45	0.0285	0.05	Q	| V| | |
11+50	0.0289	0.05	Q	| V| | |
11+55	0.0292	0.05	Q	| V| | |
12+ 0	0.0296	0.05	Q	| V| | |
12+ 5	0.0301	0.07	Q	| V | |
12+10	0.0306	0.07	Q	| V | |
12+15	0.0311	0.07	Q	| V | |
12+20	0.0316	0.08	Q	| |V | |
12+25	0.0322	0.08	Q	| |V | |
12+30	0.0327	0.08	Q	| |V | |
12+35	0.0332	0.08	Q	| | V | |
12+40	0.0338	0.08	Q	| | V | |
12+45	0.0344	0.08	Q	| | V | |
12+50	0.0349	0.08	Q	| | V | |
12+55	0.0355	0.08	Q	| | V | |
13+ 0	0.0361	0.08	Q	| | V | |
13+ 5	0.0368	0.10	Q	| | V | |
13+10	0.0375	0.10	Q	| | V | |
13+15	0.0381	0.10	Q	| | V | |
13+20	0.0388	0.10	Q	| | V | |
13+25	0.0395	0.10	Q	| | V | |
13+30	0.0402	0.10	Q	| | V | |
13+35	0.0406	0.07	Q	| | V |
13+40	0.0411	0.07	Q	| | V |
13+45	0.0416	0.07	Q	| | V |
13+50	0.0420	0.07	Q	| | V |

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13+55       0.0425      0.07  Q          |           |         V |           |
14+ 0       0.0429      0.07  Q          |           |         V |           |
14+ 5       0.0435      0.08  Q          |           |         V |           |
14+10       0.0440      0.08  Q          |           |          V|           |
14+15       0.0446      0.08  Q          |           |          V|           |
14+20       0.0451      0.08  Q          |           |           V           |
14+25       0.0456      0.08  Q          |           |           V           |
14+30       0.0461      0.08  Q          |           |           V           |
14+35       0.0466      0.08  Q          |           |           |V          |
14+40       0.0472      0.08  Q          |           |           |V          |
14+45       0.0477      0.08  Q          |           |           |V          |
14+50       0.0482      0.07  Q          |           |           | V         |
14+55       0.0487      0.07  Q          |           |           | V         |
15+ 0       0.0492      0.07  Q          |           |           | V         |
15+ 5       0.0497      0.07  Q          |           |           |  V        |
15+10       0.0501      0.07  Q          |           |           |  V        |
15+15       0.0506      0.07  Q          |           |           |  V        |
15+20       0.0511      0.07  Q          |           |           |   V       |
15+25       0.0515      0.07  Q          |           |           |   V       |
15+30       0.0520      0.07  Q          |           |           |   V       |
15+35       0.0524      0.06  Q          |           |           |   V       |
15+40       0.0528      0.06  Q          |           |           |    V      |
15+45       0.0531      0.06  Q          |           |           |    V      |
15+50       0.0535      0.06  Q          |           |           |    V      |
15+55       0.0539      0.06  Q          |           |           |    V      |
16+ 0       0.0543      0.06  Q          |           |           |     V     |
16+ 5       0.0544      0.01  Q          |           |           |     V     |
16+10       0.0545      0.01  Q          |           |           |     V     |
16+15       0.0545      0.01  Q          |           |           |     V     |
16+20       0.0546      0.01  Q          |           |           |     V     |
16+25       0.0547      0.01  Q          |           |           |     V     |
16+30       0.0548      0.01  Q          |           |           |     V     |
16+35       0.0548      0.01  Q          |           |           |     V     |
16+40       0.0549      0.01  Q          |           |           |     V     |
16+45       0.0550      0.01  Q          |           |           |     V     |
16+50       0.0550      0.01  Q          |           |           |     V     |
16+55       0.0551      0.01  Q          |           |           |     V     |
17+ 0       0.0551      0.01  Q          |           |           |     V     |
17+ 5       0.0552      0.01  Q          |           |           |     V     |
17+10       0.0553      0.01  Q          |           |           |     V     |
17+15       0.0554      0.01  Q          |           |           |     V     |
17+20       0.0555      0.01  Q          |           |           |     V     |
17+25       0.0556      0.01  Q          |           |           |      V    |
17+30       0.0557      0.01  Q          |           |           |      V    |
17+35       0.0558      0.01  Q          |           |           |      V    |
17+40       0.0559      0.01  Q          |           |           |      V    |
17+45       0.0560      0.01  Q          |           |           |      V    |
17+50       0.0561      0.01  Q          |           |           |      V    |
17+55       0.0562      0.01  Q          |           |           |      V    |
18+ 0       0.0563      0.01  Q          |           |           |      V    |
18+ 5       0.0564      0.01  Q          |           |           |      V    |
18+10       0.0564      0.01  Q          |           |           |      V    |
18+15       0.0565      0.01  Q          |           |           |      V    |
18+20       0.0566      0.01  Q          |           |           |      V    |
18+25       0.0567      0.01  Q          |           |           |      V    |
18+30       0.0568      0.01  Q          |           |           |      V    |
18+35       0.0568      0.01  Q          |           |           |      V    |
18+40       0.0569      0.01  Q          |           |           |      V    |
18+45       0.0569      0.01  Q          |           |           |      V    |
18+50       0.0570      0.01  Q          |           |           |      V    |
18+55       0.0570      0.01  Q          |           |           |      V    |
19+ 0       0.0571      0.01  Q          |           |           |       V   |
19+ 5       0.0571      0.01  Q          |           |           |       V   |
19+10       0.0572      0.01  Q          |           |           |       V   |
19+15       0.0572      0.01  Q          |           |           |       V   |
19+20       0.0573      0.01  Q          |           |           |       V   |
19+25       0.0574      0.01  Q          |           |           |       V   |
19+30       0.0575      0.01  Q          |           |           |       V   |
19+35       0.0575      0.01  Q          |           |           |       V   |
19+40       0.0576      0.01  Q          |           |           |       V   |
19+45       0.0577      0.01  Q          |           |           |       V   |
19+50       0.0577      0.01  Q          |           |           |       V   |
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19+55	0.0577	0.01	Q	|	|	|	V |
20+ 0	0.0578	0.01	Q	|	|	|	V |
20+ 5	0.0578	0.01	Q	|	|	|	V |
20+10	0.0579	0.01	Q	|	|	|	V |
20+15	0.0580	0.01	Q	|	|	|	V |
20+20	0.0580	0.01	Q	|	|	|	V |
20+25	0.0581	0.01	Q	|	|	|	V |
20+30	0.0581	0.01	Q	|	|	|	V |
20+35	0.0582	0.01	Q	|	|	|	V |
20+40	0.0583	0.01	Q	|	|	|	V |
20+45	0.0583	0.01	Q	|	|	|	V |
20+50	0.0584	0.01	Q	|	|	|	V |
20+55	0.0584	0.01	Q	|	|	|	V |
21+ 0	0.0584	0.01	Q	|	|	|	V |
21+ 5	0.0585	0.01	Q	|	|	|	V |
21+10	0.0586	0.01	Q	|	|	|	V|
21+15	0.0586	0.01	Q	|	|	|	V|
21+20	0.0587	0.01	Q	|	|	|	V|
21+25	0.0587	0.01	Q	|	|	|	V|
21+30	0.0587	0.01	Q	|	|	|	V|
21+35	0.0588	0.01	Q	|	|	|	V|
21+40	0.0589	0.01	Q	|	|	|	V|
21+45	0.0589	0.01	Q	|	|	|	V|
21+50	0.0590	0.01	Q	|	|	|	V|
21+55	0.0590	0.01	Q	|	|	|	V|
22+ 0	0.0590	0.01	Q	|	|	|	V|
22+ 5	0.0591	0.01	Q	|	|	|	V|
22+10	0.0592	0.01	Q	|	|	|	V|
22+15	0.0592	0.01	Q	|	|	|	V|
22+20	0.0593	0.01	Q	|	|	|	V|
22+25	0.0593	0.01	Q	|	|	|	V|
22+30	0.0593	0.01	Q	|	|	|	V|
22+35	0.0594	0.01	Q	|	|	|	V|
22+40	0.0594	0.01	Q	|	|	|	V|
22+45	0.0595	0.01	Q	|	|	|	V|
22+50	0.0595	0.01	Q	|	|	|	V|
22+55	0.0595	0.01	Q	|	|	|	V|
23+ 0	0.0596	0.01	Q	|	|	|	V|
23+ 5	0.0596	0.01	Q	|	|	|	V|
23+10	0.0597	0.01	Q	|	|	|	V|
23+15	0.0597	0.01	Q	|	|	|	V|
23+20	0.0597	0.01	Q	|	|	|	V|
23+25	0.0598	0.01	Q	|	|	|	V|
23+30	0.0598	0.01	Q	|	|	|	V|
23+35	0.0599	0.01	Q	|	|	|	V|
23+40	0.0599	0.01	Q	|	|	|	V|
23+45	0.0599	0.01	Q	|	|	|	V|
23+50	0.0600	0.01	Q	|	|	|	V|
23+55	0.0600	0.01	Q	|	|	|	V|
24+ 0	0.0601	0.01	Q	|	|	|	V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC0565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	1.20	0.35

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	3.00	0.87

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.622(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.622(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
		Sum =	100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.097	(0.134)	0.018	0.080
2	0.17	0.60	0.117	(0.134)	0.021	0.096
3	0.25	0.60	0.117	(0.134)	0.021	0.096
4	0.33	0.60	0.117	(0.134)	0.021	0.096
5	0.42	0.60	0.117	(0.134)	0.021	0.096
6	0.50	0.70	0.136	(0.134)	0.025	0.112
7	0.58	0.70	0.136	(0.134)	0.025	0.112
8	0.67	0.70	0.136	(0.134)	0.025	0.112
9	0.75	0.70	0.136	(0.134)	0.025	0.112
10	0.83	0.70	0.136	(0.134)	0.025	0.112
11	0.92	0.70	0.136	(0.134)	0.025	0.112
12	1.00	0.80	0.156	(0.134)	0.028	0.128
13	1.08	0.80	0.156	(0.134)	0.028	0.128
14	1.17	0.80	0.156	(0.134)	0.028	0.128
15	1.25	0.80	0.156	(0.134)	0.028	0.128
16	1.33	0.80	0.156	(0.134)	0.028	0.128
17	1.42	0.80	0.156	(0.134)	0.028	0.128
18	1.50	0.80	0.156	(0.134)	0.028	0.128
19	1.58	0.80	0.156	(0.134)	0.028	0.128
20	1.67	0.80	0.156	(0.134)	0.028	0.128
21	1.75	0.80	0.156	(0.134)	0.028	0.128
22	1.83	0.80	0.156	(0.134)	0.028	0.128
23	1.92	0.80	0.156	(0.134)	0.028	0.128
24	2.00	0.90	0.175	(0.134)	0.032	0.144
25	2.08	0.80	0.156	(0.134)	0.028	0.128
26	2.17	0.90	0.175	(0.134)	0.032	0.144
27	2.25	0.90	0.175	(0.134)	0.032	0.144
28	2.33	0.90	0.175	(0.134)	0.032	0.144
29	2.42	0.90	0.175	(0.134)	0.032	0.144
30	2.50	0.90	0.175	(0.134)	0.032	0.144
31	2.58	0.90	0.175	(0.134)	0.032	0.144
32	2.67	0.90	0.175	(0.134)	0.032	0.144
33	2.75	1.00	0.195	(0.134)	0.035	0.160
34	2.83	1.00	0.195	(0.134)	0.035	0.160
35	2.92	1.00	0.195	(0.134)	0.035	0.160
36	3.00	1.00	0.195	(0.134)	0.035	0.160
37	3.08	1.00	0.195	(0.134)	0.035	0.160
38	3.17	1.10	0.214	(0.134)	0.039	0.176
39	3.25	1.10	0.214	(0.134)	0.039	0.176
40	3.33	1.10	0.214	(0.134)	0.039	0.176
41	3.42	1.20	0.234	(0.134)	0.042	0.191
42	3.50	1.30	0.253	(0.134)	0.046	0.207
43	3.58	1.40	0.272	(0.134)	0.049	0.223

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44   3.67     1.40      0.272       (  0.134)       0.049        0.223
45   3.75     1.50      0.292       (  0.134)       0.053        0.239
46   3.83     1.50      0.292       (  0.134)       0.053        0.239
47   3.92     1.60      0.311       (  0.134)       0.056        0.255
48   4.00     1.60      0.311       (  0.134)       0.056        0.255
49   4.08     1.70      0.331       (  0.134)       0.060        0.271
50   4.17     1.80      0.350       (  0.134)       0.063        0.287
51   4.25     1.90      0.370       (  0.134)       0.067        0.303
52   4.33     2.00      0.389       (  0.134)       0.070        0.319
53   4.42     2.10      0.409       (  0.134)       0.074        0.335
54   4.50     2.10      0.409       (  0.134)       0.074        0.335
55   4.58     2.20      0.428       (  0.134)       0.077        0.351
56   4.67     2.30      0.448       (  0.134)       0.081        0.367
57   4.75     2.40      0.467       (  0.134)       0.084        0.383
58   4.83     2.40      0.467       (  0.134)       0.084        0.383
59   4.92     2.50      0.486       (  0.134)       0.088        0.399
60   5.00     2.60      0.506       (  0.134)       0.091        0.415
61   5.08     3.10      0.603       (  0.134)       0.109        0.495
62   5.17     3.60      0.701       (  0.134)       0.126        0.574
63   5.25     3.90      0.759          0.134    (  0.137)       0.625
64   5.33     4.20      0.817          0.134    (  0.147)       0.683
65   5.42     4.70      0.915          0.134    (  0.165)       0.780
66   5.50     5.60      1.090          0.134    (  0.196)       0.956
67   5.58     1.90      0.370       (  0.134)       0.067        0.303
68   5.67     0.90      0.175       (  0.134)       0.032        0.144
69   5.75     0.60      0.117       (  0.134)       0.021        0.096
70   5.83     0.50      0.097       (  0.134)       0.018        0.080
71   5.92     0.30      0.058       (  0.134)       0.011        0.048
72   6.00     0.20      0.039       (  0.134)       0.007        0.032
              (Loss Rate Not Used)
   Sum =     100.0                                   Sum =    16.1
      Flood volume = Effective rainfall      1.34(In)
       times area       0.3(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
      Total soil loss =      0.28(In)
      Total soil loss =     0.007(Ac.Ft)
      Total rainfall =      1.62(In)
      Flood volume =        1409.3 Cubic Feet
      Total soil loss =         297.8 Cubic Feet
      ---------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.279(CFS)
      ---------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0002      0.02  Q          |         |         |         |
  0+10       0.0004      0.03  Q          |         |         |         |
  0+15       0.0005      0.03  Q          |         |         |         |
  0+20       0.0007      0.03  Q          |         |         |         |
  0+25       0.0009      0.03  QV         |         |         |         |
  0+30       0.0012      0.03  QV         |         |         |         |
  0+35       0.0014      0.03  QV         |         |         |         |
  0+40       0.0016      0.03  QV         |         |         |         |
  0+45       0.0018      0.03  Q V        |         |         |         |
  0+50       0.0021      0.03  Q V        |         |         |         |
  0+55       0.0023      0.03  Q V        |         |         |         |
  1+ 0       0.0025      0.04  Q  V       |         |         |         |
  1+ 5       0.0028      0.04  Q  V       |         |         |         |
  1+10       0.0031      0.04  Q  V       |         |         |         |
  1+15       0.0033      0.04  Q   V      |         |         |         |
  1+20       0.0036      0.04  Q   V      |         |         |         |
  1+25       0.0038      0.04  Q   V      |         |         |         |
  1+30       0.0041      0.04  Q    V     |         |         |         |
  1+35       0.0043      0.04  Q    V     |         |         |         |
  1+40       0.0046      0.04  Q    V     |         |         |         |
  1+45       0.0049      0.04  Q    V     |         |         |         |
  1+50       0.0051      0.04  Q     V    |         |         |         |
```

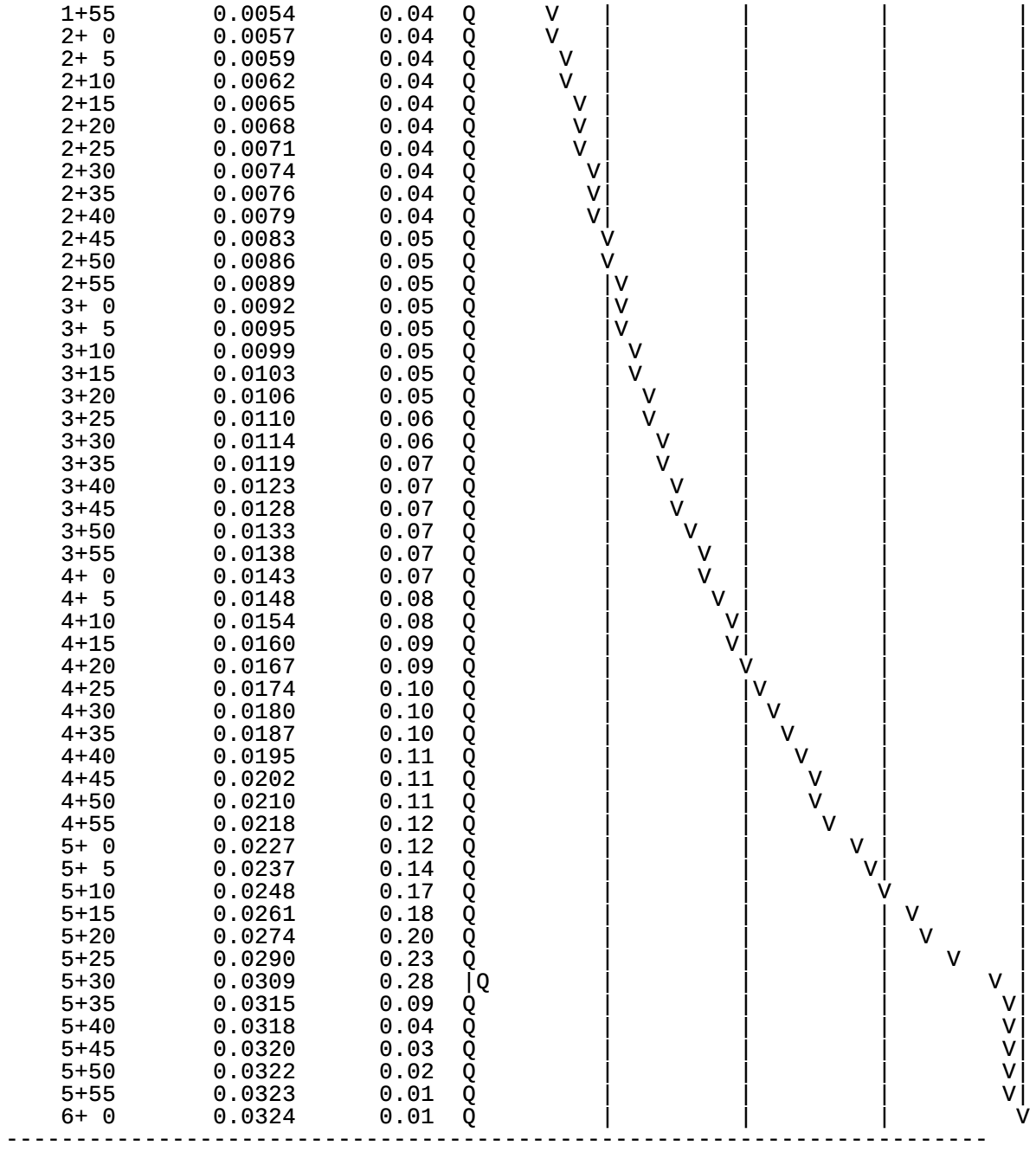
1+55 0.0054 0.04 Q
2+ 0 0.0057 0.04 Q
2+ 5 0.0059 0.04 Q
2+10 0.0062 0.04 Q
2+15 0.0065 0.04 Q
2+20 0.0068 0.04 Q
2+25 0.0071 0.04 Q
2+30 0.0074 0.04 Q
2+35 0.0076 0.04 Q
2+40 0.0079 0.04 Q
2+45 0.0083 0.05 Q
2+50 0.0086 0.05 Q
2+55 0.0089 0.05 Q
3+ 0 0.0092 0.05 Q
3+ 5 0.0095 0.05 Q
3+10 0.0099 0.05 Q
3+15 0.0103 0.05 Q
3+20 0.0106 0.05 Q
3+25 0.0110 0.06 Q
3+30 0.0114 0.06 Q
3+35 0.0119 0.07 Q
3+40 0.0123 0.07 Q
3+45 0.0128 0.07 Q
3+50 0.0133 0.07 Q
3+55 0.0138 0.07 Q
4+ 0 0.0143 0.07 Q
4+ 5 0.0148 0.08 Q
4+10 0.0154 0.08 Q
4+15 0.0160 0.09 Q
4+20 0.0167 0.09 Q
4+25 0.0174 0.10 Q
4+30 0.0180 0.10 Q
4+35 0.0187 0.10 Q
4+40 0.0195 0.11 Q
4+45 0.0202 0.11 Q
4+50 0.0210 0.11 Q
4+55 0.0218 0.12 Q
5+ 0 0.0227 0.12 Q
5+ 5 0.0237 0.14 Q
5+10 0.0248 0.17 Q
5+15 0.0261 0.18 Q
5+20 0.0274 0.20 Q
5+25 0.0290 0.23 Q
5+30 0.0309 0.28 Q
5+35 0.0315 0.09 Q
5+40 0.0318 0.04 Q
5+45 0.0320 0.03 Q
5+50 0.0322 0.02 Q
5+55 0.0323 0.01 Q
6+ 0 0.0324 0.01 Q

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC0535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	0.90	0.26

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	2.35	0.68

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.240(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.240(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
			Sum = 100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.193	(0.134)	0.035	0.159
2	0.17	1.30	0.193	(0.134)	0.035	0.159
3	0.25	1.10	0.164	(0.134)	0.029	0.134
4	0.33	1.50	0.223	(0.134)	0.040	0.183
5	0.42	1.50	0.223	(0.134)	0.040	0.183
6	0.50	1.80	0.268	(0.134)	0.048	0.220
7	0.58	1.50	0.223	(0.134)	0.040	0.183
8	0.67	1.80	0.268	(0.134)	0.048	0.220
9	0.75	1.80	0.268	(0.134)	0.048	0.220
10	0.83	1.50	0.223	(0.134)	0.040	0.183
11	0.92	1.60	0.238	(0.134)	0.043	0.195
12	1.00	1.80	0.268	(0.134)	0.048	0.220
13	1.08	2.20	0.327	(0.134)	0.059	0.268
14	1.17	2.20	0.327	(0.134)	0.059	0.268
15	1.25	2.20	0.327	(0.134)	0.059	0.268
16	1.33	2.00	0.298	(0.134)	0.054	0.244
17	1.42	2.60	0.387	(0.134)	0.070	0.317
18	1.50	2.70	0.402	(0.134)	0.072	0.329
19	1.58	2.40	0.357	(0.134)	0.064	0.293
20	1.67	2.70	0.402	(0.134)	0.072	0.329
21	1.75	3.30	0.491	(0.134)	0.088	0.403
22	1.83	3.10	0.461	(0.134)	0.083	0.378
23	1.92	2.90	0.431	(0.134)	0.078	0.354
24	2.00	3.00	0.446	(0.134)	0.080	0.366
25	2.08	3.10	0.461	(0.134)	0.083	0.378
26	2.17	4.20	0.625	(0.134)	0.112	0.512
27	2.25	5.00	0.744	(0.134)	0.134	0.610
28	2.33	3.50	0.521	(0.134)	0.094	0.427
29	2.42	6.80	1.012	0.134	(0.182)	0.877
30	2.50	7.30	1.086	0.134	(0.195)	0.952
31	2.58	8.20	1.220	0.134	(0.220)	1.086
32	2.67	5.90	0.878	0.134	(0.158)	0.744
33	2.75	2.00	0.298	(0.134)	0.054	0.244
34	2.83	1.80	0.268	(0.134)	0.048	0.220
35	2.92	1.80	0.268	(0.134)	0.048	0.220
36	3.00	0.60	0.089	(0.134)	0.016	0.073
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	12.4

Flood volume = Effective rainfall 1.03(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.005(Ac.Ft)
Total rainfall = 1.24(In)

Flood volume = 1089.2 Cubic Feet
Total soil loss = 215.7 Cubic Feet

Peak flow rate of this hydrograph = 0.317(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0003	0.05	Q
0+10	0.0006	0.05	QV
0+15	0.0009	0.04	QV
0+20	0.0013	0.05	Q V
0+25	0.0016	0.05	Q V
0+30	0.0021	0.06	Q V
0+35	0.0025	0.05	Q V
0+40	0.0029	0.06	Q V
0+45	0.0033	0.06	Q V
0+50	0.0037	0.05	Q V
0+55	0.0041	0.06	Q V
1+ 0	0.0045	0.06	Q V
1+ 5	0.0051	0.08	Q V
1+10	0.0056	0.08	Q V
1+15	0.0062	0.08	Q V
1+20	0.0067	0.07	Q V
1+25	0.0073	0.09	Q V
1+30	0.0080	0.10	Q V
1+35	0.0085	0.09	Q V
1+40	0.0092	0.10	Q V
1+45	0.0100	0.12	Q V
1+50	0.0108	0.11	Q V
1+55	0.0115	0.10	Q V
2+ 0	0.0122	0.11	Q V
2+ 5	0.0130	0.11	Q V
2+10	0.0140	0.15	Q V
2+15	0.0153	0.18	Q V
2+20	0.0161	0.12	Q V
2+25	0.0179	0.26	Q V
2+30	0.0198	0.28	Q V
2+35	0.0220	0.32	Q V
2+40	0.0235	0.22	Q V
2+45	0.0240	0.07	Q V
2+50	0.0244	0.06	Q V
2+55	0.0249	0.06	Q V
3+ 0	0.0250	0.02	Q V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC0515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	0.54	0.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	1.36	0.39

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.732(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.732(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	100.000	0.292
	1529.917	Sum = 100.000	Sum= 0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.387	(0.134)	0.070	0.317
2	0.17	4.50	0.395	(0.134)	0.071	0.324
3	0.25	5.40	0.474	(0.134)	0.085	0.389
4	0.33	5.40	0.474	(0.134)	0.085	0.389
5	0.42	5.70	0.501	(0.134)	0.090	0.411
6	0.50	6.40	0.562	(0.134)	0.101	0.461
7	0.58	7.90	0.694	(0.134)	0.125	0.569
8	0.67	9.10	0.799	0.134	(0.144)	0.665
9	0.75	12.80	1.124	0.134	(0.202)	0.990
10	0.83	25.60	2.249	0.134	(0.405)	2.115
11	0.92	7.90	0.694	(0.134)	0.125	0.569
12	1.00	4.90	0.430	(0.134)	0.077	0.353
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.6

Flood volume = Effective rainfall 0.63(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.10(In)
Total soil loss = 0.002(Ac.Ft)
Total rainfall = 0.73(In)
Flood volume = 662.5 Cubic Feet
Total soil loss = 108.1 Cubic Feet

Peak flow rate of this hydrograph = 0.618(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0006	0.09	QV				
0+10	0.0013	0.09	Q V				
0+15	0.0021	0.11	Q V				
0+20	0.0029	0.11	Q V				
0+25	0.0037	0.12	Q V				
0+30	0.0046	0.13	Q V				
0+35	0.0058	0.17	Q V				
0+40	0.0071	0.19	Q V				

```
   0+45       0.0091      0.29  |Q        |         |  V      |         |
   0+50       0.0134      0.62  | Q       |         |         |    V    |
   0+55       0.0145      0.17  Q         |         |         |       V |
   1+ 0       0.0152      0.10  Q         |         |         |         V
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	2.00	0.58

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	6.40	1.86

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.810(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.810(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
			Sum = 100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.030	(0.172)	0.005	0.025
2	0.17	0.07	0.030	(0.171)	0.005	0.025
3	0.25	0.07	0.030	(0.171)	0.005	0.025
4	0.33	0.10	0.046	(0.170)	0.008	0.037
5	0.42	0.10	0.046	(0.169)	0.008	0.037
6	0.50	0.10	0.046	(0.169)	0.008	0.037
7	0.58	0.10	0.046	(0.168)	0.008	0.037
8	0.67	0.10	0.046	(0.167)	0.008	0.037
9	0.75	0.10	0.046	(0.167)	0.008	0.037
10	0.83	0.13	0.061	(0.166)	0.011	0.050
11	0.92	0.13	0.061	(0.165)	0.011	0.050
12	1.00	0.13	0.061	(0.165)	0.011	0.050
13	1.08	0.10	0.046	(0.164)	0.008	0.037
14	1.17	0.10	0.046	(0.163)	0.008	0.037
15	1.25	0.10	0.046	(0.163)	0.008	0.037
16	1.33	0.10	0.046	(0.162)	0.008	0.037
17	1.42	0.10	0.046	(0.162)	0.008	0.037
18	1.50	0.10	0.046	(0.161)	0.008	0.037
19	1.58	0.10	0.046	(0.160)	0.008	0.037
20	1.67	0.10	0.046	(0.160)	0.008	0.037
21	1.75	0.10	0.046	(0.159)	0.008	0.037
22	1.83	0.13	0.061	(0.158)	0.011	0.050
23	1.92	0.13	0.061	(0.158)	0.011	0.050
24	2.00	0.13	0.061	(0.157)	0.011	0.050
25	2.08	0.13	0.061	(0.156)	0.011	0.050
26	2.17	0.13	0.061	(0.156)	0.011	0.050
27	2.25	0.13	0.061	(0.155)	0.011	0.050
28	2.33	0.13	0.061	(0.155)	0.011	0.050
29	2.42	0.13	0.061	(0.154)	0.011	0.050
30	2.50	0.13	0.061	(0.153)	0.011	0.050
31	2.58	0.17	0.076	(0.153)	0.014	0.062
32	2.67	0.17	0.076	(0.152)	0.014	0.062
33	2.75	0.17	0.076	(0.151)	0.014	0.062
34	2.83	0.17	0.076	(0.151)	0.014	0.062
35	2.92	0.17	0.076	(0.150)	0.014	0.062
36	3.00	0.17	0.076	(0.150)	0.014	0.062
37	3.08	0.17	0.076	(0.149)	0.014	0.062
38	3.17	0.17	0.076	(0.148)	0.014	0.062
39	3.25	0.17	0.076	(0.148)	0.014	0.062
40	3.33	0.17	0.076	(0.147)	0.014	0.062
41	3.42	0.17	0.076	(0.146)	0.014	0.062
42	3.50	0.17	0.076	(0.146)	0.014	0.062
43	3.58	0.17	0.076	(0.145)	0.014	0.062

44	3.67	0.17	0.076	(0.145)	0.014	0.062
45	3.75	0.17	0.076	(0.144)	0.014	0.062
46	3.83	0.20	0.091	(0.143)	0.016	0.075
47	3.92	0.20	0.091	(0.143)	0.016	0.075
48	4.00	0.20	0.091	(0.142)	0.016	0.075
49	4.08	0.20	0.091	(0.142)	0.016	0.075
50	4.17	0.20	0.091	(0.141)	0.016	0.075
51	4.25	0.20	0.091	(0.140)	0.016	0.075
52	4.33	0.23	0.107	(0.140)	0.019	0.087
53	4.42	0.23	0.107	(0.139)	0.019	0.087
54	4.50	0.23	0.107	(0.139)	0.019	0.087
55	4.58	0.23	0.107	(0.138)	0.019	0.087
56	4.67	0.23	0.107	(0.137)	0.019	0.087
57	4.75	0.23	0.107	(0.137)	0.019	0.087
58	4.83	0.27	0.122	(0.136)	0.022	0.100
59	4.92	0.27	0.122	(0.136)	0.022	0.100
60	5.00	0.27	0.122	(0.135)	0.022	0.100
61	5.08	0.20	0.091	(0.134)	0.016	0.075
62	5.17	0.20	0.091	(0.134)	0.016	0.075
63	5.25	0.20	0.091	(0.133)	0.016	0.075
64	5.33	0.23	0.107	(0.133)	0.019	0.087
65	5.42	0.23	0.107	(0.132)	0.019	0.087
66	5.50	0.23	0.107	(0.132)	0.019	0.087
67	5.58	0.27	0.122	(0.131)	0.022	0.100
68	5.67	0.27	0.122	(0.130)	0.022	0.100
69	5.75	0.27	0.122	(0.130)	0.022	0.100
70	5.83	0.27	0.122	(0.129)	0.022	0.100
71	5.92	0.27	0.122	(0.129)	0.022	0.100
72	6.00	0.27	0.122	(0.128)	0.022	0.100
73	6.08	0.30	0.137	(0.128)	0.025	0.112
74	6.17	0.30	0.137	(0.127)	0.025	0.112
75	6.25	0.30	0.137	(0.126)	0.025	0.112
76	6.33	0.30	0.137	(0.126)	0.025	0.112
77	6.42	0.30	0.137	(0.125)	0.025	0.112
78	6.50	0.30	0.137	(0.125)	0.025	0.112
79	6.58	0.33	0.152	(0.124)	0.027	0.125
80	6.67	0.33	0.152	(0.124)	0.027	0.125
81	6.75	0.33	0.152	(0.123)	0.027	0.125
82	6.83	0.33	0.152	(0.122)	0.027	0.125
83	6.92	0.33	0.152	(0.122)	0.027	0.125
84	7.00	0.33	0.152	(0.121)	0.027	0.125
85	7.08	0.33	0.152	(0.121)	0.027	0.125
86	7.17	0.33	0.152	(0.120)	0.027	0.125
87	7.25	0.33	0.152	(0.120)	0.027	0.125
88	7.33	0.37	0.168	(0.119)	0.030	0.137
89	7.42	0.37	0.168	(0.119)	0.030	0.137
90	7.50	0.37	0.168	(0.118)	0.030	0.137
91	7.58	0.40	0.183	(0.118)	0.033	0.150
92	7.67	0.40	0.183	(0.117)	0.033	0.150
93	7.75	0.40	0.183	(0.116)	0.033	0.150
94	7.83	0.43	0.198	(0.116)	0.036	0.162
95	7.92	0.43	0.198	(0.115)	0.036	0.162
96	8.00	0.43	0.198	(0.115)	0.036	0.162
97	8.08	0.50	0.229	(0.114)	0.041	0.187
98	8.17	0.50	0.229	(0.114)	0.041	0.187
99	8.25	0.50	0.229	(0.113)	0.041	0.187
100	8.33	0.50	0.229	(0.113)	0.041	0.187
101	8.42	0.50	0.229	(0.112)	0.041	0.187
102	8.50	0.50	0.229	(0.112)	0.041	0.187
103	8.58	0.53	0.244	(0.111)	0.044	0.200
104	8.67	0.53	0.244	(0.111)	0.044	0.200
105	8.75	0.53	0.244	(0.110)	0.044	0.200
106	8.83	0.57	0.259	(0.110)	0.047	0.212
107	8.92	0.57	0.259	(0.109)	0.047	0.212
108	9.00	0.57	0.259	(0.109)	0.047	0.212
109	9.08	0.63	0.290	(0.108)	0.052	0.237
110	9.17	0.63	0.290	(0.108)	0.052	0.237
111	9.25	0.63	0.290	(0.107)	0.052	0.237
112	9.33	0.67	0.305	(0.107)	0.055	0.250
113	9.42	0.67	0.305	(0.106)	0.055	0.250
114	9.50	0.67	0.305	(0.105)	0.055	0.250
115	9.58	0.70	0.320	(0.105)	0.058	0.262

116	9.67	0.70	0.320	(0.104)	0.058	0.262
117	9.75	0.70	0.320	(0.104)	0.058	0.262
118	9.83	0.73	0.335	(0.103)	0.060	0.275
119	9.92	0.73	0.335	(0.103)	0.060	0.275
120	10.00	0.73	0.335	(0.102)	0.060	0.275
121	10.08	0.50	0.229	(0.102)	0.041	0.187
122	10.17	0.50	0.229	(0.101)	0.041	0.187
123	10.25	0.50	0.229	(0.101)	0.041	0.187
124	10.33	0.50	0.229	(0.101)	0.041	0.187
125	10.42	0.50	0.229	(0.100)	0.041	0.187
126	10.50	0.50	0.229	(0.100)	0.041	0.187
127	10.58	0.67	0.305	(0.099)	0.055	0.250
128	10.67	0.67	0.305	(0.099)	0.055	0.250
129	10.75	0.67	0.305	(0.098)	0.055	0.250
130	10.83	0.67	0.305	(0.098)	0.055	0.250
131	10.92	0.67	0.305	(0.097)	0.055	0.250
132	11.00	0.67	0.305	(0.097)	0.055	0.250
133	11.08	0.63	0.290	(0.096)	0.052	0.237
134	11.17	0.63	0.290	(0.096)	0.052	0.237
135	11.25	0.63	0.290	(0.095)	0.052	0.237
136	11.33	0.63	0.290	(0.095)	0.052	0.237
137	11.42	0.63	0.290	(0.094)	0.052	0.237
138	11.50	0.63	0.290	(0.094)	0.052	0.237
139	11.58	0.57	0.259	(0.093)	0.047	0.212
140	11.67	0.57	0.259	(0.093)	0.047	0.212
141	11.75	0.57	0.259	(0.092)	0.047	0.212
142	11.83	0.60	0.274	(0.092)	0.049	0.225
143	11.92	0.60	0.274	(0.092)	0.049	0.225
144	12.00	0.60	0.274	(0.091)	0.049	0.225
145	12.08	0.83	0.381	(0.091)	0.069	0.312
146	12.17	0.83	0.381	(0.090)	0.069	0.312
147	12.25	0.83	0.381	(0.090)	0.069	0.312
148	12.33	0.87	0.396	(0.089)	0.071	0.325
149	12.42	0.87	0.396	(0.089)	0.071	0.325
150	12.50	0.87	0.396	(0.088)	0.071	0.325
151	12.58	0.93	0.427	(0.088)	0.077	0.350
152	12.67	0.93	0.427	(0.087)	0.077	0.350
153	12.75	0.93	0.427	(0.087)	0.077	0.350
154	12.83	0.97	0.442	(0.087)	0.080	0.362
155	12.92	0.97	0.442	(0.086)	0.080	0.362
156	13.00	0.97	0.442	(0.086)	0.080	0.362
157	13.08	1.13	0.518	0.085	(0.093)	0.433
158	13.17	1.13	0.518	0.085	(0.093)	0.433
159	13.25	1.13	0.518	0.084	(0.093)	0.434
160	13.33	1.13	0.518	0.084	(0.093)	0.434
161	13.42	1.13	0.518	0.084	(0.093)	0.435
162	13.50	1.13	0.518	0.083	(0.093)	0.435
163	13.58	0.77	0.351	(0.083)	0.063	0.287
164	13.67	0.77	0.351	(0.082)	0.063	0.287
165	13.75	0.77	0.351	(0.082)	0.063	0.287
166	13.83	0.77	0.351	(0.081)	0.063	0.287
167	13.92	0.77	0.351	(0.081)	0.063	0.287
168	14.00	0.77	0.351	(0.081)	0.063	0.287
169	14.08	0.90	0.412	(0.080)	0.074	0.337
170	14.17	0.90	0.412	(0.080)	0.074	0.337
171	14.25	0.90	0.412	(0.079)	0.074	0.337
172	14.33	0.87	0.396	(0.079)	0.071	0.325
173	14.42	0.87	0.396	(0.079)	0.071	0.325
174	14.50	0.87	0.396	(0.078)	0.071	0.325
175	14.58	0.87	0.396	(0.078)	0.071	0.325
176	14.67	0.87	0.396	(0.077)	0.071	0.325
177	14.75	0.87	0.396	(0.077)	0.071	0.325
178	14.83	0.83	0.381	(0.077)	0.069	0.312
179	14.92	0.83	0.381	(0.076)	0.069	0.312
180	15.00	0.83	0.381	(0.076)	0.069	0.312
181	15.08	0.80	0.366	(0.075)	0.066	0.300
182	15.17	0.80	0.366	(0.075)	0.066	0.300
183	15.25	0.80	0.366	(0.075)	0.066	0.300
184	15.33	0.77	0.351	(0.074)	0.063	0.287
185	15.42	0.77	0.351	(0.074)	0.063	0.287
186	15.50	0.77	0.351	(0.073)	0.063	0.287
187	15.58	0.63	0.290	(0.073)	0.052	0.237

188	15.67	0.63	0.290	(0.073)	0.052	0.237
189	15.75	0.63	0.290	(0.072)	0.052	0.237
190	15.83	0.63	0.290	(0.072)	0.052	0.237
191	15.92	0.63	0.290	(0.072)	0.052	0.237
192	16.00	0.63	0.290	(0.071)	0.052	0.237
193	16.08	0.13	0.061	(0.071)	0.011	0.050
194	16.17	0.13	0.061	(0.071)	0.011	0.050
195	16.25	0.13	0.061	(0.070)	0.011	0.050
196	16.33	0.13	0.061	(0.070)	0.011	0.050
197	16.42	0.13	0.061	(0.069)	0.011	0.050
198	16.50	0.13	0.061	(0.069)	0.011	0.050
199	16.58	0.10	0.046	(0.069)	0.008	0.037
200	16.67	0.10	0.046	(0.068)	0.008	0.037
201	16.75	0.10	0.046	(0.068)	0.008	0.037
202	16.83	0.10	0.046	(0.068)	0.008	0.037
203	16.92	0.10	0.046	(0.067)	0.008	0.037
204	17.00	0.10	0.046	(0.067)	0.008	0.037
205	17.08	0.17	0.076	(0.067)	0.014	0.062
206	17.17	0.17	0.076	(0.066)	0.014	0.062
207	17.25	0.17	0.076	(0.066)	0.014	0.062
208	17.33	0.17	0.076	(0.066)	0.014	0.062
209	17.42	0.17	0.076	(0.065)	0.014	0.062
210	17.50	0.17	0.076	(0.065)	0.014	0.062
211	17.58	0.17	0.076	(0.065)	0.014	0.062
212	17.67	0.17	0.076	(0.064)	0.014	0.062
213	17.75	0.17	0.076	(0.064)	0.014	0.062
214	17.83	0.13	0.061	(0.064)	0.011	0.050
215	17.92	0.13	0.061	(0.063)	0.011	0.050
216	18.00	0.13	0.061	(0.063)	0.011	0.050
217	18.08	0.13	0.061	(0.063)	0.011	0.050
218	18.17	0.13	0.061	(0.063)	0.011	0.050
219	18.25	0.13	0.061	(0.062)	0.011	0.050
220	18.33	0.13	0.061	(0.062)	0.011	0.050
221	18.42	0.13	0.061	(0.062)	0.011	0.050
222	18.50	0.13	0.061	(0.061)	0.011	0.050
223	18.58	0.10	0.046	(0.061)	0.008	0.037
224	18.67	0.10	0.046	(0.061)	0.008	0.037
225	18.75	0.10	0.046	(0.060)	0.008	0.037
226	18.83	0.07	0.030	(0.060)	0.005	0.025
227	18.92	0.07	0.030	(0.060)	0.005	0.025
228	19.00	0.07	0.030	(0.060)	0.005	0.025
229	19.08	0.10	0.046	(0.059)	0.008	0.037
230	19.17	0.10	0.046	(0.059)	0.008	0.037
231	19.25	0.10	0.046	(0.059)	0.008	0.037
232	19.33	0.13	0.061	(0.058)	0.011	0.050
233	19.42	0.13	0.061	(0.058)	0.011	0.050
234	19.50	0.13	0.061	(0.058)	0.011	0.050
235	19.58	0.10	0.046	(0.058)	0.008	0.037
236	19.67	0.10	0.046	(0.057)	0.008	0.037
237	19.75	0.10	0.046	(0.057)	0.008	0.037
238	19.83	0.07	0.030	(0.057)	0.005	0.025
239	19.92	0.07	0.030	(0.057)	0.005	0.025
240	20.00	0.07	0.030	(0.056)	0.005	0.025
241	20.08	0.10	0.046	(0.056)	0.008	0.037
242	20.17	0.10	0.046	(0.056)	0.008	0.037
243	20.25	0.10	0.046	(0.056)	0.008	0.037
244	20.33	0.10	0.046	(0.055)	0.008	0.037
245	20.42	0.10	0.046	(0.055)	0.008	0.037
246	20.50	0.10	0.046	(0.055)	0.008	0.037
247	20.58	0.10	0.046	(0.055)	0.008	0.037
248	20.67	0.10	0.046	(0.054)	0.008	0.037
249	20.75	0.10	0.046	(0.054)	0.008	0.037
250	20.83	0.07	0.030	(0.054)	0.005	0.025
251	20.92	0.07	0.030	(0.054)	0.005	0.025
252	21.00	0.07	0.030	(0.054)	0.005	0.025
253	21.08	0.10	0.046	(0.053)	0.008	0.037
254	21.17	0.10	0.046	(0.053)	0.008	0.037
255	21.25	0.10	0.046	(0.053)	0.008	0.037
256	21.33	0.07	0.030	(0.053)	0.005	0.025
257	21.42	0.07	0.030	(0.053)	0.005	0.025
258	21.50	0.07	0.030	(0.052)	0.005	0.025
259	21.58	0.10	0.046	(0.052)	0.008	0.037

260	21.67	0.10	0.046	(0.052)	0.008	0.037
261	21.75	0.10	0.046	(0.052)	0.008	0.037
262	21.83	0.07	0.030	(0.052)	0.005	0.025
263	21.92	0.07	0.030	(0.051)	0.005	0.025
264	22.00	0.07	0.030	(0.051)	0.005	0.025
265	22.08	0.10	0.046	(0.051)	0.008	0.037
266	22.17	0.10	0.046	(0.051)	0.008	0.037
267	22.25	0.10	0.046	(0.051)	0.008	0.037
268	22.33	0.07	0.030	(0.051)	0.005	0.025
269	22.42	0.07	0.030	(0.050)	0.005	0.025
270	22.50	0.07	0.030	(0.050)	0.005	0.025
271	22.58	0.07	0.030	(0.050)	0.005	0.025
272	22.67	0.07	0.030	(0.050)	0.005	0.025
273	22.75	0.07	0.030	(0.050)	0.005	0.025
274	22.83	0.07	0.030	(0.050)	0.005	0.025
275	22.92	0.07	0.030	(0.050)	0.005	0.025
276	23.00	0.07	0.030	(0.049)	0.005	0.025
277	23.08	0.07	0.030	(0.049)	0.005	0.025
278	23.17	0.07	0.030	(0.049)	0.005	0.025
279	23.25	0.07	0.030	(0.049)	0.005	0.025
280	23.33	0.07	0.030	(0.049)	0.005	0.025
281	23.42	0.07	0.030	(0.049)	0.005	0.025
282	23.50	0.07	0.030	(0.049)	0.005	0.025
283	23.58	0.07	0.030	(0.049)	0.005	0.025
284	23.67	0.07	0.030	(0.049)	0.005	0.025
285	23.75	0.07	0.030	(0.049)	0.005	0.025
286	23.83	0.07	0.030	(0.049)	0.005	0.025
287	23.92	0.07	0.030	(0.049)	0.005	0.025
288	24.00	0.07	0.030	(0.049)	0.005	0.025

(Loss Rate Not Used)

Sum = 100.0 Sum = 37.5

Flood volume = Effective rainfall 3.13(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.68(In)
Total soil loss = 0.016(Ac.Ft)
Total rainfall = 3.81(In)
Flood volume = 3293.8 Cubic Feet
Total soil loss = 717.2 Cubic Feet

Peak flow rate of this hydrograph = 0.127(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q				
0+10	0.0001	0.01	Q				
0+15	0.0002	0.01	Q				
0+20	0.0002	0.01	Q				
0+25	0.0003	0.01	Q				
0+30	0.0004	0.01	Q				
0+35	0.0005	0.01	Q				
0+40	0.0005	0.01	Q				
0+45	0.0006	0.01	Q				
0+50	0.0007	0.01	Q				
0+55	0.0008	0.01	Q				
1+ 0	0.0009	0.01	Q				
1+ 5	0.0010	0.01	Q				
1+10	0.0011	0.01	Q				
1+15	0.0011	0.01	Q				
1+20	0.0012	0.01	Q				
1+25	0.0013	0.01	Q				
1+30	0.0014	0.01	Q				
1+35	0.0014	0.01	Q				
1+40	0.0015	0.01	Q				
1+45	0.0016	0.01	Q				
1+50	0.0017	0.01	Q				

```
1+55       0.0018      0.01  Q          |          |          |          |
2+ 0       0.0019      0.01  Q          |          |          |          |
2+ 5       0.0020      0.01  QV         |          |          |          |
2+10       0.0021      0.01  QV         |          |          |          |
2+15       0.0022      0.01  QV         |          |          |          |
2+20       0.0023      0.01  QV         |          |          |          |
2+25       0.0024      0.01  QV         |          |          |          |
2+30       0.0025      0.01  QV         |          |          |          |
2+35       0.0026      0.02  QV         |          |          |          |
2+40       0.0027      0.02  QV         |          |          |          |
2+45       0.0029      0.02  QV         |          |          |          |
2+50       0.0030      0.02  QV         |          |          |          |
2+55       0.0031      0.02  QV         |          |          |          |
3+ 0       0.0032      0.02  QV         |          |          |          |
3+ 5       0.0034      0.02  QV         |          |          |          |
3+10       0.0035      0.02  QV         |          |          |          |
3+15       0.0036      0.02  QV         |          |          |          |
3+20       0.0038      0.02  QV         |          |          |          |
3+25       0.0039      0.02  Q V        |          |          |          |
3+30       0.0040      0.02  Q V        |          |          |          |
3+35       0.0041      0.02  Q V        |          |          |          |
3+40       0.0043      0.02  Q V        |          |          |          |
3+45       0.0044      0.02  Q V        |          |          |          |
3+50       0.0045      0.02  Q V        |          |          |          |
3+55       0.0047      0.02  Q V        |          |          |          |
4+ 0       0.0048      0.02  Q V        |          |          |          |
4+ 5       0.0050      0.02  Q V        |          |          |          |
4+10       0.0051      0.02  Q V        |          |          |          |
4+15       0.0053      0.02  Q V        |          |          |          |
4+20       0.0055      0.03  Q V        |          |          |          |
4+25       0.0056      0.03  Q V        |          |          |          |
4+30       0.0058      0.03  Q  V       |          |          |          |
4+35       0.0060      0.03  Q  V       |          |          |          |
4+40       0.0062      0.03  Q  V       |          |          |          |
4+45       0.0063      0.03  Q  V       |          |          |          |
4+50       0.0065      0.03  Q  V       |          |          |          |
4+55       0.0067      0.03  Q  V       |          |          |          |
5+ 0       0.0069      0.03  Q  V       |          |          |          |
5+ 5       0.0071      0.02  Q  V       |          |          |          |
5+10       0.0072      0.02  Q  V       |          |          |          |
5+15       0.0074      0.02  Q  V       |          |          |          |
5+20       0.0076      0.03  Q   V      |          |          |          |
5+25       0.0078      0.03  Q   V      |          |          |          |
5+30       0.0079      0.03  Q   V      |          |          |          |
5+35       0.0081      0.03  Q   V      |          |          |          |
5+40       0.0083      0.03  Q   V      |          |          |          |
5+45       0.0085      0.03  Q   V      |          |          |          |
5+50       0.0087      0.03  Q   V      |          |          |          |
5+55       0.0089      0.03  Q   V      |          |          |          |
6+ 0       0.0091      0.03  Q   V      |          |          |          |
6+ 5       0.0094      0.03  Q   V      |          |          |          |
6+10       0.0096      0.03  Q    V     |          |          |          |
6+15       0.0098      0.03  Q    V     |          |          |          |
6+20       0.0100      0.03  Q    V     |          |          |          |
6+25       0.0103      0.03  Q    V     |          |          |          |
6+30       0.0105      0.03  Q    V     |          |          |          |
6+35       0.0107      0.04  Q    V     |          |          |          |
6+40       0.0110      0.04  Q    V     |          |          |          |
6+45       0.0113      0.04  Q    V     |          |          |          |
6+50       0.0115      0.04  Q     V    |          |          |          |
6+55       0.0118      0.04  Q     V    |          |          |          |
7+ 0       0.0120      0.04  Q     V    |          |          |          |
7+ 5       0.0123      0.04  Q     V    |          |          |          |
7+10       0.0125      0.04  Q     V    |          |          |          |
7+15       0.0128      0.04  Q     V    |          |          |          |
7+20       0.0130      0.04  Q     V    |          |          |          |
7+25       0.0133      0.04  Q      V   |          |          |          |
7+30       0.0136      0.04  Q      V   |          |          |          |
7+35       0.0139      0.04  Q      V   |          |          |          |
7+40       0.0142      0.04  Q      V   |          |          |          |
7+45       0.0145      0.04  Q      V   |          |          |          |
7+50       0.0148      0.05  Q      V   |          |          |          |
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7+55	0.0152	0.05	Q	V | | | |
8+ 0	0.0155	0.05	Q	V | | | |
8+ 5	0.0159	0.05	Q	V | | | |
8+10	0.0162	0.05	Q	V | | | |
8+15	0.0166	0.05	Q	V | | | |
8+20	0.0170	0.05	Q	V | | | |
8+25	0.0174	0.05	Q	V| | | |
8+30	0.0177	0.05	Q	V| | | |
8+35	0.0181	0.06	Q	V| | | |
8+40	0.0185	0.06	Q	V| | | |
8+45	0.0190	0.06	Q	V | | |
8+50	0.0194	0.06	Q	V | | |
8+55	0.0198	0.06	Q	V | | |
9+ 0	0.0202	0.06	Q	V | | |
9+ 5	0.0207	0.07	Q	V | | |
9+10	0.0212	0.07	Q	|V | |
9+15	0.0217	0.07	Q	|V | |
9+20	0.0222	0.07	Q	|V | |
9+25	0.0227	0.07	Q	|V | |
9+30	0.0232	0.07	Q	| V | |
9+35	0.0237	0.08	Q	| V | |
9+40	0.0242	0.08	Q	| V | |
9+45	0.0248	0.08	Q	| V | |
9+50	0.0253	0.08	Q	| V | |
9+55	0.0259	0.08	Q	| V | |
10+ 0	0.0264	0.08	Q	| V | |
10+ 5	0.0268	0.05	Q	| V | |
10+10	0.0272	0.05	Q	| V | |
10+15	0.0276	0.05	Q	| V | |
10+20	0.0279	0.05	Q	| V | |
10+25	0.0283	0.05	Q	| V | |
10+30	0.0287	0.05	Q	| V | |
10+35	0.0292	0.07	Q	| V | |
10+40	0.0297	0.07	Q	| V | |
10+45	0.0302	0.07	Q	| V | |
10+50	0.0307	0.07	Q	| V | |
10+55	0.0312	0.07	Q	| V | |
11+ 0	0.0317	0.07	Q	| V | |
11+ 5	0.0322	0.07	Q	| V | |
11+10	0.0327	0.07	Q	| V | |
11+15	0.0331	0.07	Q	| V | |
11+20	0.0336	0.07	Q	| V | |
11+25	0.0341	0.07	Q	| V | |
11+30	0.0346	0.07	Q	| V | |
11+35	0.0350	0.06	Q	| V | |
11+40	0.0354	0.06	Q	| V | |
11+45	0.0359	0.06	Q	| V | |
11+50	0.0363	0.07	Q	| V| |
11+55	0.0368	0.07	Q	| V| |
12+ 0	0.0372	0.07	Q	| V| |
12+ 5	0.0379	0.09	Q	| V |
12+10	0.0385	0.09	Q	| V |
12+15	0.0391	0.09	Q	| V |
12+20	0.0398	0.10	Q	| |V |
12+25	0.0404	0.10	Q	| |V |
12+30	0.0411	0.10	Q	| |V |
12+35	0.0418	0.10	Q	| | V |
12+40	0.0425	0.10	Q	| | V |
12+45	0.0432	0.10	Q	| | V |
12+50	0.0439	0.11	Q	| | V |
12+55	0.0446	0.11	Q	| | V |
13+ 0	0.0454	0.11	Q	| | V |
13+ 5	0.0463	0.13	Q	| | V |
13+10	0.0471	0.13	Q	| | V |
13+15	0.0480	0.13	Q	| | V |
13+20	0.0489	0.13	Q	| | V |
13+25	0.0497	0.13	Q	| | V |
13+30	0.0506	0.13	Q	| | V |
13+35	0.0512	0.08	Q	| | V |
13+40	0.0518	0.08	Q	| | V |
13+45	0.0524	0.08	Q	| | V |
13+50	0.0529	0.08	Q	| | V |

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13+55       0.0535      0.08  Q          |           |         V |           |
14+ 0       0.0541      0.08  Q          |           |         V |           |
14+ 5       0.0548      0.10  Q          |           |         V |           |
14+10       0.0555      0.10  Q          |           |          V|           |
14+15       0.0561      0.10  Q          |           |          V|           |
14+20       0.0568      0.10  Q          |           |           V           |
14+25       0.0574      0.10  Q          |           |           V           |
14+30       0.0581      0.10  Q          |           |           V           |
14+35       0.0588      0.10  Q          |           |           |V          |
14+40       0.0594      0.10  Q          |           |           |V          |
14+45       0.0601      0.10  Q          |           |           |V          |
14+50       0.0607      0.09  Q          |           |           | V         |
14+55       0.0613      0.09  Q          |           |           | V         |
15+ 0       0.0619      0.09  Q          |           |           | V         |
15+ 5       0.0626      0.09  Q          |           |           |  V        |
15+10       0.0632      0.09  Q          |           |           |  V        |
15+15       0.0638      0.09  Q          |           |           |  V        |
15+20       0.0643      0.08  Q          |           |           |   V       |
15+25       0.0649      0.08  Q          |           |           |   V       |
15+30       0.0655      0.08  Q          |           |           |   V       |
15+35       0.0660      0.07  Q          |           |           |   V       |
15+40       0.0665      0.07  Q          |           |           |    V      |
15+45       0.0669      0.07  Q          |           |           |    V      |
15+50       0.0674      0.07  Q          |           |           |    V      |
15+55       0.0679      0.07  Q          |           |           |    V      |
16+ 0       0.0684      0.07  Q          |           |           |     V     |
16+ 5       0.0685      0.01  Q          |           |           |     V     |
16+10       0.0686      0.01  Q          |           |           |     V     |
16+15       0.0687      0.01  Q          |           |           |     V     |
16+20       0.0688      0.01  Q          |           |           |     V     |
16+25       0.0689      0.01  Q          |           |           |     V     |
16+30       0.0690      0.01  Q          |           |           |     V     |
16+35       0.0690      0.01  Q          |           |           |     V     |
16+40       0.0691      0.01  Q          |           |           |     V     |
16+45       0.0692      0.01  Q          |           |           |     V     |
16+50       0.0693      0.01  Q          |           |           |     V     |
16+55       0.0693      0.01  Q          |           |           |     V     |
17+ 0       0.0694      0.01  Q          |           |           |     V     |
17+ 5       0.0695      0.02  Q          |           |           |     V     |
17+10       0.0697      0.02  Q          |           |           |     V     |
17+15       0.0698      0.02  Q          |           |           |     V     |
17+20       0.0699      0.02  Q          |           |           |     V     |
17+25       0.0701      0.02  Q          |           |           |      V    |
17+30       0.0702      0.02  Q          |           |           |      V    |
17+35       0.0703      0.02  Q          |           |           |      V    |
17+40       0.0704      0.02  Q          |           |           |      V    |
17+45       0.0706      0.02  Q          |           |           |      V    |
17+50       0.0707      0.01  Q          |           |           |      V    |
17+55       0.0708      0.01  Q          |           |           |      V    |
18+ 0       0.0709      0.01  Q          |           |           |      V    |
18+ 5       0.0710      0.01  Q          |           |           |      V    |
18+10       0.0711      0.01  Q          |           |           |      V    |
18+15       0.0712      0.01  Q          |           |           |      V    |
18+20       0.0713      0.01  Q          |           |           |      V    |
18+25       0.0714      0.01  Q          |           |           |      V    |
18+30       0.0715      0.01  Q          |           |           |      V    |
18+35       0.0715      0.01  Q          |           |           |      V    |
18+40       0.0716      0.01  Q          |           |           |      V    |
18+45       0.0717      0.01  Q          |           |           |      V    |
18+50       0.0717      0.01  Q          |           |           |      V    |
18+55       0.0718      0.01  Q          |           |           |      V    |
19+ 0       0.0718      0.01  Q          |           |           |       V   |
19+ 5       0.0719      0.01  Q          |           |           |       V   |
19+10       0.0720      0.01  Q          |           |           |       V   |
19+15       0.0721      0.01  Q          |           |           |       V   |
19+20       0.0722      0.01  Q          |           |           |       V   |
19+25       0.0723      0.01  Q          |           |           |       V   |
19+30       0.0724      0.01  Q          |           |           |       V   |
19+35       0.0724      0.01  Q          |           |           |       V   |
19+40       0.0725      0.01  Q          |           |           |       V   |
19+45       0.0726      0.01  Q          |           |           |       V   |
19+50       0.0726      0.01  Q          |           |           |       V   |
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19+55	0.0727	0.01	Q	|	|	|	V |
20+ 0	0.0727	0.01	Q	|	|	|	V |
20+ 5	0.0728	0.01	Q	|	|	|	V |
20+10	0.0729	0.01	Q	|	|	|	V |
20+15	0.0730	0.01	Q	|	|	|	V |
20+20	0.0730	0.01	Q	|	|	|	V |
20+25	0.0731	0.01	Q	|	|	|	V |
20+30	0.0732	0.01	Q	|	|	|	V |
20+35	0.0733	0.01	Q	|	|	|	V |
20+40	0.0733	0.01	Q	|	|	|	V |
20+45	0.0734	0.01	Q	|	|	|	V |
20+50	0.0735	0.01	Q	|	|	|	V |
20+55	0.0735	0.01	Q	|	|	|	V |
21+ 0	0.0736	0.01	Q	|	|	|	V |
21+ 5	0.0737	0.01	Q	|	|	|	V |
21+10	0.0737	0.01	Q	|	|	|	V|
21+15	0.0738	0.01	Q	|	|	|	V|
21+20	0.0739	0.01	Q	|	|	|	V|
21+25	0.0739	0.01	Q	|	|	|	V|
21+30	0.0740	0.01	Q	|	|	|	V|
21+35	0.0740	0.01	Q	|	|	|	V|
21+40	0.0741	0.01	Q	|	|	|	V|
21+45	0.0742	0.01	Q	|	|	|	V|
21+50	0.0742	0.01	Q	|	|	|	V|
21+55	0.0743	0.01	Q	|	|	|	V|
22+ 0	0.0743	0.01	Q	|	|	|	V|
22+ 5	0.0744	0.01	Q	|	|	|	V|
22+10	0.0745	0.01	Q	|	|	|	V|
22+15	0.0746	0.01	Q	|	|	|	V|
22+20	0.0746	0.01	Q	|	|	|	V|
22+25	0.0747	0.01	Q	|	|	|	V|
22+30	0.0747	0.01	Q	|	|	|	V|
22+35	0.0748	0.01	Q	|	|	|	V|
22+40	0.0748	0.01	Q	|	|	|	V|
22+45	0.0749	0.01	Q	|	|	|	V|
22+50	0.0749	0.01	Q	|	|	|	V|
22+55	0.0750	0.01	Q	|	|	|	V|
23+ 0	0.0750	0.01	Q	|	|	|	V|
23+ 5	0.0751	0.01	Q	|	|	|	V|
23+10	0.0751	0.01	Q	|	|	|	V|
23+15	0.0752	0.01	Q	|	|	|	V|
23+20	0.0752	0.01	Q	|	|	|	V|
23+25	0.0753	0.01	Q	|	|	|	V|
23+30	0.0753	0.01	Q	|	|	|	V|
23+35	0.0754	0.01	Q	|	|	|	V|
23+40	0.0754	0.01	Q	|	|	|	V|
23+45	0.0755	0.01	Q	|	|	|	V|
23+50	0.0755	0.01	Q	|	|	|	V|
23+55	0.0756	0.01	Q	|	|	|	V|
24+ 0	0.0756	0.01	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC10610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	1.20	0.35

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	3.00	0.87

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.941(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.941(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
			Sum = 100.000 Sum=	0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.116	(0.097)	0.021	0.095
2	0.17	0.60	0.140	(0.097)	0.025	0.115
3	0.25	0.60	0.140	(0.097)	0.025	0.115
4	0.33	0.60	0.140	(0.097)	0.025	0.115
5	0.42	0.60	0.140	(0.097)	0.025	0.115
6	0.50	0.70	0.163	(0.097)	0.029	0.134
7	0.58	0.70	0.163	(0.097)	0.029	0.134
8	0.67	0.70	0.163	(0.097)	0.029	0.134
9	0.75	0.70	0.163	(0.097)	0.029	0.134
10	0.83	0.70	0.163	(0.097)	0.029	0.134
11	0.92	0.70	0.163	(0.097)	0.029	0.134
12	1.00	0.80	0.186	(0.097)	0.034	0.153
13	1.08	0.80	0.186	(0.097)	0.034	0.153
14	1.17	0.80	0.186	(0.097)	0.034	0.153
15	1.25	0.80	0.186	(0.097)	0.034	0.153
16	1.33	0.80	0.186	(0.097)	0.034	0.153
17	1.42	0.80	0.186	(0.097)	0.034	0.153
18	1.50	0.80	0.186	(0.097)	0.034	0.153
19	1.58	0.80	0.186	(0.097)	0.034	0.153
20	1.67	0.80	0.186	(0.097)	0.034	0.153
21	1.75	0.80	0.186	(0.097)	0.034	0.153
22	1.83	0.80	0.186	(0.097)	0.034	0.153
23	1.92	0.80	0.186	(0.097)	0.034	0.153
24	2.00	0.90	0.210	(0.097)	0.038	0.172
25	2.08	0.80	0.186	(0.097)	0.034	0.153
26	2.17	0.90	0.210	(0.097)	0.038	0.172
27	2.25	0.90	0.210	(0.097)	0.038	0.172
28	2.33	0.90	0.210	(0.097)	0.038	0.172
29	2.42	0.90	0.210	(0.097)	0.038	0.172
30	2.50	0.90	0.210	(0.097)	0.038	0.172
31	2.58	0.90	0.210	(0.097)	0.038	0.172
32	2.67	0.90	0.210	(0.097)	0.038	0.172
33	2.75	1.00	0.233	(0.097)	0.042	0.191
34	2.83	1.00	0.233	(0.097)	0.042	0.191
35	2.92	1.00	0.233	(0.097)	0.042	0.191
36	3.00	1.00	0.233	(0.097)	0.042	0.191
37	3.08	1.00	0.233	(0.097)	0.042	0.191
38	3.17	1.10	0.256	(0.097)	0.046	0.210
39	3.25	1.10	0.256	(0.097)	0.046	0.210
40	3.33	1.10	0.256	(0.097)	0.046	0.210
41	3.42	1.20	0.279	(0.097)	0.050	0.229
42	3.50	1.30	0.303	(0.097)	0.054	0.248
43	3.58	1.40	0.326	(0.097)	0.059	0.267

44	3.67	1.40	0.326	(0.097)	0.059	0.267
45	3.75	1.50	0.349	(0.097)	0.063	0.286
46	3.83	1.50	0.349	(0.097)	0.063	0.286
47	3.92	1.60	0.373	(0.097)	0.067	0.306
48	4.00	1.60	0.373	(0.097)	0.067	0.306
49	4.08	1.70	0.396	(0.097)	0.071	0.325
50	4.17	1.80	0.419	(0.097)	0.075	0.344
51	4.25	1.90	0.442	(0.097)	0.080	0.363
52	4.33	2.00	0.466	(0.097)	0.084	0.382
53	4.42	2.10	0.489	(0.097)	0.088	0.401
54	4.50	2.10	0.489	(0.097)	0.088	0.401
55	4.58	2.20	0.512	(0.097)	0.092	0.420
56	4.67	2.30	0.536	(0.097)	0.096	0.439
57	4.75	2.40	0.559	0.097	(0.101)	0.462
58	4.83	2.40	0.559	0.097	(0.101)	0.462
59	4.92	2.50	0.582	0.097	(0.105)	0.485
60	5.00	2.60	0.605	0.097	(0.109)	0.508
61	5.08	3.10	0.722	0.097	(0.130)	0.625
62	5.17	3.60	0.838	0.097	(0.151)	0.741
63	5.25	3.90	0.908	0.097	(0.163)	0.811
64	5.33	4.20	0.978	0.097	(0.176)	0.881
65	5.42	4.70	1.094	0.097	(0.197)	0.997
66	5.50	5.60	1.304	0.097	(0.235)	1.207
67	5.58	1.90	0.442	(0.097)	0.080	0.363
68	5.67	0.90	0.210	(0.097)	0.038	0.172
69	5.75	0.60	0.140	(0.097)	0.025	0.115
70	5.83	0.50	0.116	(0.097)	0.021	0.095
71	5.92	0.30	0.070	(0.097)	0.013	0.057
72	6.00	0.20	0.047	(0.097)	0.008	0.038

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.6

Flood volume = Effective rainfall 1.63(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.31(In)
Total soil loss = 0.007(Ac.Ft)
Total rainfall = 1.94(In)
Flood volume = 1718.7 Cubic Feet
Total soil loss = 324.1 Cubic Feet

Peak flow rate of this hydrograph = 0.353(CFS)

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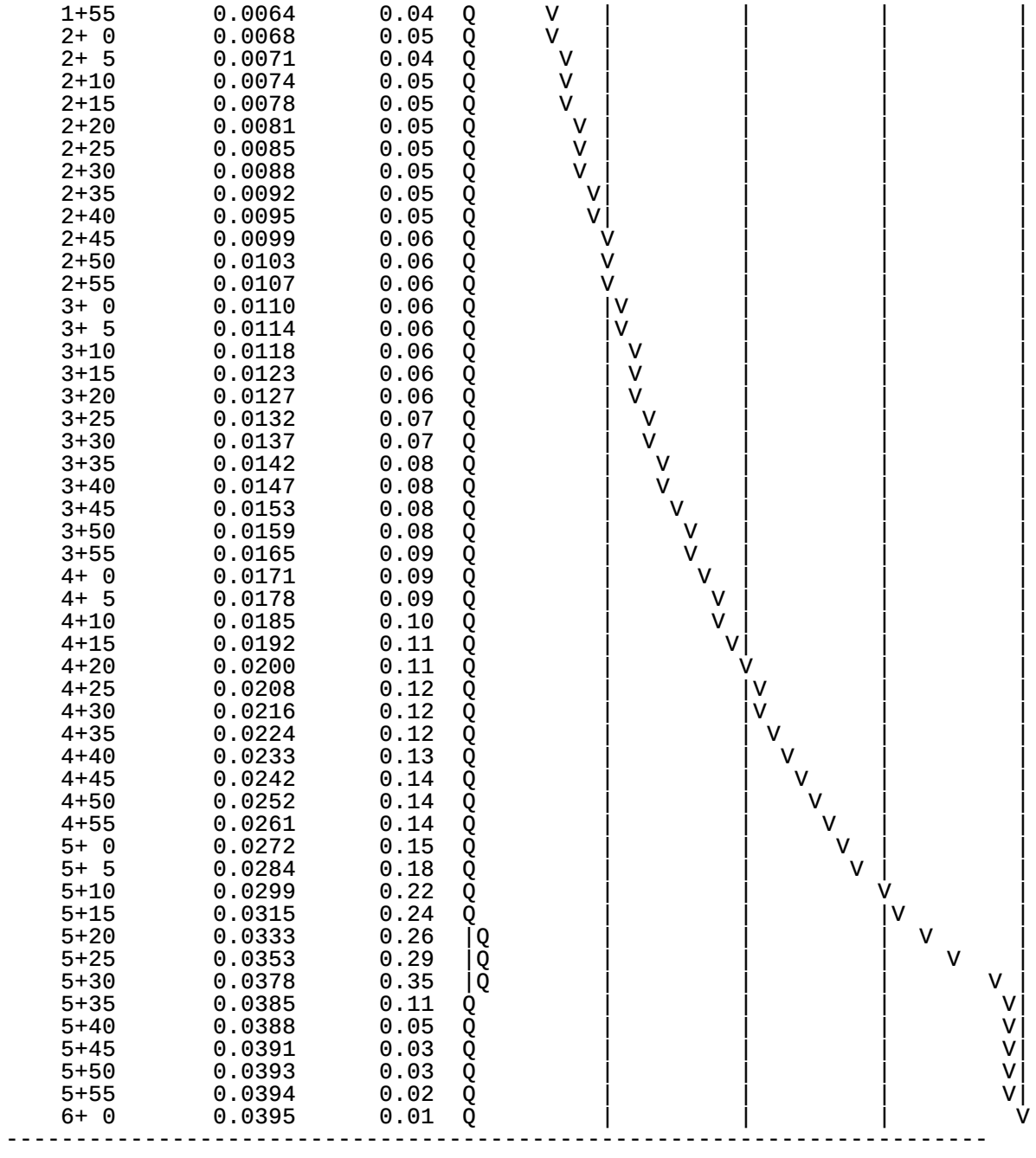
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0002	0.03	Q				
0+10	0.0004	0.03	Q				
0+15	0.0007	0.03	Q				
0+20	0.0009	0.03	Q				
0+25	0.0011	0.03	QV				
0+30	0.0014	0.04	QV				
0+35	0.0017	0.04	QV				
0+40	0.0019	0.04	QV				
0+45	0.0022	0.04	Q V				
0+50	0.0025	0.04	Q V				
0+55	0.0027	0.04	Q V				
1+ 0	0.0030	0.04	Q V				
1+ 5	0.0033	0.04	Q V				
1+10	0.0037	0.04	Q V				
1+15	0.0040	0.04	Q V				
1+20	0.0043	0.04	Q V				
1+25	0.0046	0.04	Q V				
1+30	0.0049	0.04	Q V				
1+35	0.0052	0.04	Q V				
1+40	0.0055	0.04	Q V				
1+45	0.0058	0.04	Q V				
1+50	0.0061	0.04	Q V				


1+55 0.0064 0.04 Q
2+ 0 0.0068 0.05 Q
2+ 5 0.0071 0.04 Q
2+10 0.0074 0.05 Q
2+15 0.0078 0.05 Q
2+20 0.0081 0.05 Q
2+25 0.0085 0.05 Q
2+30 0.0088 0.05 Q
2+35 0.0092 0.05 Q
2+40 0.0095 0.05 Q
2+45 0.0099 0.06 Q
2+50 0.0103 0.06 Q
2+55 0.0107 0.06 Q
3+ 0 0.0110 0.06 Q
3+ 5 0.0114 0.06 Q
3+10 0.0118 0.06 Q
3+15 0.0123 0.06 Q
3+20 0.0127 0.06 Q
3+25 0.0132 0.07 Q
3+30 0.0137 0.07 Q
3+35 0.0142 0.08 Q
3+40 0.0147 0.08 Q
3+45 0.0153 0.08 Q
3+50 0.0159 0.08 Q
3+55 0.0165 0.09 Q
4+ 0 0.0171 0.09 Q
4+ 5 0.0178 0.09 Q
4+10 0.0185 0.10 Q
4+15 0.0192 0.11 Q
4+20 0.0200 0.11 Q
4+25 0.0208 0.12 Q
4+30 0.0216 0.12 Q
4+35 0.0224 0.12 Q
4+40 0.0233 0.13 Q
4+45 0.0242 0.14 Q
4+50 0.0252 0.14 Q
4+55 0.0261 0.14 Q
5+ 0 0.0272 0.15 Q
5+ 5 0.0284 0.18 Q
5+10 0.0299 0.22 Q
5+15 0.0315 0.24 Q
5+20 0.0333 0.26 Q
5+25 0.0353 0.29 Q
5+30 0.0378 0.35 Q
5+35 0.0385 0.11 Q
5+40 0.0388 0.05 Q
5+45 0.0391 0.03 Q
5+50 0.0393 0.03 Q
5+55 0.0394 0.02 Q
6+ 0 0.0395 0.01 Q

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC10310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	0.90	0.26

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	2.35	0.68

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.497(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.497(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	1529.917	100.000	0.292
		Sum = 100.000	Sum= 0.292

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.233	(0.097)	0.042	0.191
2	0.17	1.30	0.233	(0.097)	0.042	0.191
3	0.25	1.10	0.198	(0.097)	0.036	0.162
4	0.33	1.50	0.269	(0.097)	0.048	0.221
5	0.42	1.50	0.269	(0.097)	0.048	0.221
6	0.50	1.80	0.323	(0.097)	0.058	0.265
7	0.58	1.50	0.269	(0.097)	0.048	0.221
8	0.67	1.80	0.323	(0.097)	0.058	0.265
9	0.75	1.80	0.323	(0.097)	0.058	0.265
10	0.83	1.50	0.269	(0.097)	0.048	0.221
11	0.92	1.60	0.287	(0.097)	0.052	0.236
12	1.00	1.80	0.323	(0.097)	0.058	0.265
13	1.08	2.20	0.395	(0.097)	0.071	0.324
14	1.17	2.20	0.395	(0.097)	0.071	0.324
15	1.25	2.20	0.395	(0.097)	0.071	0.324
16	1.33	2.00	0.359	(0.097)	0.065	0.295
17	1.42	2.60	0.467	(0.097)	0.084	0.383
18	1.50	2.70	0.485	(0.097)	0.087	0.398
19	1.58	2.40	0.431	(0.097)	0.078	0.353
20	1.67	2.70	0.485	(0.097)	0.087	0.398
21	1.75	3.30	0.593	0.097	(0.107)	0.496
22	1.83	3.10	0.557	0.097	(0.100)	0.460
23	1.92	2.90	0.521	(0.097)	0.094	0.427
24	2.00	3.00	0.539	(0.097)	0.097	0.442
25	2.08	3.10	0.557	0.097	(0.100)	0.460
26	2.17	4.20	0.754	0.097	(0.136)	0.657
27	2.25	5.00	0.898	0.097	(0.162)	0.801
28	2.33	3.50	0.629	0.097	(0.113)	0.531
29	2.42	6.80	1.221	0.097	(0.220)	1.124
30	2.50	7.30	1.311	0.097	(0.236)	1.214
31	2.58	8.20	1.473	0.097	(0.265)	1.376
32	2.67	5.90	1.060	0.097	(0.191)	0.962
33	2.75	2.00	0.359	(0.097)	0.065	0.295
34	2.83	1.80	0.323	(0.097)	0.058	0.265
35	2.92	1.80	0.323	(0.097)	0.058	0.265
36	3.00	0.60	0.108	(0.097)	0.019	0.088
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	15.4

Flood volume = Effective rainfall 1.28(In)
times area 0.3(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.005(Ac.Ft)
Total rainfall = 1.50(In)

```
      Flood volume =        1349.6 Cubic Feet
      Total soil loss =          225.8 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.402(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ----------------------------------------------------------------------------
   0+ 5       0.0004      0.06  Q         |         |         |         |
   0+10       0.0008      0.06  Q         |         |         |         |
   0+15       0.0011      0.05  QV        |         |         |         |
   0+20       0.0015      0.06  QV        |         |         |         |
   0+25       0.0020      0.06  Q V       |         |         |         |
   0+30       0.0025      0.08  Q  V      |         |         |         |
   0+35       0.0030      0.06  Q  V      |         |         |         |
   0+40       0.0035      0.08  Q   V     |         |         |         |
   0+45       0.0040      0.08  Q    V    |         |         |         |
   0+50       0.0045      0.06  Q    V    |         |         |         |
   0+55       0.0050      0.07  Q     V   |         |         |         |
   1+ 0       0.0055      0.08  Q      V  |         |         |         |
   1+ 5       0.0061      0.09  Q      V  |         |         |         |
   1+10       0.0068      0.09  Q       V |         |         |         |
   1+15       0.0074      0.09  Q        V|         |         |         |
   1+20       0.0080      0.09  Q         V         |         |         |
   1+25       0.0088      0.11  Q         |V        |         |         |
   1+30       0.0096      0.12  Q         | V       |         |         |
   1+35       0.0103      0.10  Q         |  V      |         |         |
   1+40       0.0111      0.12  Q         |   V     |         |         |
   1+45       0.0121      0.14  Q         |    V    |         |         |
   1+50       0.0130      0.13  Q         |     V   |         |         |
   1+55       0.0139      0.12  Q         |      V  |         |         |
   2+ 0       0.0148      0.13  Q         |       V |         |         |
   2+ 5       0.0157      0.13  Q         |        V|         |         |
   2+10       0.0170      0.19  Q         |         | V       |         |
   2+15       0.0187      0.23  Q         |         |  V      |         |
   2+20       0.0197      0.16  Q         |         |   V     |         |
   2+25       0.0220      0.33  |Q        |         |    V    |         |
   2+30       0.0244      0.35  |Q        |         |     V   |         |
   2+35       0.0272      0.40  |Q        |         |      V  |         |
   2+40       0.0291      0.28  |Q        |         |       V |         |
   2+45       0.0297      0.09  Q         |         |        V|         |
   2+50       0.0303      0.08  Q         |         |         V|        |
   2+55       0.0308      0.08  Q         |         |         V|        |
   3+ 0       0.0310      0.03  Q         |         |          V        |
----------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PC10110.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODE 133
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 0.29(Ac.) = 0.000 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.29(Ac.) = 0.000 Sq. Mi.
Length along longest watercourse = 120.00(Ft.)
Length along longest watercourse measured to centroid = 25.00(Ft.)
Length along longest watercourse = 0.023 Mi.
Length along longest watercourse measured to centroid = 0.005 Mi.
Difference in elevation = 1.00(Ft.)
Slope along watercourse = 44.0000 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.005 Hr.
Lag time = 0.33 Min.
25% of lag time = 0.08 Min.
40% of lag time = 0.13 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	0.54	0.16

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.29	1.36	0.39

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.877(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.877(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.290	56.00	0.900

Total Area Entered = 0.29(Ac.)

```
      RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
      AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
      56.0  56.0      0.511     0.900        0.097       1.000      0.097
                                                       Sum (F) =    0.097
      Area averaged mean soil loss (F) (In/Hr) =  0.097
      Minimum soil loss rate ((In/Hr)) =  0.049
      (for 24 hour storm duration)
      Soil low loss rate (decimal) =   0.180
      ------------------------------------------------------------------------
      Slope of intensity-duration curve for a 1 hour storm =0.4800
      ------------------------------------------------------------------------

                    U n i t  H y d r o g r a p h
                           VALLEY S-Curve
      ------------------------------------------------------------------------
                    Unit Hydrograph Data
      ------------------------------------------------------------------------
      Unit time period   Time % of lag   Distribution   Unit Hydrograph
          (hrs)                          Graph %           (CFS)
      ------------------------------------------------------------------------
          1   0.083       1529.917        100.000             0.292
                                    Sum = 100.000   Sum=       0.292
-----------------------------------------------------------------------------


 The following loss rate calculations reflect use of the minimum calculated loss
 rate subtracted from the Storm Rain to produce the maximum Effective Rain value

  Unit Time   Pattern   Storm Rain     Loss rate(In./Hr)     Effective
       (Hr.)  Percent   (In/Hr)          Max   |   Low        (In/Hr)
   1   0.08     4.40      0.463       (  0.097)       0.083        0.380
   2   0.17     4.50      0.474       (  0.097)       0.085        0.388
   3   0.25     5.40      0.569          0.097    (  0.102)        0.471
   4   0.33     5.40      0.569          0.097    (  0.102)        0.471
   5   0.42     5.70      0.600          0.097    (  0.108)        0.503
   6   0.50     6.40      0.674          0.097    (  0.121)        0.577
   7   0.58     7.90      0.832          0.097    (  0.150)        0.735
   8   0.67     9.10      0.958          0.097    (  0.172)        0.861
   9   0.75    12.80      1.348          0.097    (  0.243)        1.251
  10   0.83    25.60      2.695          0.097    (  0.485)        2.598
  11   0.92     7.90      0.832          0.097    (  0.150)        0.735
  12   1.00     4.90      0.516       (  0.097)       0.093        0.423
                (Loss Rate Not Used)
     Sum =     100.0                                  Sum =     9.4
        Flood volume = Effective rainfall      0.78(In)
         times area       0.3(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
        Total soil loss =      0.09(In)
        Total soil loss =     0.002(Ac.Ft)
        Total rainfall =      0.88(In)
        Flood volume =         824.0 Cubic Feet
        Total soil loss =          99.6 Cubic Feet
        ------------------------------------------------------------------
         Peak flow rate of this hydrograph =      0.760(CFS)
        ------------------------------------------------------------------
        ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          1 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
        ------------------------------------------------------------------
                    Hydrograph in   5   Minute intervals ((CFS))

        ------------------------------------------------------------------
  Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
  ----------------------------------------------------------------------
    0+ 5       0.0008      0.11  QV        |         |         |         |
    0+10       0.0015      0.11  Q  V      |         |         |         |
    0+15       0.0025      0.14  Q    V    |         |         |         |
    0+20       0.0034      0.14  Q      V  |         |         |         |
    0+25       0.0045      0.15  Q        V|         |         |         |
    0+30       0.0056      0.17  Q         |V        |         |         |
    0+35       0.0071      0.21  Q         |    V    |         |         |
    0+40       0.0088      0.25  |Q        |       V |         |         |
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   0+45       0.0114      0.37  |Q        |         |   V     |         |
   0+50       0.0166      0.76  |  Q      |         |         |    V    |
   0+55       0.0181      0.21  Q         |         |         |       V |
   1+ 0       0.0189      0.12  Q         |         |         |        V|
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD02242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	2.00	12.14

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	6.40	38.85

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(0.238)	0.003	0.013
2	0.17	0.07	0.016	(0.237)	0.003	0.013
3	0.25	0.07	0.016	(0.236)	0.003	0.013
4	0.33	0.10	0.024	(0.235)	0.004	0.020
5	0.42	0.10	0.024	(0.234)	0.004	0.020
6	0.50	0.10	0.024	(0.233)	0.004	0.020
7	0.58	0.10	0.024	(0.232)	0.004	0.020
8	0.67	0.10	0.024	(0.231)	0.004	0.020
9	0.75	0.10	0.024	(0.230)	0.004	0.020
10	0.83	0.13	0.032	(0.230)	0.006	0.026
11	0.92	0.13	0.032	(0.229)	0.006	0.026
12	1.00	0.13	0.032	(0.228)	0.006	0.026
13	1.08	0.10	0.024	(0.227)	0.004	0.020
14	1.17	0.10	0.024	(0.226)	0.004	0.020
15	1.25	0.10	0.024	(0.225)	0.004	0.020
16	1.33	0.10	0.024	(0.224)	0.004	0.020
17	1.42	0.10	0.024	(0.223)	0.004	0.020
18	1.50	0.10	0.024	(0.222)	0.004	0.020
19	1.58	0.10	0.024	(0.222)	0.004	0.020
20	1.67	0.10	0.024	(0.221)	0.004	0.020
21	1.75	0.10	0.024	(0.220)	0.004	0.020
22	1.83	0.13	0.032	(0.219)	0.006	0.026
23	1.92	0.13	0.032	(0.218)	0.006	0.026
24	2.00	0.13	0.032	(0.217)	0.006	0.026
25	2.08	0.13	0.032	(0.216)	0.006	0.026
26	2.17	0.13	0.032	(0.215)	0.006	0.026
27	2.25	0.13	0.032	(0.214)	0.006	0.026
28	2.33	0.13	0.032	(0.214)	0.006	0.026
29	2.42	0.13	0.032	(0.213)	0.006	0.026
30	2.50	0.13	0.032	(0.212)	0.006	0.026
31	2.58	0.17	0.040	(0.211)	0.007	0.033
32	2.67	0.17	0.040	(0.210)	0.007	0.033
33	2.75	0.17	0.040	(0.209)	0.007	0.033
34	2.83	0.17	0.040	(0.208)	0.007	0.033
35	2.92	0.17	0.040	(0.208)	0.007	0.033
36	3.00	0.17	0.040	(0.207)	0.007	0.033
37	3.08	0.17	0.040	(0.206)	0.007	0.033
38	3.17	0.17	0.040	(0.205)	0.007	0.033
39	3.25	0.17	0.040	(0.204)	0.007	0.033
40	3.33	0.17	0.040	(0.203)	0.007	0.033
41	3.42	0.17	0.040	(0.202)	0.007	0.033
42	3.50	0.17	0.040	(0.202)	0.007	0.033

43	3.58	0.17	0.040	(0.201)	0.007	0.033
44	3.67	0.17	0.040	(0.200)	0.007	0.033
45	3.75	0.17	0.040	(0.199)	0.007	0.033
46	3.83	0.20	0.048	(0.198)	0.009	0.039
47	3.92	0.20	0.048	(0.197)	0.009	0.039
48	4.00	0.20	0.048	(0.197)	0.009	0.039
49	4.08	0.20	0.048	(0.196)	0.009	0.039
50	4.17	0.20	0.048	(0.195)	0.009	0.039
51	4.25	0.20	0.048	(0.194)	0.009	0.039
52	4.33	0.23	0.056	(0.193)	0.010	0.046
53	4.42	0.23	0.056	(0.192)	0.010	0.046
54	4.50	0.23	0.056	(0.192)	0.010	0.046
55	4.58	0.23	0.056	(0.191)	0.010	0.046
56	4.67	0.23	0.056	(0.190)	0.010	0.046
57	4.75	0.23	0.056	(0.189)	0.010	0.046
58	4.83	0.27	0.064	(0.188)	0.012	0.052
59	4.92	0.27	0.064	(0.187)	0.012	0.052
60	5.00	0.27	0.064	(0.187)	0.012	0.052
61	5.08	0.20	0.048	(0.186)	0.009	0.039
62	5.17	0.20	0.048	(0.185)	0.009	0.039
63	5.25	0.20	0.048	(0.184)	0.009	0.039
64	5.33	0.23	0.056	(0.183)	0.010	0.046
65	5.42	0.23	0.056	(0.183)	0.010	0.046
66	5.50	0.23	0.056	(0.182)	0.010	0.046
67	5.58	0.27	0.064	(0.181)	0.012	0.052
68	5.67	0.27	0.064	(0.180)	0.012	0.052
69	5.75	0.27	0.064	(0.179)	0.012	0.052
70	5.83	0.27	0.064	(0.179)	0.012	0.052
71	5.92	0.27	0.064	(0.178)	0.012	0.052
72	6.00	0.27	0.064	(0.177)	0.012	0.052
73	6.08	0.30	0.072	(0.176)	0.013	0.059
74	6.17	0.30	0.072	(0.175)	0.013	0.059
75	6.25	0.30	0.072	(0.175)	0.013	0.059
76	6.33	0.30	0.072	(0.174)	0.013	0.059
77	6.42	0.30	0.072	(0.173)	0.013	0.059
78	6.50	0.30	0.072	(0.172)	0.013	0.059
79	6.58	0.33	0.080	(0.172)	0.014	0.066
80	6.67	0.33	0.080	(0.171)	0.014	0.066
81	6.75	0.33	0.080	(0.170)	0.014	0.066
82	6.83	0.33	0.080	(0.169)	0.014	0.066
83	6.92	0.33	0.080	(0.169)	0.014	0.066
84	7.00	0.33	0.080	(0.168)	0.014	0.066
85	7.08	0.33	0.080	(0.167)	0.014	0.066
86	7.17	0.33	0.080	(0.166)	0.014	0.066
87	7.25	0.33	0.080	(0.165)	0.014	0.066
88	7.33	0.37	0.088	(0.165)	0.016	0.072
89	7.42	0.37	0.088	(0.164)	0.016	0.072
90	7.50	0.37	0.088	(0.163)	0.016	0.072
91	7.58	0.40	0.096	(0.162)	0.017	0.079
92	7.67	0.40	0.096	(0.162)	0.017	0.079
93	7.75	0.40	0.096	(0.161)	0.017	0.079
94	7.83	0.43	0.104	(0.160)	0.019	0.085
95	7.92	0.43	0.104	(0.159)	0.019	0.085
96	8.00	0.43	0.104	(0.159)	0.019	0.085
97	8.08	0.50	0.120	(0.158)	0.022	0.098
98	8.17	0.50	0.120	(0.157)	0.022	0.098
99	8.25	0.50	0.120	(0.157)	0.022	0.098
100	8.33	0.50	0.120	(0.156)	0.022	0.098
101	8.42	0.50	0.120	(0.155)	0.022	0.098
102	8.50	0.50	0.120	(0.154)	0.022	0.098
103	8.58	0.53	0.128	(0.154)	0.023	0.105
104	8.67	0.53	0.128	(0.153)	0.023	0.105
105	8.75	0.53	0.128	(0.152)	0.023	0.105
106	8.83	0.57	0.136	(0.151)	0.024	0.112
107	8.92	0.57	0.136	(0.151)	0.024	0.112
108	9.00	0.57	0.136	(0.150)	0.024	0.112
109	9.08	0.63	0.152	(0.149)	0.027	0.125
110	9.17	0.63	0.152	(0.149)	0.027	0.125
111	9.25	0.63	0.152	(0.148)	0.027	0.125
112	9.33	0.67	0.160	(0.147)	0.029	0.131
113	9.42	0.67	0.160	(0.147)	0.029	0.131
114	9.50	0.67	0.160	(0.146)	0.029	0.131

115	9.58	0.70	0.168	(0.145)	0.030	0.138
116	9.67	0.70	0.168	(0.144)	0.030	0.138
117	9.75	0.70	0.168	(0.144)	0.030	0.138
118	9.83	0.73	0.176	(0.143)	0.032	0.144
119	9.92	0.73	0.176	(0.142)	0.032	0.144
120	10.00	0.73	0.176	(0.142)	0.032	0.144
121	10.08	0.50	0.120	(0.141)	0.022	0.098
122	10.17	0.50	0.120	(0.140)	0.022	0.098
123	10.25	0.50	0.120	(0.140)	0.022	0.098
124	10.33	0.50	0.120	(0.139)	0.022	0.098
125	10.42	0.50	0.120	(0.138)	0.022	0.098
126	10.50	0.50	0.120	(0.138)	0.022	0.098
127	10.58	0.67	0.160	(0.137)	0.029	0.131
128	10.67	0.67	0.160	(0.136)	0.029	0.131
129	10.75	0.67	0.160	(0.136)	0.029	0.131
130	10.83	0.67	0.160	(0.135)	0.029	0.131
131	10.92	0.67	0.160	(0.134)	0.029	0.131
132	11.00	0.67	0.160	(0.134)	0.029	0.131
133	11.08	0.63	0.152	(0.133)	0.027	0.125
134	11.17	0.63	0.152	(0.132)	0.027	0.125
135	11.25	0.63	0.152	(0.132)	0.027	0.125
136	11.33	0.63	0.152	(0.131)	0.027	0.125
137	11.42	0.63	0.152	(0.130)	0.027	0.125
138	11.50	0.63	0.152	(0.130)	0.027	0.125
139	11.58	0.57	0.136	(0.129)	0.024	0.112
140	11.67	0.57	0.136	(0.128)	0.024	0.112
141	11.75	0.57	0.136	(0.128)	0.024	0.112
142	11.83	0.60	0.144	(0.127)	0.026	0.118
143	11.92	0.60	0.144	(0.126)	0.026	0.118
144	12.00	0.60	0.144	(0.126)	0.026	0.118
145	12.08	0.83	0.200	(0.125)	0.036	0.164
146	12.17	0.83	0.200	(0.125)	0.036	0.164
147	12.25	0.83	0.200	(0.124)	0.036	0.164
148	12.33	0.87	0.208	(0.123)	0.037	0.171
149	12.42	0.87	0.208	(0.123)	0.037	0.171
150	12.50	0.87	0.208	(0.122)	0.037	0.171
151	12.58	0.93	0.224	(0.121)	0.040	0.184
152	12.67	0.93	0.224	(0.121)	0.040	0.184
153	12.75	0.93	0.224	(0.120)	0.040	0.184
154	12.83	0.97	0.232	(0.120)	0.042	0.190
155	12.92	0.97	0.232	(0.119)	0.042	0.190
156	13.00	0.97	0.232	(0.118)	0.042	0.190
157	13.08	1.13	0.272	(0.118)	0.049	0.223
158	13.17	1.13	0.272	(0.117)	0.049	0.223
159	13.25	1.13	0.272	(0.117)	0.049	0.223
160	13.33	1.13	0.272	(0.116)	0.049	0.223
161	13.42	1.13	0.272	(0.115)	0.049	0.223
162	13.50	1.13	0.272	(0.115)	0.049	0.223
163	13.58	0.77	0.184	(0.114)	0.033	0.151
164	13.67	0.77	0.184	(0.114)	0.033	0.151
165	13.75	0.77	0.184	(0.113)	0.033	0.151
166	13.83	0.77	0.184	(0.113)	0.033	0.151
167	13.92	0.77	0.184	(0.112)	0.033	0.151
168	14.00	0.77	0.184	(0.111)	0.033	0.151
169	14.08	0.90	0.216	(0.111)	0.039	0.177
170	14.17	0.90	0.216	(0.110)	0.039	0.177
171	14.25	0.90	0.216	(0.110)	0.039	0.177
172	14.33	0.87	0.208	(0.109)	0.037	0.171
173	14.42	0.87	0.208	(0.109)	0.037	0.171
174	14.50	0.87	0.208	(0.108)	0.037	0.171
175	14.58	0.87	0.208	(0.107)	0.037	0.171
176	14.67	0.87	0.208	(0.107)	0.037	0.171
177	14.75	0.87	0.208	(0.106)	0.037	0.171
178	14.83	0.83	0.200	(0.106)	0.036	0.164
179	14.92	0.83	0.200	(0.105)	0.036	0.164
180	15.00	0.83	0.200	(0.105)	0.036	0.164
181	15.08	0.80	0.192	(0.104)	0.035	0.157
182	15.17	0.80	0.192	(0.104)	0.035	0.157
183	15.25	0.80	0.192	(0.103)	0.035	0.157
184	15.33	0.77	0.184	(0.103)	0.033	0.151
185	15.42	0.77	0.184	(0.102)	0.033	0.151
186	15.50	0.77	0.184	(0.102)	0.033	0.151

187	15.58	0.63	0.152	(0.101)	0.027	0.125
188	15.67	0.63	0.152	(0.101)	0.027	0.125
189	15.75	0.63	0.152	(0.100)	0.027	0.125
190	15.83	0.63	0.152	(0.100)	0.027	0.125
191	15.92	0.63	0.152	(0.099)	0.027	0.125
192	16.00	0.63	0.152	(0.099)	0.027	0.125
193	16.08	0.13	0.032	(0.098)	0.006	0.026
194	16.17	0.13	0.032	(0.098)	0.006	0.026
195	16.25	0.13	0.032	(0.097)	0.006	0.026
196	16.33	0.13	0.032	(0.097)	0.006	0.026
197	16.42	0.13	0.032	(0.096)	0.006	0.026
198	16.50	0.13	0.032	(0.096)	0.006	0.026
199	16.58	0.10	0.024	(0.095)	0.004	0.020
200	16.67	0.10	0.024	(0.095)	0.004	0.020
201	16.75	0.10	0.024	(0.094)	0.004	0.020
202	16.83	0.10	0.024	(0.094)	0.004	0.020
203	16.92	0.10	0.024	(0.093)	0.004	0.020
204	17.00	0.10	0.024	(0.093)	0.004	0.020
205	17.08	0.17	0.040	(0.092)	0.007	0.033
206	17.17	0.17	0.040	(0.092)	0.007	0.033
207	17.25	0.17	0.040	(0.091)	0.007	0.033
208	17.33	0.17	0.040	(0.091)	0.007	0.033
209	17.42	0.17	0.040	(0.090)	0.007	0.033
210	17.50	0.17	0.040	(0.090)	0.007	0.033
211	17.58	0.17	0.040	(0.089)	0.007	0.033
212	17.67	0.17	0.040	(0.089)	0.007	0.033
213	17.75	0.17	0.040	(0.089)	0.007	0.033
214	17.83	0.13	0.032	(0.088)	0.006	0.026
215	17.92	0.13	0.032	(0.088)	0.006	0.026
216	18.00	0.13	0.032	(0.087)	0.006	0.026
217	18.08	0.13	0.032	(0.087)	0.006	0.026
218	18.17	0.13	0.032	(0.086)	0.006	0.026
219	18.25	0.13	0.032	(0.086)	0.006	0.026
220	18.33	0.13	0.032	(0.086)	0.006	0.026
221	18.42	0.13	0.032	(0.085)	0.006	0.026
222	18.50	0.13	0.032	(0.085)	0.006	0.026
223	18.58	0.10	0.024	(0.084)	0.004	0.020
224	18.67	0.10	0.024	(0.084)	0.004	0.020
225	18.75	0.10	0.024	(0.084)	0.004	0.020
226	18.83	0.07	0.016	(0.083)	0.003	0.013
227	18.92	0.07	0.016	(0.083)	0.003	0.013
228	19.00	0.07	0.016	(0.082)	0.003	0.013
229	19.08	0.10	0.024	(0.082)	0.004	0.020
230	19.17	0.10	0.024	(0.082)	0.004	0.020
231	19.25	0.10	0.024	(0.081)	0.004	0.020
232	19.33	0.13	0.032	(0.081)	0.006	0.026
233	19.42	0.13	0.032	(0.080)	0.006	0.026
234	19.50	0.13	0.032	(0.080)	0.006	0.026
235	19.58	0.10	0.024	(0.080)	0.004	0.020
236	19.67	0.10	0.024	(0.079)	0.004	0.020
237	19.75	0.10	0.024	(0.079)	0.004	0.020
238	19.83	0.07	0.016	(0.079)	0.003	0.013
239	19.92	0.07	0.016	(0.078)	0.003	0.013
240	20.00	0.07	0.016	(0.078)	0.003	0.013
241	20.08	0.10	0.024	(0.078)	0.004	0.020
242	20.17	0.10	0.024	(0.077)	0.004	0.020
243	20.25	0.10	0.024	(0.077)	0.004	0.020
244	20.33	0.10	0.024	(0.077)	0.004	0.020
245	20.42	0.10	0.024	(0.076)	0.004	0.020
246	20.50	0.10	0.024	(0.076)	0.004	0.020
247	20.58	0.10	0.024	(0.076)	0.004	0.020
248	20.67	0.10	0.024	(0.075)	0.004	0.020
249	20.75	0.10	0.024	(0.075)	0.004	0.020
250	20.83	0.07	0.016	(0.075)	0.003	0.013
251	20.92	0.07	0.016	(0.074)	0.003	0.013
252	21.00	0.07	0.016	(0.074)	0.003	0.013
253	21.08	0.10	0.024	(0.074)	0.004	0.020
254	21.17	0.10	0.024	(0.073)	0.004	0.020
255	21.25	0.10	0.024	(0.073)	0.004	0.020
256	21.33	0.07	0.016	(0.073)	0.003	0.013
257	21.42	0.07	0.016	(0.073)	0.003	0.013
258	21.50	0.07	0.016	(0.072)	0.003	0.013

259	21.58	0.10	0.024	(0.072)	0.004	0.020
260	21.67	0.10	0.024	(0.072)	0.004	0.020
261	21.75	0.10	0.024	(0.072)	0.004	0.020
262	21.83	0.07	0.016	(0.071)	0.003	0.013
263	21.92	0.07	0.016	(0.071)	0.003	0.013
264	22.00	0.07	0.016	(0.071)	0.003	0.013
265	22.08	0.10	0.024	(0.071)	0.004	0.020
266	22.17	0.10	0.024	(0.070)	0.004	0.020
267	22.25	0.10	0.024	(0.070)	0.004	0.020
268	22.33	0.07	0.016	(0.070)	0.003	0.013
269	22.42	0.07	0.016	(0.070)	0.003	0.013
270	22.50	0.07	0.016	(0.069)	0.003	0.013
271	22.58	0.07	0.016	(0.069)	0.003	0.013
272	22.67	0.07	0.016	(0.069)	0.003	0.013
273	22.75	0.07	0.016	(0.069)	0.003	0.013
274	22.83	0.07	0.016	(0.069)	0.003	0.013
275	22.92	0.07	0.016	(0.069)	0.003	0.013
276	23.00	0.07	0.016	(0.068)	0.003	0.013
277	23.08	0.07	0.016	(0.068)	0.003	0.013
278	23.17	0.07	0.016	(0.068)	0.003	0.013
279	23.25	0.07	0.016	(0.068)	0.003	0.013
280	23.33	0.07	0.016	(0.068)	0.003	0.013
281	23.42	0.07	0.016	(0.068)	0.003	0.013
282	23.50	0.07	0.016	(0.068)	0.003	0.013
283	23.58	0.07	0.016	(0.067)	0.003	0.013
284	23.67	0.07	0.016	(0.067)	0.003	0.013
285	23.75	0.07	0.016	(0.067)	0.003	0.013
286	23.83	0.07	0.016	(0.067)	0.003	0.013
287	23.92	0.07	0.016	(0.067)	0.003	0.013
288	24.00	0.07	0.016	(0.067)	0.003	0.013

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.7

Flood volume = Effective rainfall 1.64(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.8(Ac.Ft)
Total soil loss = 0.36(In)
Total soil loss = 0.182(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 36135.5 Cubic Feet
Total soil loss = 7932.2 Cubic Feet

Peak flow rate of this hydrograph = 1.365(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0004	0.06	Q	|	|	|	|
0+10	0.0010	0.08	Q	|	|	|	|
0+15	0.0015	0.08	Q	|	|	|	|
0+20	0.0023	0.11	Q	|	|	|	|
0+25	0.0031	0.12	Q	|	|	|	|
0+30	0.0039	0.12	Q	|	|	|	|
0+35	0.0048	0.12	Q	|	|	|	|
0+40	0.0056	0.12	Q	|	|	|	|
0+45	0.0064	0.12	Q	|	|	|	|
0+50	0.0075	0.15	Q	|	|	|	|
0+55	0.0086	0.16	Q	|	|	|	|
1+ 0	0.0097	0.16	Q	|	|	|	|
1+ 5	0.0106	0.13	Q	|	|	|	|
1+10	0.0114	0.12	Q	|	|	|	|
1+15	0.0122	0.12	Q	|	|	|	|
1+20	0.0131	0.12	Q	|	|	|	|
1+25	0.0139	0.12	Q	|	|	|	|
1+30	0.0147	0.12	Q	|	|	|	|
1+35	0.0156	0.12	Q	|	|	|	|
1+40	0.0164	0.12	Q	|	|	|	|
1+45	0.0172	0.12	Q	|	|	|	|

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1+50       0.0182      0.15  Q         |          |          |          |
1+55       0.0194      0.16  Q         |          |          |          |
2+ 0       0.0205      0.16  Q         |          |          |          |
2+ 5       0.0216      0.16  QV        |          |          |          |
2+10       0.0227      0.16  QV        |          |          |          |
2+15       0.0238      0.16  QV        |          |          |          |
2+20       0.0249      0.16  QV        |          |          |          |
2+25       0.0260      0.16  QV        |          |          |          |
2+30       0.0271      0.16  QV        |          |          |          |
2+35       0.0284      0.19  QV        |          |          |          |
2+40       0.0298      0.20  QV        |          |          |          |
2+45       0.0312      0.20  QV        |          |          |          |
2+50       0.0326      0.20  QV        |          |          |          |
2+55       0.0339      0.20  QV        |          |          |          |
3+ 0       0.0353      0.20  QV        |          |          |          |
3+ 5       0.0367      0.20  QV        |          |          |          |
3+10       0.0381      0.20  QV        |          |          |          |
3+15       0.0395      0.20  QV        |          |          |          |
3+20       0.0408      0.20  QV        |          |          |          |
3+25       0.0422      0.20  Q V       |          |          |          |
3+30       0.0436      0.20  Q V       |          |          |          |
3+35       0.0450      0.20  Q V       |          |          |          |
3+40       0.0464      0.20  Q V       |          |          |          |
3+45       0.0478      0.20  Q V       |          |          |          |
3+50       0.0494      0.23  Q V       |          |          |          |
3+55       0.0510      0.24  Q V       |          |          |          |
4+ 0       0.0527      0.24  Q V       |          |          |          |
4+ 5       0.0543      0.24  Q V       |          |          |          |
4+10       0.0560      0.24  Q V       |          |          |          |
4+15       0.0576      0.24  Q V       |          |          |          |
4+20       0.0595      0.27  |QV       |          |          |          |
4+25       0.0614      0.28  |QV       |          |          |          |
4+30       0.0634      0.28  |Q V      |          |          |          |
4+35       0.0653      0.28  |Q V      |          |          |          |
4+40       0.0673      0.28  |Q V      |          |          |          |
4+45       0.0692      0.28  |Q V      |          |          |          |
4+50       0.0713      0.31  |Q V      |          |          |          |
4+55       0.0735      0.32  |Q V      |          |          |          |
5+ 0       0.0758      0.32  |Q V      |          |          |          |
5+ 5       0.0776      0.26  |Q V      |          |          |          |
5+10       0.0792      0.24  Q  V      |          |          |          |
5+15       0.0809      0.24  Q  V      |          |          |          |
5+20       0.0827      0.27  |Q V      |          |          |          |
5+25       0.0847      0.28  |Q  V     |          |          |          |
5+30       0.0866      0.28  |Q  V     |          |          |          |
5+35       0.0888      0.31  |Q  V     |          |          |          |
5+40       0.0910      0.32  |Q  V     |          |          |          |
5+45       0.0932      0.32  |Q  V     |          |          |          |
5+50       0.0954      0.32  |Q  V     |          |          |          |
5+55       0.0976      0.32  |Q  V     |          |          |          |
6+ 0       0.0998      0.32  |Q  V     |          |          |          |
6+ 5       0.1022      0.35  |Q  V     |          |          |          |
6+10       0.1047      0.36  |Q   V    |          |          |          |
6+15       0.1072      0.36  |Q   V    |          |          |          |
6+20       0.1097      0.36  |Q   V    |          |          |          |
6+25       0.1122      0.36  |Q   V    |          |          |          |
6+30       0.1147      0.36  |Q   V    |          |          |          |
6+35       0.1174      0.39  |Q   V    |          |          |          |
6+40       0.1201      0.40  |Q   V    |          |          |          |
6+45       0.1229      0.40  |Q   V    |          |          |          |
6+50       0.1257      0.40  |Q    V   |          |          |          |
6+55       0.1284      0.40  |Q    V   |          |          |          |
7+ 0       0.1312      0.40  |Q    V   |          |          |          |
7+ 5       0.1340      0.40  |Q    V   |          |          |          |
7+10       0.1367      0.40  |Q    V   |          |          |          |
7+15       0.1395      0.40  |Q    V   |          |          |          |
7+20       0.1425      0.43  |Q    V   |          |          |          |
7+25       0.1455      0.44  |Q     V  |          |          |          |
7+30       0.1485      0.44  |Q     V  |          |          |          |
7+35       0.1518      0.47  |Q     V  |          |          |          |
7+40       0.1551      0.48  |Q     V  |          |          |          |
7+45       0.1584      0.48  |Q     V  |          |          |          |
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7+50	0.1620	0.51	Q V				
7+55	0.1656	0.52	Q V				
8+ 0	0.1691	0.52	Q V				
8+ 5	0.1732	0.58	Q V				
8+10	0.1773	0.60	Q V				
8+15	0.1814	0.60	Q V				
8+20	0.1856	0.60	Q V				
8+25	0.1897	0.60	Q V				
8+30	0.1939	0.60	Q V				
8+35	0.1982	0.63	Q V				
8+40	0.2027	0.64	Q V				
8+45	0.2071	0.64	Q V				
8+50	0.2117	0.67	Q V				
8+55	0.2164	0.68	Q V				
9+ 0	0.2211	0.68	Q V				
9+ 5	0.2262	0.74	Q V				
9+10	0.2315	0.76	Q V				
9+15	0.2367	0.76	Q V				
9+20	0.2422	0.79	Q V				
9+25	0.2477	0.80	Q V				
9+30	0.2533	0.80	Q V				
9+35	0.2590	0.83	Q V				
9+40	0.2648	0.84	Q V				
9+45	0.2706	0.84	Q V				
9+50	0.2766	0.87	Q V				
9+55	0.2827	0.88	Q V				
10+ 0	0.2888	0.88	Q V				
10+ 5	0.2934	0.67	Q V				
10+10	0.2976	0.60	Q V				
10+15	0.3017	0.60	Q V				
10+20	0.3059	0.60	Q V				
10+25	0.3100	0.60	Q V				
10+30	0.3142	0.60	Q V				
10+35	0.3194	0.75	Q V				
10+40	0.3249	0.80	Q V				
10+45	0.3304	0.80	Q V				
10+50	0.3359	0.80	Q V				
10+55	0.3415	0.80	Q V				
11+ 0	0.3470	0.80	Q V				
11+ 5	0.3523	0.77	Q V				
11+10	0.3576	0.76	Q V				
11+15	0.3628	0.76	Q V				
11+20	0.3681	0.76	Q V				
11+25	0.3733	0.76	Q V				
11+30	0.3786	0.76	Q V				
11+35	0.3834	0.70	Q V				
11+40	0.3881	0.68	Q V				
11+45	0.3928	0.68	Q V				
11+50	0.3978	0.71	Q V				
11+55	0.4027	0.72	Q V				
12+ 0	0.4077	0.72	Q V				
12+ 5	0.4141	0.93	Q V				
12+10	0.4210	1.00	Q V				
12+15	0.4280	1.00	Q V				
12+20	0.4351	1.03	Q V				
12+25	0.4423	1.04	Q V				
12+30	0.4495	1.04	Q V				
12+35	0.4571	1.10	Q V				
12+40	0.4648	1.12	Q V				
12+45	0.4725	1.12	Q V				
12+50	0.4805	1.15	Q V				
12+55	0.4885	1.16	Q V				
13+ 0	0.4965	1.16	Q V				
13+ 5	0.5056	1.31	Q V				
13+10	0.5150	1.37	Q V				
13+15	0.5244	1.37	Q V				
13+20	0.5338	1.37	Q V				
13+25	0.5432	1.37	Q V				
13+30	0.5526	1.37	Q V				
13+35	0.5597	1.04	Q V				
13+40	0.5661	0.92	Q V				
13+45	0.5724	0.92	Q V				

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13+50       0.5788      0.92  |  Q       |          |       V  |          |
13+55       0.5852      0.92  |  Q       |          |        V |          |
14+ 0       0.5915      0.92  |  Q       |          |        V |          |
14+ 5       0.5987      1.04  |   Q      |          |        V |          |
14+10       0.6062      1.08  |   Q      |          |         V|          |
14+15       0.6136      1.08  |   Q      |          |         V|          |
14+20       0.6209      1.05  |   Q      |          |         V|          |
14+25       0.6281      1.04  |   Q      |          |          V          |
14+30       0.6353      1.04  |   Q      |          |          V          |
14+35       0.6425      1.04  |   Q      |          |          V          |
14+40       0.6496      1.04  |   Q      |          |          |V         |
14+45       0.6568      1.04  |   Q      |          |          |V         |
14+50       0.6638      1.01  |   Q      |          |          | V        |
14+55       0.6707      1.00  |   Q      |          |          | V        |
15+ 0       0.6776      1.00  |   Q      |          |          | V        |
15+ 5       0.6844      0.97  |  Q       |          |          | V        |
15+10       0.6910      0.96  |  Q       |          |          |  V       |
15+15       0.6976      0.96  |  Q       |          |          |  V       |
15+20       0.7041      0.93  |  Q       |          |          |  V       |
15+25       0.7104      0.92  |  Q       |          |          |   V      |
15+30       0.7168      0.92  |  Q       |          |          |   V      |
15+35       0.7223      0.80  |  Q       |          |          |   V      |
15+40       0.7276      0.76  |  Q       |          |          |    V     |
15+45       0.7328      0.76  |  Q       |          |          |    V     |
15+50       0.7381      0.76  |  Q       |          |          |    V     |
15+55       0.7433      0.76  |  Q       |          |          |    V     |
16+ 0       0.7486      0.76  |  Q       |          |          |     V    |
16+ 5       0.7507      0.31  |Q         |          |          |     V    |
16+10       0.7519      0.16  Q          |          |          |     V    |
16+15       0.7530      0.16  Q          |          |          |     V    |
16+20       0.7541      0.16  Q          |          |          |     V    |
16+25       0.7552      0.16  Q          |          |          |     V    |
16+30       0.7563      0.16  Q          |          |          |     V    |
16+35       0.7572      0.13  Q          |          |          |     V    |
16+40       0.7580      0.12  Q          |          |          |     V    |
16+45       0.7588      0.12  Q          |          |          |     V    |
16+50       0.7597      0.12  Q          |          |          |     V    |
16+55       0.7605      0.12  Q          |          |          |     V    |
17+ 0       0.7613      0.12  Q          |          |          |     V    |
17+ 5       0.7626      0.18  Q          |          |          |     V    |
17+10       0.7639      0.20  Q          |          |          |     V    |
17+15       0.7653      0.20  Q          |          |          |     V    |
17+20       0.7667      0.20  Q          |          |          |     V    |
17+25       0.7681      0.20  Q          |          |          |      V   |
17+30       0.7695      0.20  Q          |          |          |      V   |
17+35       0.7709      0.20  Q          |          |          |      V   |
17+40       0.7722      0.20  Q          |          |          |      V   |
17+45       0.7736      0.20  Q          |          |          |      V   |
17+50       0.7748      0.17  Q          |          |          |      V   |
17+55       0.7759      0.16  Q          |          |          |      V   |
18+ 0       0.7770      0.16  Q          |          |          |      V   |
18+ 5       0.7781      0.16  Q          |          |          |      V   |
18+10       0.7792      0.16  Q          |          |          |      V   |
18+15       0.7803      0.16  Q          |          |          |      V   |
18+20       0.7814      0.16  Q          |          |          |      V   |
18+25       0.7825      0.16  Q          |          |          |      V   |
18+30       0.7836      0.16  Q          |          |          |      V   |
18+35       0.7845      0.13  Q          |          |          |      V   |
18+40       0.7854      0.12  Q          |          |          |      V   |
18+45       0.7862      0.12  Q          |          |          |      V   |
18+50       0.7868      0.09  Q          |          |          |      V   |
18+55       0.7874      0.08  Q          |          |          |      V   |
19+ 0       0.7879      0.08  Q          |          |          |      V   |
19+ 5       0.7887      0.11  Q          |          |          |       V  |
19+10       0.7895      0.12  Q          |          |          |       V  |
19+15       0.7904      0.12  Q          |          |          |       V  |
19+20       0.7914      0.15  Q          |          |          |       V  |
19+25       0.7925      0.16  Q          |          |          |       V  |
19+30       0.7936      0.16  Q          |          |          |       V  |
19+35       0.7945      0.13  Q          |          |          |       V  |
19+40       0.7953      0.12  Q          |          |          |       V  |
19+45       0.7962      0.12  Q          |          |          |       V  |
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  19+50       0.7968      0.09  Q          |          |          |        V |
  19+55       0.7973      0.08  Q          |          |          |        V |
  20+ 0       0.7979      0.08  Q          |          |          |        V |
  20+ 5       0.7987      0.11  Q          |          |          |        V |
  20+10       0.7995      0.12  Q          |          |          |        V |
  20+15       0.8003      0.12  Q          |          |          |        V |
  20+20       0.8011      0.12  Q          |          |          |        V |
  20+25       0.8020      0.12  Q          |          |          |        V |
  20+30       0.8028      0.12  Q          |          |          |        V |
  20+35       0.8036      0.12  Q          |          |          |        V |
  20+40       0.8045      0.12  Q          |          |          |        V |
  20+45       0.8053      0.12  Q          |          |          |        V |
  20+50       0.8059      0.09  Q          |          |          |        V |
  20+55       0.8065      0.08  Q          |          |          |        V |
  21+ 0       0.8070      0.08  Q          |          |          |        V |
  21+ 5       0.8078      0.11  Q          |          |          |        V |
  21+10       0.8086      0.12  Q          |          |          |        V |
  21+15       0.8094      0.12  Q          |          |          |         V|
  21+20       0.8101      0.09  Q          |          |          |         V|
  21+25       0.8106      0.08  Q          |          |          |         V|
  21+30       0.8112      0.08  Q          |          |          |         V|
  21+35       0.8119      0.11  Q          |          |          |         V|
  21+40       0.8128      0.12  Q          |          |          |         V|
  21+45       0.8136      0.12  Q          |          |          |         V|
  21+50       0.8142      0.09  Q          |          |          |         V|
  21+55       0.8148      0.08  Q          |          |          |         V|
  22+ 0       0.8153      0.08  Q          |          |          |         V|
  22+ 5       0.8161      0.11  Q          |          |          |         V|
  22+10       0.8169      0.12  Q          |          |          |         V|
  22+15       0.8177      0.12  Q          |          |          |         V|
  22+20       0.8184      0.09  Q          |          |          |         V|
  22+25       0.8189      0.08  Q          |          |          |         V|
  22+30       0.8195      0.08  Q          |          |          |         V|
  22+35       0.8200      0.08  Q          |          |          |         V|
  22+40       0.8206      0.08  Q          |          |          |         V|
  22+45       0.8211      0.08  Q          |          |          |         V|
  22+50       0.8217      0.08  Q          |          |          |         V|
  22+55       0.8222      0.08  Q          |          |          |         V|
  23+ 0       0.8228      0.08  Q          |          |          |         V|
  23+ 5       0.8233      0.08  Q          |          |          |         V|
  23+10       0.8239      0.08  Q          |          |          |         V|
  23+15       0.8244      0.08  Q          |          |          |         V|
  23+20       0.8250      0.08  Q          |          |          |         V|
  23+25       0.8255      0.08  Q          |          |          |         V|
  23+30       0.8261      0.08  Q          |          |          |         V|
  23+35       0.8267      0.08  Q          |          |          |         V|
  23+40       0.8272      0.08  Q          |          |          |         V|
  23+45       0.8278      0.08  Q          |          |          |         V|
  23+50       0.8283      0.08  Q          |          |          |         V|
  23+55       0.8289      0.08  Q          |          |          |         V|
  24+ 0       0.8294      0.08  Q          |          |          |         V|
  24+ 5       0.8296      0.02  Q          |          |          |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD0262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	1.20	7.28

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	3.00	18.21

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.200(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.072	(0.134)	0.013	0.059
2	0.17	0.60	0.086	(0.134)	0.016	0.071
3	0.25	0.60	0.086	(0.134)	0.016	0.071
4	0.33	0.60	0.086	(0.134)	0.016	0.071
5	0.42	0.60	0.086	(0.134)	0.016	0.071
6	0.50	0.70	0.101	(0.134)	0.018	0.083
7	0.58	0.70	0.101	(0.134)	0.018	0.083
8	0.67	0.70	0.101	(0.134)	0.018	0.083
9	0.75	0.70	0.101	(0.134)	0.018	0.083
10	0.83	0.70	0.101	(0.134)	0.018	0.083
11	0.92	0.70	0.101	(0.134)	0.018	0.083
12	1.00	0.80	0.115	(0.134)	0.021	0.094
13	1.08	0.80	0.115	(0.134)	0.021	0.094
14	1.17	0.80	0.115	(0.134)	0.021	0.094
15	1.25	0.80	0.115	(0.134)	0.021	0.094
16	1.33	0.80	0.115	(0.134)	0.021	0.094
17	1.42	0.80	0.115	(0.134)	0.021	0.094
18	1.50	0.80	0.115	(0.134)	0.021	0.094
19	1.58	0.80	0.115	(0.134)	0.021	0.094
20	1.67	0.80	0.115	(0.134)	0.021	0.094
21	1.75	0.80	0.115	(0.134)	0.021	0.094
22	1.83	0.80	0.115	(0.134)	0.021	0.094
23	1.92	0.80	0.115	(0.134)	0.021	0.094
24	2.00	0.90	0.130	(0.134)	0.023	0.106
25	2.08	0.80	0.115	(0.134)	0.021	0.094
26	2.17	0.90	0.130	(0.134)	0.023	0.106
27	2.25	0.90	0.130	(0.134)	0.023	0.106
28	2.33	0.90	0.130	(0.134)	0.023	0.106
29	2.42	0.90	0.130	(0.134)	0.023	0.106
30	2.50	0.90	0.130	(0.134)	0.023	0.106
31	2.58	0.90	0.130	(0.134)	0.023	0.106
32	2.67	0.90	0.130	(0.134)	0.023	0.106
33	2.75	1.00	0.144	(0.134)	0.026	0.118
34	2.83	1.00	0.144	(0.134)	0.026	0.118
35	2.92	1.00	0.144	(0.134)	0.026	0.118
36	3.00	1.00	0.144	(0.134)	0.026	0.118
37	3.08	1.00	0.144	(0.134)	0.026	0.118
38	3.17	1.10	0.158	(0.134)	0.029	0.130
39	3.25	1.10	0.158	(0.134)	0.029	0.130
40	3.33	1.10	0.158	(0.134)	0.029	0.130
41	3.42	1.20	0.173	(0.134)	0.031	0.142
42	3.50	1.30	0.187	(0.134)	0.034	0.154

43	3.58	1.40	0.202	(0.134)	0.036	0.165
44	3.67	1.40	0.202	(0.134)	0.036	0.165
45	3.75	1.50	0.216	(0.134)	0.039	0.177
46	3.83	1.50	0.216	(0.134)	0.039	0.177
47	3.92	1.60	0.230	(0.134)	0.041	0.189
48	4.00	1.60	0.230	(0.134)	0.041	0.189
49	4.08	1.70	0.245	(0.134)	0.044	0.201
50	4.17	1.80	0.259	(0.134)	0.047	0.213
51	4.25	1.90	0.274	(0.134)	0.049	0.224
52	4.33	2.00	0.288	(0.134)	0.052	0.236
53	4.42	2.10	0.302	(0.134)	0.054	0.248
54	4.50	2.10	0.302	(0.134)	0.054	0.248
55	4.58	2.20	0.317	(0.134)	0.057	0.260
56	4.67	2.30	0.331	(0.134)	0.060	0.272
57	4.75	2.40	0.346	(0.134)	0.062	0.283
58	4.83	2.40	0.346	(0.134)	0.062	0.283
59	4.92	2.50	0.360	(0.134)	0.065	0.295
60	5.00	2.60	0.374	(0.134)	0.067	0.307
61	5.08	3.10	0.446	(0.134)	0.080	0.366
62	5.17	3.60	0.518	(0.134)	0.093	0.425
63	5.25	3.90	0.562	(0.134)	0.101	0.461
64	5.33	4.20	0.605	(0.134)	0.109	0.496
65	5.42	4.70	0.677	(0.134)	0.122	0.555
66	5.50	5.60	0.806	0.134	(0.145)	0.672
67	5.58	1.90	0.274	(0.134)	0.049	0.224
68	5.67	0.90	0.130	(0.134)	0.023	0.106
69	5.75	0.60	0.086	(0.134)	0.016	0.071
70	5.83	0.50	0.072	(0.134)	0.013	0.059
71	5.92	0.30	0.043	(0.134)	0.008	0.035
72	6.00	0.20	0.029	(0.134)	0.005	0.024

(Loss Rate Not Used)

Sum = 100.0 Sum = 11.8

Flood volume = Effective rainfall 0.98(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.22(In)
Total soil loss = 0.109(Ac.Ft)
Total rainfall = 1.20(In)
Flood volume = 21701.3 Cubic Feet
Total soil loss = 4739.1 Cubic Feet

Peak flow rate of this hydrograph = 3.932(CFS)

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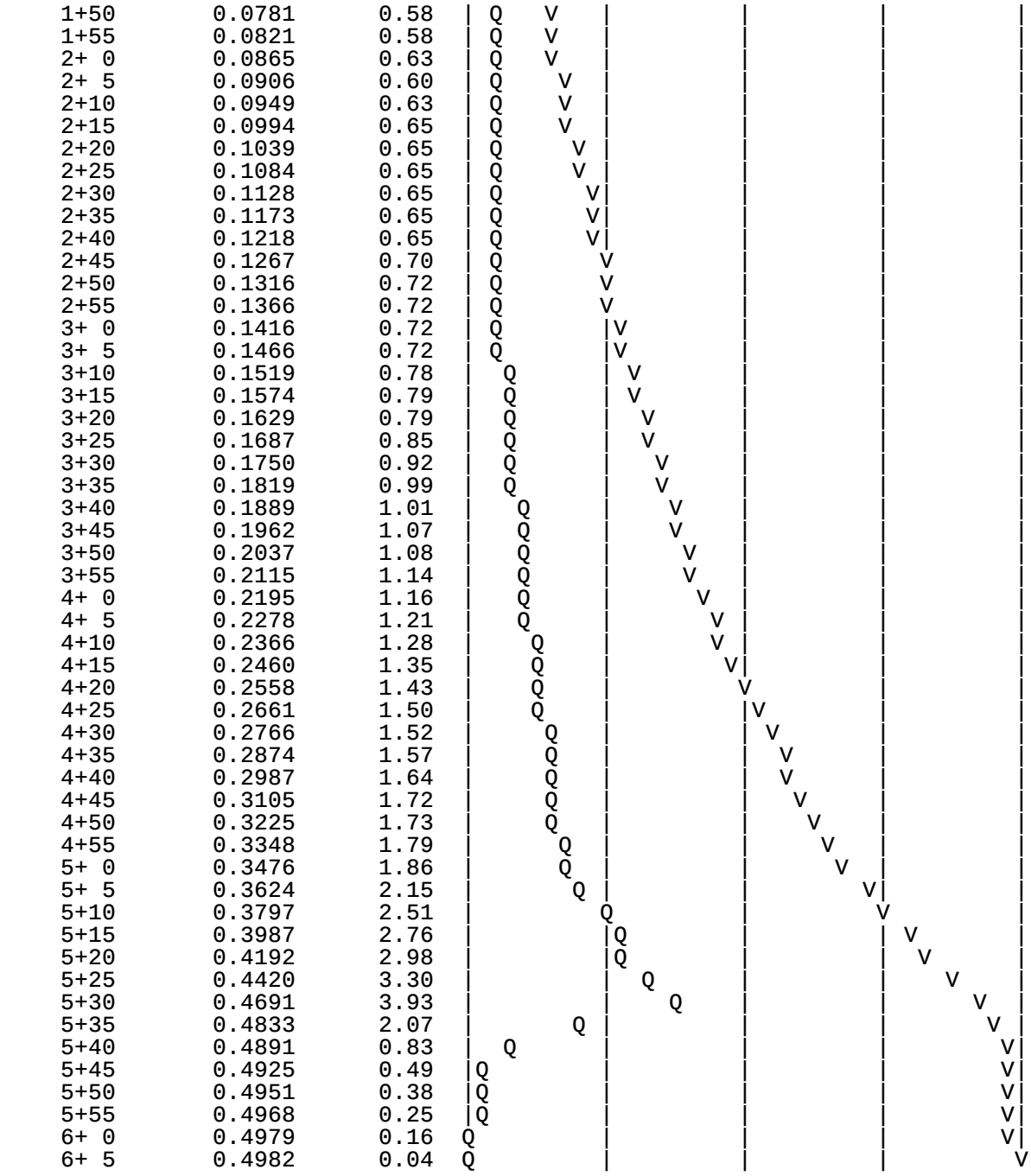
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0019	0.27	VQ				
0+10	0.0047	0.42	VQ				
0+15	0.0077	0.43	VQ				
0+20	0.0107	0.43	VQ				
0+25	0.0137	0.43	|Q				
0+30	0.0170	0.49	|Q				
0+35	0.0205	0.51	|VQ				
0+40	0.0240	0.51	|VQ				
0+45	0.0275	0.51	| Q				
0+50	0.0310	0.51	| Q				
0+55	0.0345	0.51	| Q				
1+ 0	0.0383	0.56	| QV				
1+ 5	0.0423	0.58	| QV				
1+10	0.0463	0.58	| QV				
1+15	0.0503	0.58	| Q V				
1+20	0.0542	0.58	| Q V				
1+25	0.0582	0.58	| Q V				
1+30	0.0622	0.58	| Q V				
1+35	0.0662	0.58	| Q V				
1+40	0.0702	0.58	| Q V				
1+45	0.0741	0.58	| Q V				


1+50 0.0781 0.58
1+55 0.0821 0.58
2+ 0 0.0865 0.63
2+ 5 0.0906 0.60
2+10 0.0949 0.63
2+15 0.0994 0.65
2+20 0.1039 0.65
2+25 0.1084 0.65
2+30 0.1128 0.65
2+35 0.1173 0.65
2+40 0.1218 0.65
2+45 0.1267 0.70
2+50 0.1316 0.72
2+55 0.1366 0.72
3+ 0 0.1416 0.72
3+ 5 0.1466 0.72
3+10 0.1519 0.78
3+15 0.1574 0.79
3+20 0.1629 0.79
3+25 0.1687 0.85
3+30 0.1750 0.92
3+35 0.1819 0.99
3+40 0.1889 1.01
3+45 0.1962 1.07
3+50 0.2037 1.08
3+55 0.2115 1.14
4+ 0 0.2195 1.16
4+ 5 0.2278 1.21
4+10 0.2366 1.28
4+15 0.2460 1.35
4+20 0.2558 1.43
4+25 0.2661 1.50
4+30 0.2766 1.52
4+35 0.2874 1.57
4+40 0.2987 1.64
4+45 0.3105 1.72
4+50 0.3225 1.73
4+55 0.3348 1.79
5+ 0 0.3476 1.86
5+ 5 0.3624 2.15
5+10 0.3797 2.51
5+15 0.3987 2.76
5+20 0.4192 2.98
5+25 0.4420 3.30
5+30 0.4691 3.93
5+35 0.4833 2.07
5+40 0.4891 0.83
5+45 0.4925 0.49
5+50 0.4951 0.38
5+55 0.4968 0.25
6+ 0 0.4979 0.16
6+ 5 0.4982 0.04

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD0232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	0.90	5.46

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	2.35	14.26

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 0.900(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.900(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	1.30	0.140	(0.134)		0.025	0.115
2	0.17	1.30	0.140	(0.134)		0.025	0.115
3	0.25	1.10	0.119	(0.134)		0.021	0.097
4	0.33	1.50	0.162	(0.134)		0.029	0.133
5	0.42	1.50	0.162	(0.134)		0.029	0.133
6	0.50	1.80	0.194	(0.134)		0.035	0.159
7	0.58	1.50	0.162	(0.134)		0.029	0.133
8	0.67	1.80	0.194	(0.134)		0.035	0.159
9	0.75	1.80	0.194	(0.134)		0.035	0.159
10	0.83	1.50	0.162	(0.134)		0.029	0.133
11	0.92	1.60	0.173	(0.134)		0.031	0.142
12	1.00	1.80	0.194	(0.134)		0.035	0.159
13	1.08	2.20	0.238	(0.134)		0.043	0.195
14	1.17	2.20	0.238	(0.134)		0.043	0.195
15	1.25	2.20	0.238	(0.134)		0.043	0.195
16	1.33	2.00	0.216	(0.134)		0.039	0.177
17	1.42	2.60	0.281	(0.134)		0.051	0.230
18	1.50	2.70	0.292	(0.134)		0.052	0.239
19	1.58	2.40	0.259	(0.134)		0.047	0.213
20	1.67	2.70	0.292	(0.134)		0.052	0.239
21	1.75	3.30	0.356	(0.134)		0.064	0.292
22	1.83	3.10	0.335	(0.134)		0.060	0.275
23	1.92	2.90	0.313	(0.134)		0.056	0.257
24	2.00	3.00	0.324	(0.134)		0.058	0.266
25	2.08	3.10	0.335	(0.134)		0.060	0.275
26	2.17	4.20	0.454	(0.134)		0.082	0.372
27	2.25	5.00	0.540	(0.134)		0.097	0.443
28	2.33	3.50	0.378	(0.134)		0.068	0.310
29	2.42	6.80	0.734	(0.134)		0.132	0.602
30	2.50	7.30	0.788	0.134	(	0.142)	0.654
31	2.58	8.20	0.886	0.134	(	0.159)	0.751
32	2.67	5.90	0.637	(0.134)		0.115	0.522
33	2.75	2.00	0.216	(0.134)		0.039	0.177
34	2.83	1.80	0.194	(0.134)		0.035	0.159
35	2.92	1.80	0.194	(0.134)		0.035	0.159
36	3.00	0.60	0.065	(0.134)		0.012	0.053
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	8.9

Flood volume = Effective rainfall 0.74(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.16(In)
Total soil loss = 0.081(Ac.Ft)

Total rainfall = 0.90(In)
Flood volume = 16321.4 Cubic Feet
Total soil loss = 3508.8 Cubic Feet

Peak flow rate of this hydrograph = 4.448(CFS)

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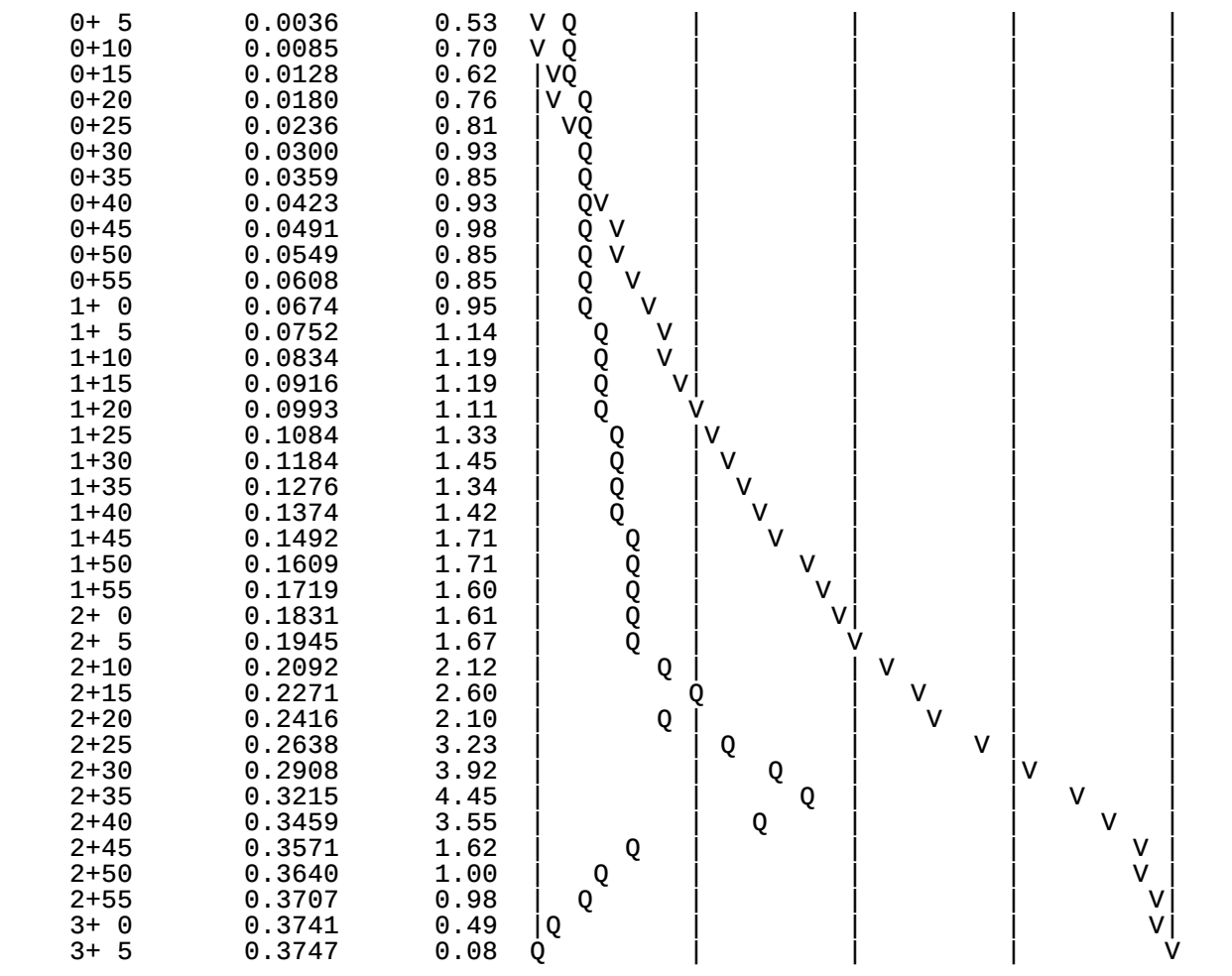
3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))



U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD0212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
2-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	0.54	3.28

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	1.36	8.26

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.540(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.540(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	582.319	74.564	4.561
2	0.167	1164.637	25.436	1.556
		Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.285	(0.134)	0.051	0.234
2	0.17	4.50	0.292	(0.134)	0.052	0.239
3	0.25	5.40	0.350	(0.134)	0.063	0.287
4	0.33	5.40	0.350	(0.134)	0.063	0.287
5	0.42	5.70	0.369	(0.134)	0.066	0.303
6	0.50	6.40	0.415	(0.134)	0.075	0.340
7	0.58	7.90	0.512	(0.134)	0.092	0.420
8	0.67	9.10	0.590	(0.134)	0.106	0.484
9	0.75	12.80	0.829	0.134	(0.149)	0.695
10	0.83	25.60	1.659	0.134	(0.299)	1.525
11	0.92	7.90	0.512	(0.134)	0.092	0.420
12	1.00	4.90	0.318	(0.134)	0.057	0.260
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.5

Flood volume = Effective rainfall 0.46(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.08(In)
Total soil loss = 0.042(Ac.Ft)
Total rainfall = 0.54(In)
Flood volume = 10085.9 Cubic Feet
Total soil loss = 1811.8 Cubic Feet

Peak flow rate of this hydrograph = 8.041(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0073	1.07	|V Q				
0+10	0.0174	1.46		V Q				
0+15	0.0290	1.68		VQ				
0+20	0.0410	1.76		Q				
0+25	0.0536	1.83		Q V				
0+30	0.0676	2.02		Q |V			
0+35	0.0844	2.45		Q| V			

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   0+40       0.1041      2.86  |          |Q     V  |          |          |
   0+45       0.1312      3.93  |          |    Q    | V        |          |
   0+50       0.1865      8.04  |          |         |          | Q        |
   0+55       0.2161      4.29  |          |       Q |          |       V  |
   1+ 0       0.2287      1.84  |       Q  |         |          |         V|
   1+ 5       0.2315      0.41  |Q         |         |          |         V|
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD05245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	2.00	12.14

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	6.40	38.85

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.031(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.031(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.024	(0.238)	0.004	0.020
2	0.17	0.07	0.024	(0.237)	0.004	0.020
3	0.25	0.07	0.024	(0.236)	0.004	0.020
4	0.33	0.10	0.036	(0.235)	0.007	0.030
5	0.42	0.10	0.036	(0.234)	0.007	0.030
6	0.50	0.10	0.036	(0.233)	0.007	0.030
7	0.58	0.10	0.036	(0.232)	0.007	0.030
8	0.67	0.10	0.036	(0.231)	0.007	0.030
9	0.75	0.10	0.036	(0.230)	0.007	0.030
10	0.83	0.13	0.048	(0.230)	0.009	0.040
11	0.92	0.13	0.048	(0.229)	0.009	0.040
12	1.00	0.13	0.048	(0.228)	0.009	0.040
13	1.08	0.10	0.036	(0.227)	0.007	0.030
14	1.17	0.10	0.036	(0.226)	0.007	0.030
15	1.25	0.10	0.036	(0.225)	0.007	0.030
16	1.33	0.10	0.036	(0.224)	0.007	0.030
17	1.42	0.10	0.036	(0.223)	0.007	0.030
18	1.50	0.10	0.036	(0.222)	0.007	0.030
19	1.58	0.10	0.036	(0.222)	0.007	0.030
20	1.67	0.10	0.036	(0.221)	0.007	0.030
21	1.75	0.10	0.036	(0.220)	0.007	0.030
22	1.83	0.13	0.048	(0.219)	0.009	0.040
23	1.92	0.13	0.048	(0.218)	0.009	0.040
24	2.00	0.13	0.048	(0.217)	0.009	0.040
25	2.08	0.13	0.048	(0.216)	0.009	0.040
26	2.17	0.13	0.048	(0.215)	0.009	0.040
27	2.25	0.13	0.048	(0.214)	0.009	0.040
28	2.33	0.13	0.048	(0.214)	0.009	0.040
29	2.42	0.13	0.048	(0.213)	0.009	0.040
30	2.50	0.13	0.048	(0.212)	0.009	0.040
31	2.58	0.17	0.061	(0.211)	0.011	0.050
32	2.67	0.17	0.061	(0.210)	0.011	0.050
33	2.75	0.17	0.061	(0.209)	0.011	0.050
34	2.83	0.17	0.061	(0.208)	0.011	0.050
35	2.92	0.17	0.061	(0.208)	0.011	0.050
36	3.00	0.17	0.061	(0.207)	0.011	0.050
37	3.08	0.17	0.061	(0.206)	0.011	0.050
38	3.17	0.17	0.061	(0.205)	0.011	0.050
39	3.25	0.17	0.061	(0.204)	0.011	0.050
40	3.33	0.17	0.061	(0.203)	0.011	0.050
41	3.42	0.17	0.061	(0.202)	0.011	0.050
42	3.50	0.17	0.061	(0.202)	0.011	0.050

43	3.58	0.17	0.061	(0.201)	0.011	0.050
44	3.67	0.17	0.061	(0.200)	0.011	0.050
45	3.75	0.17	0.061	(0.199)	0.011	0.050
46	3.83	0.20	0.073	(0.198)	0.013	0.060
47	3.92	0.20	0.073	(0.197)	0.013	0.060
48	4.00	0.20	0.073	(0.197)	0.013	0.060
49	4.08	0.20	0.073	(0.196)	0.013	0.060
50	4.17	0.20	0.073	(0.195)	0.013	0.060
51	4.25	0.20	0.073	(0.194)	0.013	0.060
52	4.33	0.23	0.085	(0.193)	0.015	0.070
53	4.42	0.23	0.085	(0.192)	0.015	0.070
54	4.50	0.23	0.085	(0.192)	0.015	0.070
55	4.58	0.23	0.085	(0.191)	0.015	0.070
56	4.67	0.23	0.085	(0.190)	0.015	0.070
57	4.75	0.23	0.085	(0.189)	0.015	0.070
58	4.83	0.27	0.097	(0.188)	0.017	0.080
59	4.92	0.27	0.097	(0.187)	0.017	0.080
60	5.00	0.27	0.097	(0.187)	0.017	0.080
61	5.08	0.20	0.073	(0.186)	0.013	0.060
62	5.17	0.20	0.073	(0.185)	0.013	0.060
63	5.25	0.20	0.073	(0.184)	0.013	0.060
64	5.33	0.23	0.085	(0.183)	0.015	0.070
65	5.42	0.23	0.085	(0.183)	0.015	0.070
66	5.50	0.23	0.085	(0.182)	0.015	0.070
67	5.58	0.27	0.097	(0.181)	0.017	0.080
68	5.67	0.27	0.097	(0.180)	0.017	0.080
69	5.75	0.27	0.097	(0.179)	0.017	0.080
70	5.83	0.27	0.097	(0.179)	0.017	0.080
71	5.92	0.27	0.097	(0.178)	0.017	0.080
72	6.00	0.27	0.097	(0.177)	0.017	0.080
73	6.08	0.30	0.109	(0.176)	0.020	0.089
74	6.17	0.30	0.109	(0.175)	0.020	0.089
75	6.25	0.30	0.109	(0.175)	0.020	0.089
76	6.33	0.30	0.109	(0.174)	0.020	0.089
77	6.42	0.30	0.109	(0.173)	0.020	0.089
78	6.50	0.30	0.109	(0.172)	0.020	0.089
79	6.58	0.33	0.121	(0.172)	0.022	0.099
80	6.67	0.33	0.121	(0.171)	0.022	0.099
81	6.75	0.33	0.121	(0.170)	0.022	0.099
82	6.83	0.33	0.121	(0.169)	0.022	0.099
83	6.92	0.33	0.121	(0.169)	0.022	0.099
84	7.00	0.33	0.121	(0.168)	0.022	0.099
85	7.08	0.33	0.121	(0.167)	0.022	0.099
86	7.17	0.33	0.121	(0.166)	0.022	0.099
87	7.25	0.33	0.121	(0.165)	0.022	0.099
88	7.33	0.37	0.133	(0.165)	0.024	0.109
89	7.42	0.37	0.133	(0.164)	0.024	0.109
90	7.50	0.37	0.133	(0.163)	0.024	0.109
91	7.58	0.40	0.145	(0.162)	0.026	0.119
92	7.67	0.40	0.145	(0.162)	0.026	0.119
93	7.75	0.40	0.145	(0.161)	0.026	0.119
94	7.83	0.43	0.158	(0.160)	0.028	0.129
95	7.92	0.43	0.158	(0.159)	0.028	0.129
96	8.00	0.43	0.158	(0.159)	0.028	0.129
97	8.08	0.50	0.182	(0.158)	0.033	0.149
98	8.17	0.50	0.182	(0.157)	0.033	0.149
99	8.25	0.50	0.182	(0.157)	0.033	0.149
100	8.33	0.50	0.182	(0.156)	0.033	0.149
101	8.42	0.50	0.182	(0.155)	0.033	0.149
102	8.50	0.50	0.182	(0.154)	0.033	0.149
103	8.58	0.53	0.194	(0.154)	0.035	0.159
104	8.67	0.53	0.194	(0.153)	0.035	0.159
105	8.75	0.53	0.194	(0.152)	0.035	0.159
106	8.83	0.57	0.206	(0.151)	0.037	0.169
107	8.92	0.57	0.206	(0.151)	0.037	0.169
108	9.00	0.57	0.206	(0.150)	0.037	0.169
109	9.08	0.63	0.230	(0.149)	0.041	0.189
110	9.17	0.63	0.230	(0.149)	0.041	0.189
111	9.25	0.63	0.230	(0.148)	0.041	0.189
112	9.33	0.67	0.242	(0.147)	0.044	0.199
113	9.42	0.67	0.242	(0.147)	0.044	0.199
114	9.50	0.67	0.242	(0.146)	0.044	0.199

115	9.58	0.70	0.255	(0.145)	0.046	0.209
116	9.67	0.70	0.255	(0.144)	0.046	0.209
117	9.75	0.70	0.255	(0.144)	0.046	0.209
118	9.83	0.73	0.267	(0.143)	0.048	0.219
119	9.92	0.73	0.267	(0.142)	0.048	0.219
120	10.00	0.73	0.267	(0.142)	0.048	0.219
121	10.08	0.50	0.182	(0.141)	0.033	0.149
122	10.17	0.50	0.182	(0.140)	0.033	0.149
123	10.25	0.50	0.182	(0.140)	0.033	0.149
124	10.33	0.50	0.182	(0.139)	0.033	0.149
125	10.42	0.50	0.182	(0.138)	0.033	0.149
126	10.50	0.50	0.182	(0.138)	0.033	0.149
127	10.58	0.67	0.242	(0.137)	0.044	0.199
128	10.67	0.67	0.242	(0.136)	0.044	0.199
129	10.75	0.67	0.242	(0.136)	0.044	0.199
130	10.83	0.67	0.242	(0.135)	0.044	0.199
131	10.92	0.67	0.242	(0.134)	0.044	0.199
132	11.00	0.67	0.242	(0.134)	0.044	0.199
133	11.08	0.63	0.230	(0.133)	0.041	0.189
134	11.17	0.63	0.230	(0.132)	0.041	0.189
135	11.25	0.63	0.230	(0.132)	0.041	0.189
136	11.33	0.63	0.230	(0.131)	0.041	0.189
137	11.42	0.63	0.230	(0.130)	0.041	0.189
138	11.50	0.63	0.230	(0.130)	0.041	0.189
139	11.58	0.57	0.206	(0.129)	0.037	0.169
140	11.67	0.57	0.206	(0.128)	0.037	0.169
141	11.75	0.57	0.206	(0.128)	0.037	0.169
142	11.83	0.60	0.218	(0.127)	0.039	0.179
143	11.92	0.60	0.218	(0.126)	0.039	0.179
144	12.00	0.60	0.218	(0.126)	0.039	0.179
145	12.08	0.83	0.303	(0.125)	0.055	0.249
146	12.17	0.83	0.303	(0.125)	0.055	0.249
147	12.25	0.83	0.303	(0.124)	0.055	0.249
148	12.33	0.87	0.315	(0.123)	0.057	0.258
149	12.42	0.87	0.315	(0.123)	0.057	0.258
150	12.50	0.87	0.315	(0.122)	0.057	0.258
151	12.58	0.93	0.339	(0.121)	0.061	0.278
152	12.67	0.93	0.339	(0.121)	0.061	0.278
153	12.75	0.93	0.339	(0.120)	0.061	0.278
154	12.83	0.97	0.352	(0.120)	0.063	0.288
155	12.92	0.97	0.352	(0.119)	0.063	0.288
156	13.00	0.97	0.352	(0.118)	0.063	0.288
157	13.08	1.13	0.412	(0.118)	0.074	0.338
158	13.17	1.13	0.412	(0.117)	0.074	0.338
159	13.25	1.13	0.412	(0.117)	0.074	0.338
160	13.33	1.13	0.412	(0.116)	0.074	0.338
161	13.42	1.13	0.412	(0.115)	0.074	0.338
162	13.50	1.13	0.412	(0.115)	0.074	0.338
163	13.58	0.77	0.279	(0.114)	0.050	0.229
164	13.67	0.77	0.279	(0.114)	0.050	0.229
165	13.75	0.77	0.279	(0.113)	0.050	0.229
166	13.83	0.77	0.279	(0.113)	0.050	0.229
167	13.92	0.77	0.279	(0.112)	0.050	0.229
168	14.00	0.77	0.279	(0.111)	0.050	0.229
169	14.08	0.90	0.327	(0.111)	0.059	0.268
170	14.17	0.90	0.327	(0.110)	0.059	0.268
171	14.25	0.90	0.327	(0.110)	0.059	0.268
172	14.33	0.87	0.315	(0.109)	0.057	0.258
173	14.42	0.87	0.315	(0.109)	0.057	0.258
174	14.50	0.87	0.315	(0.108)	0.057	0.258
175	14.58	0.87	0.315	(0.107)	0.057	0.258
176	14.67	0.87	0.315	(0.107)	0.057	0.258
177	14.75	0.87	0.315	(0.106)	0.057	0.258
178	14.83	0.83	0.303	(0.106)	0.055	0.249
179	14.92	0.83	0.303	(0.105)	0.055	0.249
180	15.00	0.83	0.303	(0.105)	0.055	0.249
181	15.08	0.80	0.291	(0.104)	0.052	0.239
182	15.17	0.80	0.291	(0.104)	0.052	0.239
183	15.25	0.80	0.291	(0.103)	0.052	0.239
184	15.33	0.77	0.279	(0.103)	0.050	0.229
185	15.42	0.77	0.279	(0.102)	0.050	0.229
186	15.50	0.77	0.279	(0.102)	0.050	0.229

187	15.58	0.63	0.230	(0.101)	0.041	0.189
188	15.67	0.63	0.230	(0.101)	0.041	0.189
189	15.75	0.63	0.230	(0.100)	0.041	0.189
190	15.83	0.63	0.230	(0.100)	0.041	0.189
191	15.92	0.63	0.230	(0.099)	0.041	0.189
192	16.00	0.63	0.230	(0.099)	0.041	0.189
193	16.08	0.13	0.048	(0.098)	0.009	0.040
194	16.17	0.13	0.048	(0.098)	0.009	0.040
195	16.25	0.13	0.048	(0.097)	0.009	0.040
196	16.33	0.13	0.048	(0.097)	0.009	0.040
197	16.42	0.13	0.048	(0.096)	0.009	0.040
198	16.50	0.13	0.048	(0.096)	0.009	0.040
199	16.58	0.10	0.036	(0.095)	0.007	0.030
200	16.67	0.10	0.036	(0.095)	0.007	0.030
201	16.75	0.10	0.036	(0.094)	0.007	0.030
202	16.83	0.10	0.036	(0.094)	0.007	0.030
203	16.92	0.10	0.036	(0.093)	0.007	0.030
204	17.00	0.10	0.036	(0.093)	0.007	0.030
205	17.08	0.17	0.061	(0.092)	0.011	0.050
206	17.17	0.17	0.061	(0.092)	0.011	0.050
207	17.25	0.17	0.061	(0.091)	0.011	0.050
208	17.33	0.17	0.061	(0.091)	0.011	0.050
209	17.42	0.17	0.061	(0.090)	0.011	0.050
210	17.50	0.17	0.061	(0.090)	0.011	0.050
211	17.58	0.17	0.061	(0.089)	0.011	0.050
212	17.67	0.17	0.061	(0.089)	0.011	0.050
213	17.75	0.17	0.061	(0.089)	0.011	0.050
214	17.83	0.13	0.048	(0.088)	0.009	0.040
215	17.92	0.13	0.048	(0.088)	0.009	0.040
216	18.00	0.13	0.048	(0.087)	0.009	0.040
217	18.08	0.13	0.048	(0.087)	0.009	0.040
218	18.17	0.13	0.048	(0.086)	0.009	0.040
219	18.25	0.13	0.048	(0.086)	0.009	0.040
220	18.33	0.13	0.048	(0.086)	0.009	0.040
221	18.42	0.13	0.048	(0.085)	0.009	0.040
222	18.50	0.13	0.048	(0.085)	0.009	0.040
223	18.58	0.10	0.036	(0.084)	0.007	0.030
224	18.67	0.10	0.036	(0.084)	0.007	0.030
225	18.75	0.10	0.036	(0.084)	0.007	0.030
226	18.83	0.07	0.024	(0.083)	0.004	0.020
227	18.92	0.07	0.024	(0.083)	0.004	0.020
228	19.00	0.07	0.024	(0.082)	0.004	0.020
229	19.08	0.10	0.036	(0.082)	0.007	0.030
230	19.17	0.10	0.036	(0.082)	0.007	0.030
231	19.25	0.10	0.036	(0.081)	0.007	0.030
232	19.33	0.13	0.048	(0.081)	0.009	0.040
233	19.42	0.13	0.048	(0.080)	0.009	0.040
234	19.50	0.13	0.048	(0.080)	0.009	0.040
235	19.58	0.10	0.036	(0.080)	0.007	0.030
236	19.67	0.10	0.036	(0.079)	0.007	0.030
237	19.75	0.10	0.036	(0.079)	0.007	0.030
238	19.83	0.07	0.024	(0.079)	0.004	0.020
239	19.92	0.07	0.024	(0.078)	0.004	0.020
240	20.00	0.07	0.024	(0.078)	0.004	0.020
241	20.08	0.10	0.036	(0.078)	0.007	0.030
242	20.17	0.10	0.036	(0.077)	0.007	0.030
243	20.25	0.10	0.036	(0.077)	0.007	0.030
244	20.33	0.10	0.036	(0.077)	0.007	0.030
245	20.42	0.10	0.036	(0.076)	0.007	0.030
246	20.50	0.10	0.036	(0.076)	0.007	0.030
247	20.58	0.10	0.036	(0.076)	0.007	0.030
248	20.67	0.10	0.036	(0.075)	0.007	0.030
249	20.75	0.10	0.036	(0.075)	0.007	0.030
250	20.83	0.07	0.024	(0.075)	0.004	0.020
251	20.92	0.07	0.024	(0.074)	0.004	0.020
252	21.00	0.07	0.024	(0.074)	0.004	0.020
253	21.08	0.10	0.036	(0.074)	0.007	0.030
254	21.17	0.10	0.036	(0.073)	0.007	0.030
255	21.25	0.10	0.036	(0.073)	0.007	0.030
256	21.33	0.07	0.024	(0.073)	0.004	0.020
257	21.42	0.07	0.024	(0.073)	0.004	0.020
258	21.50	0.07	0.024	(0.072)	0.004	0.020

259	21.58	0.10	0.036	(0.072)	0.007	0.030
260	21.67	0.10	0.036	(0.072)	0.007	0.030
261	21.75	0.10	0.036	(0.072)	0.007	0.030
262	21.83	0.07	0.024	(0.071)	0.004	0.020
263	21.92	0.07	0.024	(0.071)	0.004	0.020
264	22.00	0.07	0.024	(0.071)	0.004	0.020
265	22.08	0.10	0.036	(0.071)	0.007	0.030
266	22.17	0.10	0.036	(0.070)	0.007	0.030
267	22.25	0.10	0.036	(0.070)	0.007	0.030
268	22.33	0.07	0.024	(0.070)	0.004	0.020
269	22.42	0.07	0.024	(0.070)	0.004	0.020
270	22.50	0.07	0.024	(0.069)	0.004	0.020
271	22.58	0.07	0.024	(0.069)	0.004	0.020
272	22.67	0.07	0.024	(0.069)	0.004	0.020
273	22.75	0.07	0.024	(0.069)	0.004	0.020
274	22.83	0.07	0.024	(0.069)	0.004	0.020
275	22.92	0.07	0.024	(0.069)	0.004	0.020
276	23.00	0.07	0.024	(0.068)	0.004	0.020
277	23.08	0.07	0.024	(0.068)	0.004	0.020
278	23.17	0.07	0.024	(0.068)	0.004	0.020
279	23.25	0.07	0.024	(0.068)	0.004	0.020
280	23.33	0.07	0.024	(0.068)	0.004	0.020
281	23.42	0.07	0.024	(0.068)	0.004	0.020
282	23.50	0.07	0.024	(0.068)	0.004	0.020
283	23.58	0.07	0.024	(0.067)	0.004	0.020
284	23.67	0.07	0.024	(0.067)	0.004	0.020
285	23.75	0.07	0.024	(0.067)	0.004	0.020
286	23.83	0.07	0.024	(0.067)	0.004	0.020
287	23.92	0.07	0.024	(0.067)	0.004	0.020
288	24.00	0.07	0.024	(0.067)	0.004	0.020

(Loss Rate Not Used)

Sum = 100.0 Sum = 29.8

Flood volume = Effective rainfall 2.49(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 1.3(Ac.Ft)
Total soil loss = 0.55(In)
Total soil loss = 0.276(Ac.Ft)
Total rainfall = 3.03(In)
Flood volume = 54755.9 Cubic Feet
Total soil loss = 12019.6 Cubic Feet

Peak flow rate of this hydrograph = 2.069(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0006	0.09	Q	|	|	|	|
0+10	0.0015	0.12	Q	|	|	|	|
0+15	0.0023	0.12	Q	|	|	|	|
0+20	0.0035	0.17	Q	|	|	|	|
0+25	0.0047	0.18	Q	|	|	|	|
0+30	0.0060	0.18	Q	|	|	|	|
0+35	0.0072	0.18	Q	|	|	|	|
0+40	0.0085	0.18	Q	|	|	|	|
0+45	0.0097	0.18	Q	|	|	|	|
0+50	0.0113	0.23	Q	|	|	|	|
0+55	0.0130	0.24	Q	|	|	|	|
1+ 0	0.0147	0.24	Q	|	|	|	|
1+ 5	0.0160	0.20	Q	|	|	|	|
1+10	0.0173	0.18	Q	|	|	|	|
1+15	0.0185	0.18	Q	|	|	|	|
1+20	0.0198	0.18	Q	|	|	|	|
1+25	0.0210	0.18	Q	|	|	|	|
1+30	0.0223	0.18	Q	|	|	|	|
1+35	0.0236	0.18	Q	|	|	|	|
1+40	0.0248	0.18	Q	|	|	|	|
1+45	0.0261	0.18	Q	|	|	|	|

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1+50       0.0276      0.23  Q          |          |          |          |
1+55       0.0293      0.24  Q          |          |          |          |
2+ 0       0.0310      0.24  Q          |          |          |          |
2+ 5       0.0327      0.24  QV         |          |          |          |
2+10       0.0344      0.24  QV         |          |          |          |
2+15       0.0360      0.24  QV         |          |          |          |
2+20       0.0377      0.24  QV         |          |          |          |
2+25       0.0394      0.24  QV         |          |          |          |
2+30       0.0411      0.24  QV         |          |          |          |
2+35       0.0430      0.29  |Q         |          |          |          |
2+40       0.0451      0.30  |Q         |          |          |          |
2+45       0.0472      0.30  |Q         |          |          |          |
2+50       0.0493      0.30  |Q         |          |          |          |
2+55       0.0514      0.30  |Q         |          |          |          |
3+ 0       0.0535      0.30  |Q         |          |          |          |
3+ 5       0.0556      0.30  |Q         |          |          |          |
3+10       0.0577      0.30  |Q         |          |          |          |
3+15       0.0598      0.30  |Q         |          |          |          |
3+20       0.0619      0.30  |Q         |          |          |          |
3+25       0.0640      0.30  |QV        |          |          |          |
3+30       0.0661      0.30  |QV        |          |          |          |
3+35       0.0682      0.30  |QV        |          |          |          |
3+40       0.0703      0.30  |QV        |          |          |          |
3+45       0.0724      0.30  |QV        |          |          |          |
3+50       0.0748      0.35  |QV        |          |          |          |
3+55       0.0773      0.37  |QV        |          |          |          |
4+ 0       0.0798      0.37  |QV        |          |          |          |
4+ 5       0.0823      0.37  |QV        |          |          |          |
4+10       0.0848      0.37  |QV        |          |          |          |
4+15       0.0874      0.37  |QV        |          |          |          |
4+20       0.0902      0.41  |QV        |          |          |          |
4+25       0.0931      0.43  |QV        |          |          |          |
4+30       0.0960      0.43  |Q V       |          |          |          |
4+35       0.0990      0.43  |Q V       |          |          |          |
4+40       0.1019      0.43  |Q V       |          |          |          |
4+45       0.1048      0.43  |Q V       |          |          |          |
4+50       0.1081      0.47  |Q V       |          |          |          |
4+55       0.1114      0.49  |Q V       |          |          |          |
5+ 0       0.1148      0.49  |Q V       |          |          |          |
5+ 5       0.1175      0.40  |Q V       |          |          |          |
5+10       0.1200      0.37  |Q V       |          |          |          |
5+15       0.1225      0.37  |Q V       |          |          |          |
5+20       0.1254      0.41  |Q V       |          |          |          |
5+25       0.1283      0.43  |Q  V      |          |          |          |
5+30       0.1312      0.43  |Q  V      |          |          |          |
5+35       0.1345      0.47  |Q  V      |          |          |          |
5+40       0.1378      0.49  |Q  V      |          |          |          |
5+45       0.1412      0.49  |Q  V      |          |          |          |
5+50       0.1445      0.49  |Q  V      |          |          |          |
5+55       0.1479      0.49  |Q  V      |          |          |          |
6+ 0       0.1512      0.49  |Q  V      |          |          |          |
6+ 5       0.1549      0.53  | Q V      |          |          |          |
6+10       0.1587      0.55  | Q  V     |          |          |          |
6+15       0.1625      0.55  | Q  V     |          |          |          |
6+20       0.1662      0.55  | Q  V     |          |          |          |
6+25       0.1700      0.55  | Q  V     |          |          |          |
6+30       0.1738      0.55  | Q  V     |          |          |          |
6+35       0.1779      0.59  | Q  V     |          |          |          |
6+40       0.1820      0.61  | Q  V     |          |          |          |
6+45       0.1862      0.61  | Q  V     |          |          |          |
6+50       0.1904      0.61  | Q   V    |          |          |          |
6+55       0.1946      0.61  | Q   V    |          |          |          |
7+ 0       0.1988      0.61  | Q   V    |          |          |          |
7+ 5       0.2030      0.61  | Q   V    |          |          |          |
7+10       0.2072      0.61  | Q   V    |          |          |          |
7+15       0.2114      0.61  | Q   V    |          |          |          |
7+20       0.2159      0.65  | Q   V    |          |          |          |
7+25       0.2205      0.67  | Q    V   |          |          |          |
7+30       0.2251      0.67  | Q    V   |          |          |          |
7+35       0.2300      0.71  | Q    V   |          |          |          |
7+40       0.2350      0.73  | Q    V   |          |          |          |
7+45       0.2401      0.73  | Q    V   |          |          |          |
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7+50	0.2454	0.78	Q V				
7+55	0.2509	0.79	Q V				
8+ 0	0.2563	0.79	Q V				
8+ 5	0.2624	0.88	Q V				
8+10	0.2687	0.91	Q V				
8+15	0.2749	0.91	Q V				
8+20	0.2812	0.91	Q V				
8+25	0.2875	0.91	Q V				
8+30	0.2938	0.91	Q V				
8+35	0.3004	0.96	Q V				
8+40	0.3071	0.97	Q V				
8+45	0.3138	0.97	Q V				
8+50	0.3208	1.02	Q V				
8+55	0.3279	1.03	Q V				
9+ 0	0.3351	1.03	Q V				
9+ 5	0.3428	1.13	Q V				
9+10	0.3508	1.16	Q V				
9+15	0.3587	1.16	Q V				
9+20	0.3670	1.20	Q V				
9+25	0.3754	1.22	Q V				
9+30	0.3838	1.22	Q V				
9+35	0.3925	1.26	Q V				
9+40	0.4013	1.28	Q V				
9+45	0.4101	1.28	Q V				
9+50	0.4192	1.32	Q V				
9+55	0.4284	1.34	Q V				
10+ 0	0.4376	1.34	Q V				
10+ 5	0.4446	1.02	Q V				
10+10	0.4509	0.91	Q V				
10+15	0.4572	0.91	Q V				
10+20	0.4635	0.91	Q V				
10+25	0.4698	0.91	Q V				
10+30	0.4761	0.91	Q V				
10+35	0.4839	1.14	Q V				
10+40	0.4923	1.22	Q V				
10+45	0.5007	1.22	Q V				
10+50	0.5091	1.22	Q V				
10+55	0.5174	1.22	Q V				
11+ 0	0.5258	1.22	Q V				
11+ 5	0.5339	1.17	Q V				
11+10	0.5418	1.16	Q V				
11+15	0.5498	1.16	Q V				
11+20	0.5578	1.16	Q V				
11+25	0.5657	1.16	Q V				
11+30	0.5737	1.16	Q V				
11+35	0.5810	1.07	Q V				
11+40	0.5882	1.03	Q V				
11+45	0.5953	1.03	Q V				
11+50	0.6027	1.08	Q V				
11+55	0.6103	1.10	Q V				
12+ 0	0.6178	1.10	Q V				
12+ 5	0.6275	1.41	Q V				
12+10	0.6380	1.52	Q V				
12+15	0.6485	1.52	Q V				
12+20	0.6593	1.57	Q V				
12+25	0.6702	1.58	Q V				
12+30	0.6810	1.58	Q V				
12+35	0.6926	1.67	Q V				
12+40	0.7043	1.70	Q V				
12+45	0.7160	1.70	Q V				
12+50	0.7281	1.75	Q V				
12+55	0.7402	1.76	Q V				
13+ 0	0.7524	1.76	Q V				
13+ 5	0.7661	1.99	Q V				
13+10	0.7803	2.07	Q V				
13+15	0.7946	2.07	Q V				
13+20	0.8088	2.07	Q V				
13+25	0.8231	2.07	Q V				
13+30	0.8373	2.07	Q V				
13+35	0.8481	1.57	Q V				
13+40	0.8578	1.40	Q V				
13+45	0.8674	1.40	Q V				

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13+50       0.8770      1.40  |    Q    |          |       V  |          |
13+55       0.8867      1.40  |    Q    |          |        V |          |
14+ 0       0.8963      1.40  |    Q    |          |        V |          |
14+ 5       0.9072      1.58  |     Q   |          |        V |          |
14+10       0.9185      1.64  |     Q   |          |         V|          |
14+15       0.9298      1.64  |     Q   |          |         V|          |
14+20       0.9408      1.60  |     Q   |          |         V|          |
14+25       0.9517      1.58  |     Q   |          |          V          |
14+30       0.9626      1.58  |     Q   |          |          V          |
14+35       0.9735      1.58  |     Q   |          |          V          |
14+40       0.9844      1.58  |     Q   |          |          |V         |
14+45       0.9953      1.58  |     Q   |          |          |V         |
14+50       1.0059      1.54  |     Q   |          |          | V        |
14+55       1.0164      1.52  |     Q   |          |          | V        |
15+ 0       1.0268      1.52  |     Q   |          |          | V        |
15+ 5       1.0370      1.48  |    Q    |          |          | V        |
15+10       1.0471      1.46  |    Q    |          |          |  V       |
15+15       1.0571      1.46  |    Q    |          |          |  V       |
15+20       1.0669      1.41  |    Q    |          |          |  V       |
15+25       1.0765      1.40  |    Q    |          |          |   V      |
15+30       1.0861      1.40  |    Q    |          |          |   V      |
15+35       1.0945      1.22  |   Q     |          |          |   V      |
15+40       1.1025      1.16  |   Q     |          |          |    V     |
15+45       1.1104      1.16  |   Q     |          |          |    V     |
15+50       1.1184      1.16  |   Q     |          |          |    V     |
15+55       1.1264      1.16  |   Q     |          |          |    V     |
16+ 0       1.1343      1.16  |   Q     |          |          |     V    |
16+ 5       1.1376      0.48  |Q        |          |          |     V    |
16+10       1.1393      0.24  Q         |          |          |     V    |
16+15       1.1409      0.24  Q         |          |          |     V    |
16+20       1.1426      0.24  Q         |          |          |     V    |
16+25       1.1443      0.24  Q         |          |          |     V    |
16+30       1.1460      0.24  Q         |          |          |     V    |
16+35       1.1473      0.20  Q         |          |          |     V    |
16+40       1.1486      0.18  Q         |          |          |     V    |
16+45       1.1499      0.18  Q         |          |          |     V    |
16+50       1.1511      0.18  Q         |          |          |     V    |
16+55       1.1524      0.18  Q         |          |          |     V    |
17+ 0       1.1536      0.18  Q         |          |          |     V    |
17+ 5       1.1555      0.27  |Q        |          |          |     V    |
17+10       1.1576      0.30  |Q        |          |          |     V    |
17+15       1.1597      0.30  |Q        |          |          |     V    |
17+20       1.1618      0.30  |Q        |          |          |     V    |
17+25       1.1639      0.30  |Q        |          |          |      V   |
17+30       1.1660      0.30  |Q        |          |          |      V   |
17+35       1.1681      0.30  |Q        |          |          |      V   |
17+40       1.1702      0.30  |Q        |          |          |      V   |
17+45       1.1723      0.30  |Q        |          |          |      V   |
17+50       1.1741      0.26  |Q        |          |          |      V   |
17+55       1.1757      0.24  Q         |          |          |      V   |
18+ 0       1.1774      0.24  Q         |          |          |      V   |
18+ 5       1.1791      0.24  Q         |          |          |      V   |
18+10       1.1808      0.24  Q         |          |          |      V   |
18+15       1.1824      0.24  Q         |          |          |      V   |
18+20       1.1841      0.24  Q         |          |          |      V   |
18+25       1.1858      0.24  Q         |          |          |      V   |
18+30       1.1875      0.24  Q         |          |          |      V   |
18+35       1.1888      0.20  Q         |          |          |      V   |
18+40       1.1901      0.18  Q         |          |          |      V   |
18+45       1.1913      0.18  Q         |          |          |      V   |
18+50       1.1923      0.14  Q         |          |          |      V   |
18+55       1.1931      0.12  Q         |          |          |      V   |
19+ 0       1.1940      0.12  Q         |          |          |      V   |
19+ 5       1.1951      0.17  Q         |          |          |       V  |
19+10       1.1964      0.18  Q         |          |          |       V  |
19+15       1.1976      0.18  Q         |          |          |       V  |
19+20       1.1992      0.23  Q         |          |          |       V  |
19+25       1.2009      0.24  Q         |          |          |       V  |
19+30       1.2025      0.24  Q         |          |          |       V  |
19+35       1.2039      0.20  Q         |          |          |       V  |
19+40       1.2052      0.18  Q         |          |          |       V  |
19+45       1.2064      0.18  Q         |          |          |       V  |
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  19+50       1.2074      0.14  Q          |           |           |        V |
  19+55       1.2082      0.12  Q          |           |           |        V |
  20+ 0       1.2090      0.12  Q          |           |           |        V |
  20+ 5       1.2102      0.17  Q          |           |           |        V |
  20+10       1.2114      0.18  Q          |           |           |        V |
  20+15       1.2127      0.18  Q          |           |           |        V |
  20+20       1.2140      0.18  Q          |           |           |        V |
  20+25       1.2152      0.18  Q          |           |           |        V |
  20+30       1.2165      0.18  Q          |           |           |        V |
  20+35       1.2177      0.18  Q          |           |           |        V |
  20+40       1.2190      0.18  Q          |           |           |        V |
  20+45       1.2202      0.18  Q          |           |           |        V |
  20+50       1.2212      0.14  Q          |           |           |        V |
  20+55       1.2220      0.12  Q          |           |           |        V |
  21+ 0       1.2229      0.12  Q          |           |           |        V |
  21+ 5       1.2240      0.17  Q          |           |           |        V |
  21+10       1.2253      0.18  Q          |           |           |        V |
  21+15       1.2265      0.18  Q          |           |           |         V|
  21+20       1.2275      0.14  Q          |           |           |         V|
  21+25       1.2283      0.12  Q          |           |           |         V|
  21+30       1.2292      0.12  Q          |           |           |         V|
  21+35       1.2303      0.17  Q          |           |           |         V|
  21+40       1.2316      0.18  Q          |           |           |         V|
  21+45       1.2328      0.18  Q          |           |           |         V|
  21+50       1.2338      0.14  Q          |           |           |         V|
  21+55       1.2346      0.12  Q          |           |           |         V|
  22+ 0       1.2354      0.12  Q          |           |           |         V|
  22+ 5       1.2366      0.17  Q          |           |           |         V|
  22+10       1.2378      0.18  Q          |           |           |         V|
  22+15       1.2391      0.18  Q          |           |           |         V|
  22+20       1.2400      0.14  Q          |           |           |         V|
  22+25       1.2409      0.12  Q          |           |           |         V|
  22+30       1.2417      0.12  Q          |           |           |         V|
  22+35       1.2426      0.12  Q          |           |           |         V|
  22+40       1.2434      0.12  Q          |           |           |         V|
  22+45       1.2442      0.12  Q          |           |           |         V|
  22+50       1.2451      0.12  Q          |           |           |         V|
  22+55       1.2459      0.12  Q          |           |           |         V|
  23+ 0       1.2468      0.12  Q          |           |           |         V|
  23+ 5       1.2476      0.12  Q          |           |           |         V|
  23+10       1.2484      0.12  Q          |           |           |         V|
  23+15       1.2493      0.12  Q          |           |           |         V|
  23+20       1.2501      0.12  Q          |           |           |         V|
  23+25       1.2509      0.12  Q          |           |           |         V|
  23+30       1.2518      0.12  Q          |           |           |         V|
  23+35       1.2526      0.12  Q          |           |           |         V|
  23+40       1.2535      0.12  Q          |           |           |         V|
  23+45       1.2543      0.12  Q          |           |           |         V|
  23+50       1.2551      0.12  Q          |           |           |         V|
  23+55       1.2560      0.12  Q          |           |           |         V|
  24+ 0       1.2568      0.12  Q          |           |           |         V|
  24+ 5       1.2570      0.03  Q          |           |           |          V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD0565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	1.20	7.28

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	3.00	18.21

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.622(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.622(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.097	(0.134)	0.018	0.080
2	0.17	0.60	0.117	(0.134)	0.021	0.096
3	0.25	0.60	0.117	(0.134)	0.021	0.096
4	0.33	0.60	0.117	(0.134)	0.021	0.096
5	0.42	0.60	0.117	(0.134)	0.021	0.096
6	0.50	0.70	0.136	(0.134)	0.025	0.112
7	0.58	0.70	0.136	(0.134)	0.025	0.112
8	0.67	0.70	0.136	(0.134)	0.025	0.112
9	0.75	0.70	0.136	(0.134)	0.025	0.112
10	0.83	0.70	0.136	(0.134)	0.025	0.112
11	0.92	0.70	0.136	(0.134)	0.025	0.112
12	1.00	0.80	0.156	(0.134)	0.028	0.128
13	1.08	0.80	0.156	(0.134)	0.028	0.128
14	1.17	0.80	0.156	(0.134)	0.028	0.128
15	1.25	0.80	0.156	(0.134)	0.028	0.128
16	1.33	0.80	0.156	(0.134)	0.028	0.128
17	1.42	0.80	0.156	(0.134)	0.028	0.128
18	1.50	0.80	0.156	(0.134)	0.028	0.128
19	1.58	0.80	0.156	(0.134)	0.028	0.128
20	1.67	0.80	0.156	(0.134)	0.028	0.128
21	1.75	0.80	0.156	(0.134)	0.028	0.128
22	1.83	0.80	0.156	(0.134)	0.028	0.128
23	1.92	0.80	0.156	(0.134)	0.028	0.128
24	2.00	0.90	0.175	(0.134)	0.032	0.144
25	2.08	0.80	0.156	(0.134)	0.028	0.128
26	2.17	0.90	0.175	(0.134)	0.032	0.144
27	2.25	0.90	0.175	(0.134)	0.032	0.144
28	2.33	0.90	0.175	(0.134)	0.032	0.144
29	2.42	0.90	0.175	(0.134)	0.032	0.144
30	2.50	0.90	0.175	(0.134)	0.032	0.144
31	2.58	0.90	0.175	(0.134)	0.032	0.144
32	2.67	0.90	0.175	(0.134)	0.032	0.144
33	2.75	1.00	0.195	(0.134)	0.035	0.160
34	2.83	1.00	0.195	(0.134)	0.035	0.160
35	2.92	1.00	0.195	(0.134)	0.035	0.160
36	3.00	1.00	0.195	(0.134)	0.035	0.160
37	3.08	1.00	0.195	(0.134)	0.035	0.160
38	3.17	1.10	0.214	(0.134)	0.039	0.176
39	3.25	1.10	0.214	(0.134)	0.039	0.176
40	3.33	1.10	0.214	(0.134)	0.039	0.176
41	3.42	1.20	0.234	(0.134)	0.042	0.191
42	3.50	1.30	0.253	(0.134)	0.046	0.207

43	3.58	1.40	0.272	(	0.134)	0.049	0.223
44	3.67	1.40	0.272	(	0.134)	0.049	0.223
45	3.75	1.50	0.292	(	0.134)	0.053	0.239
46	3.83	1.50	0.292	(	0.134)	0.053	0.239
47	3.92	1.60	0.311	(	0.134)	0.056	0.255
48	4.00	1.60	0.311	(	0.134)	0.056	0.255
49	4.08	1.70	0.331	(	0.134)	0.060	0.271
50	4.17	1.80	0.350	(	0.134)	0.063	0.287
51	4.25	1.90	0.370	(	0.134)	0.067	0.303
52	4.33	2.00	0.389	(	0.134)	0.070	0.319
53	4.42	2.10	0.409	(	0.134)	0.074	0.335
54	4.50	2.10	0.409	(	0.134)	0.074	0.335
55	4.58	2.20	0.428	(	0.134)	0.077	0.351
56	4.67	2.30	0.448	(	0.134)	0.081	0.367
57	4.75	2.40	0.467	(	0.134)	0.084	0.383
58	4.83	2.40	0.467	(	0.134)	0.084	0.383
59	4.92	2.50	0.486	(	0.134)	0.088	0.399
60	5.00	2.60	0.506	(	0.134)	0.091	0.415
61	5.08	3.10	0.603	(	0.134)	0.109	0.495
62	5.17	3.60	0.701	(	0.134)	0.126	0.574
63	5.25	3.90	0.759		0.134	(0.137)	0.625
64	5.33	4.20	0.817		0.134	(0.147)	0.683
65	5.42	4.70	0.915		0.134	(0.165)	0.780
66	5.50	5.60	1.090		0.134	(0.196)	0.956
67	5.58	1.90	0.370	(	0.134)	0.067	0.303
68	5.67	0.90	0.175	(	0.134)	0.032	0.144
69	5.75	0.60	0.117	(	0.134)	0.021	0.096
70	5.83	0.50	0.097	(	0.134)	0.018	0.080
71	5.92	0.30	0.058	(	0.134)	0.011	0.048
72	6.00	0.20	0.039	(	0.134)	0.007	0.032

(Loss Rate Not Used)

Sum = 100.0 Sum = 16.1

Flood volume = Effective rainfall 1.34(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.7(Ac.Ft)
Total soil loss = 0.28(In)
Total soil loss = 0.143(Ac.Ft)
Total rainfall = 1.62(In)
Flood volume = 29496.6 Cubic Feet
Total soil loss = 6233.2 Cubic Feet

Peak flow rate of this hydrograph = 5.576(CFS)

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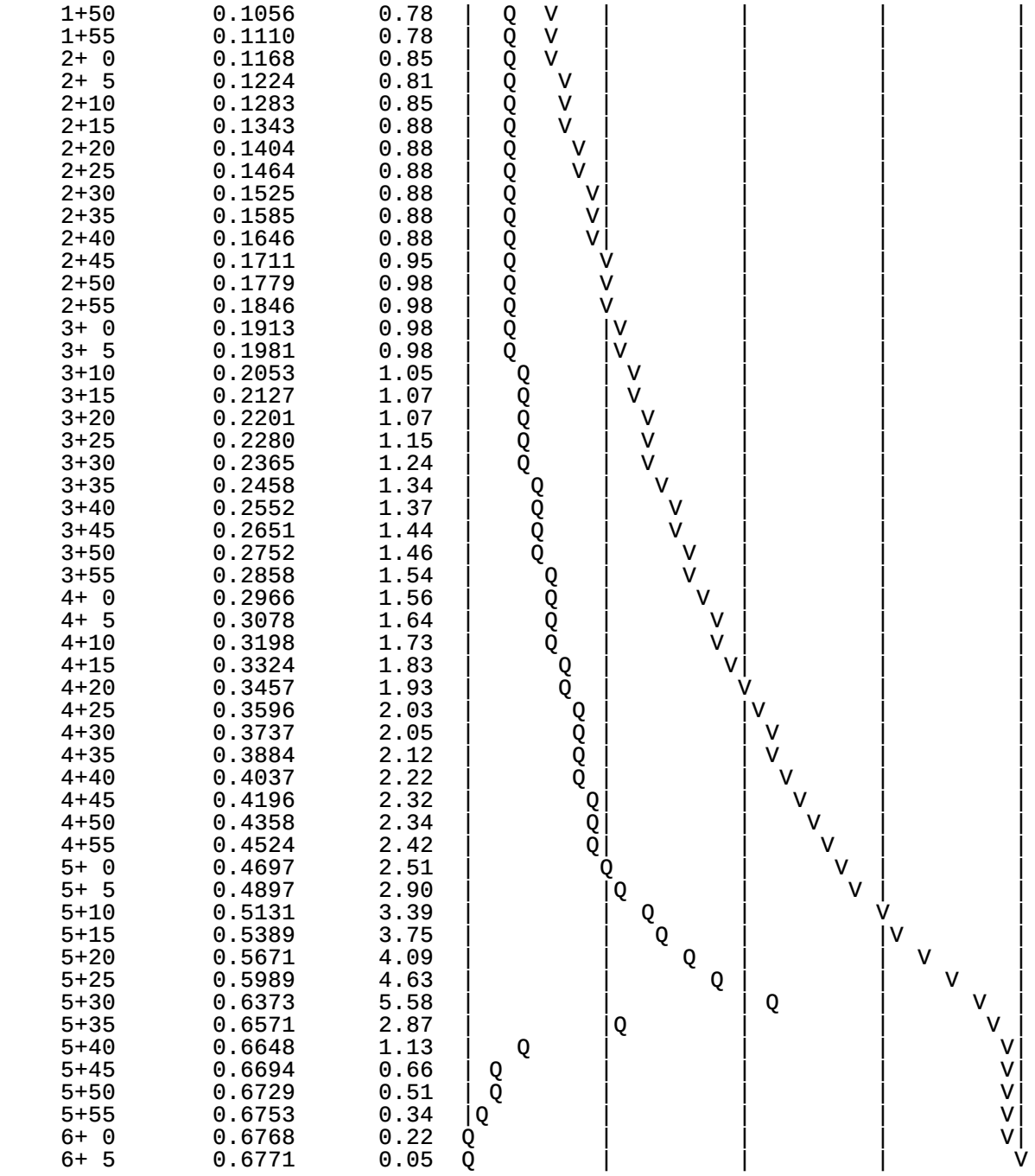
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0025	0.36	VQ				
0+10	0.0064	0.56	V Q				
0+15	0.0104	0.59	V Q				
0+20	0.0144	0.59	V Q				
0+25	0.0185	0.59	|VQ				
0+30	0.0230	0.66	|VQ				
0+35	0.0277	0.68	|VQ				
0+40	0.0324	0.68	|VQ				
0+45	0.0371	0.68	| Q				
0+50	0.0418	0.68	| Q				
0+55	0.0466	0.68	| Q				
1+ 0	0.0518	0.76	| Q				
1+ 5	0.0571	0.78	| Q				
1+10	0.0625	0.78	| Q				
1+15	0.0679	0.78	| QV				
1+20	0.0733	0.78	| QV				
1+25	0.0787	0.78	| QV				
1+30	0.0841	0.78	| QV				
1+35	0.0894	0.78	| Q V				
1+40	0.0948	0.78	| Q V				
1+45	0.1002	0.78	| Q V				



1+50	0.1056	0.78	
1+55	0.1110	0.78	
2+ 0	0.1168	0.85	
2+ 5	0.1224	0.81	
2+10	0.1283	0.85	
2+15	0.1343	0.88	
2+20	0.1404	0.88	
2+25	0.1464	0.88	
2+30	0.1525	0.88	
2+35	0.1585	0.88	
2+40	0.1646	0.88	
2+45	0.1711	0.95	
2+50	0.1779	0.98	
2+55	0.1846	0.98	
3+ 0	0.1913	0.98	
3+ 5	0.1981	0.98	
3+10	0.2053	1.05	
3+15	0.2127	1.07	
3+20	0.2201	1.07	
3+25	0.2280	1.15	
3+30	0.2365	1.24	
3+35	0.2458	1.34	
3+40	0.2552	1.37	
3+45	0.2651	1.44	
3+50	0.2752	1.46	
3+55	0.2858	1.54	
4+ 0	0.2966	1.56	
4+ 5	0.3078	1.64	
4+10	0.3198	1.73	
4+15	0.3324	1.83	
4+20	0.3457	1.93	
4+25	0.3596	2.03	
4+30	0.3737	2.05	
4+35	0.3884	2.12	
4+40	0.4037	2.22	
4+45	0.4196	2.32	
4+50	0.4358	2.34	
4+55	0.4524	2.42	
5+ 0	0.4697	2.51	
5+ 5	0.4897	2.90	
5+10	0.5131	3.39	
5+15	0.5389	3.75	
5+20	0.5671	4.09	
5+25	0.5989	4.63	
5+30	0.6373	5.58	
5+35	0.6571	2.87	
5+40	0.6648	1.13	
5+45	0.6694	0.66	
5+50	0.6729	0.51	
5+55	0.6753	0.34	
6+ 0	0.6768	0.22	
6+ 5	0.6771	0.05	

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD0535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	0.90	5.46

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	2.35	14.26

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.240(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.240(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	582.319	74.564	4.561
2	0.167	1164.637	25.436	1.556
			Sum = 100.000 Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.193	(0.134)	0.035	0.159
2	0.17	1.30	0.193	(0.134)	0.035	0.159
3	0.25	1.10	0.164	(0.134)	0.029	0.134
4	0.33	1.50	0.223	(0.134)	0.040	0.183
5	0.42	1.50	0.223	(0.134)	0.040	0.183
6	0.50	1.80	0.268	(0.134)	0.048	0.220
7	0.58	1.50	0.223	(0.134)	0.040	0.183
8	0.67	1.80	0.268	(0.134)	0.048	0.220
9	0.75	1.80	0.268	(0.134)	0.048	0.220
10	0.83	1.50	0.223	(0.134)	0.040	0.183
11	0.92	1.60	0.238	(0.134)	0.043	0.195
12	1.00	1.80	0.268	(0.134)	0.048	0.220
13	1.08	2.20	0.327	(0.134)	0.059	0.268
14	1.17	2.20	0.327	(0.134)	0.059	0.268
15	1.25	2.20	0.327	(0.134)	0.059	0.268
16	1.33	2.00	0.298	(0.134)	0.054	0.244
17	1.42	2.60	0.387	(0.134)	0.070	0.317
18	1.50	2.70	0.402	(0.134)	0.072	0.329
19	1.58	2.40	0.357	(0.134)	0.064	0.293
20	1.67	2.70	0.402	(0.134)	0.072	0.329
21	1.75	3.30	0.491	(0.134)	0.088	0.403
22	1.83	3.10	0.461	(0.134)	0.083	0.378
23	1.92	2.90	0.431	(0.134)	0.078	0.354
24	2.00	3.00	0.446	(0.134)	0.080	0.366
25	2.08	3.10	0.461	(0.134)	0.083	0.378
26	2.17	4.20	0.625	(0.134)	0.112	0.512
27	2.25	5.00	0.744	(0.134)	0.134	0.610
28	2.33	3.50	0.521	(0.134)	0.094	0.427
29	2.42	6.80	1.012	0.134	(0.182)	0.877
30	2.50	7.30	1.086	0.134	(0.195)	0.952
31	2.58	8.20	1.220	0.134	(0.220)	1.086
32	2.67	5.90	0.878	0.134	(0.158)	0.743
33	2.75	2.00	0.298	(0.134)	0.054	0.244
34	2.83	1.80	0.268	(0.134)	0.048	0.220
35	2.92	1.80	0.268	(0.134)	0.048	0.220
36	3.00	0.60	0.089	(0.134)	0.016	0.073
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	12.4

Flood volume = Effective rainfall 1.03(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.104(Ac.Ft)

Total rainfall = 1.24(In)
Flood volume = 22798.1 Cubic Feet
Total soil loss = 4515.2 Cubic Feet

Peak flow rate of this hydrograph = 6.436(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0050	0.72	V Q
0+10	0.0117	0.97	V Q
0+15	0.0176	0.86	V Q
0+20	0.0248	1.04	V Q
0+25	0.0325	1.12	V Q
0+30	0.0413	1.29	V Q
0+35	0.0495	1.18	VQ
0+40	0.0583	1.29	VQ
0+45	0.0676	1.34	Q
0+50	0.0757	1.18	QV
0+55	0.0838	1.18	Q V
1+ 0	0.0928	1.31	Q V
1+ 5	0.1036	1.57	QV
1+10	0.1149	1.64	Q V
1+15	0.1262	1.64	Q V
1+20	0.1367	1.53	Q V
1+25	0.1493	1.83	Q V
1+30	0.1631	2.00	Q V
1+35	0.1758	1.85	Q V
1+40	0.1893	1.96	Q V
1+45	0.2055	2.35	Q V
1+50	0.2217	2.35	Q V
1+55	0.2368	2.20	Q V
2+ 0	0.2521	2.22	Q V
2+ 5	0.2679	2.30	Q V
2+10	0.2881	2.93	Q V
2+15	0.3128	3.58	Q V
2+20	0.3327	2.90	Q V
2+25	0.3649	4.67	Q V
2+30	0.4042	5.71	Q V
2+35	0.4485	6.44	Q V
2+40	0.4835	5.08	Q V
2+45	0.4992	2.27	Q V
2+50	0.5087	1.38	Q V
2+55	0.5179	1.34	Q V
3+ 0	0.5226	0.68	Q V
3+ 5	0.5234	0.11	Q V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD0515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
5-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	0.54	3.28

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	1.36	8.26

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.732(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.732(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	36.0	0.706	0.900	0.134	1.000	0.134
					Sum (F) =	0.134

Area averaged mean soil loss (F) (In/Hr) = 0.134
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	582.319	74.564	4.561
2	0.167	1164.637	25.436	1.556
		Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.387	(0.134)	0.070	0.317
2	0.17	4.50	0.395	(0.134)	0.071	0.324
3	0.25	5.40	0.474	(0.134)	0.085	0.389
4	0.33	5.40	0.474	(0.134)	0.085	0.389
5	0.42	5.70	0.501	(0.134)	0.090	0.411
6	0.50	6.40	0.562	(0.134)	0.101	0.461
7	0.58	7.90	0.694	(0.134)	0.125	0.569
8	0.67	9.10	0.799	0.134	(0.144)	0.665
9	0.75	12.80	1.124	0.134	(0.202)	0.990
10	0.83	25.60	2.249	0.134	(0.405)	2.115
11	0.92	7.90	0.694	(0.134)	0.125	0.569
12	1.00	4.90	0.430	(0.134)	0.077	0.353
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.6

Flood volume = Effective rainfall 0.63(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.10(In)
Total soil loss = 0.052(Ac.Ft)
Total rainfall = 0.73(In)
Flood volume = 13866.3 Cubic Feet
Total soil loss = 2263.1 Cubic Feet

Peak flow rate of this hydrograph = 11.192(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0100	1.45	|VQ				
0+10	0.0235	1.97		VQ				
0+15	0.0392	2.28		Q				
0+20	0.0556	2.38		Q V				
0+25	0.0727	2.48		Q V|			
0+30	0.0916	2.74		Q |V			
0+35	0.1144	3.31		Q	V			

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   0+40       0.1415      3.92  |      Q  |      V  |         |         |
   0+45       0.1797      5.55  |         |Q        | V       |         |
   0+50       0.2568     11.19  |         |         | Q       | V       |
   0+55       0.2973      5.89  |         |Q        |         |      V  |
   1+ 0       0.3145      2.50  |   Q     |         |         |        V|
   1+ 5       0.3183      0.55  |Q        |         |         |         V
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	2.00	12.14

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	6.40	38.85

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 2.000(In)
Area Averaged 100-Year Rainfall = 6.400(In)

Point rain (area averaged) = 3.810(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.810(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.030	(0.172)	0.005	0.025
2	0.17	0.07	0.030	(0.171)	0.005	0.025
3	0.25	0.07	0.030	(0.171)	0.005	0.025
4	0.33	0.10	0.046	(0.170)	0.008	0.037
5	0.42	0.10	0.046	(0.169)	0.008	0.037
6	0.50	0.10	0.046	(0.169)	0.008	0.037
7	0.58	0.10	0.046	(0.168)	0.008	0.037
8	0.67	0.10	0.046	(0.167)	0.008	0.037
9	0.75	0.10	0.046	(0.167)	0.008	0.037
10	0.83	0.13	0.061	(0.166)	0.011	0.050
11	0.92	0.13	0.061	(0.165)	0.011	0.050
12	1.00	0.13	0.061	(0.165)	0.011	0.050
13	1.08	0.10	0.046	(0.164)	0.008	0.037
14	1.17	0.10	0.046	(0.163)	0.008	0.037
15	1.25	0.10	0.046	(0.163)	0.008	0.037
16	1.33	0.10	0.046	(0.162)	0.008	0.037
17	1.42	0.10	0.046	(0.162)	0.008	0.037
18	1.50	0.10	0.046	(0.161)	0.008	0.037
19	1.58	0.10	0.046	(0.160)	0.008	0.037
20	1.67	0.10	0.046	(0.160)	0.008	0.037
21	1.75	0.10	0.046	(0.159)	0.008	0.037
22	1.83	0.13	0.061	(0.158)	0.011	0.050
23	1.92	0.13	0.061	(0.158)	0.011	0.050
24	2.00	0.13	0.061	(0.157)	0.011	0.050
25	2.08	0.13	0.061	(0.156)	0.011	0.050
26	2.17	0.13	0.061	(0.156)	0.011	0.050
27	2.25	0.13	0.061	(0.155)	0.011	0.050
28	2.33	0.13	0.061	(0.155)	0.011	0.050
29	2.42	0.13	0.061	(0.154)	0.011	0.050
30	2.50	0.13	0.061	(0.153)	0.011	0.050
31	2.58	0.17	0.076	(0.153)	0.014	0.062
32	2.67	0.17	0.076	(0.152)	0.014	0.062
33	2.75	0.17	0.076	(0.151)	0.014	0.062
34	2.83	0.17	0.076	(0.151)	0.014	0.062
35	2.92	0.17	0.076	(0.150)	0.014	0.062
36	3.00	0.17	0.076	(0.150)	0.014	0.062
37	3.08	0.17	0.076	(0.149)	0.014	0.062
38	3.17	0.17	0.076	(0.148)	0.014	0.062
39	3.25	0.17	0.076	(0.148)	0.014	0.062
40	3.33	0.17	0.076	(0.147)	0.014	0.062
41	3.42	0.17	0.076	(0.146)	0.014	0.062
42	3.50	0.17	0.076	(0.146)	0.014	0.062

43	3.58	0.17	0.076	(0.145)	0.014	0.062
44	3.67	0.17	0.076	(0.145)	0.014	0.062
45	3.75	0.17	0.076	(0.144)	0.014	0.062
46	3.83	0.20	0.091	(0.143)	0.016	0.075
47	3.92	0.20	0.091	(0.143)	0.016	0.075
48	4.00	0.20	0.091	(0.142)	0.016	0.075
49	4.08	0.20	0.091	(0.142)	0.016	0.075
50	4.17	0.20	0.091	(0.141)	0.016	0.075
51	4.25	0.20	0.091	(0.140)	0.016	0.075
52	4.33	0.23	0.107	(0.140)	0.019	0.087
53	4.42	0.23	0.107	(0.139)	0.019	0.087
54	4.50	0.23	0.107	(0.139)	0.019	0.087
55	4.58	0.23	0.107	(0.138)	0.019	0.087
56	4.67	0.23	0.107	(0.137)	0.019	0.087
57	4.75	0.23	0.107	(0.137)	0.019	0.087
58	4.83	0.27	0.122	(0.136)	0.022	0.100
59	4.92	0.27	0.122	(0.136)	0.022	0.100
60	5.00	0.27	0.122	(0.135)	0.022	0.100
61	5.08	0.20	0.091	(0.134)	0.016	0.075
62	5.17	0.20	0.091	(0.134)	0.016	0.075
63	5.25	0.20	0.091	(0.133)	0.016	0.075
64	5.33	0.23	0.107	(0.133)	0.019	0.087
65	5.42	0.23	0.107	(0.132)	0.019	0.087
66	5.50	0.23	0.107	(0.132)	0.019	0.087
67	5.58	0.27	0.122	(0.131)	0.022	0.100
68	5.67	0.27	0.122	(0.130)	0.022	0.100
69	5.75	0.27	0.122	(0.130)	0.022	0.100
70	5.83	0.27	0.122	(0.129)	0.022	0.100
71	5.92	0.27	0.122	(0.129)	0.022	0.100
72	6.00	0.27	0.122	(0.128)	0.022	0.100
73	6.08	0.30	0.137	(0.128)	0.025	0.112
74	6.17	0.30	0.137	(0.127)	0.025	0.112
75	6.25	0.30	0.137	(0.126)	0.025	0.112
76	6.33	0.30	0.137	(0.126)	0.025	0.112
77	6.42	0.30	0.137	(0.125)	0.025	0.112
78	6.50	0.30	0.137	(0.125)	0.025	0.112
79	6.58	0.33	0.152	(0.124)	0.027	0.125
80	6.67	0.33	0.152	(0.124)	0.027	0.125
81	6.75	0.33	0.152	(0.123)	0.027	0.125
82	6.83	0.33	0.152	(0.122)	0.027	0.125
83	6.92	0.33	0.152	(0.122)	0.027	0.125
84	7.00	0.33	0.152	(0.121)	0.027	0.125
85	7.08	0.33	0.152	(0.121)	0.027	0.125
86	7.17	0.33	0.152	(0.120)	0.027	0.125
87	7.25	0.33	0.152	(0.120)	0.027	0.125
88	7.33	0.37	0.168	(0.119)	0.030	0.137
89	7.42	0.37	0.168	(0.119)	0.030	0.137
90	7.50	0.37	0.168	(0.118)	0.030	0.137
91	7.58	0.40	0.183	(0.118)	0.033	0.150
92	7.67	0.40	0.183	(0.117)	0.033	0.150
93	7.75	0.40	0.183	(0.116)	0.033	0.150
94	7.83	0.43	0.198	(0.116)	0.036	0.162
95	7.92	0.43	0.198	(0.115)	0.036	0.162
96	8.00	0.43	0.198	(0.115)	0.036	0.162
97	8.08	0.50	0.229	(0.114)	0.041	0.187
98	8.17	0.50	0.229	(0.114)	0.041	0.187
99	8.25	0.50	0.229	(0.113)	0.041	0.187
100	8.33	0.50	0.229	(0.113)	0.041	0.187
101	8.42	0.50	0.229	(0.112)	0.041	0.187
102	8.50	0.50	0.229	(0.112)	0.041	0.187
103	8.58	0.53	0.244	(0.111)	0.044	0.200
104	8.67	0.53	0.244	(0.111)	0.044	0.200
105	8.75	0.53	0.244	(0.110)	0.044	0.200
106	8.83	0.57	0.259	(0.110)	0.047	0.212
107	8.92	0.57	0.259	(0.109)	0.047	0.212
108	9.00	0.57	0.259	(0.109)	0.047	0.212
109	9.08	0.63	0.290	(0.108)	0.052	0.237
110	9.17	0.63	0.290	(0.108)	0.052	0.237
111	9.25	0.63	0.290	(0.107)	0.052	0.237
112	9.33	0.67	0.305	(0.107)	0.055	0.250
113	9.42	0.67	0.305	(0.106)	0.055	0.250
114	9.50	0.67	0.305	(0.105)	0.055	0.250

115	9.58	0.70	0.320	(	0.105)	0.058	0.262
116	9.67	0.70	0.320	(	0.104)	0.058	0.262
117	9.75	0.70	0.320	(	0.104)	0.058	0.262
118	9.83	0.73	0.335	(	0.103)	0.060	0.275
119	9.92	0.73	0.335	(	0.103)	0.060	0.275
120	10.00	0.73	0.335	(	0.102)	0.060	0.275
121	10.08	0.50	0.229	(	0.102)	0.041	0.187
122	10.17	0.50	0.229	(	0.101)	0.041	0.187
123	10.25	0.50	0.229	(	0.101)	0.041	0.187
124	10.33	0.50	0.229	(	0.101)	0.041	0.187
125	10.42	0.50	0.229	(	0.100)	0.041	0.187
126	10.50	0.50	0.229	(	0.100)	0.041	0.187
127	10.58	0.67	0.305	(	0.099)	0.055	0.250
128	10.67	0.67	0.305	(	0.099)	0.055	0.250
129	10.75	0.67	0.305	(	0.098)	0.055	0.250
130	10.83	0.67	0.305	(	0.098)	0.055	0.250
131	10.92	0.67	0.305	(	0.097)	0.055	0.250
132	11.00	0.67	0.305	(	0.097)	0.055	0.250
133	11.08	0.63	0.290	(	0.096)	0.052	0.237
134	11.17	0.63	0.290	(	0.096)	0.052	0.237
135	11.25	0.63	0.290	(	0.095)	0.052	0.237
136	11.33	0.63	0.290	(	0.095)	0.052	0.237
137	11.42	0.63	0.290	(	0.094)	0.052	0.237
138	11.50	0.63	0.290	(	0.094)	0.052	0.237
139	11.58	0.57	0.259	(	0.093)	0.047	0.212
140	11.67	0.57	0.259	(	0.093)	0.047	0.212
141	11.75	0.57	0.259	(	0.092)	0.047	0.212
142	11.83	0.60	0.274	(	0.092)	0.049	0.225
143	11.92	0.60	0.274	(	0.092)	0.049	0.225
144	12.00	0.60	0.274	(	0.091)	0.049	0.225
145	12.08	0.83	0.381	(	0.091)	0.069	0.312
146	12.17	0.83	0.381	(	0.090)	0.069	0.312
147	12.25	0.83	0.381	(	0.090)	0.069	0.312
148	12.33	0.87	0.396	(	0.089)	0.071	0.325
149	12.42	0.87	0.396	(	0.089)	0.071	0.325
150	12.50	0.87	0.396	(	0.088)	0.071	0.325
151	12.58	0.93	0.427	(	0.088)	0.077	0.350
152	12.67	0.93	0.427	(	0.087)	0.077	0.350
153	12.75	0.93	0.427	(	0.087)	0.077	0.350
154	12.83	0.97	0.442	(	0.087)	0.080	0.362
155	12.92	0.97	0.442	(	0.086)	0.080	0.362
156	13.00	0.97	0.442	(	0.086)	0.080	0.362
157	13.08	1.13	0.518		0.085	(0.093)	0.433
158	13.17	1.13	0.518		0.085	(0.093)	0.433
159	13.25	1.13	0.518		0.084	(0.093)	0.434
160	13.33	1.13	0.518		0.084	(0.093)	0.434
161	13.42	1.13	0.518		0.084	(0.093)	0.435
162	13.50	1.13	0.518		0.083	(0.093)	0.435
163	13.58	0.77	0.351	(	0.083)	0.063	0.287
164	13.67	0.77	0.351	(	0.082)	0.063	0.287
165	13.75	0.77	0.351	(	0.082)	0.063	0.287
166	13.83	0.77	0.351	(	0.081)	0.063	0.287
167	13.92	0.77	0.351	(	0.081)	0.063	0.287
168	14.00	0.77	0.351	(	0.081)	0.063	0.287
169	14.08	0.90	0.411	(	0.080)	0.074	0.337
170	14.17	0.90	0.411	(	0.080)	0.074	0.337
171	14.25	0.90	0.411	(	0.079)	0.074	0.337
172	14.33	0.87	0.396	(	0.079)	0.071	0.325
173	14.42	0.87	0.396	(	0.079)	0.071	0.325
174	14.50	0.87	0.396	(	0.078)	0.071	0.325
175	14.58	0.87	0.396	(	0.078)	0.071	0.325
176	14.67	0.87	0.396	(	0.077)	0.071	0.325
177	14.75	0.87	0.396	(	0.077)	0.071	0.325
178	14.83	0.83	0.381	(	0.077)	0.069	0.312
179	14.92	0.83	0.381	(	0.076)	0.069	0.312
180	15.00	0.83	0.381	(	0.076)	0.069	0.312
181	15.08	0.80	0.366	(	0.075)	0.066	0.300
182	15.17	0.80	0.366	(	0.075)	0.066	0.300
183	15.25	0.80	0.366	(	0.075)	0.066	0.300
184	15.33	0.77	0.351	(	0.074)	0.063	0.287
185	15.42	0.77	0.351	(	0.074)	0.063	0.287
186	15.50	0.77	0.351	(	0.073)	0.063	0.287

187	15.58	0.63	0.290	(0.073)	0.052	0.237
188	15.67	0.63	0.290	(0.073)	0.052	0.237
189	15.75	0.63	0.290	(0.072)	0.052	0.237
190	15.83	0.63	0.290	(0.072)	0.052	0.237
191	15.92	0.63	0.290	(0.072)	0.052	0.237
192	16.00	0.63	0.290	(0.071)	0.052	0.237
193	16.08	0.13	0.061	(0.071)	0.011	0.050
194	16.17	0.13	0.061	(0.071)	0.011	0.050
195	16.25	0.13	0.061	(0.070)	0.011	0.050
196	16.33	0.13	0.061	(0.070)	0.011	0.050
197	16.42	0.13	0.061	(0.069)	0.011	0.050
198	16.50	0.13	0.061	(0.069)	0.011	0.050
199	16.58	0.10	0.046	(0.069)	0.008	0.037
200	16.67	0.10	0.046	(0.068)	0.008	0.037
201	16.75	0.10	0.046	(0.068)	0.008	0.037
202	16.83	0.10	0.046	(0.068)	0.008	0.037
203	16.92	0.10	0.046	(0.067)	0.008	0.037
204	17.00	0.10	0.046	(0.067)	0.008	0.037
205	17.08	0.17	0.076	(0.067)	0.014	0.062
206	17.17	0.17	0.076	(0.066)	0.014	0.062
207	17.25	0.17	0.076	(0.066)	0.014	0.062
208	17.33	0.17	0.076	(0.066)	0.014	0.062
209	17.42	0.17	0.076	(0.065)	0.014	0.062
210	17.50	0.17	0.076	(0.065)	0.014	0.062
211	17.58	0.17	0.076	(0.065)	0.014	0.062
212	17.67	0.17	0.076	(0.064)	0.014	0.062
213	17.75	0.17	0.076	(0.064)	0.014	0.062
214	17.83	0.13	0.061	(0.064)	0.011	0.050
215	17.92	0.13	0.061	(0.063)	0.011	0.050
216	18.00	0.13	0.061	(0.063)	0.011	0.050
217	18.08	0.13	0.061	(0.063)	0.011	0.050
218	18.17	0.13	0.061	(0.063)	0.011	0.050
219	18.25	0.13	0.061	(0.062)	0.011	0.050
220	18.33	0.13	0.061	(0.062)	0.011	0.050
221	18.42	0.13	0.061	(0.062)	0.011	0.050
222	18.50	0.13	0.061	(0.061)	0.011	0.050
223	18.58	0.10	0.046	(0.061)	0.008	0.037
224	18.67	0.10	0.046	(0.061)	0.008	0.037
225	18.75	0.10	0.046	(0.060)	0.008	0.037
226	18.83	0.07	0.030	(0.060)	0.005	0.025
227	18.92	0.07	0.030	(0.060)	0.005	0.025
228	19.00	0.07	0.030	(0.060)	0.005	0.025
229	19.08	0.10	0.046	(0.059)	0.008	0.037
230	19.17	0.10	0.046	(0.059)	0.008	0.037
231	19.25	0.10	0.046	(0.059)	0.008	0.037
232	19.33	0.13	0.061	(0.058)	0.011	0.050
233	19.42	0.13	0.061	(0.058)	0.011	0.050
234	19.50	0.13	0.061	(0.058)	0.011	0.050
235	19.58	0.10	0.046	(0.058)	0.008	0.037
236	19.67	0.10	0.046	(0.057)	0.008	0.037
237	19.75	0.10	0.046	(0.057)	0.008	0.037
238	19.83	0.07	0.030	(0.057)	0.005	0.025
239	19.92	0.07	0.030	(0.057)	0.005	0.025
240	20.00	0.07	0.030	(0.056)	0.005	0.025
241	20.08	0.10	0.046	(0.056)	0.008	0.037
242	20.17	0.10	0.046	(0.056)	0.008	0.037
243	20.25	0.10	0.046	(0.056)	0.008	0.037
244	20.33	0.10	0.046	(0.055)	0.008	0.037
245	20.42	0.10	0.046	(0.055)	0.008	0.037
246	20.50	0.10	0.046	(0.055)	0.008	0.037
247	20.58	0.10	0.046	(0.055)	0.008	0.037
248	20.67	0.10	0.046	(0.054)	0.008	0.037
249	20.75	0.10	0.046	(0.054)	0.008	0.037
250	20.83	0.07	0.030	(0.054)	0.005	0.025
251	20.92	0.07	0.030	(0.054)	0.005	0.025
252	21.00	0.07	0.030	(0.054)	0.005	0.025
253	21.08	0.10	0.046	(0.053)	0.008	0.037
254	21.17	0.10	0.046	(0.053)	0.008	0.037
255	21.25	0.10	0.046	(0.053)	0.008	0.037
256	21.33	0.07	0.030	(0.053)	0.005	0.025
257	21.42	0.07	0.030	(0.053)	0.005	0.025
258	21.50	0.07	0.030	(0.052)	0.005	0.025

259	21.58	0.10	0.046	(0.052)	0.008	0.037
260	21.67	0.10	0.046	(0.052)	0.008	0.037
261	21.75	0.10	0.046	(0.052)	0.008	0.037
262	21.83	0.07	0.030	(0.052)	0.005	0.025
263	21.92	0.07	0.030	(0.051)	0.005	0.025
264	22.00	0.07	0.030	(0.051)	0.005	0.025
265	22.08	0.10	0.046	(0.051)	0.008	0.037
266	22.17	0.10	0.046	(0.051)	0.008	0.037
267	22.25	0.10	0.046	(0.051)	0.008	0.037
268	22.33	0.07	0.030	(0.051)	0.005	0.025
269	22.42	0.07	0.030	(0.050)	0.005	0.025
270	22.50	0.07	0.030	(0.050)	0.005	0.025
271	22.58	0.07	0.030	(0.050)	0.005	0.025
272	22.67	0.07	0.030	(0.050)	0.005	0.025
273	22.75	0.07	0.030	(0.050)	0.005	0.025
274	22.83	0.07	0.030	(0.050)	0.005	0.025
275	22.92	0.07	0.030	(0.050)	0.005	0.025
276	23.00	0.07	0.030	(0.049)	0.005	0.025
277	23.08	0.07	0.030	(0.049)	0.005	0.025
278	23.17	0.07	0.030	(0.049)	0.005	0.025
279	23.25	0.07	0.030	(0.049)	0.005	0.025
280	23.33	0.07	0.030	(0.049)	0.005	0.025
281	23.42	0.07	0.030	(0.049)	0.005	0.025
282	23.50	0.07	0.030	(0.049)	0.005	0.025
283	23.58	0.07	0.030	(0.049)	0.005	0.025
284	23.67	0.07	0.030	(0.049)	0.005	0.025
285	23.75	0.07	0.030	(0.049)	0.005	0.025
286	23.83	0.07	0.030	(0.049)	0.005	0.025
287	23.92	0.07	0.030	(0.049)	0.005	0.025
288	24.00	0.07	0.030	(0.049)	0.005	0.025

(Loss Rate Not Used)

Sum = 100.0 Sum = 37.5

Flood volume = Effective rainfall 3.13(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 1.6(Ac.Ft)
Total soil loss = 0.68(In)
Total soil loss = 0.345(Ac.Ft)
Total rainfall = 3.81(In)
Flood volume = 68941.7 Cubic Feet
Total soil loss = 15011.6 Cubic Feet

Peak flow rate of this hydrograph = 2.662(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0008	0.11	Q				
0+10	0.0018	0.15	Q				
0+15	0.0029	0.15	Q				
0+20	0.0043	0.21	Q				
0+25	0.0059	0.23	Q				
0+30	0.0075	0.23	Q				
0+35	0.0091	0.23	Q				
0+40	0.0107	0.23	Q				
0+45	0.0122	0.23	Q				
0+50	0.0142	0.29	VQ				
0+55	0.0163	0.31	VQ				
1+ 0	0.0184	0.31	VQ				
1+ 5	0.0201	0.25	Q				
1+10	0.0217	0.23	Q				
1+15	0.0233	0.23	Q				
1+20	0.0249	0.23	Q				
1+25	0.0265	0.23	Q				
1+30	0.0280	0.23	Q				
1+35	0.0296	0.23	Q				
1+40	0.0312	0.23	Q				
1+45	0.0328	0.23	Q				

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1+50       0.0348      0.29  VQ        |          |          |          |
1+55       0.0369      0.31  VQ        |          |          |          |
2+ 0       0.0390      0.31  VQ        |          |          |          |
2+ 5       0.0411      0.31  |Q        |          |          |          |
2+10       0.0432      0.31  |Q        |          |          |          |
2+15       0.0453      0.31  |Q        |          |          |          |
2+20       0.0474      0.31  |Q        |          |          |          |
2+25       0.0495      0.31  |Q        |          |          |          |
2+30       0.0516      0.31  |Q        |          |          |          |
2+35       0.0541      0.36  |Q        |          |          |          |
2+40       0.0568      0.38  |Q        |          |          |          |
2+45       0.0594      0.38  |Q        |          |          |          |
2+50       0.0620      0.38  |Q        |          |          |          |
2+55       0.0647      0.38  |Q        |          |          |          |
3+ 0       0.0673      0.38  |Q        |          |          |          |
3+ 5       0.0699      0.38  |Q        |          |          |          |
3+10       0.0726      0.38  |Q        |          |          |          |
3+15       0.0752      0.38  |Q        |          |          |          |
3+20       0.0778      0.38  |Q        |          |          |          |
3+25       0.0805      0.38  |QV       |          |          |          |
3+30       0.0831      0.38  |QV       |          |          |          |
3+35       0.0857      0.38  |QV       |          |          |          |
3+40       0.0884      0.38  |QV       |          |          |          |
3+45       0.0910      0.38  |QV       |          |          |          |
3+50       0.0940      0.44  |QV       |          |          |          |
3+55       0.0972      0.46  |QV       |          |          |          |
4+ 0       0.1003      0.46  |QV       |          |          |          |
4+ 5       0.1035      0.46  |QV       |          |          |          |
4+10       0.1067      0.46  |QV       |          |          |          |
4+15       0.1098      0.46  |QV       |          |          |          |
4+20       0.1134      0.52  | Q       |          |          |          |
4+25       0.1171      0.54  | Q       |          |          |          |
4+30       0.1208      0.54  | QV      |          |          |          |
4+35       0.1244      0.54  | QV      |          |          |          |
4+40       0.1281      0.54  | QV      |          |          |          |
4+45       0.1318      0.54  | QV      |          |          |          |
4+50       0.1359      0.59  | QV      |          |          |          |
4+55       0.1401      0.61  | QV      |          |          |          |
5+ 0       0.1443      0.61  | QV      |          |          |          |
5+ 5       0.1478      0.50  |Q V      |          |          |          |
5+10       0.1509      0.46  |Q V      |          |          |          |
5+15       0.1541      0.46  |Q V      |          |          |          |
5+20       0.1576      0.52  | QV      |          |          |          |
5+25       0.1613      0.54  | Q V     |          |          |          |
5+30       0.1650      0.54  | Q V     |          |          |          |
5+35       0.1691      0.59  | Q V     |          |          |          |
5+40       0.1733      0.61  | Q V     |          |          |          |
5+45       0.1775      0.61  | Q V     |          |          |          |
5+50       0.1817      0.61  | Q V     |          |          |          |
5+55       0.1859      0.61  | Q V     |          |          |          |
6+ 0       0.1902      0.61  | Q V     |          |          |          |
6+ 5       0.1948      0.67  | Q V     |          |          |          |
6+10       0.1995      0.69  | Q  V    |          |          |          |
6+15       0.2042      0.69  | Q  V    |          |          |          |
6+20       0.2090      0.69  | Q  V    |          |          |          |
6+25       0.2137      0.69  | Q  V    |          |          |          |
6+30       0.2185      0.69  | Q  V    |          |          |          |
6+35       0.2236      0.75  | Q  V    |          |          |          |
6+40       0.2289      0.76  |  Q V    |          |          |          |
6+45       0.2341      0.76  |  Q V    |          |          |          |
6+50       0.2394      0.76  |  Q  V   |          |          |          |
6+55       0.2447      0.76  |  Q  V   |          |          |          |
7+ 0       0.2499      0.76  |  Q  V   |          |          |          |
7+ 5       0.2552      0.76  |  Q  V   |          |          |          |
7+10       0.2605      0.76  |  Q  V   |          |          |          |
7+15       0.2657      0.76  |  Q  V   |          |          |          |
7+20       0.2714      0.82  |  Q  V   |          |          |          |
7+25       0.2772      0.84  |  Q   V  |          |          |          |
7+30       0.2830      0.84  |  Q   V  |          |          |          |
7+35       0.2892      0.90  |  Q   V  |          |          |          |
7+40       0.2955      0.92  |  Q   V  |          |          |          |
7+45       0.3018      0.92  |  Q   V  |          |          |          |
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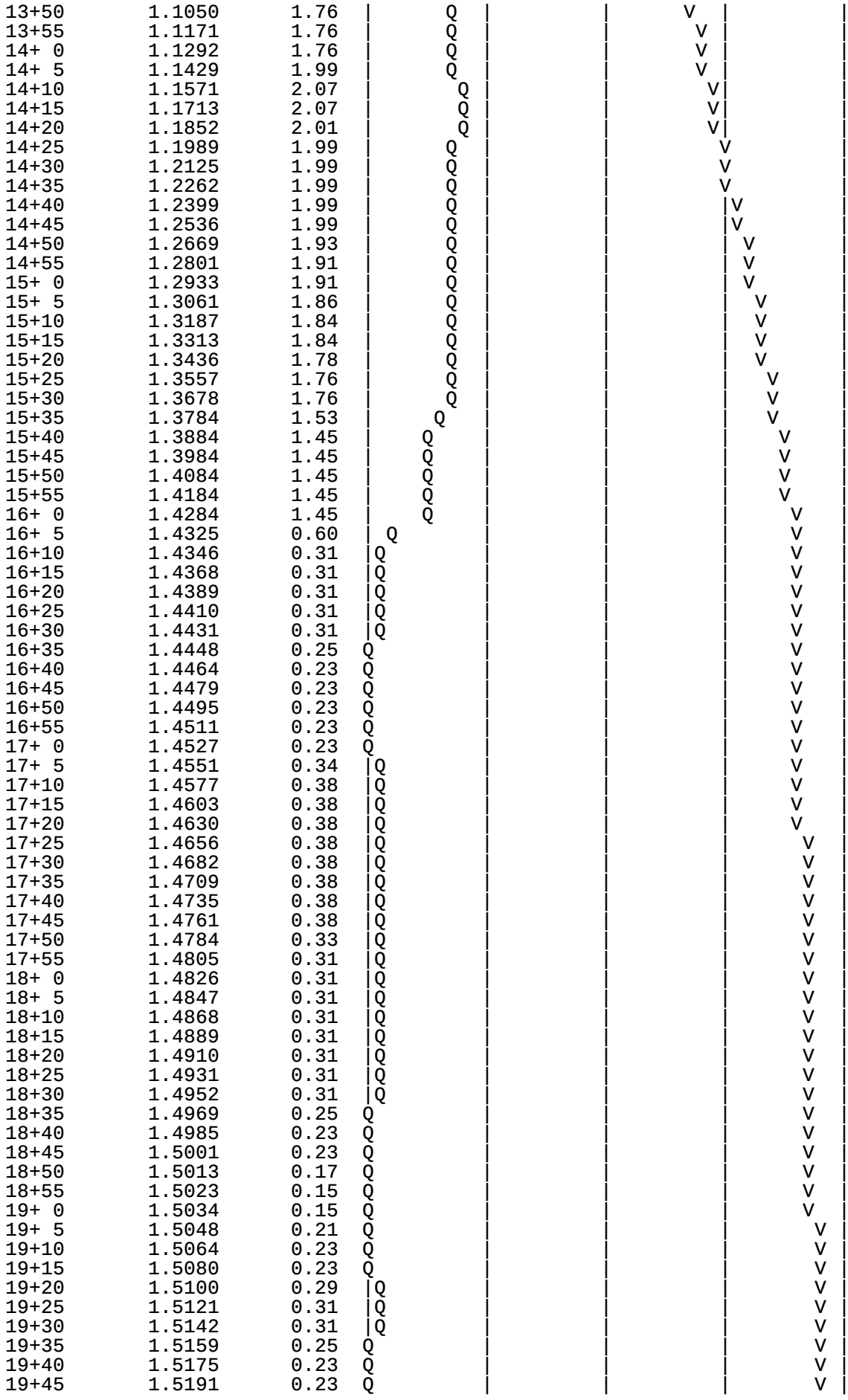
7+50	0.3085	0.97	Q V				
7+55	0.3154	0.99	Q V				
8+ 0	0.3222	0.99	Q V				
8+ 5	0.3299	1.11	Q V				
8+10	0.3378	1.15	Q V				
8+15	0.3457	1.15	Q V				
8+20	0.3536	1.15	Q V				
8+25	0.3615	1.15	Q V				
8+30	0.3694	1.15	Q V				
8+35	0.3777	1.20	Q V				
8+40	0.3861	1.22	Q V				
8+45	0.3945	1.22	Q V				
8+50	0.4034	1.28	Q V				
8+55	0.4123	1.30	Q V				
9+ 0	0.4213	1.30	Q V				
9+ 5	0.4310	1.41	Q V				
9+10	0.4410	1.45	Q V				
9+15	0.4510	1.45	Q V				
9+20	0.4614	1.51	Q V				
9+25	0.4720	1.53	Q V				
9+30	0.4825	1.53	Q V				
9+35	0.4934	1.59	Q V				
9+40	0.5045	1.61	Q V				
9+45	0.5156	1.61	Q V				
9+50	0.5270	1.66	Q V				
9+55	0.5386	1.68	Q V				
10+ 0	0.5502	1.68	Q V				
10+ 5	0.5590	1.28	Q V				
10+10	0.5669	1.15	Q V				
10+15	0.5748	1.15	Q V				
10+20	0.5827	1.15	Q V				
10+25	0.5906	1.15	Q V				
10+30	0.5985	1.15	Q V				
10+35	0.6084	1.43	Q V				
10+40	0.6189	1.53	Q V				
10+45	0.6295	1.53	Q V				
10+50	0.6400	1.53	Q V				
10+55	0.6505	1.53	Q V				
11+ 0	0.6611	1.53	Q V				
11+ 5	0.6712	1.47	Q V				
11+10	0.6812	1.45	Q V				
11+15	0.6912	1.45	Q V				
11+20	0.7013	1.45	Q V				
11+25	0.7113	1.45	Q V				
11+30	0.7213	1.45	Q V				
11+35	0.7305	1.34	Q V				
11+40	0.7395	1.30	Q V				
11+45	0.7484	1.30	Q V				
11+50	0.7578	1.36	Q V				
11+55	0.7672	1.38	Q V				
12+ 0	0.7767	1.38	Q V				
12+ 5	0.7890	1.78	Q V				
12+10	0.8021	1.91	Q V				
12+15	0.8153	1.91	Q V				
12+20	0.8289	1.97	Q V				
12+25	0.8425	1.99	Q V				
12+30	0.8562	1.99	Q V				
12+35	0.8707	2.10	Q V				
12+40	0.8855	2.14	Q V				
12+45	0.9002	2.14	Q V				
12+50	0.9154	2.20	Q V				
12+55	0.9306	2.22	Q V				
13+ 0	0.9459	2.22	Q V				
13+ 5	0.9634	2.54	Q V				
13+10	0.9817	2.65	Q V				
13+15	1.0000	2.65	Q V				
13+20	1.0183	2.66	Q V				
13+25	1.0366	2.66	Q V				
13+30	1.0549	2.66	Q V				
13+35	1.0686	1.99	Q V				
13+40	1.0807	1.76	Q V				
13+45	1.0928	1.76	Q V				


13+50 1.1050 1.76
13+55 1.1171 1.76
14+ 0 1.1292 1.76
14+ 5 1.1429 1.99
14+10 1.1571 2.07
14+15 1.1713 2.07
14+20 1.1852 2.01
14+25 1.1989 1.99
14+30 1.2125 1.99
14+35 1.2262 1.99
14+40 1.2399 1.99
14+45 1.2536 1.99
14+50 1.2669 1.93
14+55 1.2801 1.91
15+ 0 1.2933 1.91
15+ 5 1.3061 1.86
15+10 1.3187 1.84
15+15 1.3313 1.84
15+20 1.3436 1.78
15+25 1.3557 1.76
15+30 1.3678 1.76
15+35 1.3784 1.53
15+40 1.3884 1.45
15+45 1.3984 1.45
15+50 1.4084 1.45
15+55 1.4184 1.45
16+ 0 1.4284 1.45
16+ 5 1.4325 0.60
16+10 1.4346 0.31
16+15 1.4368 0.31
16+20 1.4389 0.31
16+25 1.4410 0.31
16+30 1.4431 0.31
16+35 1.4448 0.25
16+40 1.4464 0.23
16+45 1.4479 0.23
16+50 1.4495 0.23
16+55 1.4511 0.23
17+ 0 1.4527 0.23
17+ 5 1.4551 0.34
17+10 1.4577 0.38
17+15 1.4603 0.38
17+20 1.4630 0.38
17+25 1.4656 0.38
17+30 1.4682 0.38
17+35 1.4709 0.38
17+40 1.4735 0.38
17+45 1.4761 0.38
17+50 1.4784 0.33
17+55 1.4805 0.31
18+ 0 1.4826 0.31
18+ 5 1.4847 0.31
18+10 1.4868 0.31
18+15 1.4889 0.31
18+20 1.4910 0.31
18+25 1.4931 0.31
18+30 1.4952 0.31
18+35 1.4969 0.25
18+40 1.4985 0.23
18+45 1.5001 0.23
18+50 1.5013 0.17
18+55 1.5023 0.15
19+ 0 1.5034 0.15
19+ 5 1.5048 0.21
19+10 1.5064 0.23
19+15 1.5080 0.23
19+20 1.5100 0.29
19+25 1.5121 0.31
19+30 1.5142 0.31
19+35 1.5159 0.25
19+40 1.5175 0.23
19+45 1.5191 0.23

19+50	1.5203	0.17	Q	|	|	|	V |
19+55	1.5213	0.15	Q	|	|	|	V |
20+ 0	1.5224	0.15	Q	|	|	|	V |
20+ 5	1.5238	0.21	Q	|	|	|	V |
20+10	1.5254	0.23	Q	|	|	|	V |
20+15	1.5270	0.23	Q	|	|	|	V |
20+20	1.5285	0.23	Q	|	|	|	V |
20+25	1.5301	0.23	Q	|	|	|	V |
20+30	1.5317	0.23	Q	|	|	|	V |
20+35	1.5333	0.23	Q	|	|	|	V |
20+40	1.5349	0.23	Q	|	|	|	V |
20+45	1.5364	0.23	Q	|	|	|	V |
20+50	1.5376	0.17	Q	|	|	|	V |
20+55	1.5387	0.15	Q	|	|	|	V |
21+ 0	1.5397	0.15	Q	|	|	|	V |
21+ 5	1.5412	0.21	Q	|	|	|	V |
21+10	1.5428	0.23	Q	|	|	|	V |
21+15	1.5444	0.23	Q	|	|	|	V|
21+20	1.5455	0.17	Q	|	|	|	V|
21+25	1.5466	0.15	Q	|	|	|	V|
21+30	1.5476	0.15	Q	|	|	|	V|
21+35	1.5491	0.21	Q	|	|	|	V|
21+40	1.5507	0.23	Q	|	|	|	V|
21+45	1.5523	0.23	Q	|	|	|	V|
21+50	1.5534	0.17	Q	|	|	|	V|
21+55	1.5545	0.15	Q	|	|	|	V|
22+ 0	1.5555	0.15	Q	|	|	|	V|
22+ 5	1.5570	0.21	Q	|	|	|	V|
22+10	1.5586	0.23	Q	|	|	|	V|
22+15	1.5602	0.23	Q	|	|	|	V|
22+20	1.5613	0.17	Q	|	|	|	V|
22+25	1.5624	0.15	Q	|	|	|	V|
22+30	1.5634	0.15	Q	|	|	|	V|
22+35	1.5645	0.15	Q	|	|	|	V|
22+40	1.5656	0.15	Q	|	|	|	V|
22+45	1.5666	0.15	Q	|	|	|	V|
22+50	1.5677	0.15	Q	|	|	|	V|
22+55	1.5687	0.15	Q	|	|	|	V|
23+ 0	1.5698	0.15	Q	|	|	|	V|
23+ 5	1.5708	0.15	Q	|	|	|	V|
23+10	1.5719	0.15	Q	|	|	|	V|
23+15	1.5729	0.15	Q	|	|	|	V|
23+20	1.5740	0.15	Q	|	|	|	V|
23+25	1.5750	0.15	Q	|	|	|	V|
23+30	1.5761	0.15	Q	|	|	|	V|
23+35	1.5771	0.15	Q	|	|	|	V|
23+40	1.5782	0.15	Q	|	|	|	V|
23+45	1.5793	0.15	Q	|	|	|	V|
23+50	1.5803	0.15	Q	|	|	|	V|
23+55	1.5814	0.15	Q	|	|	|	V|
24+ 0	1.5824	0.15	Q	|	|	|	V|
24+ 5	1.5827	0.04	Q	|	|	|	V

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD10610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	1.20	7.28

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	3.00	18.21

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.200(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.941(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.940(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %		Unit Hydrograph (CFS)
1	0.083	582.319	74.564		4.561
2	0.167	1164.637	25.436		1.556
			Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.116	(0.097)	0.021	0.095
2	0.17	0.60	0.140	(0.097)	0.025	0.115
3	0.25	0.60	0.140	(0.097)	0.025	0.115
4	0.33	0.60	0.140	(0.097)	0.025	0.115
5	0.42	0.60	0.140	(0.097)	0.025	0.115
6	0.50	0.70	0.163	(0.097)	0.029	0.134
7	0.58	0.70	0.163	(0.097)	0.029	0.134
8	0.67	0.70	0.163	(0.097)	0.029	0.134
9	0.75	0.70	0.163	(0.097)	0.029	0.134
10	0.83	0.70	0.163	(0.097)	0.029	0.134
11	0.92	0.70	0.163	(0.097)	0.029	0.134
12	1.00	0.80	0.186	(0.097)	0.034	0.153
13	1.08	0.80	0.186	(0.097)	0.034	0.153
14	1.17	0.80	0.186	(0.097)	0.034	0.153
15	1.25	0.80	0.186	(0.097)	0.034	0.153
16	1.33	0.80	0.186	(0.097)	0.034	0.153
17	1.42	0.80	0.186	(0.097)	0.034	0.153
18	1.50	0.80	0.186	(0.097)	0.034	0.153
19	1.58	0.80	0.186	(0.097)	0.034	0.153
20	1.67	0.80	0.186	(0.097)	0.034	0.153
21	1.75	0.80	0.186	(0.097)	0.034	0.153
22	1.83	0.80	0.186	(0.097)	0.034	0.153
23	1.92	0.80	0.186	(0.097)	0.034	0.153
24	2.00	0.90	0.210	(0.097)	0.038	0.172
25	2.08	0.80	0.186	(0.097)	0.034	0.153
26	2.17	0.90	0.210	(0.097)	0.038	0.172
27	2.25	0.90	0.210	(0.097)	0.038	0.172
28	2.33	0.90	0.210	(0.097)	0.038	0.172
29	2.42	0.90	0.210	(0.097)	0.038	0.172
30	2.50	0.90	0.210	(0.097)	0.038	0.172
31	2.58	0.90	0.210	(0.097)	0.038	0.172
32	2.67	0.90	0.210	(0.097)	0.038	0.172
33	2.75	1.00	0.233	(0.097)	0.042	0.191
34	2.83	1.00	0.233	(0.097)	0.042	0.191
35	2.92	1.00	0.233	(0.097)	0.042	0.191
36	3.00	1.00	0.233	(0.097)	0.042	0.191
37	3.08	1.00	0.233	(0.097)	0.042	0.191
38	3.17	1.10	0.256	(0.097)	0.046	0.210
39	3.25	1.10	0.256	(0.097)	0.046	0.210
40	3.33	1.10	0.256	(0.097)	0.046	0.210
41	3.42	1.20	0.279	(0.097)	0.050	0.229
42	3.50	1.30	0.303	(0.097)	0.054	0.248

43	3.58	1.40	0.326	(	0.097)	0.059	0.267
44	3.67	1.40	0.326	(	0.097)	0.059	0.267
45	3.75	1.50	0.349	(	0.097)	0.063	0.286
46	3.83	1.50	0.349	(	0.097)	0.063	0.286
47	3.92	1.60	0.373	(	0.097)	0.067	0.306
48	4.00	1.60	0.373	(	0.097)	0.067	0.306
49	4.08	1.70	0.396	(	0.097)	0.071	0.325
50	4.17	1.80	0.419	(	0.097)	0.075	0.344
51	4.25	1.90	0.442	(	0.097)	0.080	0.363
52	4.33	2.00	0.466	(	0.097)	0.084	0.382
53	4.42	2.10	0.489	(	0.097)	0.088	0.401
54	4.50	2.10	0.489	(	0.097)	0.088	0.401
55	4.58	2.20	0.512	(	0.097)	0.092	0.420
56	4.67	2.30	0.536	(	0.097)	0.096	0.439
57	4.75	2.40	0.559		0.097	(0.101)	0.462
58	4.83	2.40	0.559		0.097	(0.101)	0.462
59	4.92	2.50	0.582		0.097	(0.105)	0.485
60	5.00	2.60	0.605		0.097	(0.109)	0.508
61	5.08	3.10	0.722		0.097	(0.130)	0.625
62	5.17	3.60	0.838		0.097	(0.151)	0.741
63	5.25	3.90	0.908		0.097	(0.163)	0.811
64	5.33	4.20	0.978		0.097	(0.176)	0.881
65	5.42	4.70	1.094		0.097	(0.197)	0.997
66	5.50	5.60	1.304		0.097	(0.235)	1.207
67	5.58	1.90	0.442	(	0.097)	0.080	0.363
68	5.67	0.90	0.210	(	0.097)	0.038	0.172
69	5.75	0.60	0.140	(	0.097)	0.025	0.115
70	5.83	0.50	0.116	(	0.097)	0.021	0.095
71	5.92	0.30	0.070	(	0.097)	0.013	0.057
72	6.00	0.20	0.047	(	0.097)	0.008	0.038

(Loss Rate Not Used)

Sum = 100.0 Sum = 19.6

Flood volume = Effective rainfall 1.63(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.8(Ac.Ft)
Total soil loss = 0.31(In)
Total soil loss = 0.156(Ac.Ft)
Total rainfall = 1.94(In)
Flood volume = 35972.4 Cubic Feet
Total soil loss = 6784.6 Cubic Feet

Peak flow rate of this hydrograph = 7.061(CFS)

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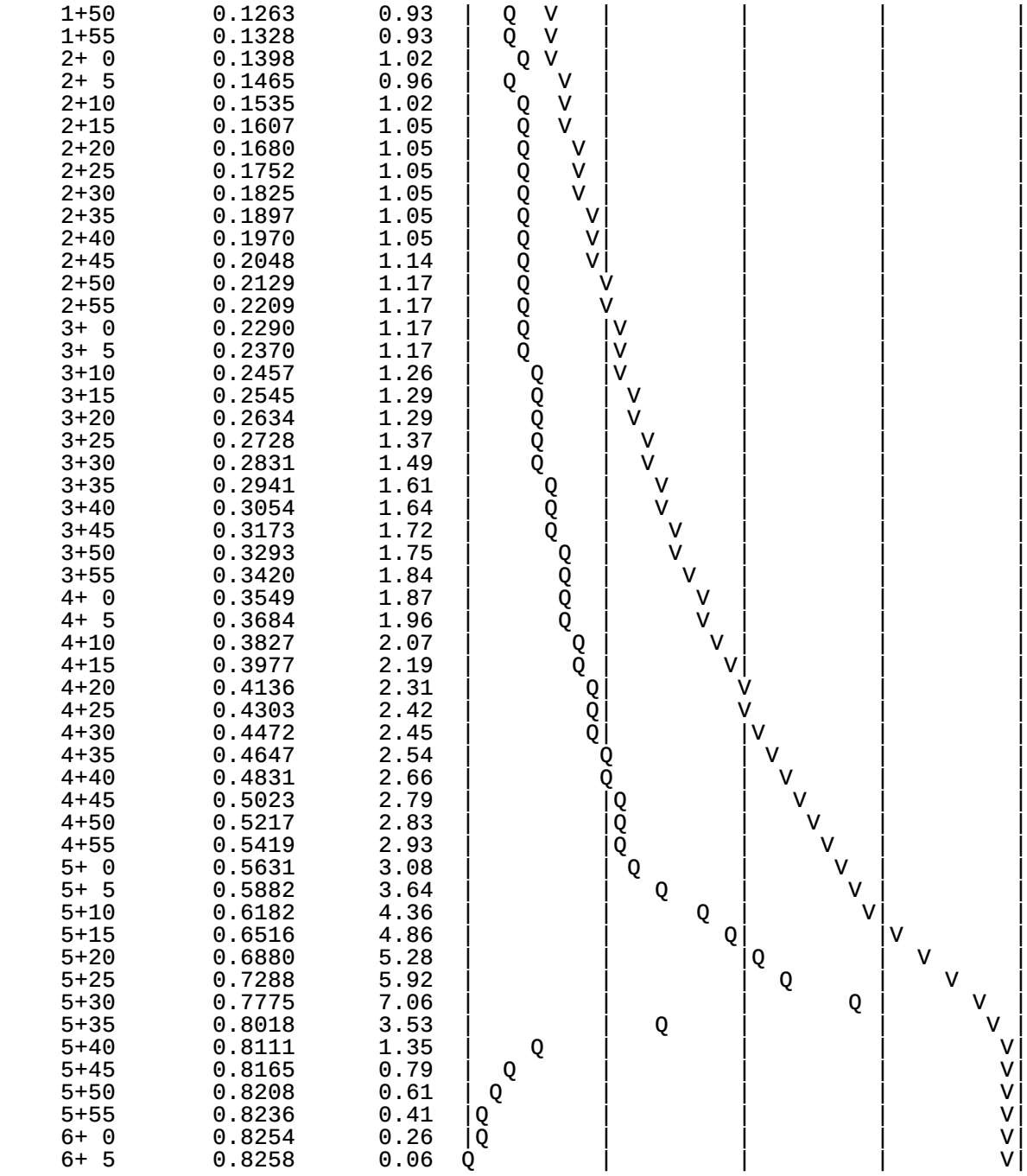
6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0030	0.44	VQ				
0+10	0.0076	0.67	V Q				
0+15	0.0125	0.70	V Q				
0+20	0.0173	0.70	V Q				
0+25	0.0221	0.70	|VQ				
0+30	0.0275	0.79	|V Q				
0+35	0.0332	0.82	|V Q				
0+40	0.0388	0.82	|V Q				
0+45	0.0444	0.82	| VQ				
0+50	0.0501	0.82	| VQ				
0+55	0.0557	0.82	| VQ				
1+ 0	0.0619	0.91	| Q				
1+ 5	0.0684	0.93	| Q				
1+10	0.0748	0.93	| Q				
1+15	0.0813	0.93	| Q				
1+20	0.0877	0.93	| QV				
1+25	0.0941	0.93	| QV				
1+30	0.1006	0.93	| QV				
1+35	0.1070	0.93	| Q V				
1+40	0.1135	0.93	| Q V				
1+45	0.1199	0.93	| Q V				


1+50 0.1263 0.93
1+55 0.1328 0.93
2+ 0 0.1398 1.02
2+ 5 0.1465 0.96
2+10 0.1535 1.02
2+15 0.1607 1.05
2+20 0.1680 1.05
2+25 0.1752 1.05
2+30 0.1825 1.05
2+35 0.1897 1.05
2+40 0.1970 1.05
2+45 0.2048 1.14
2+50 0.2129 1.17
2+55 0.2209 1.17
3+ 0 0.2290 1.17
3+ 5 0.2370 1.17
3+10 0.2457 1.26
3+15 0.2545 1.29
3+20 0.2634 1.29
3+25 0.2728 1.37
3+30 0.2831 1.49
3+35 0.2941 1.61
3+40 0.3054 1.64
3+45 0.3173 1.72
3+50 0.3293 1.75
3+55 0.3420 1.84
4+ 0 0.3549 1.87
4+ 5 0.3684 1.96
4+10 0.3827 2.07
4+15 0.3977 2.19
4+20 0.4136 2.31
4+25 0.4303 2.42
4+30 0.4472 2.45
4+35 0.4647 2.54
4+40 0.4831 2.66
4+45 0.5023 2.79
4+50 0.5217 2.83
4+55 0.5419 2.93
5+ 0 0.5631 3.08
5+ 5 0.5882 3.64
5+10 0.6182 4.36
5+15 0.6516 4.86
5+20 0.6880 5.28
5+25 0.7288 5.92
5+30 0.7775 7.06
5+35 0.8018 3.53
5+40 0.8111 1.35
5+45 0.8165 0.79
5+50 0.8208 0.61
5+55 0.8236 0.41
6+ 0 0.8254 0.26
6+ 5 0.8258 0.06

U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD10310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	0.90	5.46

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	2.35	14.26

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.900(In)
Area Averaged 100-Year Rainfall = 2.350(In)

Point rain (area averaged) = 1.497(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.497(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	582.319	74.564	4.561
2	0.167	1164.637	25.436	1.556
			Sum = 100.000 Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.233	(0.097)	0.042	0.191
2	0.17	1.30	0.233	(0.097)	0.042	0.191
3	0.25	1.10	0.198	(0.097)	0.036	0.162
4	0.33	1.50	0.269	(0.097)	0.048	0.221
5	0.42	1.50	0.269	(0.097)	0.048	0.221
6	0.50	1.80	0.323	(0.097)	0.058	0.265
7	0.58	1.50	0.269	(0.097)	0.048	0.221
8	0.67	1.80	0.323	(0.097)	0.058	0.265
9	0.75	1.80	0.323	(0.097)	0.058	0.265
10	0.83	1.50	0.269	(0.097)	0.048	0.221
11	0.92	1.60	0.287	(0.097)	0.052	0.236
12	1.00	1.80	0.323	(0.097)	0.058	0.265
13	1.08	2.20	0.395	(0.097)	0.071	0.324
14	1.17	2.20	0.395	(0.097)	0.071	0.324
15	1.25	2.20	0.395	(0.097)	0.071	0.324
16	1.33	2.00	0.359	(0.097)	0.065	0.295
17	1.42	2.60	0.467	(0.097)	0.084	0.383
18	1.50	2.70	0.485	(0.097)	0.087	0.398
19	1.58	2.40	0.431	(0.097)	0.078	0.353
20	1.67	2.70	0.485	(0.097)	0.087	0.398
21	1.75	3.30	0.593	0.097	(0.107)	0.496
22	1.83	3.10	0.557	0.097	(0.100)	0.460
23	1.92	2.90	0.521	(0.097)	0.094	0.427
24	2.00	3.00	0.539	(0.097)	0.097	0.442
25	2.08	3.10	0.557	0.097	(0.100)	0.460
26	2.17	4.20	0.754	0.097	(0.136)	0.657
27	2.25	5.00	0.898	0.097	(0.162)	0.801
28	2.33	3.50	0.629	0.097	(0.113)	0.531
29	2.42	6.80	1.221	0.097	(0.220)	1.124
30	2.50	7.30	1.311	0.097	(0.236)	1.214
31	2.58	8.20	1.473	0.097	(0.265)	1.376
32	2.67	5.90	1.060	0.097	(0.191)	0.962
33	2.75	2.00	0.359	(0.097)	0.065	0.295
34	2.83	1.80	0.323	(0.097)	0.058	0.265
35	2.92	1.80	0.323	(0.097)	0.058	0.265
36	3.00	0.60	0.108	(0.097)	0.019	0.088
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	15.4

Flood volume = Effective rainfall 1.28(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.108(Ac.Ft)

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      Total rainfall =      1.50(In)
      Flood volume =       28248.1 Cubic Feet
      Total soil loss =        4726.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      8.167(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ---------------------------------------------------------------------------
   0+ 5       0.0060      0.87  V  Q      |         |         |         |
   0+10       0.0141      1.17  V   Q     |         |         |         |
   0+15       0.0212      1.04  |V  Q     |         |         |         |
   0+20       0.0299      1.26  |V   Q    |         |         |         |
   0+25       0.0392      1.35  | V  Q    |         |         |         |
   0+30       0.0499      1.55  |  V  Q   |         |         |         |
   0+35       0.0597      1.42  |  V Q    |         |         |         |
   0+40       0.0704      1.55  |   V Q   |         |         |         |
   0+45       0.0816      1.62  |    VQ   |         |         |         |
   0+50       0.0914      1.42  |    Q    |         |         |         |
   0+55       0.1011      1.42  |    QV   |         |         |         |
   1+ 0       0.1120      1.58  |     Q   |         |         |         |
   1+ 5       0.1250      1.89  |      Q  |         |         |         |
   1+10       0.1387      1.98  |      QV |         |         |         |
   1+15       0.1523      1.98  |      Q V|         |         |         |
   1+20       0.1651      1.85  |      Q  V         |         |         |
   1+25       0.1802      2.21  |       Q |V        |         |         |
   1+30       0.1969      2.41  |        Q| V       |         |         |
   1+35       0.2122      2.23  |       Q |  V      |         |         |
   1+40       0.2285      2.36  |        Q|   V     |         |         |
   1+45       0.2483      2.88  |         |Q   V    |         |         |
   1+50       0.2681      2.87  |         |Q    V   |         |         |
   1+55       0.2865      2.66  |         Q     V   |         |         |
   2+ 0       0.3049      2.68  |         Q      V  |         |         |
   2+ 5       0.3241      2.79  |         |Q      V |         |         |
   2+10       0.3497      3.71  |         |   Q     |V        |         |
   2+15       0.3819      4.68  |         |     Q   |  V      |         |
   2+20       0.4072      3.67  |         |   Q     |    V    |         |
   2+25       0.4482      5.96  |         |         |  Q   V  |         |
   2+30       0.4984      7.29  |         |         |       QV|         |
   2+35       0.5547      8.17  |         |         |         | Q V     |
   2+40       0.5997      6.53  |         |         |     Q   |     V   |
   2+45       0.6193      2.84  |         |Q        |         |       V |
   2+50       0.6307      1.67  |      Q  |         |         |       V |
   2+55       0.6419      1.62  |      Q  |         |         |        V|
   3+ 0       0.6475      0.82  |  Q      |         |         |        V|
   3+ 5       0.6485      0.14  Q         |         |         |        V|
---------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

Study date 01/04/23 File: 2216PD10110.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6310

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
HYDROLOGIC ANALYSIS
10-YEAR

Drainage Area = 6.07(Ac.) = 0.009 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 6.07(Ac.) = 0.009 Sq. Mi.
Length along longest watercourse = 687.00(Ft.)
Length along longest watercourse measured to centroid = 100.00(Ft.)
Length along longest watercourse = 0.130 Mi.
Length along longest watercourse measured to centroid = 0.019 Mi.
Difference in elevation = 18.60(Ft.)
Slope along watercourse = 142.9520 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.014 Hr.
Lag time = 0.86 Min.
25% of lag time = 0.21 Min.
40% of lag time = 0.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	0.54	3.28

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
6.07	1.36	8.26

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.540(In)
Area Averaged 100-Year Rainfall = 1.360(In)

Point rain (area averaged) = 0.877(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.877(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
6.070	56.00	0.900

Total Area Entered = 6.07(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.900	0.097	1.000	0.097
					Sum (F) =	0.097

Area averaged mean soil loss (F) (In/Hr) = 0.097
Minimum soil loss rate ((In/Hr)) = 0.049
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.180

Slope of intensity-duration curve for a 1 hour storm =0.4800

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	582.319	74.564	4.561
2	0.167	1164.637	25.436	1.556
		Sum = 100.000	Sum=	6.117

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.40	0.463	(0.097)	0.083	0.380
2	0.17	4.50	0.474	(0.097)	0.085	0.388
3	0.25	5.40	0.568	0.097	(0.102)	0.471
4	0.33	5.40	0.568	0.097	(0.102)	0.471
5	0.42	5.70	0.600	0.097	(0.108)	0.503
6	0.50	6.40	0.674	0.097	(0.121)	0.577
7	0.58	7.90	0.832	0.097	(0.150)	0.735
8	0.67	9.10	0.958	0.097	(0.172)	0.861
9	0.75	12.80	1.348	0.097	(0.243)	1.250
10	0.83	25.60	2.695	0.097	(0.485)	2.598
11	0.92	7.90	0.832	0.097	(0.150)	0.735
12	1.00	4.90	0.516	(0.097)	0.093	0.423
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	9.4

Flood volume = Effective rainfall 0.78(In)
times area 6.1(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.09(In)
Total soil loss = 0.048(Ac.Ft)
Total rainfall = 0.88(In)
Flood volume = 17246.6 Cubic Feet
Total soil loss = 2084.0 Cubic Feet

Peak flow rate of this hydrograph = 13.804(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0119	1.73	|V Q				
0+10	0.0282	2.36		V Q				
0+15	0.0472	2.76		VQ				
0+20	0.0671	2.89		QV				
0+25	0.0879	3.03		Q V				
0+30	0.1115	3.42		Q |V			
0+35	0.1407	4.25		Q	V			

```
   0+40       0.1757       5.07  |          Q       V  |           |           |
   0+45       0.2242       7.05  |          |   Q      | V         |           |
   0+50       0.3193      13.80  |          |          |       Q   | V         |
   0+55       0.3702       7.40  |          |   Q      |           |       V   |
   1+ 0       0.3914       3.07  |     Q    |          |           |         V |
   1+ 5       0.3959       0.66  |Q         |          |           |           V
-------------------------------------------------------------------------------
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Technical Appendix F

Underground Storage Analysis
Proposed Condition

Temescal Canyon Self Storage - Riverside County
Underground Storage Analysis

West

Storage

Arch Span (ft)	Arch Rise (ft)	Number Rows (#)	Row Length (ft)	Row Slope (ft/ft)	Invert (D/S) (ft)	Invert U/S (ft)
16	4	2	340	0.0010	900.50	900.84

Low Flow Discharge

Orifice C ()	Number Outlets (#)	Outlet Diameter (in)	Outlet Invert (ft)	Outlet Soffit (ft)
0.60	1	3	900.50	900.75

High Flow Discharge

Orifice C ()	Number Outlets (#)	Outlet Diameter (in)	Outlet Invert (ft)	Outlet Soffit (ft)
0.60	1	12	903.60	904.60

Rating Curve

Elevation (ft)	Depth (ft)	Storage (cu-ft)	Storage (ac-ft)	Low Flow Discharge (cfs)	High Flow Discharge (cfs)	Total Discharge (cfs)
900.50	0.00	0	0.000	0.000	0.000	0.000
900.75	0.25	960	0.022	0.118	0.000	0.118
900.84	0.34	1,850	0.042	0.138	0.000	0.138
901.00	0.50	3,536	0.081	0.167	0.000	0.167
901.50	1.00	8,967	0.206	0.236	0.000	0.236
901.85	1.35	12,742	0.293	0.275	0.000	0.275
902.00	1.50	14,349	0.329	0.289	0.000	0.289
902.50	2.00	19,624	0.451	0.334	0.000	0.334
903.00	2.50	24,712	0.567	0.374	0.000	0.374
903.50	3.00	29,507	0.677	0.409	0.000	0.409
903.60	3.10	30,377	0.697	0.416	0.000	0.416
904.00	3.50	33,761	0.775	0.442	0.893	1.336
904.50	4.00	36,637	0.841	0.473	3.401	3.874
904.60	4.10	36,863	0.846	0.479	3.782	4.260
904.84	4.34	37,427	0.859	0.492	4.211	4.703

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
24-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA02242.rte
**********HYDROGRAPH DATA**********
Number of intervals = 290
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.194 (CFS)
Total volume = 0.726 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 290
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.3	0.60	0.90	1.19	Depth (Ft.)
0.083	0.04	0.00	0.000	OI					0.00
0.167	0.07	0.00	0.000	OI					0.01
0.250	0.07	0.01	0.001	OI					0.01
0.333	0.09	0.01	0.001	O I					0.02
0.417	0.10	0.01	0.002	O I					0.02
0.500	0.11	0.01	0.003	O I					0.03
0.583	0.11	0.02	0.003	O I					0.04
0.667	0.11	0.02	0.004	O I					0.04
0.750	0.11	0.02	0.004	O I					0.05
0.833	0.13	0.03	0.005	O I					0.06
0.917	0.14	0.03	0.006	O I					0.07
1.000	0.14	0.03	0.007	O I					0.07
1.083	0.12	0.04	0.007	O I					0.08
1.167	0.11	0.04	0.008	OI					0.09
1.250	0.11	0.04	0.008	OI					0.09
1.333	0.11	0.05	0.009	OI					0.10
1.417	0.11	0.05	0.009	OI					0.10
1.500	0.11	0.05	0.009	OI					0.11
1.583	0.11	0.05	0.010	OI					0.11
1.667	0.11	0.05	0.010	OI					0.11
1.750	0.11	0.06	0.010	OI					0.12
1.833	0.13	0.06	0.011	O I					0.12
1.917	0.14	0.06	0.011	O I					0.13
2.000	0.14	0.06	0.012	O I					0.13
2.083	0.14	0.07	0.012	O I					0.14
2.167	0.14	0.07	0.013	O I					0.15
2.250	0.14	0.07	0.013	O I					0.15
2.333	0.14	0.07	0.014	O I					0.16
2.417	0.14	0.08	0.014	OI					0.16
2.500	0.14	0.08	0.015	OI					0.17
2.583	0.16	0.08	0.015	O I					0.17
2.667	0.17	0.08	0.016	O I					0.18
2.750	0.18	0.09	0.016	O I					0.19
2.833	0.18	0.09	0.017	O I					0.19
2.917	0.18	0.09	0.018	O I					0.20
3.000	0.18	0.10	0.018	O I					0.21
3.083	0.18	0.10	0.019	O I					0.21
3.167	0.18	0.10	0.019	O I					0.22
3.250	0.18	0.11	0.020	O I					0.22
3.333	0.18	0.11	0.020	O I					0.23
3.417	0.18	0.11	0.021	O I					0.23
3.500	0.18	0.11	0.021	OI					0.24
3.583	0.18	0.11	0.021	OI					0.24
3.667	0.18	0.12	0.022	OI					0.25
3.750	0.18	0.12	0.022	OI					0.25
3.833	0.20	0.12	0.023	O I					0.25
3.917	0.21	0.12	0.023	O I					0.26
4.000	0.21	0.12	0.024	O I					0.26
4.083	0.21	0.12	0.025	O I					0.26
4.167	0.21	0.12	0.025	O I					0.26
4.250	0.21	0.12	0.026	O I					0.27
4.333	0.23	0.12	0.026	O I					0.27
4.417	0.24	0.12	0.027	O I					0.27
4.500	0.25	0.12	0.028	O I					0.28
4.583	0.25	0.12	0.029	O I					0.28
4.667	0.25	0.13	0.030	O I					0.28
4.750	0.25	0.13	0.031	O I					0.29
4.833	0.27	0.13	0.031	O I					0.29
4.917	0.28	0.13	0.032	O I					0.30
5.000	0.28	0.13	0.033	O I					0.30
5.083	0.24	0.13	0.034	O I					0.31
5.167	0.21	0.13	0.035	O I					0.31
5.250	0.21	0.13	0.036	O I					0.31
5.333	0.23	0.13	0.036	O I					0.31
5.417	0.24	0.13	0.037	O I					0.32

5.500	0.25	0.13	0.038	O I				0.32
5.583	0.27	0.13	0.039	O I				0.32
5.667	0.28	0.14	0.039	O I				0.33
5.750	0.28	0.14	0.040	O I				0.33
5.833	0.28	0.14	0.041	O I				0.34
5.917	0.28	0.14	0.042	O I				0.34
6.000	0.28	0.14	0.043	O I				0.35
6.083	0.30	0.14	0.044	O I				0.35
6.167	0.31	0.14	0.046	O I				0.35
6.250	0.32	0.14	0.047	O I				0.36
6.333	0.32	0.14	0.048	O I				0.36
6.417	0.32	0.14	0.049	O I				0.37
6.500	0.32	0.14	0.050	O I				0.37
6.583	0.34	0.15	0.052	O I				0.38
6.667	0.35	0.15	0.053	O I				0.39
6.750	0.35	0.15	0.054	O I				0.39
6.833	0.35	0.15	0.056	O I				0.40
6.917	0.35	0.15	0.057	O I				0.40
7.000	0.35	0.15	0.059	O I				0.41
7.083	0.35	0.15	0.060	O I				0.41
7.167	0.35	0.15	0.061	O I				0.42
7.250	0.35	0.15	0.063	O I				0.43
7.333	0.37	0.15	0.064	O I				0.43
7.417	0.38	0.16	0.066	O I				0.44
7.500	0.39	0.16	0.067	O I				0.44
7.583	0.41	0.16	0.069	O I				0.45
7.667	0.42	0.16	0.071	O I				0.46
7.750	0.42	0.16	0.072	O I				0.46
7.833	0.44	0.16	0.074	O I				0.47
7.917	0.45	0.16	0.076	O I				0.48
8.000	0.46	0.16	0.078	O I				0.49
8.083	0.50	0.17	0.080	O I				0.50
8.167	0.52	0.17	0.083	O I				0.51
8.250	0.53	0.17	0.085	O I				0.52
8.333	0.53	0.17	0.088	O I				0.53
8.417	0.53	0.17	0.090	O I				0.54
8.500	0.53	0.17	0.093	O I				0.55
8.583	0.55	0.17	0.095	O I				0.56
8.667	0.56	0.18	0.098	O I				0.57
8.750	0.56	0.18	0.100	O I				0.58
8.833	0.58	0.18	0.103	O I				0.59
8.917	0.60	0.18	0.106	O I				0.60
9.000	0.60	0.18	0.109	O I				0.61
9.083	0.64	0.18	0.112	O I				0.62
9.167	0.66	0.19	0.115	O I				0.64
9.250	0.67	0.19	0.118	O I				0.65
9.333	0.69	0.19	0.122	O I				0.66
9.417	0.70	0.19	0.125	O I				0.68
9.500	0.70	0.19	0.129	O I				0.69
9.583	0.72	0.20	0.132	O I				0.70
9.667	0.74	0.20	0.136	O I				0.72
9.750	0.74	0.20	0.140	O I				0.73
9.833	0.76	0.20	0.143	O I				0.75
9.917	0.77	0.20	0.147	O I				0.76
10.000	0.77	0.21	0.151	O I				0.78
10.083	0.63	0.21	0.154	O I				0.79
10.167	0.54	0.21	0.157	O I				0.80
10.250	0.53	0.21	0.159	O I				0.81
10.333	0.53	0.21	0.161	O I				0.82
10.417	0.53	0.21	0.164	O I				0.83
10.500	0.53	0.21	0.166	O I				0.84
10.583	0.63	0.22	0.168	O I				0.85
10.667	0.69	0.22	0.171	O I				0.86
10.750	0.70	0.22	0.175	O I				0.87
10.833	0.70	0.22	0.178	O I				0.89
10.917	0.70	0.22	0.181	O I				0.90
11.000	0.70	0.22	0.185	O I				0.91
11.083	0.68	0.23	0.188	O I				0.93
11.167	0.67	0.23	0.191	O I				0.94
11.250	0.67	0.23	0.194	O I				0.95
11.333	0.67	0.23	0.197	O I				0.96
11.417	0.67	0.23	0.200	O I				0.98

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11.500    0.67    0.23      0.203  |     O |       |I      |       |     0.99
11.583    0.63    0.24      0.206  |     O |       I       |       |     1.00
11.667    0.60    0.24      0.208  |     O |       I       |       |     1.01
11.750    0.60    0.24      0.211  |     O |       I       |       |     1.02
11.833    0.62    0.24      0.213  |     O |       I       |       |     1.03
11.917    0.63    0.24      0.216  |     O |       I       |       |     1.04
12.000    0.63    0.24      0.219  |     O |       I       |       |     1.05
12.083    0.77    0.24      0.222  |     O |       |   I   |       |     1.06
12.167    0.86    0.24      0.226  |     O |       |     I|       |     1.08
12.250    0.88    0.25      0.230  |     O |       |      I|       |     1.10
12.333    0.90    0.25      0.235  |     O |       |       I       |     1.12
12.417    0.91    0.25      0.239  |     O |       |       I       |     1.13
12.500    0.91    0.25      0.244  |     O |       |       I       |     1.15
12.583    0.95    0.25      0.248  |     O |       |       |I      |     1.17
12.667    0.98    0.26      0.253  |     O |       |       | I     |     1.19
12.750    0.98    0.26      0.258  |     O |       |       | I     |     1.21
12.833    1.00    0.26      0.263  |      O|       |       | I     |     1.23
12.917    1.02    0.26      0.268  |      O|       |       |  I    |     1.25
13.000    1.02    0.27      0.274  |      O|       |       |  I    |     1.27
13.083    1.12    0.27      0.279  |      O|       |       |    I  |     1.29
13.167    1.18    0.27      0.285  |      O|       |       |     I|     1.32
13.250    1.19    0.27      0.291  |      O|       |       |      I     1.34
13.333    1.19    0.28      0.298  |      O|       |       |      I     1.37
13.417    1.19    0.28      0.304  |      O|       |       |      I     1.40
13.500    1.19    0.28      0.310  |      O|       |       |      I     1.42
13.583    0.97    0.28      0.316  |      O|       |       | I     |     1.45
13.667    0.83    0.29      0.320  |      O|       |     I |       |     1.46
13.750    0.81    0.29      0.324  |      O|       |    I  |       |     1.48
13.833    0.81    0.29      0.327  |      O|       |    I  |       |     1.49
13.917    0.81    0.29      0.331  |      O|       |    I  |       |     1.51
14.000    0.81    0.29      0.335  |      O|       |    I  |       |     1.52
14.083    0.89    0.29      0.338  |      O|       |      I|       |     1.54
14.167    0.94    0.29      0.343  |      O|       |       |I      |     1.56
14.250    0.95    0.30      0.347  |      O|       |       |I      |     1.57
14.333    0.93    0.30      0.352  |      O|       |       I       |     1.59
14.417    0.92    0.30      0.356  |       O       |       I       |     1.61
14.500    0.91    0.30      0.360  |       O       |       I       |     1.63
14.583    0.91    0.30      0.364  |       O       |       I       |     1.64
14.667    0.91    0.30      0.369  |       O       |       I       |     1.66
14.750    0.91    0.31      0.373  |       O       |       I       |     1.68
14.833    0.89    0.31      0.377  |       O       |      I|       |     1.70
14.917    0.88    0.31      0.381  |       O       |      I|       |     1.71
15.000    0.88    0.31      0.385  |       O       |      I|       |     1.73
15.083    0.86    0.31      0.389  |       O       |     I |       |     1.74
15.167    0.84    0.31      0.392  |       O       |     I |       |     1.76
15.250    0.84    0.31      0.396  |       O       |     I |       |     1.77
15.333    0.82    0.32      0.400  |       O       |     I |       |     1.79
15.417    0.81    0.32      0.403  |       O       |    I  |       |     1.80
15.500    0.81    0.32      0.406  |       O       |    I  |       |     1.82
15.583    0.73    0.32      0.409  |       O       |  I    |       |     1.83
15.667    0.68    0.32      0.412  |       O       | I     |       |     1.84
15.750    0.67    0.32      0.414  |       O       |I      |       |     1.85
15.833    0.67    0.32      0.417  |       O       |I      |       |     1.86
15.917    0.67    0.32      0.419  |       O       |I      |       |     1.87
16.000    0.67    0.32      0.422  |       O       |I      |       |     1.88
16.083    0.36    0.32      0.423  |       OI      |       |       |     1.89
16.167    0.17    0.32      0.423  |    I  O       |       |       |     1.88
16.250    0.14    0.32      0.421  |   I   O       |       |       |     1.88
16.333    0.14    0.32      0.420  |   I   O       |       |       |     1.87
16.417    0.14    0.32      0.419  |   I   O       |       |       |     1.87
16.500    0.14    0.32      0.418  |   I   O       |       |       |     1.86
16.583    0.12    0.32      0.416  |   I   O       |       |       |     1.86
16.667    0.11    0.32      0.415  | I     O       |       |       |     1.85
16.750    0.11    0.32      0.413  | I     O       |       |       |     1.85
16.833    0.11    0.32      0.412  | I     O       |       |       |     1.84
16.917    0.11    0.32      0.410  | I     O       |       |       |     1.83
17.000    0.11    0.32      0.409  | I     O       |       |       |     1.83
17.083    0.15    0.32      0.408  |  I    O       |       |       |     1.82
17.167    0.17    0.32      0.407  |    I  O       |       |       |     1.82
17.250    0.18    0.32      0.406  |    I  O       |       |       |     1.81
17.333    0.18    0.32      0.405  |    I  O       |       |       |     1.81
17.417    0.18    0.32      0.404  |    I  O       |       |       |     1.81
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17.500	0.18	0.32	0.403	| I O |	|	|	1.80
17.583	0.18	0.32	0.402	| I O |	|	|	1.80
17.667	0.18	0.32	0.401	| I O |	|	|	1.79
17.750	0.18	0.32	0.400	| I O |	|	|	1.79
17.833	0.16	0.31	0.399	| I O |	|	|	1.79
17.917	0.14	0.31	0.398	| I O |	|	|	1.78
18.000	0.14	0.31	0.396	| I O |	|	|	1.78
18.083	0.14	0.31	0.395	| I O |	|	|	1.77
18.167	0.14	0.31	0.394	| I O |	|	|	1.77
18.250	0.14	0.31	0.393	| I O |	|	|	1.76
18.333	0.14	0.31	0.392	| I O |	|	|	1.76
18.417	0.14	0.31	0.390	| I O |	|	|	1.75
18.500	0.14	0.31	0.389	| I O |	|	|	1.75
18.583	0.12	0.31	0.388	| I O |	|	|	1.74
18.667	0.11	0.31	0.387	| I O |	|	|	1.74
18.750	0.11	0.31	0.385	| I O |	|	|	1.73
18.833	0.09	0.31	0.384	| I O |	|	|	1.72
18.917	0.07	0.31	0.382	|I O |	|	|	1.72
19.000	0.07	0.31	0.381	|I O |	|	|	1.71
19.083	0.09	0.31	0.379	| I O |	|	|	1.71
19.167	0.10	0.31	0.378	| I O |	|	|	1.70
19.250	0.11	0.31	0.376	| I O |	|	|	1.69
19.333	0.13	0.31	0.375	| I O |	|	|	1.69
19.417	0.14	0.31	0.374	| I O |	|	|	1.68
19.500	0.14	0.31	0.373	| I O |	|	|	1.68
19.583	0.12	0.30	0.371	| I O |	|	|	1.67
19.667	0.11	0.30	0.370	| I O |	|	|	1.67
19.750	0.11	0.30	0.369	| I O |	|	|	1.66
19.833	0.09	0.30	0.367	| I O |	|	|	1.66
19.917	0.07	0.30	0.366	|I O |	|	|	1.65
20.000	0.07	0.30	0.364	|I O |	|	|	1.64
20.083	0.09	0.30	0.363	| I O |	|	|	1.64
20.167	0.10	0.30	0.361	| I O |	|	|	1.63
20.250	0.11	0.30	0.360	| I O |	|	|	1.63
20.333	0.11	0.30	0.358	| I O |	|	|	1.62
20.417	0.11	0.30	0.357	| I O |	|	|	1.62
20.500	0.11	0.30	0.356	| I O |	|	|	1.61
20.583	0.11	0.30	0.354	| I O|	|	|	1.60
20.667	0.11	0.30	0.353	| I O|	|	|	1.60
20.750	0.11	0.30	0.352	| I O|	|	|	1.59
20.833	0.09	0.30	0.350	| I O|	|	|	1.59
20.917	0.07	0.30	0.349	|I O|	|	|	1.58
21.000	0.07	0.30	0.347	|I O|	|	|	1.58
21.083	0.09	0.30	0.346	| I O|	|	|	1.57
21.167	0.10	0.29	0.345	| I O|	|	|	1.56
21.250	0.11	0.29	0.343	| I O|	|	|	1.56
21.333	0.09	0.29	0.342	| I O|	|	|	1.55
21.417	0.07	0.29	0.340	|I O|	|	|	1.55
21.500	0.07	0.29	0.339	|I O|	|	|	1.54
21.583	0.09	0.29	0.337	| I O|	|	|	1.53
21.667	0.10	0.29	0.336	| I O|	|	|	1.53
21.750	0.11	0.29	0.335	| I O|	|	|	1.52
21.833	0.09	0.29	0.333	| I O|	|	|	1.52
21.917	0.07	0.29	0.332	|I O|	|	|	1.51
22.000	0.07	0.29	0.330	|I O|	|	|	1.51
22.083	0.09	0.29	0.329	| I O|	|	|	1.50
22.167	0.10	0.29	0.328	| I O|	|	|	1.49
22.250	0.11	0.29	0.326	| I O|	|	|	1.49
22.333	0.09	0.29	0.325	| I O|	|	|	1.48
22.417	0.07	0.29	0.324	|I O|	|	|	1.48
22.500	0.07	0.29	0.322	|I O|	|	|	1.47
22.583	0.07	0.29	0.321	|I O|	|	|	1.47
22.667	0.07	0.29	0.319	|I O|	|	|	1.46
22.750	0.07	0.28	0.318	|I O|	|	|	1.45
22.833	0.07	0.28	0.316	|I O|	|	|	1.45
22.917	0.07	0.28	0.315	|I O|	|	|	1.44
23.000	0.07	0.28	0.313	|I O|	|	|	1.43
23.083	0.07	0.28	0.312	|I O|	|	|	1.43
23.167	0.07	0.28	0.310	|I O|	|	|	1.42
23.250	0.07	0.28	0.309	|I O|	|	|	1.42
23.333	0.07	0.28	0.308	|I O|	|	|	1.41
23.417	0.07	0.28	0.306	|I O|	|	|	1.40

23.500	0.07	0.28	0.305	|I	O|	|	|	|	1.40
23.583	0.07	0.28	0.303	|I	O|	|	|	|	1.39
23.667	0.07	0.28	0.302	|I	O|	|	|	|	1.39
23.750	0.07	0.28	0.300	|I	O|	|	|	|	1.38
23.833	0.07	0.28	0.299	|I	O|	|	|	|	1.37
23.917	0.07	0.28	0.297	|I	O|	|	|	|	1.37
24.000	0.07	0.28	0.296	|I	O|	|	|	|	1.36
24.083	0.03	0.28	0.294	I	O|	|	|	|	1.36
24.167	0.00	0.27	0.293	I	O|	|	|	|	1.35
24.250	0.00	0.27	0.291	I	O|	|	|	|	1.34
24.333	0.00	0.27	0.289	I	O|	|	|	|	1.33
24.417	0.00	0.27	0.287	I	O|	|	|	|	1.33
24.500	0.00	0.27	0.285	I	O|	|	|	|	1.32
24.583	0.00	0.27	0.283	I	O|	|	|	|	1.31
24.667	0.00	0.27	0.281	I	O|	|	|	|	1.30
24.750	0.00	0.27	0.280	I	O|	|	|	|	1.30
24.833	0.00	0.27	0.278	I	O|	|	|	|	1.29
24.917	0.00	0.27	0.276	I	O|	|	|	|	1.28
25.000	0.00	0.27	0.274	I	O|	|	|	|	1.27
25.083	0.00	0.27	0.272	I	O|	|	|	|	1.27
25.167	0.00	0.26	0.270	I	O|	|	|	|	1.26
25.250	0.00	0.26	0.269	I	O|	|	|	|	1.25
25.333	0.00	0.26	0.267	I	O|	|	|	|	1.24
25.417	0.00	0.26	0.265	I	O|	|	|	|	1.24
25.500	0.00	0.26	0.263	I	O|	|	|	|	1.23
25.583	0.00	0.26	0.261	I	O |	|	|	|	1.22
25.667	0.00	0.26	0.260	I	O |	|	|	|	1.22
25.750	0.00	0.26	0.258	I	O |	|	|	|	1.21
25.833	0.00	0.26	0.256	I	O |	|	|	|	1.20
25.917	0.00	0.26	0.254	I	O |	|	|	|	1.19
26.000	0.00	0.26	0.252	I	O |	|	|	|	1.19
26.083	0.00	0.26	0.251	I	O |	|	|	|	1.18
26.167	0.00	0.26	0.249	I	O |	|	|	|	1.17
26.250	0.00	0.25	0.247	I	O |	|	|	|	1.17
26.333	0.00	0.25	0.245	I	O |	|	|	|	1.16
26.417	0.00	0.25	0.244	I	O |	|	|	|	1.15
26.500	0.00	0.25	0.242	I	O |	|	|	|	1.14
26.583	0.00	0.25	0.240	I	O |	|	|	|	1.14
26.667	0.00	0.25	0.238	I	O |	|	|	|	1.13
26.750	0.00	0.25	0.237	I	O |	|	|	|	1.12
26.833	0.00	0.25	0.235	I	O |	|	|	|	1.12
26.917	0.00	0.25	0.233	I	O |	|	|	|	1.11
27.000	0.00	0.25	0.232	I	O |	|	|	|	1.10
27.083	0.00	0.25	0.230	I	O |	|	|	|	1.10
27.167	0.00	0.25	0.228	I	O |	|	|	|	1.09
27.250	0.00	0.25	0.227	I	O |	|	|	|	1.08
27.333	0.00	0.24	0.225	I	O |	|	|	|	1.08
27.417	0.00	0.24	0.223	I	O |	|	|	|	1.07
27.500	0.00	0.24	0.221	I	O |	|	|	|	1.06
27.583	0.00	0.24	0.220	I	O |	|	|	|	1.06
27.667	0.00	0.24	0.218	I	O |	|	|	|	1.05
27.750	0.00	0.24	0.216	I	O |	|	|	|	1.04
27.833	0.00	0.24	0.215	I	O |	|	|	|	1.04
27.917	0.00	0.24	0.213	I	O |	|	|	|	1.03
28.000	0.00	0.24	0.212	I	O |	|	|	|	1.02
28.083	0.00	0.24	0.210	I	O |	|	|	|	1.02
28.167	0.00	0.24	0.208	I	O |	|	|	|	1.01
28.250	0.00	0.24	0.207	I	O |	|	|	|	1.00
28.333	0.00	0.24	0.205	I	O |	|	|	|	1.00
28.417	0.00	0.23	0.203	I	O |	|	|	|	0.99
28.500	0.00	0.23	0.202	I	O |	|	|	|	0.98
28.583	0.00	0.23	0.200	I	O |	|	|	|	0.98
28.667	0.00	0.23	0.199	I	O |	|	|	|	0.97
28.750	0.00	0.23	0.197	I	O |	|	|	|	0.96
28.833	0.00	0.23	0.195	I	O |	|	|	|	0.96
28.917	0.00	0.23	0.194	I	O |	|	|	|	0.95
29.000	0.00	0.23	0.192	I	O |	|	|	|	0.94
29.083	0.00	0.23	0.191	I	O |	|	|	|	0.94
29.167	0.00	0.23	0.189	I	O |	|	|	|	0.93
29.250	0.00	0.23	0.188	I	O |	|	|	|	0.93
29.333	0.00	0.22	0.186	I	O |	|	|	|	0.92
29.417	0.00	0.22	0.184	I	O |	|	|	|	0.91

29.500	0.00	0.22	0.183	I	O	|	|	|	0.91
29.583	0.00	0.22	0.181	I	O	|	|	|	0.90
29.667	0.00	0.22	0.180	I	O	|	|	|	0.90
29.750	0.00	0.22	0.178	I	O	|	|	|	0.89
29.833	0.00	0.22	0.177	I	O	|	|	|	0.88
29.917	0.00	0.22	0.175	I	O	|	|	|	0.88
30.000	0.00	0.22	0.174	I	O	|	|	|	0.87
30.083	0.00	0.22	0.172	I	O	|	|	|	0.87
30.167	0.00	0.22	0.171	I	O	|	|	|	0.86
30.250	0.00	0.22	0.169	I	O	|	|	|	0.85
30.333	0.00	0.21	0.168	I	O	|	|	|	0.85
30.417	0.00	0.21	0.166	I	O	|	|	|	0.84
30.500	0.00	0.21	0.165	I	O	|	|	|	0.84
30.583	0.00	0.21	0.163	I	O	|	|	|	0.83
30.667	0.00	0.21	0.162	I	O	|	|	|	0.82
30.750	0.00	0.21	0.160	I	O	|	|	|	0.82
30.833	0.00	0.21	0.159	I	O	|	|	|	0.81
30.917	0.00	0.21	0.158	I	O	|	|	|	0.81
31.000	0.00	0.21	0.156	I	O	|	|	|	0.80
31.083	0.00	0.21	0.155	I	O	|	|	|	0.79
31.167	0.00	0.21	0.153	I	O	|	|	|	0.79
31.250	0.00	0.21	0.152	I	O	|	|	|	0.78
31.333	0.00	0.21	0.150	I	O	|	|	|	0.78
31.417	0.00	0.20	0.149	I	O	|	|	|	0.77
31.500	0.00	0.20	0.148	I	O	|	|	|	0.77
31.583	0.00	0.20	0.146	I	O	|	|	|	0.76
31.667	0.00	0.20	0.145	I	O	|	|	|	0.76
31.750	0.00	0.20	0.143	I	O	|	|	|	0.75
31.833	0.00	0.20	0.142	I	O	|	|	|	0.74
31.917	0.00	0.20	0.141	I	O	|	|	|	0.74
32.000	0.00	0.20	0.139	I	O	|	|	|	0.73
32.083	0.00	0.20	0.138	I	O	|	|	|	0.73
32.167	0.00	0.20	0.137	I	O	|	|	|	0.72
32.250	0.00	0.20	0.135	I	O	|	|	|	0.72
32.333	0.00	0.20	0.134	I	O	|	|	|	0.71
32.417	0.00	0.20	0.133	I	O	|	|	|	0.71
32.500	0.00	0.19	0.131	I	O	|	|	|	0.70
32.583	0.00	0.19	0.130	I	O	|	|	|	0.70
32.667	0.00	0.19	0.128	I	O	|	|	|	0.69
32.750	0.00	0.19	0.127	I	O	|	|	|	0.68
32.833	0.00	0.19	0.126	I	O	|	|	|	0.68
32.917	0.00	0.19	0.125	I	O	|	|	|	0.67
33.000	0.00	0.19	0.123	I	O	|	|	|	0.67
33.083	0.00	0.19	0.122	I	O	|	|	|	0.66
33.167	0.00	0.19	0.121	I	O	|	|	|	0.66
33.250	0.00	0.19	0.119	I	O	|	|	|	0.65
33.333	0.00	0.19	0.118	I	O	|	|	|	0.65
33.417	0.00	0.19	0.117	I	O	|	|	|	0.64
33.500	0.00	0.19	0.115	I	O	|	|	|	0.64
33.583	0.00	0.19	0.114	I	O	|	|	|	0.63
33.667	0.00	0.18	0.113	I	O	|	|	|	0.63
33.750	0.00	0.18	0.112	I	O	|	|	|	0.62
33.833	0.00	0.18	0.110	I	O	|	|	|	0.62
33.917	0.00	0.18	0.109	I	O	|	|	|	0.61
34.000	0.00	0.18	0.108	I	O	|	|	|	0.61
34.083	0.00	0.18	0.107	I	O	|	|	|	0.60
34.167	0.00	0.18	0.105	I	O	|	|	|	0.60
34.250	0.00	0.18	0.104	I	O	|	|	|	0.59
34.333	0.00	0.18	0.103	I	O	|	|	|	0.59
34.417	0.00	0.18	0.102	I	O	|	|	|	0.58
34.500	0.00	0.18	0.100	I	O	|	|	|	0.58
34.583	0.00	0.18	0.099	I	O	|	|	|	0.57
34.667	0.00	0.18	0.098	I	O	|	|	|	0.57
34.750	0.00	0.18	0.097	I	O	|	|	|	0.56
34.833	0.00	0.18	0.096	I	O	|	|	|	0.56
34.917	0.00	0.17	0.094	I	O	|	|	|	0.55
35.000	0.00	0.17	0.093	I	O	|	|	|	0.55
35.083	0.00	0.17	0.092	I	O	|	|	|	0.54
35.167	0.00	0.17	0.091	I	O	|	|	|	0.54
35.250	0.00	0.17	0.090	I	O	|	|	|	0.53
35.333	0.00	0.17	0.088	I	O	|	|	|	0.53
35.417	0.00	0.17	0.087	I	O	|	|	|	0.52

35.500	0.00	0.17	0.086	I	O	|	|	|	0.52
35.583	0.00	0.17	0.085	I	O	|	|	|	0.52
35.667	0.00	0.17	0.084	I	O	|	|	|	0.51
35.750	0.00	0.17	0.083	I	O	|	|	|	0.51
35.833	0.00	0.17	0.081	I	O	|	|	|	0.50
35.917	0.00	0.17	0.080	I	O	|	|	|	0.50
36.000	0.00	0.17	0.079	I	O	|	|	|	0.49
36.083	0.00	0.16	0.078	I	O	|	|	|	0.49
36.167	0.00	0.16	0.077	I	O	|	|	|	0.48
36.250	0.00	0.16	0.076	I	O	|	|	|	0.48
36.333	0.00	0.16	0.075	I	O	|	|	|	0.47
36.417	0.00	0.16	0.073	I	O	|	|	|	0.47
36.500	0.00	0.16	0.072	I	O	|	|	|	0.46
36.583	0.00	0.16	0.071	I	O	|	|	|	0.46
36.667	0.00	0.16	0.070	I	O	|	|	|	0.46
36.750	0.00	0.16	0.069	I	O	|	|	|	0.45
36.833	0.00	0.16	0.068	I	O	|	|	|	0.45
36.917	0.00	0.16	0.067	I	O	|	|	|	0.44
37.000	0.00	0.16	0.066	I	O	|	|	|	0.44
37.083	0.00	0.15	0.065	I	O	|	|	|	0.43
37.167	0.00	0.15	0.064	I	O	|	|	|	0.43
37.250	0.00	0.15	0.063	I	O	|	|	|	0.42
37.333	0.00	0.15	0.062	I	O	|	|	|	0.42
37.417	0.00	0.15	0.061	I	O	|	|	|	0.42
37.500	0.00	0.15	0.060	I	O	|	|	|	0.41
37.583	0.00	0.15	0.058	I	O	|	|	|	0.41
37.667	0.00	0.15	0.057	I	O	|	|	|	0.40
37.750	0.00	0.15	0.056	I	O	|	|	|	0.40
37.833	0.00	0.15	0.055	I	O	|	|	|	0.39
37.917	0.00	0.15	0.054	I	O	|	|	|	0.39
38.000	0.00	0.15	0.053	I	O	|	|	|	0.39
38.083	0.00	0.15	0.052	I	O	|	|	|	0.38
38.167	0.00	0.14	0.051	I	O	|	|	|	0.38
38.250	0.00	0.14	0.050	I	O	|	|	|	0.37
38.333	0.00	0.14	0.049	I	O	|	|	|	0.37
38.417	0.00	0.14	0.048	I	O	|	|	|	0.37
38.500	0.00	0.14	0.047	I	O	|	|	|	0.36
38.583	0.00	0.14	0.046	I	O	|	|	|	0.36
38.667	0.00	0.14	0.045	I	O	|	|	|	0.35
38.750	0.00	0.14	0.044	I	O	|	|	|	0.35
38.833	0.00	0.14	0.044	I	O	|	|	|	0.35
38.917	0.00	0.14	0.043	I	O	|	|	|	0.34
39.000	0.00	0.14	0.042	I	O	|	|	|	0.34
39.083	0.00	0.14	0.041	I	O	|	|	|	0.33
39.167	0.00	0.14	0.040	I	O	|	|	|	0.33
39.250	0.00	0.13	0.039	I	O	|	|	|	0.33
39.333	0.00	0.13	0.038	I	O	|	|	|	0.32
39.417	0.00	0.13	0.037	I	O	|	|	|	0.32
39.500	0.00	0.13	0.036	I	O	|	|	|	0.31
39.583	0.00	0.13	0.035	I	O	|	|	|	0.31
39.667	0.00	0.13	0.034	I	O	|	|	|	0.31
39.750	0.00	0.13	0.033	I	O	|	|	|	0.30
39.833	0.00	0.13	0.032	I	O	|	|	|	0.30
39.917	0.00	0.13	0.032	I	O	|	|	|	0.29
40.000	0.00	0.13	0.031	I	O	|	|	|	0.29
40.083	0.00	0.13	0.030	I	O	|	|	|	0.29
40.167	0.00	0.12	0.029	I	O	|	|	|	0.28
40.250	0.00	0.12	0.028	I	O	|	|	|	0.28
40.333	0.00	0.12	0.027	I	O	|	|	|	0.27
40.417	0.00	0.12	0.026	I	O	|	|	|	0.27
40.500	0.00	0.12	0.026	I	O	|	|	|	0.27
40.583	0.00	0.12	0.025	I	O	|	|	|	0.26
40.667	0.00	0.12	0.024	I	O	|	|	|	0.26
40.750	0.00	0.12	0.023	I	O	|	|	|	0.25
40.833	0.00	0.12	0.022	I	O	|	|	|	0.25
40.917	0.00	0.12	0.021	I	O	|	|	|	0.24
41.000	0.00	0.11	0.021	I	O	|	|	|	0.24
41.083	0.00	0.11	0.020	I	O	|	|	|	0.23
41.167	0.00	0.10	0.019	I	O	|	|	|	0.22
41.250	0.00	0.10	0.019	I	O	|	|	|	0.21
41.333	0.00	0.10	0.018	I	O	|	|	|	0.20
41.417	0.00	0.09	0.017	I	O	|	|	|	0.20

41.500	0.00	0.09	0.017	I O	|	|	|	0.19
41.583	0.00	0.09	0.016	I O	|	|	|	0.18
41.667	0.00	0.08	0.015	I O	|	|	|	0.17
41.750	0.00	0.08	0.015	I O	|	|	|	0.17
41.833	0.00	0.08	0.014	I O	|	|	|	0.16
41.917	0.00	0.07	0.014	IO	|	|	|	0.16
42.000	0.00	0.07	0.013	IO	|	|	|	0.15
42.083	0.00	0.07	0.013	IO	|	|	|	0.15
42.167	0.00	0.07	0.012	IO	|	|	|	0.14
42.250	0.00	0.06	0.012	IO	|	|	|	0.14
42.333	0.00	0.06	0.011	IO	|	|	|	0.13
42.417	0.00	0.06	0.011	IO	|	|	|	0.13
42.500	0.00	0.06	0.011	IO	|	|	|	0.12
42.583	0.00	0.06	0.010	IO	|	|	|	0.12
42.667	0.00	0.05	0.010	IO	|	|	|	0.11
42.750	0.00	0.05	0.010	IO	|	|	|	0.11
42.833	0.00	0.05	0.009	IO	|	|	|	0.10
42.917	0.00	0.05	0.009	IO	|	|	|	0.10
43.000	0.00	0.05	0.009	IO	|	|	|	0.10
43.083	0.00	0.04	0.008	IO	|	|	|	0.09
43.167	0.00	0.04	0.008	IO	|	|	|	0.09
43.250	0.00	0.04	0.008	IO	|	|	|	0.09
43.333	0.00	0.04	0.007	IO	|	|	|	0.08
43.417	0.00	0.04	0.007	IO	|	|	|	0.08
43.500	0.00	0.04	0.007	O	|	|	|	0.08
43.583	0.00	0.04	0.007	O	|	|	|	0.07
43.667	0.00	0.03	0.006	O	|	|	|	0.07
43.750	0.00	0.03	0.006	O	|	|	|	0.07
43.833	0.00	0.03	0.006	O	|	|	|	0.07
43.917	0.00	0.03	0.006	O	|	|	|	0.06
44.000	0.00	0.03	0.005	O	|	|	|	0.06
44.083	0.00	0.03	0.005	O	|	|	|	0.06
44.167	0.00	0.03	0.005	O	|	|	|	0.06
44.250	0.00	0.03	0.005	O	|	|	|	0.06
44.333	0.00	0.03	0.005	O	|	|	|	0.05
44.417	0.00	0.02	0.005	O	|	|	|	0.05
44.500	0.00	0.02	0.004	O	|	|	|	0.05
44.583	0.00	0.02	0.004	O	|	|	|	0.05
44.667	0.00	0.02	0.004	O	|	|	|	0.05
44.750	0.00	0.02	0.004	O	|	|	|	0.04
44.833	0.00	0.02	0.004	O	|	|	|	0.04
44.917	0.00	0.02	0.004	O	|	|	|	0.04
45.000	0.00	0.02	0.004	O	|	|	|	0.04
45.083	0.00	0.02	0.003	O	|	|	|	0.04
45.167	0.00	0.02	0.003	O	|	|	|	0.04
45.250	0.00	0.02	0.003	O	|	|	|	0.04
45.333	0.00	0.02	0.003	O	|	|	|	0.03
45.417	0.00	0.02	0.003	O	|	|	|	0.03
45.500	0.00	0.02	0.003	O	|	|	|	0.03
45.583	0.00	0.01	0.003	O	|	|	|	0.03
45.667	0.00	0.01	0.003	O	|	|	|	0.03
45.750	0.00	0.01	0.003	O	|	|	|	0.03
45.833	0.00	0.01	0.002	O	|	|	|	0.03
45.917	0.00	0.01	0.002	O	|	|	|	0.03
46.000	0.00	0.01	0.002	O	|	|	|	0.03
46.083	0.00	0.01	0.002	O	|	|	|	0.02
46.167	0.00	0.01	0.002	O	|	|	|	0.02
46.250	0.00	0.01	0.002	O	|	|	|	0.02
46.333	0.00	0.01	0.002	O	|	|	|	0.02
46.417	0.00	0.01	0.002	O	|	|	|	0.02
46.500	0.00	0.01	0.002	O	|	|	|	0.02
46.583	0.00	0.01	0.002	O	|	|	|	0.02
46.667	0.00	0.01	0.002	O	|	|	|	0.02
46.750	0.00	0.01	0.002	O	|	|	|	0.02
46.833	0.00	0.01	0.002	O	|	|	|	0.02
46.917	0.00	0.01	0.002	O	|	|	|	0.02
47.000	0.00	0.01	0.001	O	|	|	|	0.02
47.083	0.00	0.01	0.001	O	|	|	|	0.02
47.167	0.00	0.01	0.001	O	|	|	|	0.02
47.250	0.00	0.01	0.001	O	|	|	|	0.01
47.333	0.00	0.01	0.001	O	|	|	|	0.01
47.417	0.00	0.01	0.001	O	|	|	|	0.01

47.500	0.00	0.01	0.001	O	|	|	|	0.01
47.583	0.00	0.01	0.001	O	|	|	|	0.01
47.667	0.00	0.01	0.001	O	|	|	|	0.01
47.750	0.00	0.01	0.001	O	|	|	|	0.01
47.833	0.00	0.01	0.001	O	|	|	|	0.01
47.917	0.00	0.01	0.001	O	|	|	|	0.01
48.000	0.00	0.00	0.001	O	|	|	|	0.01
48.083	0.00	0.00	0.001	O	|	|	|	0.01
48.167	0.00	0.00	0.001	O	|	|	|	0.01
48.250	0.00	0.00	0.001	O	|	|	|	0.01
48.333	0.00	0.00	0.001	O	|	|	|	0.01
48.417	0.00	0.00	0.001	O	|	|	|	0.01
48.500	0.00	0.00	0.001	O	|	|	|	0.01
48.583	0.00	0.00	0.001	O	|	|	|	0.01
48.667	0.00	0.00	0.001	O	|	|	|	0.01
48.750	0.00	0.00	0.001	O	|	|	|	0.01
48.833	0.00	0.00	0.001	O	|	|	|	0.01
48.917	0.00	0.00	0.001	O	|	|	|	0.01
49.000	0.00	0.00	0.001	O	|	|	|	0.01
49.083	0.00	0.00	0.001	O	|	|	|	0.01
49.167	0.00	0.00	0.001	O	|	|	|	0.01
49.250	0.00	0.00	0.001	O	|	|	|	0.01
49.333	0.00	0.00	0.001	O	|	|	|	0.01
49.417	0.00	0.00	0.000	O	|	|	|	0.01
49.500	0.00	0.00	0.000	O	|	|	|	0.01
49.583	0.00	0.00	0.000	O	|	|	|	0.01
49.667	0.00	0.00	0.000	O	|	|	|	0.01
49.750	0.00	0.00	0.000	O	|	|	|	0.00
49.833	0.00	0.00	0.000	O	|	|	|	0.00
49.917	0.00	0.00	0.000	O	|	|	|	0.00
50.000	0.00	0.00	0.000	O	|	|	|	0.00
50.083	0.00	0.00	0.000	O	|	|	|	0.00
50.167	0.00	0.00	0.000	O	|	|	|	0.00
50.250	0.00	0.00	0.000	O	|	|	|	0.00
50.333	0.00	0.00	0.000	O	|	|	|	0.00
50.417	0.00	0.00	0.000	O	|	|	|	0.00
50.500	0.00	0.00	0.000	O	|	|	|	0.00
50.583	0.00	0.00	0.000	O	|	|	|	0.00
50.667	0.00	0.00	0.000	O	|	|	|	0.00
50.750	0.00	0.00	0.000	O	|	|	|	0.00
50.833	0.00	0.00	0.000	O	|	|	|	0.00
50.917	0.00	0.00	0.000	O	|	|	|	0.00
51.000	0.00	0.00	0.000	O	|	|	|	0.00
51.083	0.00	0.00	0.000	O	|	|	|	0.00
51.167	0.00	0.00	0.000	O	|	|	|	0.00
51.250	0.00	0.00	0.000	O	|	|	|	0.00
51.333	0.00	0.00	0.000	O	|	|	|	0.00
51.417	0.00	0.00	0.000	O	|	|	|	0.00
51.500	0.00	0.00	0.000	O	|	|	|	0.00
51.583	0.00	0.00	0.000	O	|	|	|	0.00
51.667	0.00	0.00	0.000	O	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 620
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.324 (CFS)
Total volume = 0.726 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
6-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA0262.rte
**********HYDROGRAPH DATA**********
Number of intervals = 74
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.317 (CFS)
Total volume = 0.436 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 74
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.8	1.66	2.49	3.32	Depth (Ft.)
0.083	0.18	0.00	0.001	OI					0.01
0.167	0.33	0.01	0.002	O I					0.03
0.250	0.38	0.03	0.005	O I					0.05
0.333	0.38	0.04	0.007	O I					0.08
0.417	0.38	0.05	0.009	O I					0.11
0.500	0.42	0.06	0.012	O I					0.13
0.583	0.44	0.08	0.014	O I					0.16
0.667	0.44	0.09	0.017	O I					0.19
0.750	0.44	0.10	0.019	O I					0.22
0.833	0.44	0.11	0.021	O I					0.24
0.917	0.44	0.12	0.024	O I					0.26
1.000	0.48	0.12	0.026	O I					0.27
1.083	0.50	0.12	0.028	O I					0.28
1.167	0.51	0.13	0.031	O I					0.29
1.250	0.51	0.13	0.034	O I					0.30
1.333	0.51	0.13	0.036	O I					0.31
1.417	0.51	0.13	0.039	O I					0.33
1.500	0.51	0.14	0.041	O I					0.34
1.583	0.51	0.14	0.044	O I					0.35
1.667	0.51	0.14	0.046	O I					0.36
1.750	0.51	0.14	0.049	O I					0.37
1.833	0.51	0.14	0.051	O I					0.38
1.917	0.51	0.15	0.054	O I					0.39
2.000	0.54	0.15	0.056	O I					0.40
2.083	0.53	0.15	0.059	O I					0.41
2.167	0.55	0.15	0.062	O I					0.42
2.250	0.57	0.15	0.065	O I					0.43
2.333	0.57	0.16	0.067	O I					0.44
2.417	0.57	0.16	0.070	O I					0.46
2.500	0.57	0.16	0.073	O I					0.47
2.583	0.57	0.16	0.076	O I					0.48
2.667	0.57	0.17	0.079	O I					0.49
2.750	0.61	0.17	0.082	O I					0.50
2.833	0.63	0.17	0.085	O I					0.51
2.917	0.63	0.17	0.088	O I					0.53
3.000	0.63	0.17	0.091	O I					0.54
3.083	0.63	0.17	0.094	O I					0.55
3.167	0.67	0.18	0.097	O I					0.57
3.250	0.69	0.18	0.101	O I					0.58
3.333	0.70	0.18	0.104	O I					0.59
3.417	0.73	0.18	0.108	O I					0.61
3.500	0.79	0.18	0.112	O I					0.62
3.583	0.85	0.19	0.116	O I					0.64
3.667	0.88	0.19	0.121	O I					0.66
3.750	0.92	0.19	0.126	O I					0.68
3.833	0.94	0.19	0.131	O I					0.70
3.917	0.98	0.20	0.136	O I					0.72
4.000	1.01	0.20	0.142	O I					0.74
4.083	1.05	0.20	0.148	O I					0.77
4.167	1.11	0.21	0.154	O I					0.79
4.250	1.17	0.21	0.160	O I					0.82
4.333	1.23	0.21	0.167	O I					0.84
4.417	1.30	0.22	0.174	O I					0.87
4.500	1.32	0.22	0.182	O I					0.90
4.583	1.36	0.23	0.189	O I					0.93
4.667	1.42	0.23	0.197	O I					0.97
4.750	1.49	0.24	0.206	O I					1.00
4.833	1.51	0.24	0.214	O I					1.03
4.917	1.55	0.24	0.223	O I					1.07
5.000	1.61	0.25	0.233	O I					1.11
5.083	1.82	0.25	0.243	O I					1.15
5.167	2.12	0.26	0.254	O I					1.19
5.250	2.37	0.26	0.268	O I					1.25
5.333	2.56	0.27	0.283	O I					1.31
5.417	2.83	0.28	0.300	O I					1.38

5.500	3.32	0.29	0.319	| O	|	|	|	I	1.46
5.583	2.18	0.29	0.336	| O	|	| I	|	|	1.53
5.667	0.97	0.29	0.345	| O	I	|	|	|	1.57
5.750	0.50	0.30	0.348	| O I	|	|	|	|	1.58
5.833	0.35	0.30	0.349	| OI	|	|	|	|	1.58
5.917	0.25	0.30	0.349	| O	|	|	|	|	1.58
6.000	0.16	0.30	0.348	|IO	|	|	|	|	1.58
6.083	0.06	0.30	0.347	I O	|	|	|	|	1.57
6.167	0.01	0.29	0.345	I O	|	|	|	|	1.57
6.250	0.00	0.29	0.343	I O	|	|	|	|	1.56
6.333	0.00	0.29	0.341	I O	|	|	|	|	1.55
6.417	0.00	0.29	0.339	I O	|	|	|	|	1.54
6.500	0.00	0.29	0.337	I O	|	|	|	|	1.53
6.583	0.00	0.29	0.335	I O	|	|	|	|	1.52
6.667	0.00	0.29	0.333	I O	|	|	|	|	1.52
6.750	0.00	0.29	0.331	I O	|	|	|	|	1.51
6.833	0.00	0.29	0.329	I O	|	|	|	|	1.50
6.917	0.00	0.29	0.327	I O	|	|	|	|	1.49
7.000	0.00	0.29	0.325	I O	|	|	|	|	1.48
7.083	0.00	0.29	0.323	I O	|	|	|	|	1.48
7.167	0.00	0.29	0.321	I O	|	|	|	|	1.47
7.250	0.00	0.29	0.319	I O	|	|	|	|	1.46
7.333	0.00	0.28	0.317	I O	|	|	|	|	1.45
7.417	0.00	0.28	0.315	I O	|	|	|	|	1.44
7.500	0.00	0.28	0.313	I O	|	|	|	|	1.43
7.583	0.00	0.28	0.311	I O	|	|	|	|	1.43
7.667	0.00	0.28	0.309	I O	|	|	|	|	1.42
7.750	0.00	0.28	0.307	I O	|	|	|	|	1.41
7.833	0.00	0.28	0.306	I O	|	|	|	|	1.40
7.917	0.00	0.28	0.304	I O	|	|	|	|	1.39
8.000	0.00	0.28	0.302	I O	|	|	|	|	1.39
8.083	0.00	0.28	0.300	I O	|	|	|	|	1.38
8.167	0.00	0.28	0.298	I O	|	|	|	|	1.37
8.250	0.00	0.28	0.296	I O	|	|	|	|	1.36
8.333	0.00	0.28	0.294	I O	|	|	|	|	1.35
8.417	0.00	0.27	0.292	I O	|	|	|	|	1.35
8.500	0.00	0.27	0.290	I O	|	|	|	|	1.34
8.583	0.00	0.27	0.288	I O	|	|	|	|	1.33
8.667	0.00	0.27	0.287	I O	|	|	|	|	1.32
8.750	0.00	0.27	0.285	I O	|	|	|	|	1.32
8.833	0.00	0.27	0.283	I O	|	|	|	|	1.31
8.917	0.00	0.27	0.281	I O	|	|	|	|	1.30
9.000	0.00	0.27	0.279	I O	|	|	|	|	1.29
9.083	0.00	0.27	0.277	I O	|	|	|	|	1.29
9.167	0.00	0.27	0.275	I O	|	|	|	|	1.28
9.250	0.00	0.27	0.274	I O	|	|	|	|	1.27
9.333	0.00	0.27	0.272	I O	|	|	|	|	1.26
9.417	0.00	0.26	0.270	I O	|	|	|	|	1.26
9.500	0.00	0.26	0.268	I O	|	|	|	|	1.25
9.583	0.00	0.26	0.266	I O	|	|	|	|	1.24
9.667	0.00	0.26	0.264	I O	|	|	|	|	1.24
9.750	0.00	0.26	0.263	I O	|	|	|	|	1.23
9.833	0.00	0.26	0.261	I O	|	|	|	|	1.22
9.917	0.00	0.26	0.259	I O	|	|	|	|	1.21
10.000	0.00	0.26	0.257	I O	|	|	|	|	1.21
10.083	0.00	0.26	0.255	I O	|	|	|	|	1.20
10.167	0.00	0.26	0.254	I O	|	|	|	|	1.19
10.250	0.00	0.26	0.252	I O	|	|	|	|	1.18
10.333	0.00	0.26	0.250	I O	|	|	|	|	1.18
10.417	0.00	0.26	0.248	I O	|	|	|	|	1.17
10.500	0.00	0.25	0.247	I O	|	|	|	|	1.16
10.583	0.00	0.25	0.245	I O	|	|	|	|	1.16
10.667	0.00	0.25	0.243	I O	|	|	|	|	1.15
10.750	0.00	0.25	0.241	I O	|	|	|	|	1.14
10.833	0.00	0.25	0.240	I O	|	|	|	|	1.14
10.917	0.00	0.25	0.238	I O	|	|	|	|	1.13
11.000	0.00	0.25	0.236	I O	|	|	|	|	1.12
11.083	0.00	0.25	0.235	I O	|	|	|	|	1.11
11.167	0.00	0.25	0.233	I O	|	|	|	|	1.11
11.250	0.00	0.25	0.231	I O	|	|	|	|	1.10
11.333	0.00	0.25	0.229	I O	|	|	|	|	1.09
11.417	0.00	0.25	0.228	I O	|	|	|	|	1.09

11.500	0.00	0.24	0.226	I O	|	|	|	1.08
11.583	0.00	0.24	0.224	I O	|	|	|	1.07
11.667	0.00	0.24	0.223	I O	|	|	|	1.07
11.750	0.00	0.24	0.221	I O	|	|	|	1.06
11.833	0.00	0.24	0.219	I O	|	|	|	1.05
11.917	0.00	0.24	0.218	I O	|	|	|	1.05
12.000	0.00	0.24	0.216	I O	|	|	|	1.04
12.083	0.00	0.24	0.214	I O	|	|	|	1.03
12.167	0.00	0.24	0.213	I O	|	|	|	1.03
12.250	0.00	0.24	0.211	I O	|	|	|	1.02
12.333	0.00	0.24	0.209	I O	|	|	|	1.01
12.417	0.00	0.24	0.208	I O	|	|	|	1.01
12.500	0.00	0.24	0.206	I O	|	|	|	1.00
12.583	0.00	0.24	0.205	I O	|	|	|	0.99
12.667	0.00	0.23	0.203	I O	|	|	|	0.99
12.750	0.00	0.23	0.201	I O	|	|	|	0.98
12.833	0.00	0.23	0.200	I O	|	|	|	0.97
12.917	0.00	0.23	0.198	I O	|	|	|	0.97
13.000	0.00	0.23	0.197	I O	|	|	|	0.96
13.083	0.00	0.23	0.195	I O	|	|	|	0.96
13.167	0.00	0.23	0.193	I O	|	|	|	0.95
13.250	0.00	0.23	0.192	I O	|	|	|	0.94
13.333	0.00	0.23	0.190	I O	|	|	|	0.94
13.417	0.00	0.23	0.189	I O	|	|	|	0.93
13.500	0.00	0.23	0.187	I O	|	|	|	0.92
13.583	0.00	0.22	0.186	I O	|	|	|	0.92
13.667	0.00	0.22	0.184	I O	|	|	|	0.91
13.750	0.00	0.22	0.182	I O	|	|	|	0.91
13.833	0.00	0.22	0.181	I O	|	|	|	0.90
13.917	0.00	0.22	0.179	I O	|	|	|	0.89
14.000	0.00	0.22	0.178	I O	|	|	|	0.89
14.083	0.00	0.22	0.176	I O	|	|	|	0.88
14.167	0.00	0.22	0.175	I O	|	|	|	0.88
14.250	0.00	0.22	0.173	I O	|	|	|	0.87
14.333	0.00	0.22	0.172	I O	|	|	|	0.86
14.417	0.00	0.22	0.170	I O	|	|	|	0.86
14.500	0.00	0.22	0.169	I O	|	|	|	0.85
14.583	0.00	0.21	0.167	I O	|	|	|	0.85
14.667	0.00	0.21	0.166	I O	|	|	|	0.84
14.750	0.00	0.21	0.164	I O	|	|	|	0.83
14.833	0.00	0.21	0.163	I O	|	|	|	0.83
14.917	0.00	0.21	0.162	I O	|	|	|	0.82
15.000	0.00	0.21	0.160	I O	|	|	|	0.82
15.083	0.00	0.21	0.159	I O	|	|	|	0.81
15.167	0.00	0.21	0.157	I O	|	|	|	0.80
15.250	0.00	0.21	0.156	I O	|	|	|	0.80
15.333	0.00	0.21	0.154	I O	|	|	|	0.79
15.417	0.00	0.21	0.153	IO	|	|	|	0.79
15.500	0.00	0.21	0.151	IO	|	|	|	0.78
15.583	0.00	0.21	0.150	IO	|	|	|	0.78
15.667	0.00	0.20	0.149	IO	|	|	|	0.77
15.750	0.00	0.20	0.147	IO	|	|	|	0.76
15.833	0.00	0.20	0.146	IO	|	|	|	0.76
15.917	0.00	0.20	0.144	IO	|	|	|	0.75
16.000	0.00	0.20	0.143	IO	|	|	|	0.75
16.083	0.00	0.20	0.142	IO	|	|	|	0.74
16.167	0.00	0.20	0.140	IO	|	|	|	0.74
16.250	0.00	0.20	0.139	IO	|	|	|	0.73
16.333	0.00	0.20	0.138	IO	|	|	|	0.73
16.417	0.00	0.20	0.136	IO	|	|	|	0.72
16.500	0.00	0.20	0.135	IO	|	|	|	0.72
16.583	0.00	0.20	0.133	IO	|	|	|	0.71
16.667	0.00	0.20	0.132	IO	|	|	|	0.70
16.750	0.00	0.19	0.131	IO	|	|	|	0.70
16.833	0.00	0.19	0.129	IO	|	|	|	0.69
16.917	0.00	0.19	0.128	IO	|	|	|	0.69
17.000	0.00	0.19	0.127	IO	|	|	|	0.68
17.083	0.00	0.19	0.125	IO	|	|	|	0.68
17.167	0.00	0.19	0.124	IO	|	|	|	0.67
17.250	0.00	0.19	0.123	IO	|	|	|	0.67
17.333	0.00	0.19	0.122	IO	|	|	|	0.66
17.417	0.00	0.19	0.120	IO	|	|	|	0.66

17.500	0.00	0.19	0.119	IO				0.65
17.583	0.00	0.19	0.118	IO				0.65
17.667	0.00	0.19	0.116	IO				0.64
17.750	0.00	0.19	0.115	IO				0.64
17.833	0.00	0.19	0.114	IO				0.63
17.917	0.00	0.18	0.113	IO				0.63
18.000	0.00	0.18	0.111	IO				0.62
18.083	0.00	0.18	0.110	IO				0.62
18.167	0.00	0.18	0.109	IO				0.61
18.250	0.00	0.18	0.107	IO				0.61
18.333	0.00	0.18	0.106	IO				0.60
18.417	0.00	0.18	0.105	IO				0.60
18.500	0.00	0.18	0.104	IO				0.59
18.583	0.00	0.18	0.103	IO				0.59
18.667	0.00	0.18	0.101	IO				0.58
18.750	0.00	0.18	0.100	IO				0.58
18.833	0.00	0.18	0.099	IO				0.57
18.917	0.00	0.18	0.098	IO				0.57
19.000	0.00	0.18	0.096	IO				0.56
19.083	0.00	0.17	0.095	IO				0.56
19.167	0.00	0.17	0.094	IO				0.55
19.250	0.00	0.17	0.093	IO				0.55
19.333	0.00	0.17	0.092	IO				0.54
19.417	0.00	0.17	0.090	IO				0.54
19.500	0.00	0.17	0.089	IO				0.53
19.583	0.00	0.17	0.088	IO				0.53
19.667	0.00	0.17	0.087	IO				0.52
19.750	0.00	0.17	0.086	IO				0.52
19.833	0.00	0.17	0.085	IO				0.51
19.917	0.00	0.17	0.083	IO				0.51
20.000	0.00	0.17	0.082	IO				0.50
20.083	0.00	0.17	0.081	IO				0.50
20.167	0.00	0.17	0.080	IO				0.50
20.250	0.00	0.17	0.079	IO				0.49
20.333	0.00	0.16	0.078	IO				0.49
20.417	0.00	0.16	0.077	IO				0.48
20.500	0.00	0.16	0.075	IO				0.48
20.583	0.00	0.16	0.074	IO				0.47
20.667	0.00	0.16	0.073	IO				0.47
20.750	0.00	0.16	0.072	IO				0.46
20.833	0.00	0.16	0.071	IO				0.46
20.917	0.00	0.16	0.070	IO				0.45
21.000	0.00	0.16	0.069	IO				0.45
21.083	0.00	0.16	0.068	IO				0.45
21.167	0.00	0.16	0.067	IO				0.44
21.250	0.00	0.16	0.066	IO				0.44
21.333	0.00	0.15	0.064	IO				0.43
21.417	0.00	0.15	0.063	IO				0.43
21.500	0.00	0.15	0.062	IO				0.42
21.583	0.00	0.15	0.061	IO				0.42
21.667	0.00	0.15	0.060	IO				0.41
21.750	0.00	0.15	0.059	IO				0.41
21.833	0.00	0.15	0.058	IO				0.41
21.917	0.00	0.15	0.057	IO				0.40
22.000	0.00	0.15	0.056	IO				0.40
22.083	0.00	0.15	0.055	IO				0.39
22.167	0.00	0.15	0.054	IO				0.39
22.250	0.00	0.15	0.053	IO				0.39
22.333	0.00	0.15	0.052	IO				0.38
22.417	0.00	0.14	0.051	IO				0.38
22.500	0.00	0.14	0.050	IO				0.37
22.583	0.00	0.14	0.049	IO				0.37
22.667	0.00	0.14	0.048	IO				0.37
22.750	0.00	0.14	0.047	IO				0.36
22.833	0.00	0.14	0.046	IO				0.36
22.917	0.00	0.14	0.045	IO				0.35
23.000	0.00	0.14	0.044	IO				0.35
23.083	0.00	0.14	0.043	IO				0.35
23.167	0.00	0.14	0.042	IO				0.34
23.250	0.00	0.14	0.041	IO				0.34
23.333	0.00	0.14	0.040	IO				0.33
23.417	0.00	0.14	0.039	IO				0.33

23.500	0.00	0.13	0.039	IO				0.32
23.583	0.00	0.13	0.038	IO				0.32
23.667	0.00	0.13	0.037	IO				0.32
23.750	0.00	0.13	0.036	IO				0.31
23.833	0.00	0.13	0.035	IO				0.31
23.917	0.00	0.13	0.034	IO				0.30
24.000	0.00	0.13	0.033	IO				0.30
24.083	0.00	0.13	0.032	IO				0.30
24.167	0.00	0.13	0.031	IO				0.29
24.250	0.00	0.13	0.030	IO				0.29
24.333	0.00	0.13	0.030	IO				0.28
24.417	0.00	0.12	0.029	IO				0.28
24.500	0.00	0.12	0.028	IO				0.28
24.583	0.00	0.12	0.027	IO				0.27
24.667	0.00	0.12	0.026	IO				0.27
24.750	0.00	0.12	0.025	IO				0.27
24.833	0.00	0.12	0.025	IO				0.26
24.917	0.00	0.12	0.024	IO				0.26
25.000	0.00	0.12	0.023	IO				0.25
25.083	0.00	0.12	0.022	IO				0.25
25.167	0.00	0.11	0.021	IO				0.24
25.250	0.00	0.11	0.020	IO				0.23
25.333	0.00	0.11	0.020	IO				0.22
25.417	0.00	0.10	0.019	O				0.22
25.500	0.00	0.10	0.018	O				0.21
25.583	0.00	0.09	0.018	O				0.20
25.667	0.00	0.09	0.017	O				0.19
25.750	0.00	0.09	0.016	O				0.19
25.833	0.00	0.08	0.016	O				0.18
25.917	0.00	0.08	0.015	O				0.17
26.000	0.00	0.08	0.015	O				0.17
26.083	0.00	0.08	0.014	O				0.16
26.167	0.00	0.07	0.014	O				0.15
26.250	0.00	0.07	0.013	O				0.15
26.333	0.00	0.07	0.013	O				0.14
26.417	0.00	0.07	0.012	O				0.14
26.500	0.00	0.06	0.012	O				0.13
26.583	0.00	0.06	0.011	O				0.13
26.667	0.00	0.06	0.011	O				0.12
26.750	0.00	0.06	0.011	O				0.12
26.833	0.00	0.05	0.010	O				0.12
26.917	0.00	0.05	0.010	O				0.11
27.000	0.00	0.05	0.009	O				0.11
27.083	0.00	0.05	0.009	O				0.10
27.167	0.00	0.05	0.009	O				0.10
27.250	0.00	0.05	0.008	O				0.10
27.333	0.00	0.04	0.008	O				0.09
27.417	0.00	0.04	0.008	O				0.09
27.500	0.00	0.04	0.008	O				0.09
27.583	0.00	0.04	0.007	O				0.08
27.667	0.00	0.04	0.007	O				0.08
27.750	0.00	0.04	0.007	O				0.08
27.833	0.00	0.03	0.007	O				0.07
27.917	0.00	0.03	0.006	O				0.07
28.000	0.00	0.03	0.006	O				0.07
28.083	0.00	0.03	0.006	O				0.07
28.167	0.00	0.03	0.006	O				0.06
28.250	0.00	0.03	0.005	O				0.06
28.333	0.00	0.03	0.005	O				0.06
28.417	0.00	0.03	0.005	O				0.06
28.500	0.00	0.03	0.005	O				0.06
28.583	0.00	0.03	0.005	O				0.05
28.667	0.00	0.02	0.005	O				0.05
28.750	0.00	0.02	0.004	O				0.05
28.833	0.00	0.02	0.004	O				0.05
28.917	0.00	0.02	0.004	O				0.05
29.000	0.00	0.02	0.004	O				0.04
29.083	0.00	0.02	0.004	O				0.04
29.167	0.00	0.02	0.004	O				0.04
29.250	0.00	0.02	0.003	O				0.04
29.333	0.00	0.02	0.003	O				0.04
29.417	0.00	0.02	0.003	O				0.04

29.500	0.00	0.02	0.003	O	|	|	|	0.04
29.583	0.00	0.02	0.003	O	|	|	|	0.03
29.667	0.00	0.02	0.003	O	|	|	|	0.03
29.750	0.00	0.01	0.003	O	|	|	|	0.03
29.833	0.00	0.01	0.003	O	|	|	|	0.03
29.917	0.00	0.01	0.003	O	|	|	|	0.03
30.000	0.00	0.01	0.002	O	|	|	|	0.03
30.083	0.00	0.01	0.002	O	|	|	|	0.03
30.167	0.00	0.01	0.002	O	|	|	|	0.03
30.250	0.00	0.01	0.002	O	|	|	|	0.03
30.333	0.00	0.01	0.002	O	|	|	|	0.02
30.417	0.00	0.01	0.002	O	|	|	|	0.02
30.500	0.00	0.01	0.002	O	|	|	|	0.02
30.583	0.00	0.01	0.002	O	|	|	|	0.02
30.667	0.00	0.01	0.002	O	|	|	|	0.02
30.750	0.00	0.01	0.002	O	|	|	|	0.02
30.833	0.00	0.01	0.002	O	|	|	|	0.02
30.917	0.00	0.01	0.002	O	|	|	|	0.02
31.000	0.00	0.01	0.002	O	|	|	|	0.02
31.083	0.00	0.01	0.002	O	|	|	|	0.02
31.167	0.00	0.01	0.001	O	|	|	|	0.02
31.250	0.00	0.01	0.001	O	|	|	|	0.02
31.333	0.00	0.01	0.001	O	|	|	|	0.02
31.417	0.00	0.01	0.001	O	|	|	|	0.02
31.500	0.00	0.01	0.001	O	|	|	|	0.01
31.583	0.00	0.01	0.001	O	|	|	|	0.01
31.667	0.00	0.01	0.001	O	|	|	|	0.01
31.750	0.00	0.01	0.001	O	|	|	|	0.01
31.833	0.00	0.01	0.001	O	|	|	|	0.01
31.917	0.00	0.01	0.001	O	|	|	|	0.01
32.000	0.00	0.01	0.001	O	|	|	|	0.01
32.083	0.00	0.01	0.001	O	|	|	|	0.01
32.167	0.00	0.01	0.001	O	|	|	|	0.01
32.250	0.00	0.00	0.001	O	|	|	|	0.01
32.333	0.00	0.00	0.001	O	|	|	|	0.01
32.417	0.00	0.00	0.001	O	|	|	|	0.01
32.500	0.00	0.00	0.001	O	|	|	|	0.01
32.583	0.00	0.00	0.001	O	|	|	|	0.01
32.667	0.00	0.00	0.001	O	|	|	|	0.01
32.750	0.00	0.00	0.001	O	|	|	|	0.01
32.833	0.00	0.00	0.001	O	|	|	|	0.01
32.917	0.00	0.00	0.001	O	|	|	|	0.01
33.000	0.00	0.00	0.001	O	|	|	|	0.01
33.083	0.00	0.00	0.001	O	|	|	|	0.01
33.167	0.00	0.00	0.001	O	|	|	|	0.01
33.250	0.00	0.00	0.001	O	|	|	|	0.01
33.333	0.00	0.00	0.001	O	|	|	|	0.01
33.417	0.00	0.00	0.001	O	|	|	|	0.01
33.500	0.00	0.00	0.001	O	|	|	|	0.01
33.583	0.00	0.00	0.001	O	|	|	|	0.01
33.667	0.00	0.00	0.000	O	|	|	|	0.01
33.750	0.00	0.00	0.000	O	|	|	|	0.01
33.833	0.00	0.00	0.000	O	|	|	|	0.01
33.917	0.00	0.00	0.000	O	|	|	|	0.00
34.000	0.00	0.00	0.000	O	|	|	|	0.00
34.083	0.00	0.00	0.000	O	|	|	|	0.00
34.167	0.00	0.00	0.000	O	|	|	|	0.00
34.250	0.00	0.00	0.000	O	|	|	|	0.00
34.333	0.00	0.00	0.000	O	|	|	|	0.00
34.417	0.00	0.00	0.000	O	|	|	|	0.00
34.500	0.00	0.00	0.000	O	|	|	|	0.00
34.583	0.00	0.00	0.000	O	|	|	|	0.00
34.667	0.00	0.00	0.000	O	|	|	|	0.00
34.750	0.00	0.00	0.000	O	|	|	|	0.00
34.833	0.00	0.00	0.000	O	|	|	|	0.00
34.917	0.00	0.00	0.000	O	|	|	|	0.00
35.000	0.00	0.00	0.000	O	|	|	|	0.00
35.083	0.00	0.00	0.000	O	|	|	|	0.00
35.167	0.00	0.00	0.000	O	|	|	|	0.00
35.250	0.00	0.00	0.000	O	|	|	|	0.00
35.333	0.00	0.00	0.000	O	|	|	|	0.00
35.417	0.00	0.00	0.000	O	|	|	|	0.00

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35.500    0.00    0.00      0.000  O       |       |       |       |     0.00
35.583    0.00    0.00      0.000  O       |       |       |       |     0.00
35.667    0.00    0.00      0.000  O       |       |       |       |     0.00
35.750    0.00    0.00      0.000  O       |       |       |       |     0.00
35.833    0.00    0.00      0.000  O       |       |       |       |     0.00
35.917    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                        Number of intervals =   431
                        Time interval =    5.0 (Min.)
                        Maximum/Peak flow rate =        0.296 (CFS)
                        Total volume =       0.436 (Ac.Ft)
                Status of hydrographs being held in storage
                           Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
                Peak (CFS)      0.000     0.000     0.000     0.000     0.000
                Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
        ************************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
3-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA0232.rte
**********HYDROGRAPH DATA**********
Number of intervals = 38
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.788 (CFS)
Total volume = 0.328 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 38
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.9	1.89	2.84	3.79	Depth (Ft.)
0.083	0.36	0.01	0.001	O I					0.01
0.167	0.58	0.02	0.004	O I					0.05
0.250	0.56	0.04	0.008	O I					0.09
0.333	0.64	0.06	0.012	O I					0.13
0.417	0.70	0.09	0.016	O I					0.18
0.500	0.79	0.11	0.020	O I					0.23
0.583	0.76	0.12	0.025	O I					0.26
0.667	0.80	0.13	0.029	O I					0.28
0.750	0.85	0.13	0.034	O I					0.31
0.833	0.77	0.13	0.039	O I					0.33
0.917	0.75	0.14	0.043	O I					0.34
1.000	0.81	0.14	0.048	O I					0.36
1.083	0.96	0.15	0.053	O I					0.38
1.167	1.03	0.15	0.059	O I					0.41
1.250	1.04	0.15	0.065	O I					0.43
1.333	0.99	0.16	0.071	O I					0.46
1.417	1.12	0.16	0.077	O I					0.48
1.500	1.24	0.17	0.084	O I					0.51
1.583	1.20	0.17	0.091	O I					0.54
1.667	1.23	0.18	0.098	O I					0.57
1.750	1.44	0.18	0.106	O I					0.60
1.833	1.49	0.19	0.115	O I					0.64
1.917	1.42	0.19	0.124	O I					0.67
2.000	1.41	0.20	0.132	O I					0.70
2.083	1.45	0.20	0.140	O I					0.74
2.167	1.77	0.21	0.150	O I					0.78
2.250	2.18	0.21	0.162	O I					0.83
2.333	1.94	0.22	0.175	O I					0.88
2.417	2.60	0.23	0.189	O I					0.93
2.500	3.30	0.24	0.208	O I					1.01
2.583	3.79	0.25	0.231	O I					1.10
2.667	3.29	0.26	0.253	O I					1.19
2.750	1.80	0.26	0.269	O I					1.25
2.833	1.00	0.27	0.277	O I					1.28
2.917	0.86	0.27	0.281	O I					1.30
3.000	0.52	0.27	0.284	O I					1.31
3.083	0.15	0.27	0.285	IO					1.32
3.167	0.02	0.27	0.283	I O					1.31
3.250	0.00	0.27	0.281	I O					1.30
3.333	0.00	0.27	0.280	I O					1.30
3.417	0.00	0.27	0.278	I O					1.29
3.500	0.00	0.27	0.276	I O					1.28
3.583	0.00	0.27	0.274	I O					1.27
3.667	0.00	0.27	0.272	I O					1.27
3.750	0.00	0.26	0.270	I O					1.26
3.833	0.00	0.26	0.269	I O					1.25
3.917	0.00	0.26	0.267	I O					1.24
4.000	0.00	0.26	0.265	I O					1.24
4.083	0.00	0.26	0.263	I O					1.23
4.167	0.00	0.26	0.261	I O					1.22
4.250	0.00	0.26	0.260	I O					1.22
4.333	0.00	0.26	0.258	I O					1.21
4.417	0.00	0.26	0.256	I O					1.20
4.500	0.00	0.26	0.254	I O					1.19
4.583	0.00	0.26	0.252	I O					1.19
4.667	0.00	0.26	0.251	I O					1.18
4.750	0.00	0.26	0.249	I O					1.17
4.833	0.00	0.25	0.247	I O					1.17
4.917	0.00	0.25	0.245	I O					1.16
5.000	0.00	0.25	0.244	I O					1.15
5.083	0.00	0.25	0.242	I O					1.14
5.167	0.00	0.25	0.240	I O					1.14
5.250	0.00	0.25	0.239	I O					1.13
5.333	0.00	0.25	0.237	I O					1.12
5.417	0.00	0.25	0.235	I O					1.12

5.500	0.00	0.25	0.233	I O	|	|	|	1.11
5.583	0.00	0.25	0.232	I O	|	|	|	1.10
5.667	0.00	0.25	0.230	I O	|	|	|	1.10
5.750	0.00	0.25	0.228	I O	|	|	|	1.09
5.833	0.00	0.25	0.227	I O	|	|	|	1.08
5.917	0.00	0.24	0.225	I O	|	|	|	1.08
6.000	0.00	0.24	0.223	I O	|	|	|	1.07
6.083	0.00	0.24	0.222	I O	|	|	|	1.06
6.167	0.00	0.24	0.220	I O	|	|	|	1.06
6.250	0.00	0.24	0.218	I O	|	|	|	1.05
6.333	0.00	0.24	0.217	I O	|	|	|	1.04
6.417	0.00	0.24	0.215	I O	|	|	|	1.04
6.500	0.00	0.24	0.213	I O	|	|	|	1.03
6.583	0.00	0.24	0.212	I O	|	|	|	1.02
6.667	0.00	0.24	0.210	I O	|	|	|	1.02
6.750	0.00	0.24	0.208	I O	|	|	|	1.01
6.833	0.00	0.24	0.207	IO	|	|	|	1.00
6.917	0.00	0.24	0.205	IO	|	|	|	1.00
7.000	0.00	0.23	0.203	IO	|	|	|	0.99
7.083	0.00	0.23	0.202	IO	|	|	|	0.98
7.167	0.00	0.23	0.200	IO	|	|	|	0.98
7.250	0.00	0.23	0.199	IO	|	|	|	0.97
7.333	0.00	0.23	0.197	IO	|	|	|	0.96
7.417	0.00	0.23	0.195	IO	|	|	|	0.96
7.500	0.00	0.23	0.194	IO	|	|	|	0.95
7.583	0.00	0.23	0.192	IO	|	|	|	0.95
7.667	0.00	0.23	0.191	IO	|	|	|	0.94
7.750	0.00	0.23	0.189	IO	|	|	|	0.93
7.833	0.00	0.23	0.188	IO	|	|	|	0.93
7.917	0.00	0.22	0.186	IO	|	|	|	0.92
8.000	0.00	0.22	0.184	IO	|	|	|	0.91
8.083	0.00	0.22	0.183	IO	|	|	|	0.91
8.167	0.00	0.22	0.181	IO	|	|	|	0.90
8.250	0.00	0.22	0.180	IO	|	|	|	0.90
8.333	0.00	0.22	0.178	IO	|	|	|	0.89
8.417	0.00	0.22	0.177	IO	|	|	|	0.88
8.500	0.00	0.22	0.175	IO	|	|	|	0.88
8.583	0.00	0.22	0.174	IO	|	|	|	0.87
8.667	0.00	0.22	0.172	IO	|	|	|	0.87
8.750	0.00	0.22	0.171	IO	|	|	|	0.86
8.833	0.00	0.22	0.169	IO	|	|	|	0.85
8.917	0.00	0.21	0.168	IO	|	|	|	0.85
9.000	0.00	0.21	0.166	IO	|	|	|	0.84
9.083	0.00	0.21	0.165	IO	|	|	|	0.84
9.167	0.00	0.21	0.163	IO	|	|	|	0.83
9.250	0.00	0.21	0.162	IO	|	|	|	0.82
9.333	0.00	0.21	0.161	IO	|	|	|	0.82
9.417	0.00	0.21	0.159	IO	|	|	|	0.81
9.500	0.00	0.21	0.158	IO	|	|	|	0.81
9.583	0.00	0.21	0.156	IO	|	|	|	0.80
9.667	0.00	0.21	0.155	IO	|	|	|	0.79
9.750	0.00	0.21	0.153	IO	|	|	|	0.79
9.833	0.00	0.21	0.152	IO	|	|	|	0.78
9.917	0.00	0.21	0.150	IO	|	|	|	0.78
10.000	0.00	0.20	0.149	IO	|	|	|	0.77
10.083	0.00	0.20	0.148	IO	|	|	|	0.77
10.167	0.00	0.20	0.146	IO	|	|	|	0.76
10.250	0.00	0.20	0.145	IO	|	|	|	0.76
10.333	0.00	0.20	0.143	IO	|	|	|	0.75
10.417	0.00	0.20	0.142	IO	|	|	|	0.74
10.500	0.00	0.20	0.141	IO	|	|	|	0.74
10.583	0.00	0.20	0.139	IO	|	|	|	0.73
10.667	0.00	0.20	0.138	IO	|	|	|	0.73
10.750	0.00	0.20	0.137	IO	|	|	|	0.72
10.833	0.00	0.20	0.135	IO	|	|	|	0.72
10.917	0.00	0.20	0.134	IO	|	|	|	0.71
11.000	0.00	0.20	0.133	IO	|	|	|	0.71
11.083	0.00	0.19	0.131	IO	|	|	|	0.70
11.167	0.00	0.19	0.130	IO	|	|	|	0.70
11.250	0.00	0.19	0.129	IO	|	|	|	0.69
11.333	0.00	0.19	0.127	IO	|	|	|	0.68
11.417	0.00	0.19	0.126	IO	|	|	|	0.68

11.500	0.00	0.19	0.125	IO				0.67
11.583	0.00	0.19	0.123	IO				0.67
11.667	0.00	0.19	0.122	IO				0.66
11.750	0.00	0.19	0.121	IO				0.66
11.833	0.00	0.19	0.119	IO				0.65
11.917	0.00	0.19	0.118	IO				0.65
12.000	0.00	0.19	0.117	IO				0.64
12.083	0.00	0.19	0.115	IO				0.64
12.167	0.00	0.19	0.114	IO				0.63
12.250	0.00	0.18	0.113	IO				0.63
12.333	0.00	0.18	0.112	IO				0.62
12.417	0.00	0.18	0.110	IO				0.62
12.500	0.00	0.18	0.109	IO				0.61
12.583	0.00	0.18	0.108	IO				0.61
12.667	0.00	0.18	0.107	IO				0.60
12.750	0.00	0.18	0.105	IO				0.60
12.833	0.00	0.18	0.104	IO				0.59
12.917	0.00	0.18	0.103	IO				0.59
13.000	0.00	0.18	0.102	IO				0.58
13.083	0.00	0.18	0.100	IO				0.58
13.167	0.00	0.18	0.099	IO				0.57
13.250	0.00	0.18	0.098	IO				0.57
13.333	0.00	0.18	0.097	IO				0.56
13.417	0.00	0.18	0.096	IO				0.56
13.500	0.00	0.17	0.094	IO				0.55
13.583	0.00	0.17	0.093	IO				0.55
13.667	0.00	0.17	0.092	IO				0.54
13.750	0.00	0.17	0.091	IO				0.54
13.833	0.00	0.17	0.090	IO				0.53
13.917	0.00	0.17	0.088	IO				0.53
14.000	0.00	0.17	0.087	IO				0.52
14.083	0.00	0.17	0.086	IO				0.52
14.167	0.00	0.17	0.085	IO				0.52
14.250	0.00	0.17	0.084	IO				0.51
14.333	0.00	0.17	0.083	IO				0.51
14.417	0.00	0.17	0.081	IO				0.50
14.500	0.00	0.17	0.080	IO				0.50
14.583	0.00	0.17	0.079	IO				0.49
14.667	0.00	0.16	0.078	IO				0.49
14.750	0.00	0.16	0.077	IO				0.48
14.833	0.00	0.16	0.076	IO				0.48
14.917	0.00	0.16	0.075	IO				0.47
15.000	0.00	0.16	0.074	IO				0.47
15.083	0.00	0.16	0.072	IO				0.46
15.167	0.00	0.16	0.071	IO				0.46
15.250	0.00	0.16	0.070	IO				0.46
15.333	0.00	0.16	0.069	IO				0.45
15.417	0.00	0.16	0.068	IO				0.45
15.500	0.00	0.16	0.067	IO				0.44
15.583	0.00	0.16	0.066	IO				0.44
15.667	0.00	0.15	0.065	IO				0.43
15.750	0.00	0.15	0.064	IO				0.43
15.833	0.00	0.15	0.063	IO				0.42
15.917	0.00	0.15	0.062	IO				0.42
16.000	0.00	0.15	0.061	IO				0.42
16.083	0.00	0.15	0.060	IO				0.41
16.167	0.00	0.15	0.058	IO				0.41
16.250	0.00	0.15	0.057	IO				0.40
16.333	0.00	0.15	0.056	IO				0.40
16.417	0.00	0.15	0.055	IO				0.40
16.500	0.00	0.15	0.054	IO				0.39
16.583	0.00	0.15	0.053	IO				0.39
16.667	0.00	0.15	0.052	IO				0.38
16.750	0.00	0.14	0.051	IO				0.38
16.833	0.00	0.14	0.050	IO				0.37
16.917	0.00	0.14	0.049	IO				0.37
17.000	0.00	0.14	0.048	IO				0.37
17.083	0.00	0.14	0.047	IO				0.36
17.167	0.00	0.14	0.046	IO				0.36
17.250	0.00	0.14	0.045	IO				0.35
17.333	0.00	0.14	0.045	IO				0.35
17.417	0.00	0.14	0.044	IO				0.35

17.500	0.00	0.14	0.043	IO				0.34
17.583	0.00	0.14	0.042	IO				0.34
17.667	0.00	0.14	0.041	IO				0.33
17.750	0.00	0.14	0.040	IO				0.33
17.833	0.00	0.13	0.039	IO				0.33
17.917	0.00	0.13	0.038	IO				0.32
18.000	0.00	0.13	0.037	IO				0.32
18.083	0.00	0.13	0.036	IO				0.31
18.167	0.00	0.13	0.035	IO				0.31
18.250	0.00	0.13	0.034	IO				0.31
18.333	0.00	0.13	0.033	IO				0.30
18.417	0.00	0.13	0.032	IO				0.30
18.500	0.00	0.13	0.032	IO				0.29
18.583	0.00	0.13	0.031	IO				0.29
18.667	0.00	0.13	0.030	IO				0.29
18.750	0.00	0.12	0.029	IO				0.28
18.833	0.00	0.12	0.028	IO				0.28
18.917	0.00	0.12	0.027	IO				0.27
19.000	0.00	0.12	0.026	IO				0.27
19.083	0.00	0.12	0.026	IO				0.27
19.167	0.00	0.12	0.025	IO				0.26
19.250	0.00	0.12	0.024	IO				0.26
19.333	0.00	0.12	0.023	IO				0.25
19.417	0.00	0.12	0.022	O				0.25
19.500	0.00	0.12	0.021	O				0.24
19.583	0.00	0.11	0.021	O				0.24
19.667	0.00	0.11	0.020	O				0.23
19.750	0.00	0.10	0.019	O				0.22
19.833	0.00	0.10	0.019	O				0.21
19.917	0.00	0.10	0.018	O				0.20
20.000	0.00	0.09	0.017	O				0.20
20.083	0.00	0.09	0.017	O				0.19
20.167	0.00	0.09	0.016	O				0.18
20.250	0.00	0.08	0.015	O				0.18
20.333	0.00	0.08	0.015	O				0.17
20.417	0.00	0.08	0.014	O				0.16
20.500	0.00	0.07	0.014	O				0.16
20.583	0.00	0.07	0.013	O				0.15
20.667	0.00	0.07	0.013	O				0.15
20.750	0.00	0.07	0.012	O				0.14
20.833	0.00	0.06	0.012	O				0.14
20.917	0.00	0.06	0.011	O				0.13
21.000	0.00	0.06	0.011	O				0.13
21.083	0.00	0.06	0.011	O				0.12
21.167	0.00	0.06	0.010	O				0.12
21.250	0.00	0.05	0.010	O				0.11
21.333	0.00	0.05	0.010	O				0.11
21.417	0.00	0.05	0.009	O				0.10
21.500	0.00	0.05	0.009	O				0.10
21.583	0.00	0.05	0.009	O				0.10
21.667	0.00	0.04	0.008	O				0.09
21.750	0.00	0.04	0.008	O				0.09
21.833	0.00	0.04	0.008	O				0.09
21.917	0.00	0.04	0.007	O				0.08
22.000	0.00	0.04	0.007	O				0.08
22.083	0.00	0.04	0.007	O				0.08
22.167	0.00	0.04	0.007	O				0.07
22.250	0.00	0.03	0.006	O				0.07
22.333	0.00	0.03	0.006	O				0.07
22.417	0.00	0.03	0.006	O				0.07
22.500	0.00	0.03	0.006	O				0.06
22.583	0.00	0.03	0.005	O				0.06
22.667	0.00	0.03	0.005	O				0.06
22.750	0.00	0.03	0.005	O				0.06
22.833	0.00	0.03	0.005	O				0.06
22.917	0.00	0.03	0.005	O				0.05
23.000	0.00	0.02	0.005	O				0.05
23.083	0.00	0.02	0.004	O				0.05
23.167	0.00	0.02	0.004	O				0.05
23.250	0.00	0.02	0.004	O				0.05
23.333	0.00	0.02	0.004	O				0.04
23.417	0.00	0.02	0.004	O				0.04

23.500	0.00	0.02	0.004	O	|	|	|	0.04
23.583	0.00	0.02	0.004	O	|	|	|	0.04
23.667	0.00	0.02	0.003	O	|	|	|	0.04
23.750	0.00	0.02	0.003	O	|	|	|	0.04
23.833	0.00	0.02	0.003	O	|	|	|	0.04
23.917	0.00	0.02	0.003	O	|	|	|	0.03
24.000	0.00	0.02	0.003	O	|	|	|	0.03
24.083	0.00	0.02	0.003	O	|	|	|	0.03
24.167	0.00	0.01	0.003	O	|	|	|	0.03
24.250	0.00	0.01	0.003	O	|	|	|	0.03
24.333	0.00	0.01	0.003	O	|	|	|	0.03
24.417	0.00	0.01	0.002	O	|	|	|	0.03
24.500	0.00	0.01	0.002	O	|	|	|	0.03
24.583	0.00	0.01	0.002	O	|	|	|	0.03
24.667	0.00	0.01	0.002	O	|	|	|	0.02
24.750	0.00	0.01	0.002	O	|	|	|	0.02
24.833	0.00	0.01	0.002	O	|	|	|	0.02
24.917	0.00	0.01	0.002	O	|	|	|	0.02
25.000	0.00	0.01	0.002	O	|	|	|	0.02
25.083	0.00	0.01	0.002	O	|	|	|	0.02
25.167	0.00	0.01	0.002	O	|	|	|	0.02
25.250	0.00	0.01	0.002	O	|	|	|	0.02
25.333	0.00	0.01	0.002	O	|	|	|	0.02
25.417	0.00	0.01	0.002	O	|	|	|	0.02
25.500	0.00	0.01	0.002	O	|	|	|	0.02
25.583	0.00	0.01	0.001	O	|	|	|	0.02
25.667	0.00	0.01	0.001	O	|	|	|	0.02
25.750	0.00	0.01	0.001	O	|	|	|	0.02
25.833	0.00	0.01	0.001	O	|	|	|	0.01
25.917	0.00	0.01	0.001	O	|	|	|	0.01
26.000	0.00	0.01	0.001	O	|	|	|	0.01
26.083	0.00	0.01	0.001	O	|	|	|	0.01
26.167	0.00	0.01	0.001	O	|	|	|	0.01
26.250	0.00	0.01	0.001	O	|	|	|	0.01
26.333	0.00	0.01	0.001	O	|	|	|	0.01
26.417	0.00	0.01	0.001	O	|	|	|	0.01
26.500	0.00	0.01	0.001	O	|	|	|	0.01
26.583	0.00	0.00	0.001	O	|	|	|	0.01
26.667	0.00	0.00	0.001	O	|	|	|	0.01
26.750	0.00	0.00	0.001	O	|	|	|	0.01
26.833	0.00	0.00	0.001	O	|	|	|	0.01
26.917	0.00	0.00	0.001	O	|	|	|	0.01
27.000	0.00	0.00	0.001	O	|	|	|	0.01
27.083	0.00	0.00	0.001	O	|	|	|	0.01
27.167	0.00	0.00	0.001	O	|	|	|	0.01
27.250	0.00	0.00	0.001	O	|	|	|	0.01
27.333	0.00	0.00	0.001	O	|	|	|	0.01
27.417	0.00	0.00	0.001	O	|	|	|	0.01
27.500	0.00	0.00	0.001	O	|	|	|	0.01
27.583	0.00	0.00	0.001	O	|	|	|	0.01
27.667	0.00	0.00	0.001	O	|	|	|	0.01
27.750	0.00	0.00	0.001	O	|	|	|	0.01
27.833	0.00	0.00	0.001	O	|	|	|	0.01
27.917	0.00	0.00	0.001	O	|	|	|	0.01
28.000	0.00	0.00	0.000	O	|	|	|	0.01
28.083	0.00	0.00	0.000	O	|	|	|	0.01
28.167	0.00	0.00	0.000	O	|	|	|	0.01
28.250	0.00	0.00	0.000	O	|	|	|	0.01
28.333	0.00	0.00	0.000	O	|	|	|	0.00
28.417	0.00	0.00	0.000	O	|	|	|	0.00
28.500	0.00	0.00	0.000	O	|	|	|	0.00
28.583	0.00	0.00	0.000	O	|	|	|	0.00
28.667	0.00	0.00	0.000	O	|	|	|	0.00
28.750	0.00	0.00	0.000	O	|	|	|	0.00
28.833	0.00	0.00	0.000	O	|	|	|	0.00
28.917	0.00	0.00	0.000	O	|	|	|	0.00
29.000	0.00	0.00	0.000	O	|	|	|	0.00
29.083	0.00	0.00	0.000	O	|	|	|	0.00
29.167	0.00	0.00	0.000	O	|	|	|	0.00
29.250	0.00	0.00	0.000	O	|	|	|	0.00
29.333	0.00	0.00	0.000	O	|	|	|	0.00
29.417	0.00	0.00	0.000	O	|	|	|	0.00

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29.500    0.00    0.00      0.000  O       |       |       |       |     0.00
29.583    0.00    0.00      0.000  O       |       |       |       |     0.00
29.667    0.00    0.00      0.000  O       |       |       |       |     0.00
29.750    0.00    0.00      0.000  O       |       |       |       |     0.00
29.833    0.00    0.00      0.000  O       |       |       |       |     0.00
29.917    0.00    0.00      0.000  O       |       |       |       |     0.00
30.000    0.00    0.00      0.000  O       |       |       |       |     0.00
30.083    0.00    0.00      0.000  O       |       |       |       |     0.00
30.167    0.00    0.00      0.000  O       |       |       |       |     0.00
30.250    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =   363
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.271 (CFS)
                      Total volume =       0.328 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
1-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA0212.rte
**********HYDROGRAPH DATA**********
Number of intervals = 14
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 6.226 (CFS)
Total volume = 0.203 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 14
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.6 3.11 4.67 6.23	Depth (Ft.)
0.083	0.72	0.01	0.002	O I | | | | |	0.03
0.167	1.20	0.05	0.009	O I | | | | |	0.10
0.250	1.43	0.09	0.017	O I| | | | |	0.20
0.333	1.52	0.12	0.027	O I| | | | |	0.27
0.417	1.59	0.13	0.037	O I | | | |	0.32
0.500	1.73	0.14	0.047	O I | | | |	0.36
0.583	2.06	0.15	0.059	O | I | | |	0.41
0.667	2.42	0.16	0.073	O | I | | |	0.47
0.750	3.22	0.17	0.092	O | | I | |	0.54
0.833	6.23	0.19	0.123	O | | | | I	0.67
0.917	4.49	0.21	0.159	|O | | I| |	0.81
1.000	2.09	0.22	0.180	|O | I | | |	0.90
1.083	0.64	0.23	0.188	|O I | | | |	0.93
1.167	0.08	0.23	0.189	IO | | | |	0.93
1.250	0.00	0.23	0.187	IO | | | |	0.92
1.333	0.00	0.22	0.186	IO | | | |	0.92
1.417	0.00	0.22	0.184	IO | | | |	0.91
1.500	0.00	0.22	0.183	IO | | | |	0.91
1.583	0.00	0.22	0.181	IO | | | |	0.90
1.667	0.00	0.22	0.180	IO | | | |	0.89
1.750	0.00	0.22	0.178	IO | | | |	0.89
1.833	0.00	0.22	0.177	IO | | | |	0.88
1.917	0.00	0.22	0.175	IO | | | |	0.88
2.000	0.00	0.22	0.173	IO | | | |	0.87
2.083	0.00	0.22	0.172	IO | | | |	0.86
2.167	0.00	0.22	0.171	IO | | | |	0.86
2.250	0.00	0.22	0.169	IO | | | |	0.85
2.333	0.00	0.21	0.168	IO | | | |	0.85
2.417	0.00	0.21	0.166	IO | | | |	0.84
2.500	0.00	0.21	0.165	IO | | | |	0.83
2.583	0.00	0.21	0.163	IO | | | |	0.83
2.667	0.00	0.21	0.162	IO | | | |	0.82
2.750	0.00	0.21	0.160	IO | | | |	0.82
2.833	0.00	0.21	0.159	IO | | | |	0.81
2.917	0.00	0.21	0.157	IO | | | |	0.81
3.000	0.00	0.21	0.156	IO | | | |	0.80
3.083	0.00	0.21	0.154	IO | | | |	0.79
3.167	0.00	0.21	0.153	IO | | | |	0.79
3.250	0.00	0.21	0.152	IO | | | |	0.78
3.333	0.00	0.21	0.150	IO | | | |	0.78
3.417	0.00	0.20	0.149	IO | | | |	0.77
3.500	0.00	0.20	0.147	IO | | | |	0.77
3.583	0.00	0.20	0.146	IO | | | |	0.76
3.667	0.00	0.20	0.145	IO | | | |	0.75
3.750	0.00	0.20	0.143	IO | | | |	0.75
3.833	0.00	0.20	0.142	IO | | | |	0.74
3.917	0.00	0.20	0.140	IO | | | |	0.74
4.000	0.00	0.20	0.139	IO | | | |	0.73
4.083	0.00	0.20	0.138	IO | | | |	0.73
4.167	0.00	0.20	0.136	IO | | | |	0.72
4.250	0.00	0.20	0.135	IO | | | |	0.72
4.333	0.00	0.20	0.134	IO | | | |	0.71
4.417	0.00	0.20	0.132	IO | | | |	0.71
4.500	0.00	0.19	0.131	O | | | |	0.70
4.583	0.00	0.19	0.130	O | | | |	0.69
4.667	0.00	0.19	0.128	O | | | |	0.69
4.750	0.00	0.19	0.127	O | | | |	0.68
4.833	0.00	0.19	0.126	O | | | |	0.68
4.917	0.00	0.19	0.124	O | | | |	0.67
5.000	0.00	0.19	0.123	O | | | |	0.67
5.083	0.00	0.19	0.122	O | | | |	0.66
5.167	0.00	0.19	0.120	O | | | |	0.66
5.250	0.00	0.19	0.119	O | | | |	0.65
5.333	0.00	0.19	0.118	O | | | |	0.65
5.417	0.00	0.19	0.116	O | | | |	0.64

5.500	0.00	0.19	0.115	O	|	|	|	0.64
5.583	0.00	0.19	0.114	O	|	|	|	0.63
5.667	0.00	0.18	0.113	O	|	|	|	0.63
5.750	0.00	0.18	0.111	O	|	|	|	0.62
5.833	0.00	0.18	0.110	O	|	|	|	0.62
5.917	0.00	0.18	0.109	O	|	|	|	0.61
6.000	0.00	0.18	0.108	O	|	|	|	0.61
6.083	0.00	0.18	0.106	O	|	|	|	0.60
6.167	0.00	0.18	0.105	O	|	|	|	0.60
6.250	0.00	0.18	0.104	O	|	|	|	0.59
6.333	0.00	0.18	0.103	O	|	|	|	0.59
6.417	0.00	0.18	0.101	O	|	|	|	0.58
6.500	0.00	0.18	0.100	O	|	|	|	0.58
6.583	0.00	0.18	0.099	O	|	|	|	0.57
6.667	0.00	0.18	0.098	O	|	|	|	0.57
6.750	0.00	0.18	0.097	O	|	|	|	0.56
6.833	0.00	0.17	0.095	O	|	|	|	0.56
6.917	0.00	0.17	0.094	O	|	|	|	0.55
7.000	0.00	0.17	0.093	O	|	|	|	0.55
7.083	0.00	0.17	0.092	O	|	|	|	0.54
7.167	0.00	0.17	0.091	O	|	|	|	0.54
7.250	0.00	0.17	0.089	O	|	|	|	0.53
7.333	0.00	0.17	0.088	O	|	|	|	0.53
7.417	0.00	0.17	0.087	O	|	|	|	0.52
7.500	0.00	0.17	0.086	O	|	|	|	0.52
7.583	0.00	0.17	0.085	O	|	|	|	0.51
7.667	0.00	0.17	0.084	O	|	|	|	0.51
7.750	0.00	0.17	0.082	O	|	|	|	0.51
7.833	0.00	0.17	0.081	O	|	|	|	0.50
7.917	0.00	0.17	0.080	O	|	|	|	0.50
8.000	0.00	0.17	0.079	O	|	|	|	0.49
8.083	0.00	0.16	0.078	O	|	|	|	0.49
8.167	0.00	0.16	0.077	O	|	|	|	0.48
8.250	0.00	0.16	0.076	O	|	|	|	0.48
8.333	0.00	0.16	0.074	O	|	|	|	0.47
8.417	0.00	0.16	0.073	O	|	|	|	0.47
8.500	0.00	0.16	0.072	O	|	|	|	0.46
8.583	0.00	0.16	0.071	O	|	|	|	0.46
8.667	0.00	0.16	0.070	O	|	|	|	0.45
8.750	0.00	0.16	0.069	O	|	|	|	0.45
8.833	0.00	0.16	0.068	O	|	|	|	0.45
8.917	0.00	0.16	0.067	O	|	|	|	0.44
9.000	0.00	0.16	0.066	O	|	|	|	0.44
9.083	0.00	0.15	0.065	O	|	|	|	0.43
9.167	0.00	0.15	0.064	O	|	|	|	0.43
9.250	0.00	0.15	0.062	O	|	|	|	0.42
9.333	0.00	0.15	0.061	O	|	|	|	0.42
9.417	0.00	0.15	0.060	O	|	|	|	0.42
9.500	0.00	0.15	0.059	O	|	|	|	0.41
9.583	0.00	0.15	0.058	O	|	|	|	0.41
9.667	0.00	0.15	0.057	O	|	|	|	0.40
9.750	0.00	0.15	0.056	O	|	|	|	0.40
9.833	0.00	0.15	0.055	O	|	|	|	0.39
9.917	0.00	0.15	0.054	O	|	|	|	0.39
10.000	0.00	0.15	0.053	O	|	|	|	0.39
10.083	0.00	0.15	0.052	O	|	|	|	0.38
10.167	0.00	0.14	0.051	O	|	|	|	0.38
10.250	0.00	0.14	0.050	O	|	|	|	0.37
10.333	0.00	0.14	0.049	O	|	|	|	0.37
10.417	0.00	0.14	0.048	O	|	|	|	0.37
10.500	0.00	0.14	0.047	O	|	|	|	0.36
10.583	0.00	0.14	0.046	O	|	|	|	0.36
10.667	0.00	0.14	0.045	O	|	|	|	0.35
10.750	0.00	0.14	0.044	O	|	|	|	0.35
10.833	0.00	0.14	0.043	O	|	|	|	0.35
10.917	0.00	0.14	0.042	O	|	|	|	0.34
11.000	0.00	0.14	0.041	O	|	|	|	0.34
11.083	0.00	0.14	0.041	O	|	|	|	0.33
11.167	0.00	0.14	0.040	O	|	|	|	0.33
11.250	0.00	0.13	0.039	O	|	|	|	0.32
11.333	0.00	0.13	0.038	O	|	|	|	0.32
11.417	0.00	0.13	0.037	O	|	|	|	0.32

11.500	0.00	0.13	0.036	O	|	|	|	0.31
11.583	0.00	0.13	0.035	O	|	|	|	0.31
11.667	0.00	0.13	0.034	O	|	|	|	0.30
11.750	0.00	0.13	0.033	O	|	|	|	0.30
11.833	0.00	0.13	0.032	O	|	|	|	0.30
11.917	0.00	0.13	0.031	O	|	|	|	0.29
12.000	0.00	0.13	0.031	O	|	|	|	0.29
12.083	0.00	0.13	0.030	O	|	|	|	0.28
12.167	0.00	0.12	0.029	O	|	|	|	0.28
12.250	0.00	0.12	0.028	O	|	|	|	0.28
12.333	0.00	0.12	0.027	O	|	|	|	0.27
12.417	0.00	0.12	0.026	O	|	|	|	0.27
12.500	0.00	0.12	0.025	O	|	|	|	0.27
12.583	0.00	0.12	0.025	O	|	|	|	0.26
12.667	0.00	0.12	0.024	O	|	|	|	0.26
12.750	0.00	0.12	0.023	O	|	|	|	0.25
12.833	0.00	0.12	0.022	O	|	|	|	0.25
12.917	0.00	0.11	0.021	O	|	|	|	0.24
13.000	0.00	0.11	0.021	O	|	|	|	0.23
13.083	0.00	0.11	0.020	O	|	|	|	0.23
13.167	0.00	0.10	0.019	O	|	|	|	0.22
13.250	0.00	0.10	0.018	O	|	|	|	0.21
13.333	0.00	0.10	0.018	O	|	|	|	0.20
13.417	0.00	0.09	0.017	O	|	|	|	0.19
13.500	0.00	0.09	0.016	O	|	|	|	0.19
13.583	0.00	0.09	0.016	O	|	|	|	0.18
13.667	0.00	0.08	0.015	O	|	|	|	0.17
13.750	0.00	0.08	0.015	O	|	|	|	0.17
13.833	0.00	0.08	0.014	O	|	|	|	0.16
13.917	0.00	0.07	0.014	O	|	|	|	0.16
14.000	0.00	0.07	0.013	O	|	|	|	0.15
14.083	0.00	0.07	0.013	O	|	|	|	0.14
14.167	0.00	0.07	0.012	O	|	|	|	0.14
14.250	0.00	0.06	0.012	O	|	|	|	0.13
14.333	0.00	0.06	0.011	O	|	|	|	0.13
14.417	0.00	0.06	0.011	O	|	|	|	0.12
14.500	0.00	0.06	0.011	O	|	|	|	0.12
14.583	0.00	0.05	0.010	O	|	|	|	0.12
14.667	0.00	0.05	0.010	O	|	|	|	0.11
14.750	0.00	0.05	0.009	O	|	|	|	0.11
14.833	0.00	0.05	0.009	O	|	|	|	0.10
14.917	0.00	0.05	0.009	O	|	|	|	0.10
15.000	0.00	0.05	0.008	O	|	|	|	0.10
15.083	0.00	0.04	0.008	O	|	|	|	0.09
15.167	0.00	0.04	0.008	O	|	|	|	0.09
15.250	0.00	0.04	0.008	O	|	|	|	0.09
15.333	0.00	0.04	0.007	O	|	|	|	0.08
15.417	0.00	0.04	0.007	O	|	|	|	0.08
15.500	0.00	0.04	0.007	O	|	|	|	0.08
15.583	0.00	0.04	0.007	O	|	|	|	0.07
15.667	0.00	0.03	0.006	O	|	|	|	0.07
15.750	0.00	0.03	0.006	O	|	|	|	0.07
15.833	0.00	0.03	0.006	O	|	|	|	0.07
15.917	0.00	0.03	0.006	O	|	|	|	0.06
16.000	0.00	0.03	0.005	O	|	|	|	0.06
16.083	0.00	0.03	0.005	O	|	|	|	0.06
16.167	0.00	0.03	0.005	O	|	|	|	0.06
16.250	0.00	0.03	0.005	O	|	|	|	0.06
16.333	0.00	0.03	0.005	O	|	|	|	0.05
16.417	0.00	0.02	0.005	O	|	|	|	0.05
16.500	0.00	0.02	0.004	O	|	|	|	0.05
16.583	0.00	0.02	0.004	O	|	|	|	0.05
16.667	0.00	0.02	0.004	O	|	|	|	0.05
16.750	0.00	0.02	0.004	O	|	|	|	0.04
16.833	0.00	0.02	0.004	O	|	|	|	0.04
16.917	0.00	0.02	0.004	O	|	|	|	0.04
17.000	0.00	0.02	0.003	O	|	|	|	0.04
17.083	0.00	0.02	0.003	O	|	|	|	0.04
17.167	0.00	0.02	0.003	O	|	|	|	0.04
17.250	0.00	0.02	0.003	O	|	|	|	0.04
17.333	0.00	0.02	0.003	O	|	|	|	0.03
17.417	0.00	0.02	0.003	O	|	|	|	0.03

17.500	0.00	0.01	0.003	O	|	|	|	0.03
17.583	0.00	0.01	0.003	O	|	|	|	0.03
17.667	0.00	0.01	0.003	O	|	|	|	0.03
17.750	0.00	0.01	0.003	O	|	|	|	0.03
17.833	0.00	0.01	0.002	O	|	|	|	0.03
17.917	0.00	0.01	0.002	O	|	|	|	0.03
18.000	0.00	0.01	0.002	O	|	|	|	0.03
18.083	0.00	0.01	0.002	O	|	|	|	0.02
18.167	0.00	0.01	0.002	O	|	|	|	0.02
18.250	0.00	0.01	0.002	O	|	|	|	0.02
18.333	0.00	0.01	0.002	O	|	|	|	0.02
18.417	0.00	0.01	0.002	O	|	|	|	0.02
18.500	0.00	0.01	0.002	O	|	|	|	0.02
18.583	0.00	0.01	0.002	O	|	|	|	0.02
18.667	0.00	0.01	0.002	O	|	|	|	0.02
18.750	0.00	0.01	0.002	O	|	|	|	0.02
18.833	0.00	0.01	0.002	O	|	|	|	0.02
18.917	0.00	0.01	0.001	O	|	|	|	0.02
19.000	0.00	0.01	0.001	O	|	|	|	0.02
19.083	0.00	0.01	0.001	O	|	|	|	0.02
19.167	0.00	0.01	0.001	O	|	|	|	0.02
19.250	0.00	0.01	0.001	O	|	|	|	0.01
19.333	0.00	0.01	0.001	O	|	|	|	0.01
19.417	0.00	0.01	0.001	O	|	|	|	0.01
19.500	0.00	0.01	0.001	O	|	|	|	0.01
19.583	0.00	0.01	0.001	O	|	|	|	0.01
19.667	0.00	0.01	0.001	O	|	|	|	0.01
19.750	0.00	0.01	0.001	O	|	|	|	0.01
19.833	0.00	0.01	0.001	O	|	|	|	0.01
19.917	0.00	0.01	0.001	O	|	|	|	0.01
20.000	0.00	0.00	0.001	O	|	|	|	0.01
20.083	0.00	0.00	0.001	O	|	|	|	0.01
20.167	0.00	0.00	0.001	O	|	|	|	0.01
20.250	0.00	0.00	0.001	O	|	|	|	0.01
20.333	0.00	0.00	0.001	O	|	|	|	0.01
20.417	0.00	0.00	0.001	O	|	|	|	0.01
20.500	0.00	0.00	0.001	O	|	|	|	0.01
20.583	0.00	0.00	0.001	O	|	|	|	0.01
20.667	0.00	0.00	0.001	O	|	|	|	0.01
20.750	0.00	0.00	0.001	O	|	|	|	0.01
20.833	0.00	0.00	0.001	O	|	|	|	0.01
20.917	0.00	0.00	0.001	O	|	|	|	0.01
21.000	0.00	0.00	0.001	O	|	|	|	0.01
21.083	0.00	0.00	0.001	O	|	|	|	0.01
21.167	0.00	0.00	0.001	O	|	|	|	0.01
21.250	0.00	0.00	0.001	O	|	|	|	0.01
21.333	0.00	0.00	0.001	O	|	|	|	0.01
21.417	0.00	0.00	0.000	O	|	|	|	0.01
21.500	0.00	0.00	0.000	O	|	|	|	0.01
21.583	0.00	0.00	0.000	O	|	|	|	0.01
21.667	0.00	0.00	0.000	O	|	|	|	0.01
21.750	0.00	0.00	0.000	O	|	|	|	0.00
21.833	0.00	0.00	0.000	O	|	|	|	0.00
21.917	0.00	0.00	0.000	O	|	|	|	0.00
22.000	0.00	0.00	0.000	O	|	|	|	0.00
22.083	0.00	0.00	0.000	O	|	|	|	0.00
22.167	0.00	0.00	0.000	O	|	|	|	0.00
22.250	0.00	0.00	0.000	O	|	|	|	0.00
22.333	0.00	0.00	0.000	O	|	|	|	0.00
22.417	0.00	0.00	0.000	O	|	|	|	0.00
22.500	0.00	0.00	0.000	O	|	|	|	0.00
22.583	0.00	0.00	0.000	O	|	|	|	0.00
22.667	0.00	0.00	0.000	O	|	|	|	0.00
22.750	0.00	0.00	0.000	O	|	|	|	0.00
22.833	0.00	0.00	0.000	O	|	|	|	0.00
22.917	0.00	0.00	0.000	O	|	|	|	0.00
23.000	0.00	0.00	0.000	O	|	|	|	0.00
23.083	0.00	0.00	0.000	O	|	|	|	0.00
23.167	0.00	0.00	0.000	O	|	|	|	0.00
23.250	0.00	0.00	0.000	O	|	|	|	0.00
23.333	0.00	0.00	0.000	O	|	|	|	0.00
23.417	0.00	0.00	0.000	O	|	|	|	0.00

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23.500    0.00    0.00      0.000  O       |       |       |       |     0.00
23.583    0.00    0.00      0.000  O       |       |       |       |     0.00
23.667    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                        Number of intervals =   284
                        Time interval =    5.0 (Min.)
                        Maximum/Peak flow rate =        0.226 (CFS)
                        Total volume =       0.202 (Ac.Ft)
                Status of hydrographs being held in storage
                           Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
                Peak (CFS)      0.000     0.000     0.000     0.000     0.000
                Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
24-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA05245.rte
**********HYDROGRAPH DATA**********
Number of intervals = 290
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.810 (CFS)
Total volume = 1.100 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 290
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.5	0.90	1.36	1.81	Depth (Ft.)
0.083	0.06	0.00	0.000	OI					0.00
0.167	0.10	0.00	0.001	OI					0.01
0.250	0.11	0.01	0.001	OI					0.02
0.333	0.14	0.01	0.002	O I					0.02
0.417	0.16	0.02	0.003	O I					0.04
0.500	0.16	0.02	0.004	O I					0.05
0.583	0.16	0.03	0.005	O I					0.06
0.667	0.16	0.03	0.006	O I					0.07
0.750	0.16	0.04	0.007	O I					0.08
0.833	0.19	0.04	0.008	O I					0.09
0.917	0.21	0.05	0.009	O I					0.10
1.000	0.21	0.05	0.010	O I					0.11
1.083	0.18	0.06	0.011	O I					0.12
1.167	0.16	0.06	0.012	OI					0.13
1.250	0.16	0.07	0.012	OI					0.14
1.333	0.16	0.07	0.013	OI					0.15
1.417	0.16	0.07	0.014	OI					0.15
1.500	0.16	0.08	0.014	OI					0.16
1.583	0.16	0.08	0.015	OI					0.17
1.667	0.16	0.08	0.015	OI					0.17
1.750	0.16	0.08	0.016	OI					0.18
1.833	0.19	0.09	0.016	O I					0.19
1.917	0.21	0.09	0.017	O I					0.19
2.000	0.21	0.10	0.018	O I					0.20
2.083	0.21	0.10	0.019	O I					0.21
2.167	0.21	0.10	0.020	O I					0.22
2.250	0.21	0.11	0.020	O I					0.23
2.333	0.21	0.11	0.021	O I					0.24
2.417	0.21	0.12	0.022	OI					0.25
2.500	0.21	0.12	0.022	OI					0.25
2.583	0.24	0.12	0.023	O I					0.25
2.667	0.26	0.12	0.024	O I					0.26
2.750	0.27	0.12	0.025	O I					0.26
2.833	0.27	0.12	0.026	O I					0.27
2.917	0.27	0.12	0.027	O I					0.27
3.000	0.27	0.12	0.028	O I					0.28
3.083	0.27	0.12	0.029	O I					0.28
3.167	0.27	0.13	0.030	O I					0.29
3.250	0.27	0.13	0.031	O I					0.29
3.333	0.27	0.13	0.032	O I					0.29
3.417	0.27	0.13	0.033	O I					0.30
3.500	0.27	0.13	0.034	O I					0.30
3.583	0.27	0.13	0.035	O I					0.31
3.667	0.27	0.13	0.036	O I					0.31
3.750	0.27	0.13	0.036	O I					0.32
3.833	0.30	0.13	0.037	O I					0.32
3.917	0.32	0.13	0.039	O I					0.33
4.000	0.32	0.14	0.040	O I					0.33
4.083	0.32	0.14	0.041	O I					0.34
4.167	0.32	0.14	0.042	O I					0.34
4.250	0.32	0.14	0.044	O I					0.35
4.333	0.35	0.14	0.045	O I					0.35
4.417	0.37	0.14	0.047	O I					0.36
4.500	0.37	0.14	0.048	O I					0.37
4.583	0.37	0.14	0.050	O I					0.37
4.667	0.37	0.14	0.051	O I					0.38
4.750	0.37	0.15	0.053	O I					0.38
4.833	0.40	0.15	0.054	O I					0.39
4.917	0.42	0.15	0.056	O I					0.40
5.000	0.43	0.15	0.058	O I					0.41
5.083	0.36	0.15	0.060	O I					0.41
5.167	0.33	0.15	0.061	O I					0.42
5.250	0.32	0.15	0.062	O I					0.42
5.333	0.35	0.15	0.064	O I					0.43
5.417	0.37	0.16	0.065	O I					0.43

5.500	0.37	0.16	0.067	O I				0.44
5.583	0.40	0.16	0.068	O I				0.45
5.667	0.42	0.16	0.070	O I				0.45
5.750	0.43	0.16	0.072	O I				0.46
5.833	0.43	0.16	0.074	O I				0.47
5.917	0.43	0.16	0.075	O I				0.48
6.000	0.43	0.16	0.077	O I				0.48
6.083	0.46	0.17	0.079	O I				0.49
6.167	0.48	0.17	0.081	O I				0.50
6.250	0.48	0.17	0.083	O I				0.51
6.333	0.48	0.17	0.085	O I				0.52
6.417	0.48	0.17	0.088	O I				0.53
6.500	0.48	0.17	0.090	O I				0.53
6.583	0.51	0.17	0.092	O I				0.54
6.667	0.53	0.17	0.094	O I				0.55
6.750	0.53	0.18	0.097	O I				0.56
6.833	0.53	0.18	0.099	O I				0.57
6.917	0.53	0.18	0.102	O I				0.58
7.000	0.53	0.18	0.104	O I				0.59
7.083	0.53	0.18	0.106	O I				0.60
7.167	0.53	0.18	0.109	O I				0.61
7.250	0.53	0.18	0.111	O I				0.62
7.333	0.56	0.19	0.114	O I				0.63
7.417	0.58	0.19	0.116	O I				0.64
7.500	0.59	0.19	0.119	O I				0.65
7.583	0.62	0.19	0.122	O I				0.66
7.667	0.64	0.19	0.125	O I				0.68
7.750	0.64	0.19	0.128	O I				0.69
7.833	0.67	0.19	0.131	O I				0.70
7.917	0.69	0.20	0.135	O I				0.71
8.000	0.69	0.20	0.138	O I				0.73
8.083	0.75	0.20	0.142	O I				0.74
8.167	0.79	0.20	0.145	O I				0.76
8.250	0.80	0.20	0.150	O I				0.77
8.333	0.80	0.21	0.154	O I				0.79
8.417	0.80	0.21	0.158	O I				0.81
8.500	0.80	0.21	0.162	O I				0.82
8.583	0.83	0.21	0.166	O I				0.84
8.667	0.85	0.22	0.170	O I				0.86
8.750	0.85	0.22	0.175	O I				0.87
8.833	0.88	0.22	0.179	O I				0.89
8.917	0.90	0.22	0.184	O I				0.91
9.000	0.90	0.23	0.188	O I				0.93
9.083	0.97	0.23	0.193	O I				0.95
9.167	1.01	0.23	0.198	O I				0.97
9.250	1.01	0.23	0.204	O I				0.99
9.333	1.04	0.24	0.209	O I				1.01
9.417	1.06	0.24	0.215	O I				1.04
9.500	1.06	0.24	0.220	O I				1.06
9.583	1.10	0.25	0.226	O I				1.08
9.667	1.11	0.25	0.232	O I				1.10
9.750	1.12	0.25	0.238	O I				1.13
9.833	1.15	0.25	0.244	O I				1.15
9.917	1.17	0.26	0.250	O I				1.18
10.000	1.17	0.26	0.257	O I				1.20
10.083	0.96	0.26	0.262	O I				1.23
10.167	0.82	0.26	0.266	O I				1.24
10.250	0.80	0.26	0.270	O I				1.26
10.333	0.80	0.27	0.274	O I				1.27
10.417	0.80	0.27	0.278	O I				1.29
10.500	0.80	0.27	0.281	O I				1.30
10.583	0.95	0.27	0.285	O I				1.32
10.667	1.05	0.27	0.290	O I				1.34
10.750	1.06	0.28	0.296	O I				1.36
10.833	1.06	0.28	0.301	O I				1.38
10.917	1.06	0.28	0.307	O I				1.41
11.000	1.06	0.28	0.312	O I				1.43
11.083	1.03	0.28	0.317	O I				1.45
11.167	1.01	0.29	0.322	O I				1.47
11.250	1.01	0.29	0.327	O I				1.49
11.333	1.01	0.29	0.332	O I				1.51
11.417	1.01	0.29	0.337	O I				1.53

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11.500    1.01    0.29      0.342  |     O  |        |I       |        |      1.55
11.583    0.95    0.30      0.347  |     O  |        I        |        |      1.57
11.667    0.91    0.30      0.351  |     O  |        I        |        |      1.59
11.750    0.90    0.30      0.355  |     O  |        I        |        |      1.61
11.833    0.94    0.30      0.360  |     O  |        I        |        |      1.63
11.917    0.95    0.30      0.364  |     O  |        I        |        |      1.64
12.000    0.96    0.30      0.369  |     O  |        I        |        |      1.66
12.083    1.17    0.31      0.374  |     O  |         |   I   |        |      1.68
12.167    1.31    0.31      0.380  |     O  |         |     I|        |      1.71
12.250    1.33    0.31      0.387  |     O  |         |      I|        |      1.74
12.333    1.36    0.31      0.394  |     O  |         |       I        |      1.77
12.417    1.38    0.32      0.402  |     O  |         |       I        |      1.80
12.500    1.38    0.32      0.409  |     O  |         |       I        |      1.83
12.583    1.45    0.32      0.417  |     O  |         |       |I       |      1.86
12.667    1.48    0.32      0.424  |     O  |         |       | I      |      1.89
12.750    1.49    0.33      0.432  |     O  |         |       | I      |      1.92
12.833    1.52    0.33      0.441  |     O  |         |       | I      |      1.96
12.917    1.54    0.33      0.449  |     O  |         |       |  I     |      1.99
13.000    1.54    0.34      0.457  |     O  |         |       |  I     |      2.03
13.083    1.70    0.34      0.466  |     O  |         |       |    I   |      2.06
13.167    1.79    0.34      0.476  |      O |         |       |     I|      2.11
13.250    1.81    0.35      0.486  |      O |         |       |      I       2.15
13.333    1.81    0.35      0.496  |      O |         |       |      I       2.19
13.417    1.81    0.35      0.506  |      O |         |       |      I       2.24
13.500    1.81    0.36      0.516  |      O |         |       |      I       2.28
13.583    1.47    0.36      0.525  |      O |         |       | I      |      2.32
13.667    1.26    0.36      0.532  |      O |         |     I  |       |      2.35
13.750    1.22    0.36      0.538  |      O |         |    I   |       |      2.37
13.833    1.22    0.37      0.544  |      O |         |    I   |       |      2.40
13.917    1.22    0.37      0.549  |      O |         |    I   |       |      2.42
14.000    1.22    0.37      0.555  |      O |         |    I   |       |      2.45
14.083    1.35    0.37      0.562  |      O |         |      I|       |      2.48
14.167    1.42    0.37      0.569  |      O |         |       |I       |      2.51
14.250    1.44    0.38      0.576  |      O |         |       |I       |      2.54
14.333    1.41    0.38      0.583  |      O |         |       I        |      2.57
14.417    1.39    0.38      0.590  |      O |         |       I        |      2.60
14.500    1.38    0.38      0.597  |      O |         |       I        |      2.64
14.583    1.38    0.39      0.604  |      O |         |       I        |      2.67
14.667    1.38    0.39      0.611  |      O |         |       I        |      2.70
14.750    1.38    0.39      0.618  |      O |         |       I        |      2.73
14.833    1.35    0.39      0.624  |      O |         |      I|        |      2.76
14.917    1.33    0.39      0.631  |      O |         |      I|        |      2.79
15.000    1.33    0.40      0.637  |       O|         |      I|        |      2.82
15.083    1.30    0.40      0.644  |       O|         |     I  |       |      2.85
15.167    1.28    0.40      0.650  |       O|         |     I  |       |      2.88
15.250    1.28    0.40      0.656  |       O|         |     I  |       |      2.90
15.333    1.25    0.40      0.662  |       O|         |     I  |       |      2.93
15.417    1.23    0.41      0.667  |       O|         |    I   |       |      2.96
15.500    1.22    0.41      0.673  |       O|         |    I   |       |      2.98
15.583    1.10    0.41      0.678  |       O|         |  I     |       |      3.01
15.667    1.02    0.41      0.683  |       O|         | I      |       |      3.03
15.750    1.01    0.41      0.687  |       O|         |I       |       |      3.05
15.833    1.01    0.41      0.691  |       O|         |I       |       |      3.07
15.917    1.01    0.42      0.695  |       O|         |I       |       |      3.09
16.000    1.01    0.44      0.699  |       O|         |I       |       |      3.11
16.083    0.55    0.47      0.701  |        OI        |        |       |      3.12
16.167    0.26    0.46      0.701  |    I   O         |        |       |      3.12
16.250    0.21    0.45      0.699  |   I    O|        |        |       |      3.11
16.333    0.21    0.43      0.698  |   I    O|        |        |       |      3.10
16.417    0.21    0.42      0.697  |   I    O|        |        |       |      3.10
16.500    0.21    0.42      0.695  |   I    O|        |        |       |      3.09
16.583    0.18    0.41      0.694  |   I    O|        |        |       |      3.08
16.667    0.16    0.41      0.692  | I      O|        |        |       |      3.07
16.750    0.16    0.41      0.690  | I      O|        |        |       |      3.07
16.833    0.16    0.41      0.688  | I      O|        |        |       |      3.06
16.917    0.16    0.41      0.687  | I      O|        |        |       |      3.05
17.000    0.16    0.41      0.685  | I      O|        |        |       |      3.04
17.083    0.22    0.41      0.683  |   I    O|        |        |       |      3.03
17.167    0.26    0.41      0.682  |    I   O|        |        |       |      3.03
17.250    0.27    0.41      0.681  |    I   O|        |        |       |      3.02
17.333    0.27    0.41      0.680  |    I   O|        |        |       |      3.02
17.417    0.27    0.41      0.679  |    I   O|        |        |       |      3.01
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17.500	0.27	0.41	0.678	| I O|	|	|	|	3.01
17.583	0.27	0.41	0.677	| I O|	|	|	|	3.00
17.667	0.27	0.41	0.676	| I O|	|	|	|	3.00
17.750	0.27	0.41	0.675	| I O|	|	|	|	2.99
17.833	0.24	0.41	0.674	| I O|	|	|	|	2.99
17.917	0.22	0.41	0.673	| I O|	|	|	|	2.98
18.000	0.21	0.41	0.672	| I O|	|	|	|	2.98
18.083	0.21	0.41	0.670	| I O|	|	|	|	2.97
18.167	0.21	0.41	0.669	| I O|	|	|	|	2.96
18.250	0.21	0.41	0.668	| I O|	|	|	|	2.96
18.333	0.21	0.41	0.666	| I O|	|	|	|	2.95
18.417	0.21	0.41	0.665	| I O|	|	|	|	2.95
18.500	0.21	0.40	0.664	| I O|	|	|	|	2.94
18.583	0.18	0.40	0.662	| I O|	|	|	|	2.93
18.667	0.16	0.40	0.661	| I O|	|	|	|	2.93
18.750	0.16	0.40	0.659	| I O|	|	|	|	2.92
18.833	0.13	0.40	0.657	| I O|	|	|	|	2.91
18.917	0.11	0.40	0.655	|I O|	|	|	|	2.90
19.000	0.11	0.40	0.653	|I O|	|	|	|	2.89
19.083	0.14	0.40	0.651	| I O|	|	|	|	2.88
19.167	0.16	0.40	0.650	| I O|	|	|	|	2.88
19.250	0.16	0.40	0.648	| I O|	|	|	|	2.87
19.333	0.19	0.40	0.646	| I O|	|	|	|	2.86
19.417	0.21	0.40	0.645	| I O|	|	|	|	2.85
19.500	0.21	0.40	0.644	| I O|	|	|	|	2.85
19.583	0.18	0.40	0.642	| I O|	|	|	|	2.84
19.667	0.16	0.40	0.641	| I O|	|	|	|	2.84
19.750	0.16	0.40	0.639	| I O|	|	|	|	2.83
19.833	0.13	0.40	0.637	| I O|	|	|	|	2.82
19.917	0.11	0.40	0.636	|I O |	|	|	|	2.81
20.000	0.11	0.40	0.634	|I O |	|	|	|	2.80
20.083	0.14	0.39	0.632	| I O |	|	|	|	2.79
20.167	0.16	0.39	0.630	| I O |	|	|	|	2.79
20.250	0.16	0.39	0.628	| I O |	|	|	|	2.78
20.333	0.16	0.39	0.627	| I O |	|	|	|	2.77
20.417	0.16	0.39	0.625	| I O |	|	|	|	2.76
20.500	0.16	0.39	0.624	| I O |	|	|	|	2.76
20.583	0.16	0.39	0.622	| I O |	|	|	|	2.75
20.667	0.16	0.39	0.620	| I O |	|	|	|	2.74
20.750	0.16	0.39	0.619	| I O |	|	|	|	2.74
20.833	0.13	0.39	0.617	| I O |	|	|	|	2.73
20.917	0.11	0.39	0.615	|I O |	|	|	|	2.72
21.000	0.11	0.39	0.613	|I O |	|	|	|	2.71
21.083	0.14	0.39	0.611	| I O |	|	|	|	2.70
21.167	0.16	0.39	0.610	| I O |	|	|	|	2.69
21.250	0.16	0.39	0.608	| I O |	|	|	|	2.69
21.333	0.13	0.39	0.606	| I O |	|	|	|	2.68
21.417	0.11	0.39	0.605	|I O |	|	|	|	2.67
21.500	0.11	0.39	0.603	|I O |	|	|	|	2.66
21.583	0.14	0.38	0.601	| I O |	|	|	|	2.65
21.667	0.16	0.38	0.599	| I O |	|	|	|	2.65
21.750	0.16	0.38	0.598	| I O |	|	|	|	2.64
21.833	0.13	0.38	0.596	| I O |	|	|	|	2.63
21.917	0.11	0.38	0.594	|I O |	|	|	|	2.62
22.000	0.11	0.38	0.592	|I O |	|	|	|	2.62
22.083	0.14	0.38	0.591	| I O |	|	|	|	2.61
22.167	0.16	0.38	0.589	| I O |	|	|	|	2.60
22.250	0.16	0.38	0.587	| I O |	|	|	|	2.59
22.333	0.13	0.38	0.586	| I O |	|	|	|	2.59
22.417	0.11	0.38	0.584	|I O |	|	|	|	2.58
22.500	0.11	0.38	0.582	|I O |	|	|	|	2.57
22.583	0.11	0.38	0.580	|I O |	|	|	|	2.56
22.667	0.11	0.38	0.578	|I O |	|	|	|	2.55
22.750	0.11	0.38	0.577	|I O |	|	|	|	2.54
22.833	0.11	0.38	0.575	|I O |	|	|	|	2.53
22.917	0.11	0.38	0.573	|I O |	|	|	|	2.53
23.000	0.11	0.38	0.571	|I O |	|	|	|	2.52
23.083	0.11	0.37	0.569	|I O |	|	|	|	2.51
23.167	0.11	0.37	0.567	|I O |	|	|	|	2.50
23.250	0.11	0.37	0.565	|I O |	|	|	|	2.49
23.333	0.11	0.37	0.564	|I O |	|	|	|	2.49
23.417	0.11	0.37	0.562	|I O |	|	|	|	2.48

23.500	0.11	0.37	0.560	|I	O |	|	|	|	2.47
23.583	0.11	0.37	0.558	|I	O |	|	|	|	2.46
23.667	0.11	0.37	0.556	|I	O |	|	|	|	2.45
23.750	0.11	0.37	0.554	|I	O |	|	|	|	2.45
23.833	0.11	0.37	0.553	|I	O |	|	|	|	2.44
23.917	0.11	0.37	0.551	|I	O |	|	|	|	2.43
24.000	0.11	0.37	0.549	|I	O |	|	|	|	2.42
24.083	0.04	0.37	0.547	I	O |	|	|	|	2.41
24.167	0.01	0.37	0.545	I	O |	|	|	|	2.40
24.250	0.00	0.37	0.542	I	O |	|	|	|	2.39
24.333	0.00	0.36	0.540	I	O |	|	|	|	2.38
24.417	0.00	0.36	0.537	I	O |	|	|	|	2.37
24.500	0.00	0.36	0.535	I	O |	|	|	|	2.36
24.583	0.00	0.36	0.532	I	O |	|	|	|	2.35
24.667	0.00	0.36	0.530	I	O |	|	|	|	2.34
24.750	0.00	0.36	0.527	I	O |	|	|	|	2.33
24.833	0.00	0.36	0.525	I	O |	|	|	|	2.32
24.917	0.00	0.36	0.522	I	O |	|	|	|	2.31
25.000	0.00	0.36	0.520	I	O |	|	|	|	2.30
25.083	0.00	0.36	0.517	I	O |	|	|	|	2.29
25.167	0.00	0.36	0.515	I	O |	|	|	|	2.28
25.250	0.00	0.36	0.512	I	O |	|	|	|	2.26
25.333	0.00	0.35	0.510	I	O |	|	|	|	2.25
25.417	0.00	0.35	0.508	I	O |	|	|	|	2.24
25.500	0.00	0.35	0.505	I	O |	|	|	|	2.23
25.583	0.00	0.35	0.503	I	O |	|	|	|	2.22
25.667	0.00	0.35	0.500	I	O |	|	|	|	2.21
25.750	0.00	0.35	0.498	I	O |	|	|	|	2.20
25.833	0.00	0.35	0.495	I	O |	|	|	|	2.19
25.917	0.00	0.35	0.493	I	O |	|	|	|	2.18
26.000	0.00	0.35	0.491	I	O |	|	|	|	2.17
26.083	0.00	0.35	0.488	I	O |	|	|	|	2.16
26.167	0.00	0.35	0.486	I	O |	|	|	|	2.15
26.250	0.00	0.35	0.483	I	O |	|	|	|	2.14
26.333	0.00	0.34	0.481	I	O |	|	|	|	2.13
26.417	0.00	0.34	0.479	I	O |	|	|	|	2.12
26.500	0.00	0.34	0.476	I	O |	|	|	|	2.11
26.583	0.00	0.34	0.474	I	O |	|	|	|	2.10
26.667	0.00	0.34	0.472	I	O |	|	|	|	2.09
26.750	0.00	0.34	0.469	I	O |	|	|	|	2.08
26.833	0.00	0.34	0.467	I	O |	|	|	|	2.07
26.917	0.00	0.34	0.465	I	O |	|	|	|	2.06
27.000	0.00	0.34	0.462	I	O |	|	|	|	2.05
27.083	0.00	0.34	0.460	I	O |	|	|	|	2.04
27.167	0.00	0.34	0.458	I	O |	|	|	|	2.03
27.250	0.00	0.34	0.455	I	O |	|	|	|	2.02
27.333	0.00	0.33	0.453	I	O |	|	|	|	2.01
27.417	0.00	0.33	0.451	I	O |	|	|	|	2.00
27.500	0.00	0.33	0.448	I	O |	|	|	|	1.99
27.583	0.00	0.33	0.446	I	O |	|	|	|	1.98
27.667	0.00	0.33	0.444	I	O |	|	|	|	1.97
27.750	0.00	0.33	0.442	I	O |	|	|	|	1.96
27.833	0.00	0.33	0.439	I	O |	|	|	|	1.95
27.917	0.00	0.33	0.437	I	O |	|	|	|	1.94
28.000	0.00	0.33	0.435	I	O |	|	|	|	1.93
28.083	0.00	0.33	0.433	I	O |	|	|	|	1.92
28.167	0.00	0.33	0.430	I	O |	|	|	|	1.92
28.250	0.00	0.33	0.428	I	O |	|	|	|	1.91
28.333	0.00	0.32	0.426	I	O |	|	|	|	1.90
28.417	0.00	0.32	0.424	I	O |	|	|	|	1.89
28.500	0.00	0.32	0.421	I	O |	|	|	|	1.88
28.583	0.00	0.32	0.419	I	O |	|	|	|	1.87
28.667	0.00	0.32	0.417	I	O |	|	|	|	1.86
28.750	0.00	0.32	0.415	I	O |	|	|	|	1.85
28.833	0.00	0.32	0.412	I	O |	|	|	|	1.84
28.917	0.00	0.32	0.410	I	O |	|	|	|	1.83
29.000	0.00	0.32	0.408	I	O |	|	|	|	1.82
29.083	0.00	0.32	0.406	I	O |	|	|	|	1.82
29.167	0.00	0.32	0.404	I	O |	|	|	|	1.81
29.250	0.00	0.32	0.402	I	O |	|	|	|	1.80
29.333	0.00	0.31	0.399	I	O |	|	|	|	1.79
29.417	0.00	0.31	0.397	I	O |	|	|	|	1.78

29.500	0.00	0.31	0.395	I	O	|	|	|	1.77
29.583	0.00	0.31	0.393	I	O	|	|	|	1.76
29.667	0.00	0.31	0.391	I	O	|	|	|	1.75
29.750	0.00	0.31	0.389	I	O	|	|	|	1.74
29.833	0.00	0.31	0.386	I	O	|	|	|	1.74
29.917	0.00	0.31	0.384	I	O	|	|	|	1.73
30.000	0.00	0.31	0.382	I	O	|	|	|	1.72
30.083	0.00	0.31	0.380	I	O	|	|	|	1.71
30.167	0.00	0.31	0.378	I	O	|	|	|	1.70
30.250	0.00	0.31	0.376	I	O	|	|	|	1.69
30.333	0.00	0.31	0.374	I	O	|	|	|	1.68
30.417	0.00	0.30	0.372	I	O	|	|	|	1.67
30.500	0.00	0.30	0.370	I	O	|	|	|	1.67
30.583	0.00	0.30	0.367	I	O	|	|	|	1.66
30.667	0.00	0.30	0.365	I	O	|	|	|	1.65
30.750	0.00	0.30	0.363	I	O	|	|	|	1.64
30.833	0.00	0.30	0.361	I	O	|	|	|	1.63
30.917	0.00	0.30	0.359	I	O	|	|	|	1.62
31.000	0.00	0.30	0.357	I	O	|	|	|	1.62
31.083	0.00	0.30	0.355	I	O	|	|	|	1.61
31.167	0.00	0.30	0.353	I	O	|	|	|	1.60
31.250	0.00	0.30	0.351	I	O	|	|	|	1.59
31.333	0.00	0.30	0.349	I	O	|	|	|	1.58
31.417	0.00	0.30	0.347	I	O	|	|	|	1.57
31.500	0.00	0.29	0.345	I	O	|	|	|	1.56
31.583	0.00	0.29	0.343	I	O	|	|	|	1.56
31.667	0.00	0.29	0.341	I	O	|	|	|	1.55
31.750	0.00	0.29	0.339	I	O	|	|	|	1.54
31.833	0.00	0.29	0.337	I	O	|	|	|	1.53
31.917	0.00	0.29	0.335	I	O	|	|	|	1.52
32.000	0.00	0.29	0.333	I	O	|	|	|	1.52
32.083	0.00	0.29	0.331	I	O	|	|	|	1.51
32.167	0.00	0.29	0.329	I	O	|	|	|	1.50
32.250	0.00	0.29	0.327	I	O	|	|	|	1.49
32.333	0.00	0.29	0.325	I	O	|	|	|	1.48
32.417	0.00	0.29	0.323	I	O	|	|	|	1.47
32.500	0.00	0.29	0.321	I	O	|	|	|	1.47
32.583	0.00	0.29	0.319	I	O	|	|	|	1.46
32.667	0.00	0.28	0.317	I	O	|	|	|	1.45
32.750	0.00	0.28	0.315	I	O	|	|	|	1.44
32.833	0.00	0.28	0.313	I	O	|	|	|	1.43
32.917	0.00	0.28	0.311	I	O	|	|	|	1.43
33.000	0.00	0.28	0.309	I	O	|	|	|	1.42
33.083	0.00	0.28	0.307	I	O	|	|	|	1.41
33.167	0.00	0.28	0.305	I	O	|	|	|	1.40
33.250	0.00	0.28	0.303	I	O	|	|	|	1.39
33.333	0.00	0.28	0.301	I	O	|	|	|	1.38
33.417	0.00	0.28	0.299	I	O	|	|	|	1.38
33.500	0.00	0.28	0.298	I	O	|	|	|	1.37
33.583	0.00	0.28	0.296	I	O	|	|	|	1.36
33.667	0.00	0.28	0.294	I	O	|	|	|	1.35
33.750	0.00	0.27	0.292	I	O	|	|	|	1.35
33.833	0.00	0.27	0.290	I	O	|	|	|	1.34
33.917	0.00	0.27	0.288	I	O	|	|	|	1.33
34.000	0.00	0.27	0.286	I	O	|	|	|	1.32
34.083	0.00	0.27	0.284	I	O	|	|	|	1.32
34.167	0.00	0.27	0.282	I	O	|	|	|	1.31
34.250	0.00	0.27	0.281	I	O	|	|	|	1.30
34.333	0.00	0.27	0.279	I	O	|	|	|	1.29
34.417	0.00	0.27	0.277	I	O	|	|	|	1.29
34.500	0.00	0.27	0.275	I	O	|	|	|	1.28
34.583	0.00	0.27	0.273	I	O	|	|	|	1.27
34.667	0.00	0.27	0.271	I	O	|	|	|	1.26
34.750	0.00	0.26	0.270	I	O	|	|	|	1.26
34.833	0.00	0.26	0.268	I	O	|	|	|	1.25
34.917	0.00	0.26	0.266	I	O	|	|	|	1.24
35.000	0.00	0.26	0.264	I	O	|	|	|	1.23
35.083	0.00	0.26	0.262	I	O	|	|	|	1.23
35.167	0.00	0.26	0.261	I	O	|	|	|	1.22
35.250	0.00	0.26	0.259	I	O	|	|	|	1.21
35.333	0.00	0.26	0.257	I	O	|	|	|	1.21
35.417	0.00	0.26	0.255	I	O	|	|	|	1.20

35.500	0.00	0.26	0.253	I	O	|	|	|	1.19
35.583	0.00	0.26	0.252	I	O	|	|	|	1.18
35.667	0.00	0.26	0.250	I	O	|	|	|	1.18
35.750	0.00	0.25	0.248	I	O	|	|	|	1.17
35.833	0.00	0.25	0.246	I	O	|	|	|	1.16
35.917	0.00	0.25	0.245	I	O	|	|	|	1.16
36.000	0.00	0.25	0.243	I	O	|	|	|	1.15
36.083	0.00	0.25	0.241	I	O	|	|	|	1.14
36.167	0.00	0.25	0.239	I	O	|	|	|	1.13
36.250	0.00	0.25	0.238	I	O	|	|	|	1.13
36.333	0.00	0.25	0.236	I	O	|	|	|	1.12
36.417	0.00	0.25	0.234	I	O	|	|	|	1.11
36.500	0.00	0.25	0.233	I	O	|	|	|	1.11
36.583	0.00	0.25	0.231	I	O	|	|	|	1.10
36.667	0.00	0.25	0.229	I	O	|	|	|	1.09
36.750	0.00	0.25	0.227	I	O	|	|	|	1.09
36.833	0.00	0.24	0.226	I	O	|	|	|	1.08
36.917	0.00	0.24	0.224	I	O	|	|	|	1.07
37.000	0.00	0.24	0.222	I	O	|	|	|	1.07
37.083	0.00	0.24	0.221	I	O	|	|	|	1.06
37.167	0.00	0.24	0.219	I	O	|	|	|	1.05
37.250	0.00	0.24	0.217	I	O	|	|	|	1.05
37.333	0.00	0.24	0.216	I	O	|	|	|	1.04
37.417	0.00	0.24	0.214	I	O	|	|	|	1.03
37.500	0.00	0.24	0.212	I	O	|	|	|	1.03
37.583	0.00	0.24	0.211	I	O	|	|	|	1.02
37.667	0.00	0.24	0.209	I	O	|	|	|	1.01
37.750	0.00	0.24	0.208	I	O	|	|	|	1.01
37.833	0.00	0.24	0.206	I	O	|	|	|	1.00
37.917	0.00	0.24	0.204	I	O	|	|	|	0.99
38.000	0.00	0.23	0.203	I	O	|	|	|	0.99
38.083	0.00	0.23	0.201	I	O	|	|	|	0.98
38.167	0.00	0.23	0.199	I	O	|	|	|	0.97
38.250	0.00	0.23	0.198	I	O	|	|	|	0.97
38.333	0.00	0.23	0.196	I	O	|	|	|	0.96
38.417	0.00	0.23	0.195	I	O	|	|	|	0.95
38.500	0.00	0.23	0.193	I	O	|	|	|	0.95
38.583	0.00	0.23	0.192	I	O	|	|	|	0.94
38.667	0.00	0.23	0.190	I	O	|	|	|	0.94
38.750	0.00	0.23	0.188	I	O	|	|	|	0.93
38.833	0.00	0.23	0.187	I	O	|	|	|	0.92
38.917	0.00	0.22	0.185	I	O	|	|	|	0.92
39.000	0.00	0.22	0.184	I	O	|	|	|	0.91
39.083	0.00	0.22	0.182	I	O	|	|	|	0.90
39.167	0.00	0.22	0.181	I	O	|	|	|	0.90
39.250	0.00	0.22	0.179	I	O	|	|	|	0.89
39.333	0.00	0.22	0.178	I	O	|	|	|	0.89
39.417	0.00	0.22	0.176	I	O	|	|	|	0.88
39.500	0.00	0.22	0.175	I	O	|	|	|	0.87
39.583	0.00	0.22	0.173	I	O	|	|	|	0.87
39.667	0.00	0.22	0.172	I	O	|	|	|	0.86
39.750	0.00	0.22	0.170	I	O	|	|	|	0.86
39.833	0.00	0.22	0.169	I	O	|	|	|	0.85
39.917	0.00	0.21	0.167	I	O	|	|	|	0.84
40.000	0.00	0.21	0.166	I	O	|	|	|	0.84
40.083	0.00	0.21	0.164	I	O	|	|	|	0.83
40.167	0.00	0.21	0.163	I	O	|	|	|	0.83
40.250	0.00	0.21	0.161	I	O	|	|	|	0.82
40.333	0.00	0.21	0.160	I	O	|	|	|	0.82
40.417	0.00	0.21	0.158	I	O	|	|	|	0.81
40.500	0.00	0.21	0.157	I	O	|	|	|	0.80
40.583	0.00	0.21	0.155	I	O	|	|	|	0.80
40.667	0.00	0.21	0.154	I	O	|	|	|	0.79
40.750	0.00	0.21	0.153	I	O	|	|	|	0.79
40.833	0.00	0.21	0.151	I	O	|	|	|	0.78
40.917	0.00	0.20	0.150	I	O	|	|	|	0.78
41.000	0.00	0.20	0.148	I	O	|	|	|	0.77
41.083	0.00	0.20	0.147	I	O	|	|	|	0.76
41.167	0.00	0.20	0.146	I	O	|	|	|	0.76
41.250	0.00	0.20	0.144	I	O	|	|	|	0.75
41.333	0.00	0.20	0.143	I	O	|	|	|	0.75
41.417	0.00	0.20	0.141	I	O	|	|	|	0.74

41.500	0.00	0.20	0.140	I	O	|	|	|	| 0.74
41.583	0.00	0.20	0.139	I	O	|	|	|	| 0.73
41.667	0.00	0.20	0.137	I	O	|	|	|	| 0.73
41.750	0.00	0.20	0.136	I	O	|	|	|	| 0.72
41.833	0.00	0.20	0.135	I	O	|	|	|	| 0.71
41.917	0.00	0.20	0.133	I	O	|	|	|	| 0.71
42.000	0.00	0.20	0.132	I	O	|	|	|	| 0.70
42.083	0.00	0.19	0.131	I	O	|	|	|	| 0.70
42.167	0.00	0.19	0.129	I	O	|	|	|	| 0.69
42.250	0.00	0.19	0.128	I	O	|	|	|	| 0.69
42.333	0.00	0.19	0.127	I	O	|	|	|	| 0.68
42.417	0.00	0.19	0.125	I	O	|	|	|	| 0.68
42.500	0.00	0.19	0.124	I	O	|	|	|	| 0.67
42.583	0.00	0.19	0.123	I	O	|	|	|	| 0.67
42.667	0.00	0.19	0.121	I	O	|	|	|	| 0.66
42.750	0.00	0.19	0.120	I	O	|	|	|	| 0.66
42.833	0.00	0.19	0.119	I	O	|	|	|	| 0.65
42.917	0.00	0.19	0.117	I	O	|	|	|	| 0.65
43.000	0.00	0.19	0.116	I	O	|	|	|	| 0.64
43.083	0.00	0.19	0.115	I	O	|	|	|	| 0.64
43.167	0.00	0.18	0.114	I	O	|	|	|	| 0.63
43.250	0.00	0.18	0.112	I	O	|	|	|	| 0.63
43.333	0.00	0.18	0.111	I	O	|	|	|	| 0.62
43.417	0.00	0.18	0.110	I	O	|	|	|	| 0.62
43.500	0.00	0.18	0.109	I	O	|	|	|	| 0.61
43.583	0.00	0.18	0.107	I	O	|	|	|	| 0.61
43.667	0.00	0.18	0.106	I	O	|	|	|	| 0.60
43.750	0.00	0.18	0.105	I	O	|	|	|	| 0.60
43.833	0.00	0.18	0.104	I	O	|	|	|	| 0.59
43.917	0.00	0.18	0.102	I	O	|	|	|	| 0.59
44.000	0.00	0.18	0.101	I	O	|	|	|	| 0.58
44.083	0.00	0.18	0.100	I	O	|	|	|	| 0.58
44.167	0.00	0.18	0.099	I	O	|	|	|	| 0.57
44.250	0.00	0.18	0.097	I	O	|	|	|	| 0.57
44.333	0.00	0.18	0.096	I	O	|	|	|	| 0.56
44.417	0.00	0.17	0.095	I	O	|	|	|	| 0.56
44.500	0.00	0.17	0.094	I	O	|	|	|	| 0.55
44.583	0.00	0.17	0.093	I	O	|	|	|	| 0.55
44.667	0.00	0.17	0.091	I	O	|	|	|	| 0.54
44.750	0.00	0.17	0.090	I	O	|	|	|	| 0.54
44.833	0.00	0.17	0.089	I	O	|	|	|	| 0.53
44.917	0.00	0.17	0.088	I	O	|	|	|	| 0.53
45.000	0.00	0.17	0.087	I	O	|	|	|	| 0.52
45.083	0.00	0.17	0.086	I	O	|	|	|	| 0.52
45.167	0.00	0.17	0.084	I	O	|	|	|	| 0.51
45.250	0.00	0.17	0.083	I	O	|	|	|	| 0.51
45.333	0.00	0.17	0.082	I	O	|	|	|	| 0.50
45.417	0.00	0.17	0.081	I	O	|	|	|	| 0.50
45.500	0.00	0.17	0.080	I	O	|	|	|	| 0.49
45.583	0.00	0.17	0.079	I	O	|	|	|	| 0.49
45.667	0.00	0.16	0.077	I	O	|	|	|	| 0.49
45.750	0.00	0.16	0.076	I	O	|	|	|	| 0.48
45.833	0.00	0.16	0.075	I	O	|	|	|	| 0.48
45.917	0.00	0.16	0.074	I	O	|	|	|	| 0.47
46.000	0.00	0.16	0.073	I	O	|	|	|	| 0.47
46.083	0.00	0.16	0.072	I	O	|	|	|	| 0.46
46.167	0.00	0.16	0.071	I	O	|	|	|	| 0.46
46.250	0.00	0.16	0.070	I	O	|	|	|	| 0.45
46.333	0.00	0.16	0.069	I	O	|	|	|	| 0.45
46.417	0.00	0.16	0.068	I	O	|	|	|	| 0.44
46.500	0.00	0.16	0.066	I	O	|	|	|	| 0.44
46.583	0.00	0.16	0.065	I	O	|	|	|	| 0.44
46.667	0.00	0.15	0.064	I	O	|	|	|	| 0.43
46.750	0.00	0.15	0.063	I	O	|	|	|	| 0.43
46.833	0.00	0.15	0.062	I	O	|	|	|	| 0.42
46.917	0.00	0.15	0.061	I	O	|	|	|	| 0.42
47.000	0.00	0.15	0.060	I	O	|	|	|	| 0.41
47.083	0.00	0.15	0.059	I	O	|	|	|	| 0.41
47.167	0.00	0.15	0.058	I	O	|	|	|	| 0.41
47.250	0.00	0.15	0.057	I	O	|	|	|	| 0.40
47.333	0.00	0.15	0.056	I	O	|	|	|	| 0.40
47.417	0.00	0.15	0.055	I	O	|	|	|	| 0.39

47.500	0.00	0.15	0.054	I O	|	|	|	0.39
47.583	0.00	0.15	0.053	I O	|	|	|	0.38
47.667	0.00	0.15	0.052	I O	|	|	|	0.38
47.750	0.00	0.14	0.051	I O	|	|	|	0.38
47.833	0.00	0.14	0.050	I O	|	|	|	0.37
47.917	0.00	0.14	0.049	I O	|	|	|	0.37
48.000	0.00	0.14	0.048	I O	|	|	|	0.36
48.083	0.00	0.14	0.047	I O	|	|	|	0.36
48.167	0.00	0.14	0.046	I O	|	|	|	0.36
48.250	0.00	0.14	0.045	I O	|	|	|	0.35
48.333	0.00	0.14	0.044	I O	|	|	|	0.35
48.417	0.00	0.14	0.043	I O	|	|	|	0.34
48.500	0.00	0.14	0.042	I O	|	|	|	0.34
48.583	0.00	0.14	0.041	I O	|	|	|	0.34
48.667	0.00	0.14	0.040	I O	|	|	|	0.33
48.750	0.00	0.14	0.039	I O	|	|	|	0.33
48.833	0.00	0.13	0.038	I O	|	|	|	0.32
48.917	0.00	0.13	0.037	I O	|	|	|	0.32
49.000	0.00	0.13	0.037	I O	|	|	|	0.32
49.083	0.00	0.13	0.036	I O	|	|	|	0.31
49.167	0.00	0.13	0.035	I O	|	|	|	0.31
49.250	0.00	0.13	0.034	I O	|	|	|	0.30
49.333	0.00	0.13	0.033	I O	|	|	|	0.30
49.417	0.00	0.13	0.032	I O	|	|	|	0.30
49.500	0.00	0.13	0.031	I O	|	|	|	0.29
49.583	0.00	0.13	0.030	I O	|	|	|	0.29
49.667	0.00	0.13	0.029	I O	|	|	|	0.28
49.750	0.00	0.12	0.029	I O	|	|	|	0.28
49.833	0.00	0.12	0.028	I O	|	|	|	0.28
49.917	0.00	0.12	0.027	I O	|	|	|	0.27
50.000	0.00	0.12	0.026	I O	|	|	|	0.27
50.083	0.00	0.12	0.025	I O	|	|	|	0.26
50.167	0.00	0.12	0.024	I O	|	|	|	0.26
50.250	0.00	0.12	0.024	I O	|	|	|	0.26
50.333	0.00	0.12	0.023	I O	|	|	|	0.25
50.417	0.00	0.12	0.022	I O	|	|	|	0.25
50.500	0.00	0.11	0.021	I O	|	|	|	0.24
50.583	0.00	0.11	0.020	IO	|	|	|	0.23
50.667	0.00	0.11	0.020	IO	|	|	|	0.22
50.750	0.00	0.10	0.019	IO	|	|	|	0.21
50.833	0.00	0.10	0.018	IO	|	|	|	0.21
50.917	0.00	0.09	0.018	IO	|	|	|	0.20
51.000	0.00	0.09	0.017	IO	|	|	|	0.19
51.083	0.00	0.09	0.016	IO	|	|	|	0.19
51.167	0.00	0.08	0.016	IO	|	|	|	0.18
51.250	0.00	0.08	0.015	IO	|	|	|	0.17
51.333	0.00	0.08	0.015	IO	|	|	|	0.17
51.417	0.00	0.08	0.014	IO	|	|	|	0.16
51.500	0.00	0.07	0.014	IO	|	|	|	0.15
51.583	0.00	0.07	0.013	IO	|	|	|	0.15
51.667	0.00	0.07	0.013	IO	|	|	|	0.14
51.750	0.00	0.07	0.012	IO	|	|	|	0.14
51.833	0.00	0.06	0.012	IO	|	|	|	0.13
51.917	0.00	0.06	0.011	IO	|	|	|	0.13
52.000	0.00	0.06	0.011	IO	|	|	|	0.12
52.083	0.00	0.06	0.010	O	|	|	|	0.12
52.167	0.00	0.05	0.010	O	|	|	|	0.11
52.250	0.00	0.05	0.010	O	|	|	|	0.11
52.333	0.00	0.05	0.009	O	|	|	|	0.11
52.417	0.00	0.05	0.009	O	|	|	|	0.10
52.500	0.00	0.05	0.009	O	|	|	|	0.10
52.583	0.00	0.04	0.008	O	|	|	|	0.10
52.667	0.00	0.04	0.008	O	|	|	|	0.09
52.750	0.00	0.04	0.008	O	|	|	|	0.09
52.833	0.00	0.04	0.008	O	|	|	|	0.09
52.917	0.00	0.04	0.007	O	|	|	|	0.08
53.000	0.00	0.04	0.007	O	|	|	|	0.08
53.083	0.00	0.04	0.007	O	|	|	|	0.08
53.167	0.00	0.03	0.006	O	|	|	|	0.07
53.250	0.00	0.03	0.006	O	|	|	|	0.07
53.333	0.00	0.03	0.006	O	|	|	|	0.07
53.417	0.00	0.03	0.006	O	|	|	|	0.07

53.500	0.00	0.03	0.006	O	|	|	|	0.06
53.583	0.00	0.03	0.005	O	|	|	|	0.06
53.667	0.00	0.03	0.005	O	|	|	|	0.06
53.750	0.00	0.03	0.005	O	|	|	|	0.06
53.833	0.00	0.03	0.005	O	|	|	|	0.05
53.917	0.00	0.02	0.005	O	|	|	|	0.05
54.000	0.00	0.02	0.004	O	|	|	|	0.05
54.083	0.00	0.02	0.004	O	|	|	|	0.05
54.167	0.00	0.02	0.004	O	|	|	|	0.05
54.250	0.00	0.02	0.004	O	|	|	|	0.05
54.333	0.00	0.02	0.004	O	|	|	|	0.04
54.417	0.00	0.02	0.004	O	|	|	|	0.04
54.500	0.00	0.02	0.004	O	|	|	|	0.04
54.583	0.00	0.02	0.003	O	|	|	|	0.04
54.667	0.00	0.02	0.003	O	|	|	|	0.04
54.750	0.00	0.02	0.003	O	|	|	|	0.04
54.833	0.00	0.02	0.003	O	|	|	|	0.04
54.917	0.00	0.02	0.003	O	|	|	|	0.03
55.000	0.00	0.02	0.003	O	|	|	|	0.03
55.083	0.00	0.01	0.003	O	|	|	|	0.03
55.167	0.00	0.01	0.003	O	|	|	|	0.03
55.250	0.00	0.01	0.003	O	|	|	|	0.03
55.333	0.00	0.01	0.002	O	|	|	|	0.03
55.417	0.00	0.01	0.002	O	|	|	|	0.03
55.500	0.00	0.01	0.002	O	|	|	|	0.03
55.583	0.00	0.01	0.002	O	|	|	|	0.03
55.667	0.00	0.01	0.002	O	|	|	|	0.02
55.750	0.00	0.01	0.002	O	|	|	|	0.02
55.833	0.00	0.01	0.002	O	|	|	|	0.02
55.917	0.00	0.01	0.002	O	|	|	|	0.02
56.000	0.00	0.01	0.002	O	|	|	|	0.02
56.083	0.00	0.01	0.002	O	|	|	|	0.02
56.167	0.00	0.01	0.002	O	|	|	|	0.02
56.250	0.00	0.01	0.002	O	|	|	|	0.02
56.333	0.00	0.01	0.002	O	|	|	|	0.02
56.417	0.00	0.01	0.002	O	|	|	|	0.02
56.500	0.00	0.01	0.001	O	|	|	|	0.02
56.583	0.00	0.01	0.001	O	|	|	|	0.02
56.667	0.00	0.01	0.001	O	|	|	|	0.02
56.750	0.00	0.01	0.001	O	|	|	|	0.02
56.833	0.00	0.01	0.001	O	|	|	|	0.01
56.917	0.00	0.01	0.001	O	|	|	|	0.01
57.000	0.00	0.01	0.001	O	|	|	|	0.01
57.083	0.00	0.01	0.001	O	|	|	|	0.01
57.167	0.00	0.01	0.001	O	|	|	|	0.01
57.250	0.00	0.01	0.001	O	|	|	|	0.01
57.333	0.00	0.01	0.001	O	|	|	|	0.01
57.417	0.00	0.01	0.001	O	|	|	|	0.01
57.500	0.00	0.01	0.001	O	|	|	|	0.01
57.583	0.00	0.00	0.001	O	|	|	|	0.01
57.667	0.00	0.00	0.001	O	|	|	|	0.01
57.750	0.00	0.00	0.001	O	|	|	|	0.01
57.833	0.00	0.00	0.001	O	|	|	|	0.01
57.917	0.00	0.00	0.001	O	|	|	|	0.01
58.000	0.00	0.00	0.001	O	|	|	|	0.01
58.083	0.00	0.00	0.001	O	|	|	|	0.01
58.167	0.00	0.00	0.001	O	|	|	|	0.01
58.250	0.00	0.00	0.001	O	|	|	|	0.01
58.333	0.00	0.00	0.001	O	|	|	|	0.01
58.417	0.00	0.00	0.001	O	|	|	|	0.01
58.500	0.00	0.00	0.001	O	|	|	|	0.01
58.583	0.00	0.00	0.001	O	|	|	|	0.01
58.667	0.00	0.00	0.001	O	|	|	|	0.01
58.750	0.00	0.00	0.001	O	|	|	|	0.01
58.833	0.00	0.00	0.001	O	|	|	|	0.01
58.917	0.00	0.00	0.001	O	|	|	|	0.01
59.000	0.00	0.00	0.000	O	|	|	|	0.01
59.083	0.00	0.00	0.000	O	|	|	|	0.01
59.167	0.00	0.00	0.000	O	|	|	|	0.01
59.250	0.00	0.00	0.000	O	|	|	|	0.00
59.333	0.00	0.00	0.000	O	|	|	|	0.00
59.417	0.00	0.00	0.000	O	|	|	|	0.00

59.500	0.00	0.00	0.000	O	|	|	|	|	0.00
59.583	0.00	0.00	0.000	O	|	|	|	|	0.00
59.667	0.00	0.00	0.000	O	|	|	|	|	0.00
59.750	0.00	0.00	0.000	O	|	|	|	|	0.00
59.833	0.00	0.00	0.000	O	|	|	|	|	0.00
59.917	0.00	0.00	0.000	O	|	|	|	|	0.00
60.000	0.00	0.00	0.000	O	|	|	|	|	0.00
60.083	0.00	0.00	0.000	O	|	|	|	|	0.00
60.167	0.00	0.00	0.000	O	|	|	|	|	0.00
60.250	0.00	0.00	0.000	O	|	|	|	|	0.00
60.333	0.00	0.00	0.000	O	|	|	|	|	0.00
60.417	0.00	0.00	0.000	O	|	|	|	|	0.00
60.500	0.00	0.00	0.000	O	|	|	|	|	0.00
60.583	0.00	0.00	0.000	O	|	|	|	|	0.00
60.667	0.00	0.00	0.000	O	|	|	|	|	0.00
60.750	0.00	0.00	0.000	O	|	|	|	|	0.00
60.833	0.00	0.00	0.000	O	|	|	|	|	0.00
60.917	0.00	0.00	0.000	O	|	|	|	|	0.00
61.000	0.00	0.00	0.000	O	|	|	|	|	0.00
61.083	0.00	0.00	0.000	O	|	|	|	|	0.00
61.167	0.00	0.00	0.000	O	|	|	|	|	0.00
61.250	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 735
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.468 (CFS)
Total volume = 1.099 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
6-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA0565.rte
**********HYDROGRAPH DATA**********
Number of intervals = 74
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 4.691 (CFS)
Total volume = 0.592 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 74
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.2 2.35 3.52 4.69	Depth (Ft.)
0.083	0.25	0.00	0.001	OI	0.01
0.167	0.45	0.02	0.003	O I	0.04
0.250	0.51	0.03	0.006	O I	0.07
0.333	0.51	0.05	0.010	O I	0.11
0.417	0.51	0.07	0.013	O I	0.14
0.500	0.56	0.08	0.016	O I	0.18
0.583	0.59	0.10	0.019	O I	0.22
0.667	0.60	0.12	0.022	O I	0.25
0.750	0.60	0.12	0.026	O I	0.27
0.833	0.60	0.13	0.029	O I	0.28
0.917	0.60	0.13	0.032	O I	0.30
1.000	0.65	0.13	0.036	O I	0.31
1.083	0.68	0.14	0.039	O I	0.33
1.167	0.68	0.14	0.043	O I	0.34
1.250	0.68	0.14	0.047	O I	0.36
1.333	0.68	0.14	0.051	O I	0.38
1.417	0.68	0.15	0.054	O I	0.39
1.500	0.68	0.15	0.058	O I	0.41
1.583	0.68	0.15	0.062	O I	0.42
1.667	0.68	0.16	0.065	O I	0.44
1.750	0.68	0.16	0.069	O I	0.45
1.833	0.68	0.16	0.072	O I	0.47
1.917	0.68	0.16	0.076	O I	0.48
2.000	0.73	0.17	0.080	O I	0.50
2.083	0.71	0.17	0.084	O I	0.51
2.167	0.74	0.17	0.087	O I	0.53
2.250	0.76	0.17	0.091	O I	0.54
2.333	0.77	0.18	0.096	O I	0.56
2.417	0.77	0.18	0.100	O I	0.57
2.500	0.77	0.18	0.104	O I	0.59
2.583	0.77	0.18	0.108	O I	0.61
2.667	0.77	0.18	0.112	O I	0.62
2.750	0.82	0.19	0.116	O I	0.64
2.833	0.85	0.19	0.120	O I	0.66
2.917	0.85	0.19	0.125	O I	0.68
3.000	0.85	0.19	0.130	O I	0.69
3.083	0.85	0.20	0.134	O I	0.71
3.167	0.90	0.20	0.139	O I	0.73
3.250	0.93	0.20	0.144	O I	0.75
3.333	0.94	0.20	0.149	O I	0.77
3.417	0.99	0.21	0.154	O I	0.79
3.500	1.07	0.21	0.160	O I	0.81
3.583	1.16	0.21	0.166	O I	0.84
3.667	1.19	0.22	0.172	O I	0.87
3.750	1.25	0.22	0.179	O I	0.89
3.833	1.28	0.23	0.186	O I	0.92
3.917	1.33	0.23	0.194	O I	0.95
4.000	1.36	0.23	0.202	O I	0.98
4.083	1.42	0.24	0.210	O I	1.01
4.167	1.50	0.24	0.218	O I	1.05
4.250	1.58	0.25	0.227	O I	1.08
4.333	1.67	0.25	0.236	O I	1.12
4.417	1.75	0.25	0.246	O I	1.16
4.500	1.79	0.26	0.257	O I	1.20
4.583	1.84	0.26	0.268	O I	1.25
4.667	1.92	0.27	0.279	O I	1.29
4.750	2.01	0.27	0.290	O I	1.34
4.833	2.05	0.28	0.302	O I	1.39
4.917	2.10	0.28	0.315	O I	1.44
5.000	2.18	0.29	0.328	O I	1.49
5.083	2.46	0.29	0.341	O I	1.55
5.167	2.87	0.30	0.358	O I	1.62
5.250	3.21	0.31	0.377	O I	1.70
5.333	3.51	0.31	0.398	O I	1.78
5.417	3.94	0.32	0.421	O I	1.88

5.500	4.69	0.33	0.449	| O	|	|	|	I	1.99
5.583	3.04	0.34	0.473	| O	|	I	|	|	2.09
5.667	1.33	0.35	0.486	| O	I	|	|	|	2.15
5.750	0.67	0.35	0.490	| O I	|	|	|	|	2.17
5.833	0.48	0.35	0.492	| OI	|	|	|	|	2.18
5.917	0.33	0.35	0.492	| O	|	|	|	|	2.18
6.000	0.22	0.35	0.492	|IO	|	|	|	|	2.17
6.083	0.08	0.35	0.490	I O	|	|	|	|	2.17
6.167	0.01	0.35	0.488	I O	|	|	|	|	2.16
6.250	0.00	0.35	0.486	I O	|	|	|	|	2.15
6.333	0.00	0.35	0.483	I O	|	|	|	|	2.14
6.417	0.00	0.34	0.481	I O	|	|	|	|	2.13
6.500	0.00	0.34	0.479	I O	|	|	|	|	2.12
6.583	0.00	0.34	0.476	I O	|	|	|	|	2.11
6.667	0.00	0.34	0.474	I O	|	|	|	|	2.10
6.750	0.00	0.34	0.471	I O	|	|	|	|	2.09
6.833	0.00	0.34	0.469	I O	|	|	|	|	2.08
6.917	0.00	0.34	0.467	I O	|	|	|	|	2.07
7.000	0.00	0.34	0.464	I O	|	|	|	|	2.06
7.083	0.00	0.34	0.462	I O	|	|	|	|	2.05
7.167	0.00	0.34	0.460	I O	|	|	|	|	2.04
7.250	0.00	0.34	0.458	I O	|	|	|	|	2.03
7.333	0.00	0.34	0.455	I O	|	|	|	|	2.02
7.417	0.00	0.33	0.453	I O	|	|	|	|	2.01
7.500	0.00	0.33	0.451	I O	|	|	|	|	2.00
7.583	0.00	0.33	0.448	I O	|	|	|	|	1.99
7.667	0.00	0.33	0.446	I O	|	|	|	|	1.98
7.750	0.00	0.33	0.444	I O	|	|	|	|	1.97
7.833	0.00	0.33	0.441	I O	|	|	|	|	1.96
7.917	0.00	0.33	0.439	I O	|	|	|	|	1.95
8.000	0.00	0.33	0.437	I O	|	|	|	|	1.94
8.083	0.00	0.33	0.435	I O	|	|	|	|	1.93
8.167	0.00	0.33	0.432	I O	|	|	|	|	1.92
8.250	0.00	0.33	0.430	I O	|	|	|	|	1.91
8.333	0.00	0.33	0.428	I O	|	|	|	|	1.91
8.417	0.00	0.32	0.426	I O	|	|	|	|	1.90
8.500	0.00	0.32	0.423	I O	|	|	|	|	1.89
8.583	0.00	0.32	0.421	I O	|	|	|	|	1.88
8.667	0.00	0.32	0.419	I O	|	|	|	|	1.87
8.750	0.00	0.32	0.417	I O	|	|	|	|	1.86
8.833	0.00	0.32	0.415	I O	|	|	|	|	1.85
8.917	0.00	0.32	0.412	I O	|	|	|	|	1.84
9.000	0.00	0.32	0.410	I O	|	|	|	|	1.83
9.083	0.00	0.32	0.408	I O	|	|	|	|	1.82
9.167	0.00	0.32	0.406	I O	|	|	|	|	1.81
9.250	0.00	0.32	0.404	I O	|	|	|	|	1.81
9.333	0.00	0.32	0.401	I O	|	|	|	|	1.80
9.417	0.00	0.31	0.399	I O	|	|	|	|	1.79
9.500	0.00	0.31	0.397	I O	|	|	|	|	1.78
9.583	0.00	0.31	0.395	I O	|	|	|	|	1.77
9.667	0.00	0.31	0.393	I O	|	|	|	|	1.76
9.750	0.00	0.31	0.391	I O	|	|	|	|	1.75
9.833	0.00	0.31	0.388	I O	|	|	|	|	1.74
9.917	0.00	0.31	0.386	I O	|	|	|	|	1.73
10.000	0.00	0.31	0.384	I O	|	|	|	|	1.73
10.083	0.00	0.31	0.382	I O	|	|	|	|	1.72
10.167	0.00	0.31	0.380	I O	|	|	|	|	1.71
10.250	0.00	0.31	0.378	I O	|	|	|	|	1.70
10.333	0.00	0.31	0.376	I O	|	|	|	|	1.69
10.417	0.00	0.31	0.374	I O	|	|	|	|	1.68
10.500	0.00	0.30	0.371	I O	|	|	|	|	1.67
10.583	0.00	0.30	0.369	I O	|	|	|	|	1.67
10.667	0.00	0.30	0.367	I O	|	|	|	|	1.66
10.750	0.00	0.30	0.365	I O	|	|	|	|	1.65
10.833	0.00	0.30	0.363	I O	|	|	|	|	1.64
10.917	0.00	0.30	0.361	I O	|	|	|	|	1.63
11.000	0.00	0.30	0.359	I O	|	|	|	|	1.62
11.083	0.00	0.30	0.357	I O	|	|	|	|	1.61
11.167	0.00	0.30	0.355	I O	|	|	|	|	1.61
11.250	0.00	0.30	0.353	I O	|	|	|	|	1.60
11.333	0.00	0.30	0.351	I O	|	|	|	|	1.59
11.417	0.00	0.30	0.349	I O	|	|	|	|	1.58

11.500	0.00	0.30	0.347	I O				1.57
11.583	0.00	0.29	0.345	I O				1.56
11.667	0.00	0.29	0.343	I O				1.56
11.750	0.00	0.29	0.341	I O				1.55
11.833	0.00	0.29	0.339	IO				1.54
11.917	0.00	0.29	0.337	IO				1.53
12.000	0.00	0.29	0.335	IO				1.52
12.083	0.00	0.29	0.333	IO				1.51
12.167	0.00	0.29	0.331	IO				1.51
12.250	0.00	0.29	0.329	IO				1.50
12.333	0.00	0.29	0.327	IO				1.49
12.417	0.00	0.29	0.325	IO				1.48
12.500	0.00	0.29	0.323	IO				1.47
12.583	0.00	0.29	0.321	IO				1.47
12.667	0.00	0.28	0.319	IO				1.46
12.750	0.00	0.28	0.317	IO				1.45
12.833	0.00	0.28	0.315	IO				1.44
12.917	0.00	0.28	0.313	IO				1.43
13.000	0.00	0.28	0.311	IO				1.42
13.083	0.00	0.28	0.309	IO				1.42
13.167	0.00	0.28	0.307	IO				1.41
13.250	0.00	0.28	0.305	IO				1.40
13.333	0.00	0.28	0.303	IO				1.39
13.417	0.00	0.28	0.301	IO				1.38
13.500	0.00	0.28	0.299	IO				1.38
13.583	0.00	0.28	0.297	IO				1.37
13.667	0.00	0.28	0.296	IO				1.36
13.750	0.00	0.28	0.294	IO				1.35
13.833	0.00	0.27	0.292	IO				1.34
13.917	0.00	0.27	0.290	IO				1.34
14.000	0.00	0.27	0.288	IO				1.33
14.083	0.00	0.27	0.286	IO				1.32
14.167	0.00	0.27	0.284	IO				1.31
14.250	0.00	0.27	0.282	IO				1.31
14.333	0.00	0.27	0.280	IO				1.30
14.417	0.00	0.27	0.279	IO				1.29
14.500	0.00	0.27	0.277	IO				1.28
14.583	0.00	0.27	0.275	IO				1.28
14.667	0.00	0.27	0.273	IO				1.27
14.750	0.00	0.27	0.271	IO				1.26
14.833	0.00	0.26	0.269	IO				1.26
14.917	0.00	0.26	0.268	IO				1.25
15.000	0.00	0.26	0.266	IO				1.24
15.083	0.00	0.26	0.264	IO				1.23
15.167	0.00	0.26	0.262	IO				1.23
15.250	0.00	0.26	0.260	IO				1.22
15.333	0.00	0.26	0.259	IO				1.21
15.417	0.00	0.26	0.257	IO				1.20
15.500	0.00	0.26	0.255	IO				1.20
15.583	0.00	0.26	0.253	IO				1.19
15.667	0.00	0.26	0.252	IO				1.18
15.750	0.00	0.26	0.250	IO				1.18
15.833	0.00	0.25	0.248	IO				1.17
15.917	0.00	0.25	0.246	IO				1.16
16.000	0.00	0.25	0.245	IO				1.15
16.083	0.00	0.25	0.243	IO				1.15
16.167	0.00	0.25	0.241	IO				1.14
16.250	0.00	0.25	0.239	IO				1.13
16.333	0.00	0.25	0.238	IO				1.13
16.417	0.00	0.25	0.236	IO				1.12
16.500	0.00	0.25	0.234	IO				1.11
16.583	0.00	0.25	0.232	IO				1.11
16.667	0.00	0.25	0.231	IO				1.10
16.750	0.00	0.25	0.229	IO				1.09
16.833	0.00	0.25	0.227	IO				1.09
16.917	0.00	0.24	0.226	IO				1.08
17.000	0.00	0.24	0.224	IO				1.07
17.083	0.00	0.24	0.222	IO				1.07
17.167	0.00	0.24	0.221	IO				1.06
17.250	0.00	0.24	0.219	IO				1.05
17.333	0.00	0.24	0.217	IO				1.05
17.417	0.00	0.24	0.216	IO				1.04

17.500	0.00	0.24	0.214	IO				1.03
17.583	0.00	0.24	0.212	IO				1.03
17.667	0.00	0.24	0.211	IO				1.02
17.750	0.00	0.24	0.209	IO				1.01
17.833	0.00	0.24	0.207	IO				1.01
17.917	0.00	0.24	0.206	IO				1.00
18.000	0.00	0.23	0.204	IO				0.99
18.083	0.00	0.23	0.203	IO				0.99
18.167	0.00	0.23	0.201	IO				0.98
18.250	0.00	0.23	0.199	IO				0.97
18.333	0.00	0.23	0.198	IO				0.97
18.417	0.00	0.23	0.196	IO				0.96
18.500	0.00	0.23	0.195	IO				0.95
18.583	0.00	0.23	0.193	IO				0.95
18.667	0.00	0.23	0.191	IO				0.94
18.750	0.00	0.23	0.190	IO				0.94
18.833	0.00	0.23	0.188	IO				0.93
18.917	0.00	0.23	0.187	IO				0.92
19.000	0.00	0.22	0.185	IO				0.92
19.083	0.00	0.22	0.184	IO				0.91
19.167	0.00	0.22	0.182	IO				0.90
19.250	0.00	0.22	0.181	IO				0.90
19.333	0.00	0.22	0.179	IO				0.89
19.417	0.00	0.22	0.178	IO				0.89
19.500	0.00	0.22	0.176	IO				0.88
19.583	0.00	0.22	0.174	IO				0.87
19.667	0.00	0.22	0.173	IO				0.87
19.750	0.00	0.22	0.171	IO				0.86
19.833	0.00	0.22	0.170	IO				0.86
19.917	0.00	0.22	0.169	IO				0.85
20.000	0.00	0.21	0.167	IO				0.84
20.083	0.00	0.21	0.166	IO				0.84
20.167	0.00	0.21	0.164	IO				0.83
20.250	0.00	0.21	0.163	IO				0.83
20.333	0.00	0.21	0.161	IO				0.82
20.417	0.00	0.21	0.160	IO				0.81
20.500	0.00	0.21	0.158	IO				0.81
20.583	0.00	0.21	0.157	IO				0.80
20.667	0.00	0.21	0.155	IO				0.80
20.750	0.00	0.21	0.154	IO				0.79
20.833	0.00	0.21	0.153	IO				0.79
20.917	0.00	0.21	0.151	IO				0.78
21.000	0.00	0.20	0.150	IO				0.77
21.083	0.00	0.20	0.148	IO				0.77
21.167	0.00	0.20	0.147	IO				0.76
21.250	0.00	0.20	0.145	IO				0.76
21.333	0.00	0.20	0.144	IO				0.75
21.417	0.00	0.20	0.143	IO				0.75
21.500	0.00	0.20	0.141	IO				0.74
21.583	0.00	0.20	0.140	IO				0.74
21.667	0.00	0.20	0.139	IO				0.73
21.750	0.00	0.20	0.137	IO				0.72
21.833	0.00	0.20	0.136	IO				0.72
21.917	0.00	0.20	0.135	IO				0.71
22.000	0.00	0.20	0.133	IO				0.71
22.083	0.00	0.20	0.132	IO				0.70
22.167	0.00	0.19	0.130	IO				0.70
22.250	0.00	0.19	0.129	IO				0.69
22.333	0.00	0.19	0.128	IO				0.69
22.417	0.00	0.19	0.126	IO				0.68
22.500	0.00	0.19	0.125	IO				0.68
22.583	0.00	0.19	0.124	IO				0.67
22.667	0.00	0.19	0.123	IO				0.67
22.750	0.00	0.19	0.121	IO				0.66
22.833	0.00	0.19	0.120	IO				0.66
22.917	0.00	0.19	0.119	IO				0.65
23.000	0.00	0.19	0.117	IO				0.65
23.083	0.00	0.19	0.116	IO				0.64
23.167	0.00	0.19	0.115	IO				0.64
23.250	0.00	0.18	0.113	IO				0.63
23.333	0.00	0.18	0.112	IO				0.62
23.417	0.00	0.18	0.111	IO				0.62

23.500	0.00	0.18	0.110	IO				0.61
23.583	0.00	0.18	0.108	IO				0.61
23.667	0.00	0.18	0.107	IO				0.60
23.750	0.00	0.18	0.106	IO				0.60
23.833	0.00	0.18	0.105	IO				0.59
23.917	0.00	0.18	0.103	IO				0.59
24.000	0.00	0.18	0.102	IO				0.58
24.083	0.00	0.18	0.101	IO				0.58
24.167	0.00	0.18	0.100	IO				0.58
24.250	0.00	0.18	0.099	IO				0.57
24.333	0.00	0.18	0.097	IO				0.57
24.417	0.00	0.18	0.096	IO				0.56
24.500	0.00	0.17	0.095	IO				0.56
24.583	0.00	0.17	0.094	IO				0.55
24.667	0.00	0.17	0.093	IO				0.55
24.750	0.00	0.17	0.091	IO				0.54
24.833	0.00	0.17	0.090	IO				0.54
24.917	0.00	0.17	0.089	IO				0.53
25.000	0.00	0.17	0.088	IO				0.53
25.083	0.00	0.17	0.087	IO				0.52
25.167	0.00	0.17	0.085	IO				0.52
25.250	0.00	0.17	0.084	IO				0.51
25.333	0.00	0.17	0.083	IO				0.51
25.417	0.00	0.17	0.082	IO				0.50
25.500	0.00	0.17	0.081	IO				0.50
25.583	0.00	0.17	0.080	IO				0.49
25.667	0.00	0.17	0.079	IO				0.49
25.750	0.00	0.16	0.077	IO				0.49
25.833	0.00	0.16	0.076	IO				0.48
25.917	0.00	0.16	0.075	IO				0.48
26.000	0.00	0.16	0.074	IO				0.47
26.083	0.00	0.16	0.073	IO				0.47
26.167	0.00	0.16	0.072	IO				0.46
26.250	0.00	0.16	0.071	IO				0.46
26.333	0.00	0.16	0.070	IO				0.45
26.417	0.00	0.16	0.069	IO				0.45
26.500	0.00	0.16	0.067	IO				0.44
26.583	0.00	0.16	0.066	IO				0.44
26.667	0.00	0.16	0.065	IO				0.44
26.750	0.00	0.15	0.064	IO				0.43
26.833	0.00	0.15	0.063	IO				0.43
26.917	0.00	0.15	0.062	IO				0.42
27.000	0.00	0.15	0.061	IO				0.42
27.083	0.00	0.15	0.060	IO				0.41
27.167	0.00	0.15	0.059	IO				0.41
27.250	0.00	0.15	0.058	IO				0.41
27.333	0.00	0.15	0.057	IO				0.40
27.417	0.00	0.15	0.056	IO				0.40
27.500	0.00	0.15	0.055	IO				0.39
27.583	0.00	0.15	0.054	IO				0.39
27.667	0.00	0.15	0.053	O				0.38
27.750	0.00	0.15	0.052	O				0.38
27.833	0.00	0.14	0.051	O				0.38
27.917	0.00	0.14	0.050	O				0.37
28.000	0.00	0.14	0.049	O				0.37
28.083	0.00	0.14	0.048	O				0.36
28.167	0.00	0.14	0.047	O				0.36
28.250	0.00	0.14	0.046	O				0.36
28.333	0.00	0.14	0.045	O				0.35
28.417	0.00	0.14	0.044	O				0.35
28.500	0.00	0.14	0.043	O				0.34
28.583	0.00	0.14	0.042	O				0.34
28.667	0.00	0.14	0.041	O				0.34
28.750	0.00	0.14	0.040	O				0.33
28.833	0.00	0.14	0.039	O				0.33
28.917	0.00	0.13	0.038	O				0.32
29.000	0.00	0.13	0.037	O				0.32
29.083	0.00	0.13	0.036	O				0.32
29.167	0.00	0.13	0.036	O				0.31
29.250	0.00	0.13	0.035	O				0.31
29.333	0.00	0.13	0.034	O				0.30
29.417	0.00	0.13	0.033	O				0.30

29.500	0.00	0.13	0.032	O	|	|	|	0.30
29.583	0.00	0.13	0.031	O	|	|	|	0.29
29.667	0.00	0.13	0.030	O	|	|	|	0.29
29.750	0.00	0.13	0.029	O	|	|	|	0.28
29.833	0.00	0.12	0.029	O	|	|	|	0.28
29.917	0.00	0.12	0.028	O	|	|	|	0.28
30.000	0.00	0.12	0.027	O	|	|	|	0.27
30.083	0.00	0.12	0.026	O	|	|	|	0.27
30.167	0.00	0.12	0.025	O	|	|	|	0.26
30.250	0.00	0.12	0.024	O	|	|	|	0.26
30.333	0.00	0.12	0.023	O	|	|	|	0.26
30.417	0.00	0.12	0.023	O	|	|	|	0.25
30.500	0.00	0.12	0.022	O	|	|	|	0.25
30.583	0.00	0.11	0.021	O	|	|	|	0.24
30.667	0.00	0.11	0.020	O	|	|	|	0.23
30.750	0.00	0.10	0.020	O	|	|	|	0.22
30.833	0.00	0.10	0.019	O	|	|	|	0.21
30.917	0.00	0.10	0.018	O	|	|	|	0.21
31.000	0.00	0.09	0.018	O	|	|	|	0.20
31.083	0.00	0.09	0.017	O	|	|	|	0.19
31.167	0.00	0.09	0.016	O	|	|	|	0.18
31.250	0.00	0.08	0.016	O	|	|	|	0.18
31.333	0.00	0.08	0.015	O	|	|	|	0.17
31.417	0.00	0.08	0.015	O	|	|	|	0.17
31.500	0.00	0.08	0.014	O	|	|	|	0.16
31.583	0.00	0.07	0.014	O	|	|	|	0.15
31.667	0.00	0.07	0.013	O	|	|	|	0.15
31.750	0.00	0.07	0.013	O	|	|	|	0.14
31.833	0.00	0.06	0.012	O	|	|	|	0.14
31.917	0.00	0.06	0.012	O	|	|	|	0.13
32.000	0.00	0.06	0.011	O	|	|	|	0.13
32.083	0.00	0.06	0.011	O	|	|	|	0.12
32.167	0.00	0.06	0.010	O	|	|	|	0.12
32.250	0.00	0.05	0.010	O	|	|	|	0.11
32.333	0.00	0.05	0.010	O	|	|	|	0.11
32.417	0.00	0.05	0.009	O	|	|	|	0.11
32.500	0.00	0.05	0.009	O	|	|	|	0.10
32.583	0.00	0.05	0.009	O	|	|	|	0.10
32.667	0.00	0.04	0.008	O	|	|	|	0.10
32.750	0.00	0.04	0.008	O	|	|	|	0.09
32.833	0.00	0.04	0.008	O	|	|	|	0.09
32.917	0.00	0.04	0.007	O	|	|	|	0.09
33.000	0.00	0.04	0.007	O	|	|	|	0.08
33.083	0.00	0.04	0.007	O	|	|	|	0.08
33.167	0.00	0.04	0.007	O	|	|	|	0.08
33.250	0.00	0.03	0.006	O	|	|	|	0.07
33.333	0.00	0.03	0.006	O	|	|	|	0.07
33.417	0.00	0.03	0.006	O	|	|	|	0.07
33.500	0.00	0.03	0.006	O	|	|	|	0.07
33.583	0.00	0.03	0.006	O	|	|	|	0.06
33.667	0.00	0.03	0.005	O	|	|	|	0.06
33.750	0.00	0.03	0.005	O	|	|	|	0.06
33.833	0.00	0.03	0.005	O	|	|	|	0.06
33.917	0.00	0.03	0.005	O	|	|	|	0.05
34.000	0.00	0.02	0.005	O	|	|	|	0.05
34.083	0.00	0.02	0.004	O	|	|	|	0.05
34.167	0.00	0.02	0.004	O	|	|	|	0.05
34.250	0.00	0.02	0.004	O	|	|	|	0.05
34.333	0.00	0.02	0.004	O	|	|	|	0.05
34.417	0.00	0.02	0.004	O	|	|	|	0.04
34.500	0.00	0.02	0.004	O	|	|	|	0.04
34.583	0.00	0.02	0.004	O	|	|	|	0.04
34.667	0.00	0.02	0.003	O	|	|	|	0.04
34.750	0.00	0.02	0.003	O	|	|	|	0.04
34.833	0.00	0.02	0.003	O	|	|	|	0.04
34.917	0.00	0.02	0.003	O	|	|	|	0.04
35.000	0.00	0.02	0.003	O	|	|	|	0.03
35.083	0.00	0.02	0.003	O	|	|	|	0.03
35.167	0.00	0.01	0.003	O	|	|	|	0.03
35.250	0.00	0.01	0.003	O	|	|	|	0.03
35.333	0.00	0.01	0.003	O	|	|	|	0.03
35.417	0.00	0.01	0.002	O	|	|	|	0.03

35.500	0.00	0.01	0.002	O	|	|	|	| 0.03
35.583	0.00	0.01	0.002	O	|	|	|	| 0.03
35.667	0.00	0.01	0.002	O	|	|	|	| 0.03
35.750	0.00	0.01	0.002	O	|	|	|	| 0.02
35.833	0.00	0.01	0.002	O	|	|	|	| 0.02
35.917	0.00	0.01	0.002	O	|	|	|	| 0.02
36.000	0.00	0.01	0.002	O	|	|	|	| 0.02
36.083	0.00	0.01	0.002	O	|	|	|	| 0.02
36.167	0.00	0.01	0.002	O	|	|	|	| 0.02
36.250	0.00	0.01	0.002	O	|	|	|	| 0.02
36.333	0.00	0.01	0.002	O	|	|	|	| 0.02
36.417	0.00	0.01	0.002	O	|	|	|	| 0.02
36.500	0.00	0.01	0.002	O	|	|	|	| 0.02
36.583	0.00	0.01	0.001	O	|	|	|	| 0.02
36.667	0.00	0.01	0.001	O	|	|	|	| 0.02
36.750	0.00	0.01	0.001	O	|	|	|	| 0.02
36.833	0.00	0.01	0.001	O	|	|	|	| 0.01
36.917	0.00	0.01	0.001	O	|	|	|	| 0.01
37.000	0.00	0.01	0.001	O	|	|	|	| 0.01
37.083	0.00	0.01	0.001	O	|	|	|	| 0.01
37.167	0.00	0.01	0.001	O	|	|	|	| 0.01
37.250	0.00	0.01	0.001	O	|	|	|	| 0.01
37.333	0.00	0.01	0.001	O	|	|	|	| 0.01
37.417	0.00	0.01	0.001	O	|	|	|	| 0.01
37.500	0.00	0.01	0.001	O	|	|	|	| 0.01
37.583	0.00	0.01	0.001	O	|	|	|	| 0.01
37.667	0.00	0.00	0.001	O	|	|	|	| 0.01
37.750	0.00	0.00	0.001	O	|	|	|	| 0.01
37.833	0.00	0.00	0.001	O	|	|	|	| 0.01
37.917	0.00	0.00	0.001	O	|	|	|	| 0.01
38.000	0.00	0.00	0.001	O	|	|	|	| 0.01
38.083	0.00	0.00	0.001	O	|	|	|	| 0.01
38.167	0.00	0.00	0.001	O	|	|	|	| 0.01
38.250	0.00	0.00	0.001	O	|	|	|	| 0.01
38.333	0.00	0.00	0.001	O	|	|	|	| 0.01
38.417	0.00	0.00	0.001	O	|	|	|	| 0.01
38.500	0.00	0.00	0.001	O	|	|	|	| 0.01
38.583	0.00	0.00	0.001	O	|	|	|	| 0.01
38.667	0.00	0.00	0.001	O	|	|	|	| 0.01
38.750	0.00	0.00	0.001	O	|	|	|	| 0.01
38.833	0.00	0.00	0.001	O	|	|	|	| 0.01
38.917	0.00	0.00	0.001	O	|	|	|	| 0.01
39.000	0.00	0.00	0.001	O	|	|	|	| 0.01
39.083	0.00	0.00	0.000	O	|	|	|	| 0.01
39.167	0.00	0.00	0.000	O	|	|	|	| 0.01
39.250	0.00	0.00	0.000	O	|	|	|	| 0.01
39.333	0.00	0.00	0.000	O	|	|	|	| 0.00
39.417	0.00	0.00	0.000	O	|	|	|	| 0.00
39.500	0.00	0.00	0.000	O	|	|	|	| 0.00
39.583	0.00	0.00	0.000	O	|	|	|	| 0.00
39.667	0.00	0.00	0.000	O	|	|	|	| 0.00
39.750	0.00	0.00	0.000	O	|	|	|	| 0.00
39.833	0.00	0.00	0.000	O	|	|	|	| 0.00
39.917	0.00	0.00	0.000	O	|	|	|	| 0.00
40.000	0.00	0.00	0.000	O	|	|	|	| 0.00
40.083	0.00	0.00	0.000	O	|	|	|	| 0.00
40.167	0.00	0.00	0.000	O	|	|	|	| 0.00
40.250	0.00	0.00	0.000	O	|	|	|	| 0.00
40.333	0.00	0.00	0.000	O	|	|	|	| 0.00
40.417	0.00	0.00	0.000	O	|	|	|	| 0.00
40.500	0.00	0.00	0.000	O	|	|	|	| 0.00
40.583	0.00	0.00	0.000	O	|	|	|	| 0.00
40.667	0.00	0.00	0.000	O	|	|	|	| 0.00
40.750	0.00	0.00	0.000	O	|	|	|	| 0.00
40.833	0.00	0.00	0.000	O	|	|	|	| 0.00
40.917	0.00	0.00	0.000	O	|	|	|	| 0.00
41.000	0.00	0.00	0.000	O	|	|	|	| 0.00
41.083	0.00	0.00	0.000	O	|	|	|	| 0.00
41.167	0.00	0.00	0.000	O	|	|	|	| 0.00
41.250	0.00	0.00	0.000	O	|	|	|	| 0.00

**********HYDROGRAPH DATA**********

```
                Number of intervals =   495
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =        0.348 (CFS)
                Total volume =       0.592 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
3-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA0535.rte
**********HYDROGRAPH DATA**********
Number of intervals = 38
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 5.488 (CFS)
Total volume = 0.458 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 38
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.4 2.74 4.12 5.49	Depth (Ft.)
0.083	0.49	0.01	0.002	O I	0.02
0.167	0.80	0.03	0.006	O I	0.07
0.250	0.77	0.06	0.011	O I	0.13
0.333	0.88	0.09	0.016	O I	0.18
0.417	0.96	0.12	0.022	O I	0.25
0.500	1.09	0.12	0.028	O I	0.28
0.583	1.05	0.13	0.035	O I	0.31
0.667	1.10	0.14	0.041	O I	0.34
0.750	1.16	0.14	0.048	O I	0.36
0.833	1.06	0.15	0.055	O I	0.39
0.917	1.03	0.15	0.061	O I	0.42
1.000	1.12	0.16	0.067	O I	0.44
1.083	1.32	0.16	0.074	O I	0.47
1.167	1.42	0.17	0.083	O I	0.51
1.250	1.44	0.17	0.091	O I	0.54
1.333	1.36	0.18	0.100	O I	0.58
1.417	1.54	0.18	0.109	O I	0.61
1.500	1.71	0.19	0.119	O I	0.65
1.583	1.65	0.19	0.129	O I	0.69
1.667	1.69	0.20	0.139	O I	0.73
1.750	1.98	0.21	0.150	O I	0.78
1.833	2.06	0.21	0.163	O I	0.83
1.917	1.96	0.22	0.175	O I	0.88
2.000	1.94	0.23	0.187	O I	0.92
2.083	1.99	0.23	0.199	O I	0.97
2.167	2.44	0.24	0.212	O I	1.03
2.250	3.00	0.25	0.230	O I	1.09
2.333	2.67	0.25	0.247	O I	1.17
2.417	3.74	0.26	0.268	O I	1.25
2.500	4.79	0.28	0.295	O I	1.36
2.583	5.49	0.29	0.329	O I	1.50
2.667	4.71	0.30	0.362	O I	1.63
2.750	2.54	0.31	0.385	O I	1.73
2.833	1.38	0.31	0.396	O I	1.77
2.917	1.18	0.32	0.403	O I	1.80
3.000	0.72	0.32	0.407	O I	1.82
3.083	0.21	0.32	0.408	O	1.82
3.167	0.02	0.32	0.407	IO	1.82
3.250	0.00	0.32	0.404	IO	1.81
3.333	0.00	0.32	0.402	IO	1.80
3.417	0.00	0.32	0.400	IO	1.79
3.500	0.00	0.31	0.398	IO	1.78
3.583	0.00	0.31	0.396	IO	1.77
3.667	0.00	0.31	0.394	IO	1.76
3.750	0.00	0.31	0.391	IO	1.76
3.833	0.00	0.31	0.389	IO	1.75
3.917	0.00	0.31	0.387	IO	1.74
4.000	0.00	0.31	0.385	IO	1.73
4.083	0.00	0.31	0.383	IO	1.72
4.167	0.00	0.31	0.381	IO	1.71
4.250	0.00	0.31	0.379	IO	1.70
4.333	0.00	0.31	0.377	IO	1.69
4.417	0.00	0.31	0.374	IO	1.69
4.500	0.00	0.30	0.372	IO	1.68
4.583	0.00	0.30	0.370	IO	1.67
4.667	0.00	0.30	0.368	IO	1.66
4.750	0.00	0.30	0.366	IO	1.65
4.833	0.00	0.30	0.364	IO	1.64
4.917	0.00	0.30	0.362	IO	1.63
5.000	0.00	0.30	0.360	IO	1.63
5.083	0.00	0.30	0.358	IO	1.62
5.167	0.00	0.30	0.356	IO	1.61
5.250	0.00	0.30	0.354	IO	1.60
5.333	0.00	0.30	0.352	IO	1.59
5.417	0.00	0.30	0.350	IO	1.58

5.500	0.00	0.30	0.348	IO				1.58
5.583	0.00	0.30	0.345	IO				1.57
5.667	0.00	0.29	0.343	IO				1.56
5.750	0.00	0.29	0.341	IO				1.55
5.833	0.00	0.29	0.339	IO				1.54
5.917	0.00	0.29	0.337	IO				1.53
6.000	0.00	0.29	0.335	IO				1.53
6.083	0.00	0.29	0.333	IO				1.52
6.167	0.00	0.29	0.331	IO				1.51
6.250	0.00	0.29	0.329	IO				1.50
6.333	0.00	0.29	0.327	IO				1.49
6.417	0.00	0.29	0.325	IO				1.49
6.500	0.00	0.29	0.323	IO				1.48
6.583	0.00	0.29	0.321	IO				1.47
6.667	0.00	0.29	0.319	IO				1.46
6.750	0.00	0.28	0.318	IO				1.45
6.833	0.00	0.28	0.316	IO				1.44
6.917	0.00	0.28	0.314	IO				1.44
7.000	0.00	0.28	0.312	IO				1.43
7.083	0.00	0.28	0.310	IO				1.42
7.167	0.00	0.28	0.308	IO				1.41
7.250	0.00	0.28	0.306	IO				1.40
7.333	0.00	0.28	0.304	IO				1.40
7.417	0.00	0.28	0.302	IO				1.39
7.500	0.00	0.28	0.300	IO				1.38
7.583	0.00	0.28	0.298	IO				1.37
7.667	0.00	0.28	0.296	IO				1.36
7.750	0.00	0.28	0.294	IO				1.36
7.833	0.00	0.27	0.292	IO				1.35
7.917	0.00	0.27	0.291	IO				1.34
8.000	0.00	0.27	0.289	IO				1.33
8.083	0.00	0.27	0.287	IO				1.33
8.167	0.00	0.27	0.285	IO				1.32
8.250	0.00	0.27	0.283	IO				1.31
8.333	0.00	0.27	0.281	IO				1.30
8.417	0.00	0.27	0.279	IO				1.30
8.500	0.00	0.27	0.278	IO				1.29
8.583	0.00	0.27	0.276	IO				1.28
8.667	0.00	0.27	0.274	IO				1.27
8.750	0.00	0.27	0.272	IO				1.27
8.833	0.00	0.26	0.270	IO				1.26
8.917	0.00	0.26	0.268	IO				1.25
9.000	0.00	0.26	0.267	IO				1.24
9.083	0.00	0.26	0.265	IO				1.24
9.167	0.00	0.26	0.263	IO				1.23
9.250	0.00	0.26	0.261	IO				1.22
9.333	0.00	0.26	0.259	IO				1.21
9.417	0.00	0.26	0.258	IO				1.21
9.500	0.00	0.26	0.256	IO				1.20
9.583	0.00	0.26	0.254	IO				1.19
9.667	0.00	0.26	0.252	IO				1.19
9.750	0.00	0.26	0.250	IO				1.18
9.833	0.00	0.26	0.249	IO				1.17
9.917	0.00	0.25	0.247	IO				1.16
10.000	0.00	0.25	0.245	IO				1.16
10.083	0.00	0.25	0.243	IO				1.15
10.167	0.00	0.25	0.242	IO				1.14
10.250	0.00	0.25	0.240	IO				1.14
10.333	0.00	0.25	0.238	IO				1.13
10.417	0.00	0.25	0.237	IO				1.12
10.500	0.00	0.25	0.235	IO				1.12
10.583	0.00	0.25	0.233	IO				1.11
10.667	0.00	0.25	0.231	IO				1.10
10.750	0.00	0.25	0.230	IO				1.10
10.833	0.00	0.25	0.228	IO				1.09
10.917	0.00	0.25	0.226	IO				1.08
11.000	0.00	0.24	0.225	IO				1.08
11.083	0.00	0.24	0.223	IO				1.07
11.167	0.00	0.24	0.221	IO				1.06
11.250	0.00	0.24	0.220	IO				1.05
11.333	0.00	0.24	0.218	IO				1.05
11.417	0.00	0.24	0.216	IO				1.04

11.500	0.00	0.24	0.215	IO				1.03
11.583	0.00	0.24	0.213	IO				1.03
11.667	0.00	0.24	0.211	IO				1.02
11.750	0.00	0.24	0.210	IO				1.01
11.833	0.00	0.24	0.208	IO				1.01
11.917	0.00	0.24	0.206	IO				1.00
12.000	0.00	0.24	0.205	IO				1.00
12.083	0.00	0.23	0.203	IO				0.99
12.167	0.00	0.23	0.202	IO				0.98
12.250	0.00	0.23	0.200	IO				0.98
12.333	0.00	0.23	0.198	IO				0.97
12.417	0.00	0.23	0.197	IO				0.96
12.500	0.00	0.23	0.195	IO				0.96
12.583	0.00	0.23	0.194	IO				0.95
12.667	0.00	0.23	0.192	IO				0.94
12.750	0.00	0.23	0.190	IO				0.94
12.833	0.00	0.23	0.189	IO				0.93
12.917	0.00	0.23	0.187	IO				0.93
13.000	0.00	0.22	0.186	IO				0.92
13.083	0.00	0.22	0.184	IO				0.91
13.167	0.00	0.22	0.183	IO				0.91
13.250	0.00	0.22	0.181	IO				0.90
13.333	0.00	0.22	0.180	IO				0.89
13.417	0.00	0.22	0.178	IO				0.89
13.500	0.00	0.22	0.177	IO				0.88
13.583	0.00	0.22	0.175	IO				0.88
13.667	0.00	0.22	0.174	IO				0.87
13.750	0.00	0.22	0.172	IO				0.86
13.833	0.00	0.22	0.171	IO				0.86
13.917	0.00	0.22	0.169	IO				0.85
14.000	0.00	0.21	0.168	IO				0.85
14.083	0.00	0.21	0.166	IO				0.84
14.167	0.00	0.21	0.165	IO				0.83
14.250	0.00	0.21	0.163	IO				0.83
14.333	0.00	0.21	0.162	IO				0.82
14.417	0.00	0.21	0.160	IO				0.82
14.500	0.00	0.21	0.159	IO				0.81
14.583	0.00	0.21	0.157	IO				0.81
14.667	0.00	0.21	0.156	IO				0.80
14.750	0.00	0.21	0.155	IO				0.79
14.833	0.00	0.21	0.153	IO				0.79
14.917	0.00	0.21	0.152	IO				0.78
15.000	0.00	0.21	0.150	IO				0.78
15.083	0.00	0.20	0.149	IO				0.77
15.167	0.00	0.20	0.147	IO				0.77
15.250	0.00	0.20	0.146	IO				0.76
15.333	0.00	0.20	0.145	IO				0.75
15.417	0.00	0.20	0.143	IO				0.75
15.500	0.00	0.20	0.142	IO				0.74
15.583	0.00	0.20	0.141	IO				0.74
15.667	0.00	0.20	0.139	IO				0.73
15.750	0.00	0.20	0.138	IO				0.73
15.833	0.00	0.20	0.136	IO				0.72
15.917	0.00	0.20	0.135	IO				0.72
16.000	0.00	0.20	0.134	IO				0.71
16.083	0.00	0.20	0.132	IO				0.71
16.167	0.00	0.19	0.131	IO				0.70
16.250	0.00	0.19	0.130	IO				0.69
16.333	0.00	0.19	0.128	IO				0.69
16.417	0.00	0.19	0.127	IO				0.68
16.500	0.00	0.19	0.126	IO				0.68
16.583	0.00	0.19	0.124	IO				0.67
16.667	0.00	0.19	0.123	IO				0.67
16.750	0.00	0.19	0.122	IO				0.66
16.833	0.00	0.19	0.120	IO				0.66
16.917	0.00	0.19	0.119	IO				0.65
17.000	0.00	0.19	0.118	IO				0.65
17.083	0.00	0.19	0.117	IO				0.64
17.167	0.00	0.19	0.115	IO				0.64
17.250	0.00	0.19	0.114	IO				0.63
17.333	0.00	0.18	0.113	IO				0.63
17.417	0.00	0.18	0.111	IO				0.62

17.500	0.00	0.18	0.110	IO				0.62
17.583	0.00	0.18	0.109	IO				0.61
17.667	0.00	0.18	0.108	IO				0.61
17.750	0.00	0.18	0.106	IO				0.60
17.833	0.00	0.18	0.105	IO				0.60
17.917	0.00	0.18	0.104	IO				0.59
18.000	0.00	0.18	0.103	IO				0.59
18.083	0.00	0.18	0.101	IO				0.58
18.167	0.00	0.18	0.100	IO				0.58
18.250	0.00	0.18	0.099	IO				0.57
18.333	0.00	0.18	0.098	IO				0.57
18.417	0.00	0.18	0.097	IO				0.56
18.500	0.00	0.17	0.095	IO				0.56
18.583	0.00	0.17	0.094	IO				0.55
18.667	0.00	0.17	0.093	IO				0.55
18.750	0.00	0.17	0.092	IO				0.54
18.833	0.00	0.17	0.091	IO				0.54
18.917	0.00	0.17	0.089	IO				0.53
19.000	0.00	0.17	0.088	O				0.53
19.083	0.00	0.17	0.087	O				0.52
19.167	0.00	0.17	0.086	O				0.52
19.250	0.00	0.17	0.085	O				0.52
19.333	0.00	0.17	0.084	O				0.51
19.417	0.00	0.17	0.082	O				0.51
19.500	0.00	0.17	0.081	O				0.50
19.583	0.00	0.17	0.080	O				0.50
19.667	0.00	0.17	0.079	O				0.49
19.750	0.00	0.16	0.078	O				0.49
19.833	0.00	0.16	0.077	O				0.48
19.917	0.00	0.16	0.076	O				0.48
20.000	0.00	0.16	0.074	O				0.47
20.083	0.00	0.16	0.073	O				0.47
20.167	0.00	0.16	0.072	O				0.46
20.250	0.00	0.16	0.071	O				0.46
20.333	0.00	0.16	0.070	O				0.46
20.417	0.00	0.16	0.069	O				0.45
20.500	0.00	0.16	0.068	O				0.45
20.583	0.00	0.16	0.067	O				0.44
20.667	0.00	0.16	0.066	O				0.44
20.750	0.00	0.15	0.065	O				0.43
20.833	0.00	0.15	0.064	O				0.43
20.917	0.00	0.15	0.063	O				0.42
21.000	0.00	0.15	0.061	O				0.42
21.083	0.00	0.15	0.060	O				0.42
21.167	0.00	0.15	0.059	O				0.41
21.250	0.00	0.15	0.058	O				0.41
21.333	0.00	0.15	0.057	O				0.40
21.417	0.00	0.15	0.056	O				0.40
21.500	0.00	0.15	0.055	O				0.39
21.583	0.00	0.15	0.054	O				0.39
21.667	0.00	0.15	0.053	O				0.39
21.750	0.00	0.15	0.052	O				0.38
21.833	0.00	0.14	0.051	O				0.38
21.917	0.00	0.14	0.050	O				0.37
22.000	0.00	0.14	0.049	O				0.37
22.083	0.00	0.14	0.048	O				0.37
22.167	0.00	0.14	0.047	O				0.36
22.250	0.00	0.14	0.046	O				0.36
22.333	0.00	0.14	0.045	O				0.35
22.417	0.00	0.14	0.044	O				0.35
22.500	0.00	0.14	0.043	O				0.35
22.583	0.00	0.14	0.042	O				0.34
22.667	0.00	0.14	0.042	O				0.34
22.750	0.00	0.14	0.041	O				0.33
22.833	0.00	0.14	0.040	O				0.33
22.917	0.00	0.13	0.039	O				0.33
23.000	0.00	0.13	0.038	O				0.32
23.083	0.00	0.13	0.037	O				0.32
23.167	0.00	0.13	0.036	O				0.31
23.250	0.00	0.13	0.035	O				0.31
23.333	0.00	0.13	0.034	O				0.30
23.417	0.00	0.13	0.033	O				0.30

23.500	0.00	0.13	0.032	O	|	|	|	0.30
23.583	0.00	0.13	0.031	O	|	|	|	0.29
23.667	0.00	0.13	0.031	O	|	|	|	0.29
23.750	0.00	0.13	0.030	O	|	|	|	0.28
23.833	0.00	0.12	0.029	O	|	|	|	0.28
23.917	0.00	0.12	0.028	O	|	|	|	0.28
24.000	0.00	0.12	0.027	O	|	|	|	0.27
24.083	0.00	0.12	0.026	O	|	|	|	0.27
24.167	0.00	0.12	0.025	O	|	|	|	0.27
24.250	0.00	0.12	0.025	O	|	|	|	0.26
24.333	0.00	0.12	0.024	O	|	|	|	0.26
24.417	0.00	0.12	0.023	O	|	|	|	0.25
24.500	0.00	0.12	0.022	O	|	|	|	0.25
24.583	0.00	0.11	0.021	O	|	|	|	0.24
24.667	0.00	0.11	0.021	O	|	|	|	0.23
24.750	0.00	0.11	0.020	O	|	|	|	0.23
24.833	0.00	0.10	0.019	O	|	|	|	0.22
24.917	0.00	0.10	0.018	O	|	|	|	0.21
25.000	0.00	0.10	0.018	O	|	|	|	0.20
25.083	0.00	0.09	0.017	O	|	|	|	0.19
25.167	0.00	0.09	0.017	O	|	|	|	0.19
25.250	0.00	0.09	0.016	O	|	|	|	0.18
25.333	0.00	0.08	0.015	O	|	|	|	0.17
25.417	0.00	0.08	0.015	O	|	|	|	0.17
25.500	0.00	0.08	0.014	O	|	|	|	0.16
25.583	0.00	0.07	0.014	O	|	|	|	0.16
25.667	0.00	0.07	0.013	O	|	|	|	0.15
25.750	0.00	0.07	0.013	O	|	|	|	0.14
25.833	0.00	0.07	0.012	O	|	|	|	0.14
25.917	0.00	0.06	0.012	O	|	|	|	0.13
26.000	0.00	0.06	0.011	O	|	|	|	0.13
26.083	0.00	0.06	0.011	O	|	|	|	0.12
26.167	0.00	0.06	0.011	O	|	|	|	0.12
26.250	0.00	0.05	0.010	O	|	|	|	0.12
26.333	0.00	0.05	0.010	O	|	|	|	0.11
26.417	0.00	0.05	0.009	O	|	|	|	0.11
26.500	0.00	0.05	0.009	O	|	|	|	0.10
26.583	0.00	0.05	0.009	O	|	|	|	0.10
26.667	0.00	0.05	0.008	O	|	|	|	0.10
26.750	0.00	0.04	0.008	O	|	|	|	0.09
26.833	0.00	0.04	0.008	O	|	|	|	0.09
26.917	0.00	0.04	0.008	O	|	|	|	0.09
27.000	0.00	0.04	0.007	O	|	|	|	0.08
27.083	0.00	0.04	0.007	O	|	|	|	0.08
27.167	0.00	0.04	0.007	O	|	|	|	0.08
27.250	0.00	0.04	0.007	O	|	|	|	0.07
27.333	0.00	0.03	0.006	O	|	|	|	0.07
27.417	0.00	0.03	0.006	O	|	|	|	0.07
27.500	0.00	0.03	0.006	O	|	|	|	0.07
27.583	0.00	0.03	0.006	O	|	|	|	0.06
27.667	0.00	0.03	0.005	O	|	|	|	0.06
27.750	0.00	0.03	0.005	O	|	|	|	0.06
27.833	0.00	0.03	0.005	O	|	|	|	0.06
27.917	0.00	0.03	0.005	O	|	|	|	0.06
28.000	0.00	0.03	0.005	O	|	|	|	0.05
28.083	0.00	0.02	0.005	O	|	|	|	0.05
28.167	0.00	0.02	0.004	O	|	|	|	0.05
28.250	0.00	0.02	0.004	O	|	|	|	0.05
28.333	0.00	0.02	0.004	O	|	|	|	0.05
28.417	0.00	0.02	0.004	O	|	|	|	0.04
28.500	0.00	0.02	0.004	O	|	|	|	0.04
28.583	0.00	0.02	0.004	O	|	|	|	0.04
28.667	0.00	0.02	0.003	O	|	|	|	0.04
28.750	0.00	0.02	0.003	O	|	|	|	0.04
28.833	0.00	0.02	0.003	O	|	|	|	0.04
28.917	0.00	0.02	0.003	O	|	|	|	0.04
29.000	0.00	0.02	0.003	O	|	|	|	0.03
29.083	0.00	0.02	0.003	O	|	|	|	0.03
29.167	0.00	0.02	0.003	O	|	|	|	0.03
29.250	0.00	0.01	0.003	O	|	|	|	0.03
29.333	0.00	0.01	0.003	O	|	|	|	0.03
29.417	0.00	0.01	0.003	O	|	|	|	0.03

29.500	0.00	0.01	0.002	O	|	|	|	0.03
29.583	0.00	0.01	0.002	O	|	|	|	0.03
29.667	0.00	0.01	0.002	O	|	|	|	0.03
29.750	0.00	0.01	0.002	O	|	|	|	0.02
29.833	0.00	0.01	0.002	O	|	|	|	0.02
29.917	0.00	0.01	0.002	O	|	|	|	0.02
30.000	0.00	0.01	0.002	O	|	|	|	0.02
30.083	0.00	0.01	0.002	O	|	|	|	0.02
30.167	0.00	0.01	0.002	O	|	|	|	0.02
30.250	0.00	0.01	0.002	O	|	|	|	0.02
30.333	0.00	0.01	0.002	O	|	|	|	0.02
30.417	0.00	0.01	0.002	O	|	|	|	0.02
30.500	0.00	0.01	0.002	O	|	|	|	0.02
30.583	0.00	0.01	0.001	O	|	|	|	0.02
30.667	0.00	0.01	0.001	O	|	|	|	0.02
30.750	0.00	0.01	0.001	O	|	|	|	0.02
30.833	0.00	0.01	0.001	O	|	|	|	0.02
30.917	0.00	0.01	0.001	O	|	|	|	0.01
31.000	0.00	0.01	0.001	O	|	|	|	0.01
31.083	0.00	0.01	0.001	O	|	|	|	0.01
31.167	0.00	0.01	0.001	O	|	|	|	0.01
31.250	0.00	0.01	0.001	O	|	|	|	0.01
31.333	0.00	0.01	0.001	O	|	|	|	0.01
31.417	0.00	0.01	0.001	O	|	|	|	0.01
31.500	0.00	0.01	0.001	O	|	|	|	0.01
31.583	0.00	0.01	0.001	O	|	|	|	0.01
31.667	0.00	0.00	0.001	O	|	|	|	0.01
31.750	0.00	0.00	0.001	O	|	|	|	0.01
31.833	0.00	0.00	0.001	O	|	|	|	0.01
31.917	0.00	0.00	0.001	O	|	|	|	0.01
32.000	0.00	0.00	0.001	O	|	|	|	0.01
32.083	0.00	0.00	0.001	O	|	|	|	0.01
32.167	0.00	0.00	0.001	O	|	|	|	0.01
32.250	0.00	0.00	0.001	O	|	|	|	0.01
32.333	0.00	0.00	0.001	O	|	|	|	0.01
32.417	0.00	0.00	0.001	O	|	|	|	0.01
32.500	0.00	0.00	0.001	O	|	|	|	0.01
32.583	0.00	0.00	0.001	O	|	|	|	0.01
32.667	0.00	0.00	0.001	O	|	|	|	0.01
32.750	0.00	0.00	0.001	O	|	|	|	0.01
32.833	0.00	0.00	0.001	O	|	|	|	0.01
32.917	0.00	0.00	0.001	O	|	|	|	0.01
33.000	0.00	0.00	0.001	O	|	|	|	0.01
33.083	0.00	0.00	0.000	O	|	|	|	0.01
33.167	0.00	0.00	0.000	O	|	|	|	0.01
33.250	0.00	0.00	0.000	O	|	|	|	0.01
33.333	0.00	0.00	0.000	O	|	|	|	0.01
33.417	0.00	0.00	0.000	O	|	|	|	0.00
33.500	0.00	0.00	0.000	O	|	|	|	0.00
33.583	0.00	0.00	0.000	O	|	|	|	0.00
33.667	0.00	0.00	0.000	O	|	|	|	0.00
33.750	0.00	0.00	0.000	O	|	|	|	0.00
33.833	0.00	0.00	0.000	O	|	|	|	0.00
33.917	0.00	0.00	0.000	O	|	|	|	0.00
34.000	0.00	0.00	0.000	O	|	|	|	0.00
34.083	0.00	0.00	0.000	O	|	|	|	0.00
34.167	0.00	0.00	0.000	O	|	|	|	0.00
34.250	0.00	0.00	0.000	O	|	|	|	0.00
34.333	0.00	0.00	0.000	O	|	|	|	0.00
34.417	0.00	0.00	0.000	O	|	|	|	0.00
34.500	0.00	0.00	0.000	O	|	|	|	0.00
34.583	0.00	0.00	0.000	O	|	|	|	0.00
34.667	0.00	0.00	0.000	O	|	|	|	0.00
34.750	0.00	0.00	0.000	O	|	|	|	0.00
34.833	0.00	0.00	0.000	O	|	|	|	0.00
34.917	0.00	0.00	0.000	O	|	|	|	0.00
35.000	0.00	0.00	0.000	O	|	|	|	0.00
35.083	0.00	0.00	0.000	O	|	|	|	0.00
35.167	0.00	0.00	0.000	O	|	|	|	0.00
35.250	0.00	0.00	0.000	O	|	|	|	0.00
35.333	0.00	0.00	0.000	O	|	|	|	0.00

```
**************************HYDROGRAPH DATA**************************
               Number of intervals =   424
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.318 (CFS)
               Total volume =       0.458 (Ac.Ft)
        Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
1-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA0515.rte
**********HYDROGRAPH DATA**********
Number of intervals = 14
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 8.684 (CFS)
Total volume = 0.278 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 14
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 2.2 4.34 6.51 8.68	Depth (Ft.)
0.083	0.98	0.02	0.003	O I	0.04
0.167	1.62	0.06	0.012	O I	0.14
0.250	1.93	0.12	0.024	O I	0.26
0.333	2.06	0.13	0.037	O I	0.32
0.417	2.15	0.14	0.050	O I	0.37
0.500	2.35	0.15	0.065	O I	0.43
0.583	2.79	0.17	0.081	O I	0.50
0.667	3.31	0.18	0.101	O I	0.58
0.750	4.54	0.19	0.127	O I	0.68
0.833	8.68	0.22	0.171	O I	0.86
0.917	6.20	0.24	0.220	O I	1.06
1.000	2.85	0.26	0.250	O I	1.18
1.083	0.86	0.26	0.261	O I	1.22
1.167	0.11	0.26	0.262	O	1.23
1.250	0.00	0.26	0.261	O	1.22
1.333	0.00	0.26	0.259	O	1.21
1.417	0.00	0.26	0.257	O	1.21
1.500	0.00	0.26	0.256	O	1.20
1.583	0.00	0.26	0.254	O	1.19
1.667	0.00	0.26	0.252	O	1.19
1.750	0.00	0.26	0.250	O	1.18
1.833	0.00	0.26	0.249	O	1.17
1.917	0.00	0.25	0.247	O	1.16
2.000	0.00	0.25	0.245	O	1.16
2.083	0.00	0.25	0.243	O	1.15
2.167	0.00	0.25	0.242	O	1.14
2.250	0.00	0.25	0.240	O	1.14
2.333	0.00	0.25	0.238	O	1.13
2.417	0.00	0.25	0.236	O	1.12
2.500	0.00	0.25	0.235	O	1.12
2.583	0.00	0.25	0.233	O	1.11
2.667	0.00	0.25	0.231	O	1.10
2.750	0.00	0.25	0.230	O	1.09
2.833	0.00	0.25	0.228	O	1.09
2.917	0.00	0.25	0.226	O	1.08
3.000	0.00	0.24	0.224	O	1.07
3.083	0.00	0.24	0.223	O	1.07
3.167	0.00	0.24	0.221	O	1.06
3.250	0.00	0.24	0.219	O	1.05
3.333	0.00	0.24	0.218	O	1.05
3.417	0.00	0.24	0.216	O	1.04
3.500	0.00	0.24	0.214	O	1.03
3.583	0.00	0.24	0.213	O	1.03
3.667	0.00	0.24	0.211	O	1.02
3.750	0.00	0.24	0.210	O	1.01
3.833	0.00	0.24	0.208	O	1.01
3.917	0.00	0.24	0.206	O	1.00
4.000	0.00	0.24	0.205	O	0.99
4.083	0.00	0.23	0.203	O	0.99
4.167	0.00	0.23	0.201	O	0.98
4.250	0.00	0.23	0.200	O	0.98
4.333	0.00	0.23	0.198	O	0.97
4.417	0.00	0.23	0.197	O	0.96
4.500	0.00	0.23	0.195	O	0.96
4.583	0.00	0.23	0.193	O	0.95
4.667	0.00	0.23	0.192	O	0.94
4.750	0.00	0.23	0.190	O	0.94
4.833	0.00	0.23	0.189	O	0.93
4.917	0.00	0.23	0.187	O	0.92
5.000	0.00	0.22	0.186	O	0.92
5.083	0.00	0.22	0.184	O	0.91
5.167	0.00	0.22	0.183	O	0.91
5.250	0.00	0.22	0.181	O	0.90
5.333	0.00	0.22	0.180	O	0.89
5.417	0.00	0.22	0.178	O	0.89

5.500	0.00	0.22	0.176	O	|	|	|	0.88
5.583	0.00	0.22	0.175	O	|	|	|	0.88
5.667	0.00	0.22	0.173	O	|	|	|	0.87
5.750	0.00	0.22	0.172	O	|	|	|	0.86
5.833	0.00	0.22	0.170	O	|	|	|	0.86
5.917	0.00	0.22	0.169	O	|	|	|	0.85
6.000	0.00	0.21	0.168	O	|	|	|	0.85
6.083	0.00	0.21	0.166	O	|	|	|	0.84
6.167	0.00	0.21	0.165	O	|	|	|	0.83
6.250	0.00	0.21	0.163	O	|	|	|	0.83
6.333	0.00	0.21	0.162	O	|	|	|	0.82
6.417	0.00	0.21	0.160	O	|	|	|	0.82
6.500	0.00	0.21	0.159	O	|	|	|	0.81
6.583	0.00	0.21	0.157	O	|	|	|	0.81
6.667	0.00	0.21	0.156	O	|	|	|	0.80
6.750	0.00	0.21	0.154	O	|	|	|	0.79
6.833	0.00	0.21	0.153	O	|	|	|	0.79
6.917	0.00	0.21	0.152	O	|	|	|	0.78
7.000	0.00	0.21	0.150	O	|	|	|	0.78
7.083	0.00	0.20	0.149	O	|	|	|	0.77
7.167	0.00	0.20	0.147	O	|	|	|	0.77
7.250	0.00	0.20	0.146	O	|	|	|	0.76
7.333	0.00	0.20	0.145	O	|	|	|	0.75
7.417	0.00	0.20	0.143	O	|	|	|	0.75
7.500	0.00	0.20	0.142	O	|	|	|	0.74
7.583	0.00	0.20	0.140	O	|	|	|	0.74
7.667	0.00	0.20	0.139	O	|	|	|	0.73
7.750	0.00	0.20	0.138	O	|	|	|	0.73
7.833	0.00	0.20	0.136	O	|	|	|	0.72
7.917	0.00	0.20	0.135	O	|	|	|	0.72
8.000	0.00	0.20	0.134	O	|	|	|	0.71
8.083	0.00	0.20	0.132	O	|	|	|	0.70
8.167	0.00	0.19	0.131	O	|	|	|	0.70
8.250	0.00	0.19	0.130	O	|	|	|	0.69
8.333	0.00	0.19	0.128	O	|	|	|	0.69
8.417	0.00	0.19	0.127	O	|	|	|	0.68
8.500	0.00	0.19	0.126	O	|	|	|	0.68
8.583	0.00	0.19	0.124	O	|	|	|	0.67
8.667	0.00	0.19	0.123	O	|	|	|	0.67
8.750	0.00	0.19	0.122	O	|	|	|	0.66
8.833	0.00	0.19	0.120	O	|	|	|	0.66
8.917	0.00	0.19	0.119	O	|	|	|	0.65
9.000	0.00	0.19	0.118	O	|	|	|	0.65
9.083	0.00	0.19	0.116	O	|	|	|	0.64
9.167	0.00	0.19	0.115	O	|	|	|	0.64
9.250	0.00	0.19	0.114	O	|	|	|	0.63
9.333	0.00	0.18	0.113	O	|	|	|	0.63
9.417	0.00	0.18	0.111	O	|	|	|	0.62
9.500	0.00	0.18	0.110	O	|	|	|	0.62
9.583	0.00	0.18	0.109	O	|	|	|	0.61
9.667	0.00	0.18	0.108	O	|	|	|	0.61
9.750	0.00	0.18	0.106	O	|	|	|	0.60
9.833	0.00	0.18	0.105	O	|	|	|	0.60
9.917	0.00	0.18	0.104	O	|	|	|	0.59
10.000	0.00	0.18	0.103	O	|	|	|	0.59
10.083	0.00	0.18	0.101	O	|	|	|	0.58
10.167	0.00	0.18	0.100	O	|	|	|	0.58
10.250	0.00	0.18	0.099	O	|	|	|	0.57
10.333	0.00	0.18	0.098	O	|	|	|	0.57
10.417	0.00	0.18	0.097	O	|	|	|	0.56
10.500	0.00	0.17	0.095	O	|	|	|	0.56
10.583	0.00	0.17	0.094	O	|	|	|	0.55
10.667	0.00	0.17	0.093	O	|	|	|	0.55
10.750	0.00	0.17	0.092	O	|	|	|	0.54
10.833	0.00	0.17	0.091	O	|	|	|	0.54
10.917	0.00	0.17	0.089	O	|	|	|	0.53
11.000	0.00	0.17	0.088	O	|	|	|	0.53
11.083	0.00	0.17	0.087	O	|	|	|	0.52
11.167	0.00	0.17	0.086	O	|	|	|	0.52
11.250	0.00	0.17	0.085	O	|	|	|	0.51
11.333	0.00	0.17	0.083	O	|	|	|	0.51
11.417	0.00	0.17	0.082	O	|	|	|	0.51

11.500	0.00	0.17	0.081	O	|	|	|	0.50
11.583	0.00	0.17	0.080	O	|	|	|	0.50
11.667	0.00	0.17	0.079	O	|	|	|	0.49
11.750	0.00	0.16	0.078	O	|	|	|	0.49
11.833	0.00	0.16	0.077	O	|	|	|	0.48
11.917	0.00	0.16	0.075	O	|	|	|	0.48
12.000	0.00	0.16	0.074	O	|	|	|	0.47
12.083	0.00	0.16	0.073	O	|	|	|	0.47
12.167	0.00	0.16	0.072	O	|	|	|	0.46
12.250	0.00	0.16	0.071	O	|	|	|	0.46
12.333	0.00	0.16	0.070	O	|	|	|	0.45
12.417	0.00	0.16	0.069	O	|	|	|	0.45
12.500	0.00	0.16	0.068	O	|	|	|	0.45
12.583	0.00	0.16	0.067	O	|	|	|	0.44
12.667	0.00	0.16	0.066	O	|	|	|	0.44
12.750	0.00	0.15	0.065	O	|	|	|	0.43
12.833	0.00	0.15	0.063	O	|	|	|	0.43
12.917	0.00	0.15	0.062	O	|	|	|	0.42
13.000	0.00	0.15	0.061	O	|	|	|	0.42
13.083	0.00	0.15	0.060	O	|	|	|	0.42
13.167	0.00	0.15	0.059	O	|	|	|	0.41
13.250	0.00	0.15	0.058	O	|	|	|	0.41
13.333	0.00	0.15	0.057	O	|	|	|	0.40
13.417	0.00	0.15	0.056	O	|	|	|	0.40
13.500	0.00	0.15	0.055	O	|	|	|	0.39
13.583	0.00	0.15	0.054	O	|	|	|	0.39
13.667	0.00	0.15	0.053	O	|	|	|	0.39
13.750	0.00	0.15	0.052	O	|	|	|	0.38
13.833	0.00	0.14	0.051	O	|	|	|	0.38
13.917	0.00	0.14	0.050	O	|	|	|	0.37
14.000	0.00	0.14	0.049	O	|	|	|	0.37
14.083	0.00	0.14	0.048	O	|	|	|	0.37
14.167	0.00	0.14	0.047	O	|	|	|	0.36
14.250	0.00	0.14	0.046	O	|	|	|	0.36
14.333	0.00	0.14	0.045	O	|	|	|	0.35
14.417	0.00	0.14	0.044	O	|	|	|	0.35
14.500	0.00	0.14	0.043	O	|	|	|	0.35
14.583	0.00	0.14	0.042	O	|	|	|	0.34
14.667	0.00	0.14	0.041	O	|	|	|	0.34
14.750	0.00	0.14	0.040	O	|	|	|	0.33
14.833	0.00	0.14	0.040	O	|	|	|	0.33
14.917	0.00	0.13	0.039	O	|	|	|	0.32
15.000	0.00	0.13	0.038	O	|	|	|	0.32
15.083	0.00	0.13	0.037	O	|	|	|	0.32
15.167	0.00	0.13	0.036	O	|	|	|	0.31
15.250	0.00	0.13	0.035	O	|	|	|	0.31
15.333	0.00	0.13	0.034	O	|	|	|	0.30
15.417	0.00	0.13	0.033	O	|	|	|	0.30
15.500	0.00	0.13	0.032	O	|	|	|	0.30
15.583	0.00	0.13	0.031	O	|	|	|	0.29
15.667	0.00	0.13	0.031	O	|	|	|	0.29
15.750	0.00	0.13	0.030	O	|	|	|	0.28
15.833	0.00	0.12	0.029	O	|	|	|	0.28
15.917	0.00	0.12	0.028	O	|	|	|	0.28
16.000	0.00	0.12	0.027	O	|	|	|	0.27
16.083	0.00	0.12	0.026	O	|	|	|	0.27
16.167	0.00	0.12	0.025	O	|	|	|	0.27
16.250	0.00	0.12	0.025	O	|	|	|	0.26
16.333	0.00	0.12	0.024	O	|	|	|	0.26
16.417	0.00	0.12	0.023	O	|	|	|	0.25
16.500	0.00	0.12	0.022	O	|	|	|	0.25
16.583	0.00	0.11	0.021	O	|	|	|	0.24
16.667	0.00	0.11	0.021	O	|	|	|	0.23
16.750	0.00	0.11	0.020	O	|	|	|	0.22
16.833	0.00	0.10	0.019	O	|	|	|	0.22
16.917	0.00	0.10	0.018	O	|	|	|	0.21
17.000	0.00	0.10	0.018	O	|	|	|	0.20
17.083	0.00	0.09	0.017	O	|	|	|	0.19
17.167	0.00	0.09	0.016	O	|	|	|	0.19
17.250	0.00	0.09	0.016	O	|	|	|	0.18
17.333	0.00	0.08	0.015	O	|	|	|	0.17
17.417	0.00	0.08	0.015	O	|	|	|	0.17

17.500	0.00	0.08	0.014	O	|	|	|	0.16
17.583	0.00	0.07	0.014	O	|	|	|	0.16
17.667	0.00	0.07	0.013	O	|	|	|	0.15
17.750	0.00	0.07	0.013	O	|	|	|	0.14
17.833	0.00	0.07	0.012	O	|	|	|	0.14
17.917	0.00	0.06	0.012	O	|	|	|	0.13
18.000	0.00	0.06	0.011	O	|	|	|	0.13
18.083	0.00	0.06	0.011	O	|	|	|	0.12
18.167	0.00	0.06	0.011	O	|	|	|	0.12
18.250	0.00	0.05	0.010	O	|	|	|	0.12
18.333	0.00	0.05	0.010	O	|	|	|	0.11
18.417	0.00	0.05	0.009	O	|	|	|	0.11
18.500	0.00	0.05	0.009	O	|	|	|	0.10
18.583	0.00	0.05	0.009	O	|	|	|	0.10
18.667	0.00	0.05	0.008	O	|	|	|	0.10
18.750	0.00	0.04	0.008	O	|	|	|	0.09
18.833	0.00	0.04	0.008	O	|	|	|	0.09
18.917	0.00	0.04	0.008	O	|	|	|	0.09
19.000	0.00	0.04	0.007	O	|	|	|	0.08
19.083	0.00	0.04	0.007	O	|	|	|	0.08
19.167	0.00	0.04	0.007	O	|	|	|	0.08
19.250	0.00	0.04	0.007	O	|	|	|	0.07
19.333	0.00	0.03	0.006	O	|	|	|	0.07
19.417	0.00	0.03	0.006	O	|	|	|	0.07
19.500	0.00	0.03	0.006	O	|	|	|	0.07
19.583	0.00	0.03	0.006	O	|	|	|	0.06
19.667	0.00	0.03	0.005	O	|	|	|	0.06
19.750	0.00	0.03	0.005	O	|	|	|	0.06
19.833	0.00	0.03	0.005	O	|	|	|	0.06
19.917	0.00	0.03	0.005	O	|	|	|	0.06
20.000	0.00	0.03	0.005	O	|	|	|	0.05
20.083	0.00	0.02	0.005	O	|	|	|	0.05
20.167	0.00	0.02	0.004	O	|	|	|	0.05
20.250	0.00	0.02	0.004	O	|	|	|	0.05
20.333	0.00	0.02	0.004	O	|	|	|	0.05
20.417	0.00	0.02	0.004	O	|	|	|	0.04
20.500	0.00	0.02	0.004	O	|	|	|	0.04
20.583	0.00	0.02	0.004	O	|	|	|	0.04
20.667	0.00	0.02	0.003	O	|	|	|	0.04
20.750	0.00	0.02	0.003	O	|	|	|	0.04
20.833	0.00	0.02	0.003	O	|	|	|	0.04
20.917	0.00	0.02	0.003	O	|	|	|	0.04
21.000	0.00	0.02	0.003	O	|	|	|	0.03
21.083	0.00	0.02	0.003	O	|	|	|	0.03
21.167	0.00	0.01	0.003	O	|	|	|	0.03
21.250	0.00	0.01	0.003	O	|	|	|	0.03
21.333	0.00	0.01	0.003	O	|	|	|	0.03
21.417	0.00	0.01	0.003	O	|	|	|	0.03
21.500	0.00	0.01	0.002	O	|	|	|	0.03
21.583	0.00	0.01	0.002	O	|	|	|	0.03
21.667	0.00	0.01	0.002	O	|	|	|	0.03
21.750	0.00	0.01	0.002	O	|	|	|	0.02
21.833	0.00	0.01	0.002	O	|	|	|	0.02
21.917	0.00	0.01	0.002	O	|	|	|	0.02
22.000	0.00	0.01	0.002	O	|	|	|	0.02
22.083	0.00	0.01	0.002	O	|	|	|	0.02
22.167	0.00	0.01	0.002	O	|	|	|	0.02
22.250	0.00	0.01	0.002	O	|	|	|	0.02
22.333	0.00	0.01	0.002	O	|	|	|	0.02
22.417	0.00	0.01	0.002	O	|	|	|	0.02
22.500	0.00	0.01	0.002	O	|	|	|	0.02
22.583	0.00	0.01	0.001	O	|	|	|	0.02
22.667	0.00	0.01	0.001	O	|	|	|	0.02
22.750	0.00	0.01	0.001	O	|	|	|	0.02
22.833	0.00	0.01	0.001	O	|	|	|	0.02
22.917	0.00	0.01	0.001	O	|	|	|	0.01
23.000	0.00	0.01	0.001	O	|	|	|	0.01
23.083	0.00	0.01	0.001	O	|	|	|	0.01
23.167	0.00	0.01	0.001	O	|	|	|	0.01
23.250	0.00	0.01	0.001	O	|	|	|	0.01
23.333	0.00	0.01	0.001	O	|	|	|	0.01
23.417	0.00	0.01	0.001	O	|	|	|	0.01

23.500	0.00	0.01	0.001	O	|	|	|	|	0.01
23.583	0.00	0.01	0.001	O	|	|	|	|	0.01
23.667	0.00	0.00	0.001	O	|	|	|	|	0.01
23.750	0.00	0.00	0.001	O	|	|	|	|	0.01
23.833	0.00	0.00	0.001	O	|	|	|	|	0.01
23.917	0.00	0.00	0.001	O	|	|	|	|	0.01
24.000	0.00	0.00	0.001	O	|	|	|	|	0.01
24.083	0.00	0.00	0.001	O	|	|	|	|	0.01
24.167	0.00	0.00	0.001	O	|	|	|	|	0.01
24.250	0.00	0.00	0.001	O	|	|	|	|	0.01
24.333	0.00	0.00	0.001	O	|	|	|	|	0.01
24.417	0.00	0.00	0.001	O	|	|	|	|	0.01
24.500	0.00	0.00	0.001	O	|	|	|	|	0.01
24.583	0.00	0.00	0.001	O	|	|	|	|	0.01
24.667	0.00	0.00	0.001	O	|	|	|	|	0.01
24.750	0.00	0.00	0.001	O	|	|	|	|	0.01
24.833	0.00	0.00	0.001	O	|	|	|	|	0.01
24.917	0.00	0.00	0.001	O	|	|	|	|	0.01
25.000	0.00	0.00	0.001	O	|	|	|	|	0.01
25.083	0.00	0.00	0.000	O	|	|	|	|	0.01
25.167	0.00	0.00	0.000	O	|	|	|	|	0.01
25.250	0.00	0.00	0.000	O	|	|	|	|	0.01
25.333	0.00	0.00	0.000	O	|	|	|	|	0.01
25.417	0.00	0.00	0.000	O	|	|	|	|	0.00
25.500	0.00	0.00	0.000	O	|	|	|	|	0.00
25.583	0.00	0.00	0.000	O	|	|	|	|	0.00
25.667	0.00	0.00	0.000	O	|	|	|	|	0.00
25.750	0.00	0.00	0.000	O	|	|	|	|	0.00
25.833	0.00	0.00	0.000	O	|	|	|	|	0.00
25.917	0.00	0.00	0.000	O	|	|	|	|	0.00
26.000	0.00	0.00	0.000	O	|	|	|	|	0.00
26.083	0.00	0.00	0.000	O	|	|	|	|	0.00
26.167	0.00	0.00	0.000	O	|	|	|	|	0.00
26.250	0.00	0.00	0.000	O	|	|	|	|	0.00
26.333	0.00	0.00	0.000	O	|	|	|	|	0.00
26.417	0.00	0.00	0.000	O	|	|	|	|	0.00
26.500	0.00	0.00	0.000	O	|	|	|	|	0.00
26.583	0.00	0.00	0.000	O	|	|	|	|	0.00
26.667	0.00	0.00	0.000	O	|	|	|	|	0.00
26.750	0.00	0.00	0.000	O	|	|	|	|	0.00
26.833	0.00	0.00	0.000	O	|	|	|	|	0.00
26.917	0.00	0.00	0.000	O	|	|	|	|	0.00
27.000	0.00	0.00	0.000	O	|	|	|	|	0.00
27.083	0.00	0.00	0.000	O	|	|	|	|	0.00
27.167	0.00	0.00	0.000	O	|	|	|	|	0.00
27.250	0.00	0.00	0.000	O	|	|	|	|	0.00
27.333	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 328
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.261 (CFS)
Total volume = 0.278 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
24-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA102410.rte
**********HYDROGRAPH DATA**********
Number of intervals = 290
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.328 (CFS)
Total volume = 1.385 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 290
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

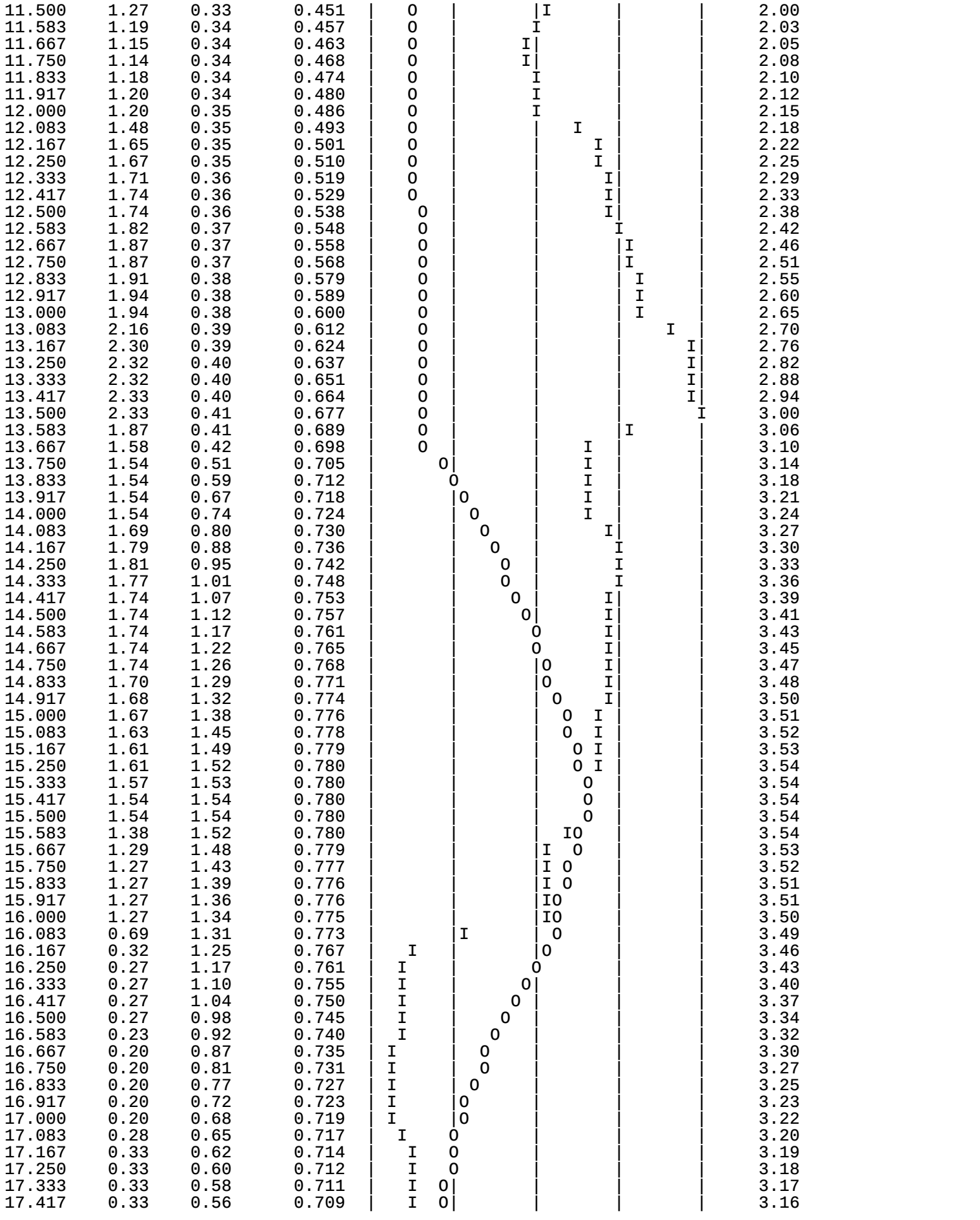
Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.6	1.16	1.75	2.33	Depth (Ft.)
0.083	0.08	0.00	0.000	OI	|	|	|	|	0.00
0.167	0.13	0.01	0.001	OI	|	|	|	|	0.01
0.250	0.13	0.01	0.002	OI	|	|	|	|	0.02
0.333	0.17	0.01	0.003	O I	|	|	|	|	0.03
0.417	0.20	0.02	0.004	O I	|	|	|	|	0.04
0.500	0.20	0.03	0.005	O I	|	|	|	|	0.06
0.583	0.20	0.03	0.006	O I	|	|	|	|	0.07
0.667	0.20	0.04	0.007	O I	|	|	|	|	0.08
0.750	0.20	0.05	0.008	O I	|	|	|	|	0.10
0.833	0.24	0.05	0.010	O I	|	|	|	|	0.11
0.917	0.26	0.06	0.011	O I	|	|	|	|	0.13
1.000	0.27	0.07	0.012	O I	|	|	|	|	0.14
1.083	0.23	0.07	0.014	|O I	|	|	|	|	0.16
1.167	0.20	0.08	0.015	|OI	|	|	|	|	0.17
1.250	0.20	0.08	0.015	|OI	|	|	|	|	0.18
1.333	0.20	0.09	0.016	|OI	|	|	|	|	0.18
1.417	0.20	0.09	0.017	|OI	|	|	|	|	0.19
1.500	0.20	0.10	0.018	|OI	|	|	|	|	0.20
1.583	0.20	0.10	0.018	|OI	|	|	|	|	0.21
1.667	0.20	0.10	0.019	|OI	|	|	|	|	0.22
1.750	0.20	0.11	0.020	|OI	|	|	|	|	0.23
1.833	0.24	0.11	0.021	|O I	|	|	|	|	0.23
1.917	0.26	0.12	0.022	|O I	|	|	|	|	0.24
2.000	0.27	0.12	0.023	|O I	|	|	|	|	0.25
2.083	0.27	0.12	0.024	|O I	|	|	|	|	0.26
2.167	0.27	0.12	0.025	|O I	|	|	|	|	0.26
2.250	0.27	0.12	0.026	|O I	|	|	|	|	0.27
2.333	0.27	0.12	0.027	|O I	|	|	|	|	0.27
2.417	0.27	0.12	0.028	|O I	|	|	|	|	0.28
2.500	0.27	0.12	0.029	|O I	|	|	|	|	0.28
2.583	0.31	0.13	0.030	|O I	|	|	|	|	0.28
2.667	0.33	0.13	0.031	|O I	|	|	|	|	0.29
2.750	0.33	0.13	0.032	|O I	|	|	|	|	0.30
2.833	0.33	0.13	0.034	|O I	|	|	|	|	0.30
2.917	0.33	0.13	0.035	|O I	|	|	|	|	0.31
3.000	0.33	0.13	0.037	|O I	|	|	|	|	0.32
3.083	0.33	0.13	0.038	|O I	|	|	|	|	0.32
3.167	0.33	0.14	0.039	|O I	|	|	|	|	0.33
3.250	0.33	0.14	0.041	|O I	|	|	|	|	0.33
3.333	0.33	0.14	0.042	|O I	|	|	|	|	0.34
3.417	0.33	0.14	0.044	|O I	|	|	|	|	0.35
3.500	0.33	0.14	0.045	|O I	|	|	|	|	0.35
3.583	0.33	0.14	0.046	|O I	|	|	|	|	0.36
3.667	0.33	0.14	0.048	|O I	|	|	|	|	0.36
3.750	0.33	0.14	0.049	|O I	|	|	|	|	0.37
3.833	0.37	0.14	0.050	|O I	|	|	|	|	0.37
3.917	0.40	0.15	0.052	|O I	|	|	|	|	0.38
4.000	0.40	0.15	0.054	| O I	|	|	|	|	0.39
4.083	0.40	0.15	0.055	| O I	|	|	|	|	0.40
4.167	0.40	0.15	0.057	| O I	|	|	|	|	0.40
4.250	0.40	0.15	0.059	| O I	|	|	|	|	0.41
4.333	0.44	0.15	0.061	| O I	|	|	|	|	0.42
4.417	0.46	0.15	0.063	| O I	|	|	|	|	0.43
4.500	0.47	0.16	0.065	| O I	|	|	|	|	0.43
4.583	0.47	0.16	0.067	| O I	|	|	|	|	0.44
4.667	0.47	0.16	0.069	| O I	|	|	|	|	0.45
4.750	0.47	0.16	0.071	| O I	|	|	|	|	0.46
4.833	0.51	0.16	0.074	| O I	|	|	|	|	0.47
4.917	0.53	0.16	0.076	| O I	|	|	|	|	0.48
5.000	0.54	0.17	0.079	| O I	|	|	|	|	0.49
5.083	0.46	0.17	0.081	| O I	|	|	|	|	0.50
5.167	0.41	0.17	0.083	| O I	|	|	|	|	0.51
5.250	0.40	0.17	0.084	| O I	|	|	|	|	0.51
5.333	0.44	0.17	0.086	| O I	|	|	|	|	0.52
5.417	0.46	0.17	0.088	| O I	|	|	|	|	0.53

5.500	0.47	0.17	0.090	O	I				0.54
5.583	0.51	0.17	0.092	O	I				0.55
5.667	0.53	0.17	0.095	O	I				0.55
5.750	0.54	0.18	0.097	O	I				0.56
5.833	0.54	0.18	0.100	O	I				0.57
5.917	0.54	0.18	0.102	O	I				0.58
6.000	0.54	0.18	0.105	O	I				0.59
6.083	0.57	0.18	0.107	O	I				0.60
6.167	0.60	0.18	0.110	O	I				0.62
6.250	0.60	0.18	0.113	O	I				0.63
6.333	0.60	0.19	0.116	O	I				0.64
6.417	0.60	0.19	0.118	O	I				0.65
6.500	0.60	0.19	0.121	O	I				0.66
6.583	0.64	0.19	0.124	O	I				0.67
6.667	0.67	0.19	0.127	O	I				0.69
6.750	0.67	0.19	0.131	O	I				0.70
6.833	0.67	0.20	0.134	O	I				0.71
6.917	0.67	0.20	0.137	O	I				0.72
7.000	0.67	0.20	0.140	O	I				0.74
7.083	0.67	0.20	0.144	O	I				0.75
7.167	0.67	0.20	0.147	O	I				0.76
7.250	0.67	0.21	0.150	O	I				0.78
7.333	0.71	0.21	0.153	O	I				0.79
7.417	0.73	0.21	0.157	O	I				0.80
7.500	0.74	0.21	0.161	O	I				0.82
7.583	0.77	0.21	0.164	O	I				0.83
7.667	0.80	0.22	0.168	O	I				0.85
7.750	0.80	0.22	0.172	O	I				0.87
7.833	0.84	0.22	0.176	O	I				0.88
7.917	0.87	0.22	0.181	O	I				0.90
8.000	0.87	0.22	0.185	O	I				0.92
8.083	0.95	0.23	0.190	O	I				0.94
8.167	1.00	0.23	0.195	O	I				0.96
8.250	1.00	0.23	0.200	O	I				0.98
8.333	1.00	0.24	0.206	O	I				1.00
8.417	1.00	0.24	0.211	O	I				1.02
8.500	1.00	0.24	0.216	O	I				1.04
8.583	1.04	0.24	0.222	O	I				1.06
8.667	1.07	0.25	0.227	O	I				1.09
8.750	1.07	0.25	0.233	O	I				1.11
8.833	1.11	0.25	0.239	O	I				1.13
8.917	1.13	0.25	0.245	O	I				1.16
9.000	1.14	0.26	0.251	O	I				1.18
9.083	1.21	0.26	0.257	O	I				1.21
9.167	1.26	0.26	0.264	O	I				1.23
9.250	1.27	0.26	0.271	O	I				1.26
9.333	1.31	0.27	0.278	O	I				1.29
9.417	1.33	0.27	0.285	O	I				1.32
9.500	1.34	0.27	0.292	O	I				1.35
9.583	1.38	0.28	0.300	O	I				1.38
9.667	1.40	0.28	0.307	O	I				1.41
9.750	1.41	0.28	0.315	O	I				1.44
9.833	1.44	0.29	0.323	O	I				1.47
9.917	1.47	0.29	0.331	O	I				1.51
10.000	1.47	0.29	0.339	O	I				1.54
10.083	1.20	0.30	0.346	O	I				1.57
10.167	1.03	0.30	0.352	O	I				1.59
10.250	1.00	0.30	0.357	O	I				1.61
10.333	1.00	0.30	0.362	O	I				1.63
10.417	1.00	0.30	0.367	O	I				1.65
10.500	1.00	0.30	0.371	O	I				1.67
10.583	1.20	0.31	0.377	O	I				1.70
10.667	1.32	0.31	0.383	O	I				1.72
10.750	1.34	0.31	0.390	O	I				1.75
10.833	1.34	0.31	0.397	O	I				1.78
10.917	1.34	0.32	0.405	O	I				1.81
11.000	1.34	0.32	0.412	O	I				1.84
11.083	1.30	0.32	0.418	O	I				1.87
11.167	1.28	0.32	0.425	O	I				1.89
11.250	1.27	0.33	0.432	O	I				1.92
11.333	1.27	0.33	0.438	O	I				1.95
11.417	1.27	0.33	0.445	O	I				1.97



11.500	1.27	0.33	0.451	O	I			2.00
11.583	1.19	0.34	0.457	O	I			2.03
11.667	1.15	0.34	0.463	O	I			2.05
11.750	1.14	0.34	0.468	O	I			2.08
11.833	1.18	0.34	0.474	O	I			2.10
11.917	1.20	0.34	0.480	O	I			2.12
12.000	1.20	0.35	0.486	O	I			2.15
12.083	1.48	0.35	0.493	O	I			2.18
12.167	1.65	0.35	0.501	O	I			2.22
12.250	1.67	0.35	0.510	O	I			2.25
12.333	1.71	0.36	0.519	O	I			2.29
12.417	1.74	0.36	0.529	O	I			2.33
12.500	1.74	0.36	0.538	O	I			2.38
12.583	1.82	0.37	0.548	O	I			2.42
12.667	1.87	0.37	0.558	O	I			2.46
12.750	1.87	0.37	0.568	O	I			2.51
12.833	1.91	0.38	0.579	O	I			2.55
12.917	1.94	0.38	0.589	O	I			2.60
13.000	1.94	0.38	0.600	O	I			2.65
13.083	2.16	0.39	0.612	O	I			2.70
13.167	2.30	0.39	0.624	O	I			2.76
13.250	2.32	0.40	0.637	O	I			2.82
13.333	2.32	0.40	0.651	O	I			2.88
13.417	2.33	0.40	0.664	O	I			2.94
13.500	2.33	0.41	0.677	O	I			3.00
13.583	1.87	0.41	0.689	O	I			3.06
13.667	1.58	0.42	0.698	O	I			3.10
13.750	1.54	0.51	0.705	O	I			3.14
13.833	1.54	0.59	0.712	O	I			3.18
13.917	1.54	0.67	0.718	O	I			3.21
14.000	1.54	0.74	0.724	O	I			3.24
14.083	1.69	0.80	0.730	O	I			3.27
14.167	1.79	0.88	0.736	O	I			3.30
14.250	1.81	0.95	0.742	O	I			3.33
14.333	1.77	1.01	0.748	O	I			3.36
14.417	1.74	1.07	0.753	O	I			3.39
14.500	1.74	1.12	0.757	O	I			3.41
14.583	1.74	1.17	0.761	O	I			3.43
14.667	1.74	1.22	0.765	O	I			3.45
14.750	1.74	1.26	0.768	O	I			3.47
14.833	1.70	1.29	0.771	O	I			3.48
14.917	1.68	1.32	0.774	O	I			3.50
15.000	1.67	1.38	0.776	O	I			3.51
15.083	1.63	1.45	0.778	O	I			3.52
15.167	1.61	1.49	0.779	O	I			3.53
15.250	1.61	1.52	0.780	O	I			3.54
15.333	1.57	1.53	0.780	O				3.54
15.417	1.54	1.54	0.780	O				3.54
15.500	1.54	1.54	0.780	O				3.54
15.583	1.38	1.52	0.780	O	I			3.54
15.667	1.29	1.48	0.779	O	I			3.53
15.750	1.27	1.43	0.777	O	I			3.52
15.833	1.27	1.39	0.776	O	I			3.51
15.917	1.27	1.36	0.776	O	I			3.51
16.000	1.27	1.34	0.775	O	I			3.50
16.083	0.69	1.31	0.773	O	I			3.49
16.167	0.32	1.25	0.767	O	I			3.46
16.250	0.27	1.17	0.761	O	I			3.43
16.333	0.27	1.10	0.755	O	I			3.40
16.417	0.27	1.04	0.750	O	I			3.37
16.500	0.27	0.98	0.745	O	I			3.34
16.583	0.23	0.92	0.740	O	I			3.32
16.667	0.20	0.87	0.735	O	I			3.30
16.750	0.20	0.81	0.731	O	I			3.27
16.833	0.20	0.77	0.727	O	I			3.25
16.917	0.20	0.72	0.723	O	I			3.23
17.000	0.20	0.68	0.719	O	I			3.22
17.083	0.28	0.65	0.717	O	I			3.20
17.167	0.33	0.62	0.714	O	I			3.19
17.250	0.33	0.60	0.712	O	I			3.18
17.333	0.33	0.58	0.711	O	I			3.17
17.417	0.33	0.56	0.709	O	I			3.16

17.500	0.33	0.54	0.708	| I O|	|	|	|	3.15
17.583	0.33	0.52	0.706	| I O|	|	|	|	3.15
17.667	0.33	0.51	0.705	| I O|	|	|	|	3.14
17.750	0.33	0.50	0.704	| I O |	|	|	|	3.13
17.833	0.30	0.48	0.703	| I O |	|	|	|	3.13
17.917	0.27	0.47	0.701	| I O |	|	|	|	3.12
18.000	0.27	0.45	0.700	| I O |	|	|	|	3.12
18.083	0.27	0.44	0.699	| I O |	|	|	|	3.11
18.167	0.27	0.42	0.698	| I O |	|	|	|	3.10
18.250	0.27	0.42	0.697	| I O |	|	|	|	3.10
18.333	0.27	0.42	0.696	| I O |	|	|	|	3.09
18.417	0.27	0.42	0.695	| I O |	|	|	|	3.09
18.500	0.27	0.41	0.694	| I O |	|	|	|	3.08
18.583	0.23	0.41	0.692	| I O |	|	|	|	3.08
18.667	0.20	0.41	0.691	| I O |	|	|	|	3.07
18.750	0.20	0.41	0.690	| I O |	|	|	|	3.06
18.833	0.16	0.41	0.688	| I O |	|	|	|	3.05
18.917	0.14	0.41	0.686	|I O |	|	|	|	3.05
19.000	0.13	0.41	0.684	|I O |	|	|	|	3.04
19.083	0.17	0.41	0.682	| I O |	|	|	|	3.03
19.167	0.20	0.41	0.681	| I O |	|	|	|	3.02
19.250	0.20	0.41	0.679	| I O |	|	|	|	3.01
19.333	0.24	0.41	0.678	| I O |	|	|	|	3.01
19.417	0.26	0.41	0.677	| I O |	|	|	|	3.00
19.500	0.27	0.41	0.676	| I O |	|	|	|	3.00
19.583	0.23	0.41	0.675	| I O |	|	|	|	2.99
19.667	0.20	0.41	0.674	| I O |	|	|	|	2.98
19.750	0.20	0.41	0.672	| I O |	|	|	|	2.98
19.833	0.16	0.41	0.671	| I O |	|	|	|	2.97
19.917	0.14	0.41	0.669	|I O |	|	|	|	2.96
20.000	0.13	0.41	0.667	|I O |	|	|	|	2.95
20.083	0.17	0.41	0.665	| I O |	|	|	|	2.95
20.167	0.20	0.40	0.664	| I O |	|	|	|	2.94
20.250	0.20	0.40	0.662	| I O |	|	|	|	2.93
20.333	0.20	0.40	0.661	| I O |	|	|	|	2.93
20.417	0.20	0.40	0.660	| I O |	|	|	|	2.92
20.500	0.20	0.40	0.658	| I O |	|	|	|	2.91
20.583	0.20	0.40	0.657	| I O |	|	|	|	2.91
20.667	0.20	0.40	0.655	| I O |	|	|	|	2.90
20.750	0.20	0.40	0.654	| I O |	|	|	|	2.90
20.833	0.16	0.40	0.653	| I O |	|	|	|	2.89
20.917	0.14	0.40	0.651	|I O |	|	|	|	2.88
21.000	0.13	0.40	0.649	|I O |	|	|	|	2.87
21.083	0.17	0.40	0.647	| I O |	|	|	|	2.86
21.167	0.20	0.40	0.646	| I O |	|	|	|	2.86
21.250	0.20	0.40	0.644	| I O |	|	|	|	2.85
21.333	0.16	0.40	0.643	| I O |	|	|	|	2.85
21.417	0.14	0.40	0.641	|I O |	|	|	|	2.84
21.500	0.13	0.40	0.639	|I O |	|	|	|	2.83
21.583	0.17	0.40	0.638	| I O |	|	|	|	2.82
21.667	0.20	0.40	0.636	| I O |	|	|	|	2.81
21.750	0.20	0.40	0.635	| I O |	|	|	|	2.81
21.833	0.16	0.40	0.633	| I O |	|	|	|	2.80
21.917	0.14	0.39	0.632	|I O |	|	|	|	2.79
22.000	0.13	0.39	0.630	|I O |	|	|	|	2.79
22.083	0.17	0.39	0.628	| I O |	|	|	|	2.78
22.167	0.20	0.39	0.627	| I O |	|	|	|	2.77
22.250	0.20	0.39	0.626	| I O |	|	|	|	2.77
22.333	0.16	0.39	0.624	| I O |	|	|	|	2.76
22.417	0.14	0.39	0.622	|I O |	|	|	|	2.75
22.500	0.13	0.39	0.621	|I O |	|	|	|	2.74
22.583	0.13	0.39	0.619	|I O |	|	|	|	2.74
22.667	0.13	0.39	0.617	|I O |	|	|	|	2.73
22.750	0.13	0.39	0.615	|I O |	|	|	|	2.72
22.833	0.13	0.39	0.614	|I O |	|	|	|	2.71
22.917	0.13	0.39	0.612	|I O |	|	|	|	2.70
23.000	0.13	0.39	0.610	|I O |	|	|	|	2.70
23.083	0.13	0.39	0.608	|I O |	|	|	|	2.69
23.167	0.13	0.39	0.607	|I O |	|	|	|	2.68
23.250	0.13	0.39	0.605	|I O |	|	|	|	2.67
23.333	0.13	0.39	0.603	|I O |	|	|	|	2.66
23.417	0.13	0.38	0.601	|I O |	|	|	|	2.66

23.500	0.13	0.38	0.600	|I	O	|	|	|	2.65
23.583	0.13	0.38	0.598	|I	O	|	|	|	2.64
23.667	0.13	0.38	0.596	|I	O	|	|	|	2.63
23.750	0.13	0.38	0.595	|I	O	|	|	|	2.63
23.833	0.13	0.38	0.593	|I	O	|	|	|	2.62
23.917	0.13	0.38	0.591	|I	O	|	|	|	2.61
24.000	0.13	0.38	0.589	|I	O	|	|	|	2.60
24.083	0.06	0.38	0.587	I	O	|	|	|	2.59
24.167	0.01	0.38	0.585	I	O	|	|	|	2.58
24.250	0.00	0.38	0.582	I	O	|	|	|	2.57
24.333	0.00	0.38	0.580	I	O	|	|	|	2.56
24.417	0.00	0.38	0.577	I	O	|	|	|	2.55
24.500	0.00	0.38	0.575	I	O	|	|	|	2.53
24.583	0.00	0.38	0.572	I	O	|	|	|	2.52
24.667	0.00	0.37	0.569	I	O	|	|	|	2.51
24.750	0.00	0.37	0.567	I	O	|	|	|	2.50
24.833	0.00	0.37	0.564	I	O	|	|	|	2.49
24.917	0.00	0.37	0.562	I	O	|	|	|	2.48
25.000	0.00	0.37	0.559	I	O	|	|	|	2.47
25.083	0.00	0.37	0.557	I	O	|	|	|	2.46
25.167	0.00	0.37	0.554	I	O	|	|	|	2.44
25.250	0.00	0.37	0.552	I	O	|	|	|	2.43
25.333	0.00	0.37	0.549	I	O	|	|	|	2.42
25.417	0.00	0.37	0.546	I	O	|	|	|	2.41
25.500	0.00	0.37	0.544	I	O	|	|	|	2.40
25.583	0.00	0.37	0.541	I	O	|	|	|	2.39
25.667	0.00	0.36	0.539	I	O	|	|	|	2.38
25.750	0.00	0.36	0.536	I	O	|	|	|	2.37
25.833	0.00	0.36	0.534	I	O	|	|	|	2.36
25.917	0.00	0.36	0.531	I	O	|	|	|	2.35
26.000	0.00	0.36	0.529	I	O	|	|	|	2.34
26.083	0.00	0.36	0.526	I	O	|	|	|	2.33
26.167	0.00	0.36	0.524	I	O	|	|	|	2.31
26.250	0.00	0.36	0.522	I	O	|	|	|	2.30
26.333	0.00	0.36	0.519	I	O	|	|	|	2.29
26.417	0.00	0.36	0.517	I	O	|	|	|	2.28
26.500	0.00	0.36	0.514	I	O	|	|	|	2.27
26.583	0.00	0.35	0.512	I	O	|	|	|	2.26
26.667	0.00	0.35	0.509	I	O	|	|	|	2.25
26.750	0.00	0.35	0.507	I	O	|	|	|	2.24
26.833	0.00	0.35	0.504	I	O	|	|	|	2.23
26.917	0.00	0.35	0.502	I	O	|	|	|	2.22
27.000	0.00	0.35	0.500	I	O	|	|	|	2.21
27.083	0.00	0.35	0.497	I	O	|	|	|	2.20
27.167	0.00	0.35	0.495	I	O	|	|	|	2.19
27.250	0.00	0.35	0.492	I	O	|	|	|	2.18
27.333	0.00	0.35	0.490	I	O	|	|	|	2.17
27.417	0.00	0.35	0.488	I	O	|	|	|	2.16
27.500	0.00	0.35	0.485	I	O	|	|	|	2.15
27.583	0.00	0.34	0.483	I	O	|	|	|	2.14
27.667	0.00	0.34	0.480	I	O	|	|	|	2.13
27.750	0.00	0.34	0.478	I	O	|	|	|	2.12
27.833	0.00	0.34	0.476	I	O	|	|	|	2.11
27.917	0.00	0.34	0.473	I	O	|	|	|	2.10
28.000	0.00	0.34	0.471	I	O	|	|	|	2.09
28.083	0.00	0.34	0.469	I	O	|	|	|	2.08
28.167	0.00	0.34	0.466	I	O	|	|	|	2.07
28.250	0.00	0.34	0.464	I	O	|	|	|	2.06
28.333	0.00	0.34	0.462	I	O	|	|	|	2.05
28.417	0.00	0.34	0.459	I	O	|	|	|	2.04
28.500	0.00	0.34	0.457	I	O	|	|	|	2.03
28.583	0.00	0.34	0.455	I	O	|	|	|	2.02
28.667	0.00	0.33	0.452	I	O	|	|	|	2.01
28.750	0.00	0.33	0.450	I	O	|	|	|	2.00
28.833	0.00	0.33	0.448	I	O	|	|	|	1.99
28.917	0.00	0.33	0.445	I	O	|	|	|	1.98
29.000	0.00	0.33	0.443	I	O	|	|	|	1.97
29.083	0.00	0.33	0.441	I	O	|	|	|	1.96
29.167	0.00	0.33	0.439	I	O	|	|	|	1.95
29.250	0.00	0.33	0.436	I	O	|	|	|	1.94
29.333	0.00	0.33	0.434	I	O	|	|	|	1.93
29.417	0.00	0.33	0.432	I	O	|	|	|	1.92

29.500	0.00	0.33	0.430	I	O	|	|	|	1.91
29.583	0.00	0.33	0.427	I	O	|	|	|	1.90
29.667	0.00	0.32	0.425	I	O	|	|	|	1.89
29.750	0.00	0.32	0.423	I	O	|	|	|	1.88
29.833	0.00	0.32	0.421	I	O	|	|	|	1.88
29.917	0.00	0.32	0.418	I	O	|	|	|	1.87
30.000	0.00	0.32	0.416	I	O	|	|	|	1.86
30.083	0.00	0.32	0.414	I	O	|	|	|	1.85
30.167	0.00	0.32	0.412	I	O	|	|	|	1.84
30.250	0.00	0.32	0.410	I	O	|	|	|	1.83
30.333	0.00	0.32	0.407	I	O	|	|	|	1.82
30.417	0.00	0.32	0.405	I	O	|	|	|	1.81
30.500	0.00	0.32	0.403	I	O	|	|	|	1.80
30.583	0.00	0.32	0.401	I	O	|	|	|	1.79
30.667	0.00	0.31	0.399	I	O	|	|	|	1.79
30.750	0.00	0.31	0.397	I	O	|	|	|	1.78
30.833	0.00	0.31	0.394	I	O	|	|	|	1.77
30.917	0.00	0.31	0.392	I	O	|	|	|	1.76
31.000	0.00	0.31	0.390	I	O	|	|	|	1.75
31.083	0.00	0.31	0.388	I	O	|	|	|	1.74
31.167	0.00	0.31	0.386	I	O	|	|	|	1.73
31.250	0.00	0.31	0.384	I	O	|	|	|	1.72
31.333	0.00	0.31	0.382	I	O	|	|	|	1.72
31.417	0.00	0.31	0.379	I	O	|	|	|	1.71
31.500	0.00	0.31	0.377	I	O	|	|	|	1.70
31.583	0.00	0.31	0.375	I	O	|	|	|	1.69
31.667	0.00	0.31	0.373	I	O	|	|	|	1.68
31.750	0.00	0.30	0.371	I	O	|	|	|	1.67
31.833	0.00	0.30	0.369	I	O	|	|	|	1.66
31.917	0.00	0.30	0.367	I	O	|	|	|	1.66
32.000	0.00	0.30	0.365	I	O	|	|	|	1.65
32.083	0.00	0.30	0.363	I	O	|	|	|	1.64
32.167	0.00	0.30	0.361	I	O	|	|	|	1.63
32.250	0.00	0.30	0.359	I	O	|	|	|	1.62
32.333	0.00	0.30	0.356	I	O	|	|	|	1.61
32.417	0.00	0.30	0.354	I	O	|	|	|	1.60
32.500	0.00	0.30	0.352	I	O	|	|	|	1.60
32.583	0.00	0.30	0.350	I	O	|	|	|	1.59
32.667	0.00	0.30	0.348	I	O	|	|	|	1.58
32.750	0.00	0.30	0.346	I	O	|	|	|	1.57
32.833	0.00	0.29	0.344	I	O	|	|	|	1.56
32.917	0.00	0.29	0.342	I	O	|	|	|	1.55
33.000	0.00	0.29	0.340	I	O	|	|	|	1.55
33.083	0.00	0.29	0.338	I	O	|	|	|	1.54
33.167	0.00	0.29	0.336	I	O	|	|	|	1.53
33.250	0.00	0.29	0.334	I	O	|	|	|	1.52
33.333	0.00	0.29	0.332	I	O	|	|	|	1.51
33.417	0.00	0.29	0.330	I	O	|	|	|	1.50
33.500	0.00	0.29	0.328	I	O	|	|	|	1.50
33.583	0.00	0.29	0.326	I	O	|	|	|	1.49
33.667	0.00	0.29	0.324	I	O	|	|	|	1.48
33.750	0.00	0.29	0.322	I	O	|	|	|	1.47
33.833	0.00	0.29	0.320	I	O	|	|	|	1.46
33.917	0.00	0.28	0.318	I	O	|	|	|	1.46
34.000	0.00	0.28	0.316	I	O	|	|	|	1.45
34.083	0.00	0.28	0.314	I	O	|	|	|	1.44
34.167	0.00	0.28	0.312	I	O	|	|	|	1.43
34.250	0.00	0.28	0.310	I	O	|	|	|	1.42
34.333	0.00	0.28	0.309	I	O	|	|	|	1.41
34.417	0.00	0.28	0.307	I	O	|	|	|	1.41
34.500	0.00	0.28	0.305	I	O	|	|	|	1.40
34.583	0.00	0.28	0.303	I	O	|	|	|	1.39
34.667	0.00	0.28	0.301	I	O	|	|	|	1.38
34.750	0.00	0.28	0.299	I	O	|	|	|	1.37
34.833	0.00	0.28	0.297	I	O	|	|	|	1.37
34.917	0.00	0.28	0.295	I	O	|	|	|	1.36
35.000	0.00	0.28	0.293	I	O	|	|	|	1.35
35.083	0.00	0.27	0.291	I	O	|	|	|	1.34
35.167	0.00	0.27	0.289	I	O	|	|	|	1.34
35.250	0.00	0.27	0.288	I	O	|	|	|	1.33
35.333	0.00	0.27	0.286	I	O	|	|	|	1.32
35.417	0.00	0.27	0.284	I	O	|	|	|	1.31

35.500	0.00	0.27	0.282	I	O	|	|	|	| 1.31
35.583	0.00	0.27	0.280	I	O	|	|	|	| 1.30
35.667	0.00	0.27	0.278	I	O	|	|	|	| 1.29
35.750	0.00	0.27	0.276	I	O	|	|	|	| 1.28
35.833	0.00	0.27	0.275	I	O	|	|	|	| 1.28
35.917	0.00	0.27	0.273	I	O	|	|	|	| 1.27
36.000	0.00	0.27	0.271	I	O	|	|	|	| 1.26
36.083	0.00	0.26	0.269	I	O	|	|	|	| 1.25
36.167	0.00	0.26	0.267	I	O	|	|	|	| 1.25
36.250	0.00	0.26	0.265	I	O	|	|	|	| 1.24
36.333	0.00	0.26	0.264	I	O	|	|	|	| 1.23
36.417	0.00	0.26	0.262	I	O	|	|	|	| 1.22
36.500	0.00	0.26	0.260	I	O	|	|	|	| 1.22
36.583	0.00	0.26	0.258	I	O	|	|	|	| 1.21
36.667	0.00	0.26	0.256	I	O	|	|	|	| 1.20
36.750	0.00	0.26	0.255	I	O	|	|	|	| 1.20
36.833	0.00	0.26	0.253	I	O	|	|	|	| 1.19
36.917	0.00	0.26	0.251	I	O	|	|	|	| 1.18
37.000	0.00	0.26	0.249	I	O	|	|	|	| 1.17
37.083	0.00	0.25	0.248	I	O	|	|	|	| 1.17
37.167	0.00	0.25	0.246	I	O	|	|	|	| 1.16
37.250	0.00	0.25	0.244	I	O	|	|	|	| 1.15
37.333	0.00	0.25	0.242	I	O	|	|	|	| 1.15
37.417	0.00	0.25	0.241	I	O	|	|	|	| 1.14
37.500	0.00	0.25	0.239	I	O	|	|	|	| 1.13
37.583	0.00	0.25	0.237	I	O	|	|	|	| 1.13
37.667	0.00	0.25	0.235	I	O	|	|	|	| 1.12
37.750	0.00	0.25	0.234	I	O	|	|	|	| 1.11
37.833	0.00	0.25	0.232	I	O	|	|	|	| 1.10
37.917	0.00	0.25	0.230	I	O	|	|	|	| 1.10
38.000	0.00	0.25	0.229	I	O	|	|	|	| 1.09
38.083	0.00	0.25	0.227	I	O	|	|	|	| 1.08
38.167	0.00	0.24	0.225	I	O	|	|	|	| 1.08
38.250	0.00	0.24	0.224	I	O	|	|	|	| 1.07
38.333	0.00	0.24	0.222	I	O	|	|	|	| 1.06
38.417	0.00	0.24	0.220	I	O	|	|	|	| 1.06
38.500	0.00	0.24	0.219	I	O	|	|	|	| 1.05
38.583	0.00	0.24	0.217	I	O	|	|	|	| 1.04
38.667	0.00	0.24	0.215	I	O	|	|	|	| 1.04
38.750	0.00	0.24	0.214	I	O	|	|	|	| 1.03
38.833	0.00	0.24	0.212	I	O	|	|	|	| 1.02
38.917	0.00	0.24	0.210	I	O	|	|	|	| 1.02
39.000	0.00	0.24	0.209	I	O	|	|	|	| 1.01
39.083	0.00	0.24	0.207	I	O	|	|	|	| 1.00
39.167	0.00	0.24	0.205	I	O	|	|	|	| 1.00
39.250	0.00	0.23	0.204	I	O	|	|	|	| 0.99
39.333	0.00	0.23	0.202	I	O	|	|	|	| 0.98
39.417	0.00	0.23	0.201	I	O	|	|	|	| 0.98
39.500	0.00	0.23	0.199	I	O	|	|	|	| 0.97
39.583	0.00	0.23	0.197	I	O	|	|	|	| 0.97
39.667	0.00	0.23	0.196	I	O	|	|	|	| 0.96
39.750	0.00	0.23	0.194	I	O	|	|	|	| 0.95
39.833	0.00	0.23	0.193	I	O	|	|	|	| 0.95
39.917	0.00	0.23	0.191	I	O	|	|	|	| 0.94
40.000	0.00	0.23	0.189	I	O	|	|	|	| 0.93
40.083	0.00	0.23	0.188	I	O	|	|	|	| 0.93
40.167	0.00	0.23	0.186	I	O	|	|	|	| 0.92
40.250	0.00	0.22	0.185	I	O	|	|	|	| 0.92
40.333	0.00	0.22	0.183	I	O	|	|	|	| 0.91
40.417	0.00	0.22	0.182	I	O	|	|	|	| 0.90
40.500	0.00	0.22	0.180	I	O	|	|	|	| 0.90
40.583	0.00	0.22	0.179	I	O	|	|	|	| 0.89
40.667	0.00	0.22	0.177	I	O	|	|	|	| 0.88
40.750	0.00	0.22	0.176	I	O	|	|	|	| 0.88
40.833	0.00	0.22	0.174	I	O	|	|	|	| 0.87
40.917	0.00	0.22	0.173	I	O	|	|	|	| 0.87
41.000	0.00	0.22	0.171	I	O	|	|	|	| 0.86
41.083	0.00	0.22	0.170	I	O	|	|	|	| 0.85
41.167	0.00	0.22	0.168	I	O	|	|	|	| 0.85
41.250	0.00	0.21	0.167	I	O	|	|	|	| 0.84
41.333	0.00	0.21	0.165	I	O	|	|	|	| 0.84
41.417	0.00	0.21	0.164	I	O	|	|	|	| 0.83

41.500	0.00	0.21	0.162	I O	|	|	|	0.83
41.583	0.00	0.21	0.161	I O	|	|	|	0.82
41.667	0.00	0.21	0.159	I O	|	|	|	0.81
41.750	0.00	0.21	0.158	I O	|	|	|	0.81
41.833	0.00	0.21	0.157	I O	|	|	|	0.80
41.917	0.00	0.21	0.155	I O	|	|	|	0.80
42.000	0.00	0.21	0.154	I O	|	|	|	0.79
42.083	0.00	0.21	0.152	I O	|	|	|	0.78
42.167	0.00	0.21	0.151	I O	|	|	|	0.78
42.250	0.00	0.20	0.149	I O	|	|	|	0.77
42.333	0.00	0.20	0.148	I O	|	|	|	0.77
42.417	0.00	0.20	0.147	I O	|	|	|	0.76
42.500	0.00	0.20	0.145	I O	|	|	|	0.76
42.583	0.00	0.20	0.144	I O	|	|	|	0.75
42.667	0.00	0.20	0.142	I O	|	|	|	0.75
42.750	0.00	0.20	0.141	I O	|	|	|	0.74
42.833	0.00	0.20	0.140	I O	|	|	|	0.73
42.917	0.00	0.20	0.138	I O	|	|	|	0.73
43.000	0.00	0.20	0.137	I O	|	|	|	0.72
43.083	0.00	0.20	0.136	I O	|	|	|	0.72
43.167	0.00	0.20	0.134	I O	|	|	|	0.71
43.250	0.00	0.20	0.133	I O	|	|	|	0.71
43.333	0.00	0.19	0.132	I O	|	|	|	0.70
43.417	0.00	0.19	0.130	I O	|	|	|	0.70
43.500	0.00	0.19	0.129	I O	|	|	|	0.69
43.583	0.00	0.19	0.128	I O	|	|	|	0.69
43.667	0.00	0.19	0.126	I O	|	|	|	0.68
43.750	0.00	0.19	0.125	I O	|	|	|	0.68
43.833	0.00	0.19	0.124	I O	|	|	|	0.67
43.917	0.00	0.19	0.122	I O	|	|	|	0.66
44.000	0.00	0.19	0.121	I O	|	|	|	0.66
44.083	0.00	0.19	0.120	I O	|	|	|	0.65
44.167	0.00	0.19	0.118	I O	|	|	|	0.65
44.250	0.00	0.19	0.117	I O	|	|	|	0.64
44.333	0.00	0.19	0.116	I O	|	|	|	0.64
44.417	0.00	0.19	0.114	I O	|	|	|	0.63
44.500	0.00	0.18	0.113	I O	|	|	|	0.63
44.583	0.00	0.18	0.112	I O	|	|	|	0.62
44.667	0.00	0.18	0.111	I O	|	|	|	0.62
44.750	0.00	0.18	0.109	I O	|	|	|	0.61
44.833	0.00	0.18	0.108	I O	|	|	|	0.61
44.917	0.00	0.18	0.107	I O	|	|	|	0.60
45.000	0.00	0.18	0.106	I O	|	|	|	0.60
45.083	0.00	0.18	0.104	I O	|	|	|	0.59
45.167	0.00	0.18	0.103	I O	|	|	|	0.59
45.250	0.00	0.18	0.102	I O	|	|	|	0.58
45.333	0.00	0.18	0.101	I O	|	|	|	0.58
45.417	0.00	0.18	0.099	I O	|	|	|	0.57
45.500	0.00	0.18	0.098	I O	|	|	|	0.57
45.583	0.00	0.18	0.097	I O	|	|	|	0.56
45.667	0.00	0.18	0.096	I O	|	|	|	0.56
45.750	0.00	0.17	0.095	I O	|	|	|	0.55
45.833	0.00	0.17	0.093	I O	|	|	|	0.55
45.917	0.00	0.17	0.092	I O	|	|	|	0.55
46.000	0.00	0.17	0.091	I O	|	|	|	0.54
46.083	0.00	0.17	0.090	I O	|	|	|	0.54
46.167	0.00	0.17	0.089	I O	|	|	|	0.53
46.250	0.00	0.17	0.088	I O	|	|	|	0.53
46.333	0.00	0.17	0.086	I O	|	|	|	0.52
46.417	0.00	0.17	0.085	I O	|	|	|	0.52
46.500	0.00	0.17	0.084	I O	|	|	|	0.51
46.583	0.00	0.17	0.083	I O	|	|	|	0.51
46.667	0.00	0.17	0.082	I O	|	|	|	0.50
46.750	0.00	0.17	0.081	I O	|	|	|	0.50
46.833	0.00	0.17	0.079	I O	|	|	|	0.49
46.917	0.00	0.16	0.078	I O	|	|	|	0.49
47.000	0.00	0.16	0.077	I O	|	|	|	0.48
47.083	0.00	0.16	0.076	I O	|	|	|	0.48
47.167	0.00	0.16	0.075	I O	|	|	|	0.47
47.250	0.00	0.16	0.074	I O	|	|	|	0.47
47.333	0.00	0.16	0.073	I O	|	|	|	0.47
47.417	0.00	0.16	0.072	I O	|	|	|	0.46

47.500	0.00	0.16	0.070	I O	|	|	|	0.46
47.583	0.00	0.16	0.069	I O	|	|	|	0.45
47.667	0.00	0.16	0.068	I O	|	|	|	0.45
47.750	0.00	0.16	0.067	I O	|	|	|	0.44
47.833	0.00	0.16	0.066	I O	|	|	|	0.44
47.917	0.00	0.16	0.065	I O	|	|	|	0.43
48.000	0.00	0.15	0.064	I O	|	|	|	0.43
48.083	0.00	0.15	0.063	I O	|	|	|	0.43
48.167	0.00	0.15	0.062	I O	|	|	|	0.42
48.250	0.00	0.15	0.061	I O	|	|	|	0.42
48.333	0.00	0.15	0.060	I O	|	|	|	0.41
48.417	0.00	0.15	0.059	I O	|	|	|	0.41
48.500	0.00	0.15	0.058	I O	|	|	|	0.40
48.583	0.00	0.15	0.057	I O	|	|	|	0.40
48.667	0.00	0.15	0.056	I O	|	|	|	0.40
48.750	0.00	0.15	0.055	I O	|	|	|	0.39
48.833	0.00	0.15	0.054	I O	|	|	|	0.39
48.917	0.00	0.15	0.053	I O	|	|	|	0.38
49.000	0.00	0.15	0.052	IO	|	|	|	0.38
49.083	0.00	0.14	0.051	IO	|	|	|	0.38
49.167	0.00	0.14	0.050	IO	|	|	|	0.37
49.250	0.00	0.14	0.049	IO	|	|	|	0.37
49.333	0.00	0.14	0.048	IO	|	|	|	0.36
49.417	0.00	0.14	0.047	IO	|	|	|	0.36
49.500	0.00	0.14	0.046	IO	|	|	|	0.36
49.583	0.00	0.14	0.045	IO	|	|	|	0.35
49.667	0.00	0.14	0.044	IO	|	|	|	0.35
49.750	0.00	0.14	0.043	IO	|	|	|	0.34
49.833	0.00	0.14	0.042	IO	|	|	|	0.34
49.917	0.00	0.14	0.041	IO	|	|	|	0.34
50.000	0.00	0.14	0.040	IO	|	|	|	0.33
50.083	0.00	0.14	0.039	IO	|	|	|	0.33
50.167	0.00	0.13	0.038	IO	|	|	|	0.32
50.250	0.00	0.13	0.037	IO	|	|	|	0.32
50.333	0.00	0.13	0.036	IO	|	|	|	0.31
50.417	0.00	0.13	0.035	IO	|	|	|	0.31
50.500	0.00	0.13	0.034	IO	|	|	|	0.31
50.583	0.00	0.13	0.034	IO	|	|	|	0.30
50.667	0.00	0.13	0.033	IO	|	|	|	0.30
50.750	0.00	0.13	0.032	IO	|	|	|	0.29
50.833	0.00	0.13	0.031	IO	|	|	|	0.29
50.917	0.00	0.13	0.030	IO	|	|	|	0.29
51.000	0.00	0.13	0.029	IO	|	|	|	0.28
51.083	0.00	0.12	0.028	IO	|	|	|	0.28
51.167	0.00	0.12	0.027	IO	|	|	|	0.27
51.250	0.00	0.12	0.027	IO	|	|	|	0.27
51.333	0.00	0.12	0.026	IO	|	|	|	0.27
51.417	0.00	0.12	0.025	IO	|	|	|	0.26
51.500	0.00	0.12	0.024	IO	|	|	|	0.26
51.583	0.00	0.12	0.023	IO	|	|	|	0.26
51.667	0.00	0.12	0.022	IO	|	|	|	0.25
51.750	0.00	0.12	0.022	IO	|	|	|	0.25
51.833	0.00	0.11	0.021	IO	|	|	|	0.24
51.917	0.00	0.11	0.020	IO	|	|	|	0.23
52.000	0.00	0.10	0.019	IO	|	|	|	0.22
52.083	0.00	0.10	0.019	IO	|	|	|	0.21
52.167	0.00	0.10	0.018	IO	|	|	|	0.20
52.250	0.00	0.09	0.017	IO	|	|	|	0.20
52.333	0.00	0.09	0.017	IO	|	|	|	0.19
52.417	0.00	0.09	0.016	IO	|	|	|	0.18
52.500	0.00	0.08	0.016	IO	|	|	|	0.18
52.583	0.00	0.08	0.015	IO	|	|	|	0.17
52.667	0.00	0.08	0.014	IO	|	|	|	0.16
52.750	0.00	0.07	0.014	IO	|	|	|	0.16
52.833	0.00	0.07	0.013	O	|	|	|	0.15
52.917	0.00	0.07	0.013	O	|	|	|	0.15
53.000	0.00	0.07	0.012	O	|	|	|	0.14
53.083	0.00	0.06	0.012	O	|	|	|	0.14
53.167	0.00	0.06	0.012	O	|	|	|	0.13
53.250	0.00	0.06	0.011	O	|	|	|	0.13
53.333	0.00	0.06	0.011	O	|	|	|	0.12
53.417	0.00	0.06	0.010	O	|	|	|	0.12

53.500	0.00	0.05	0.010	O	|	|	|	0.11
53.583	0.00	0.05	0.010	O	|	|	|	0.11
53.667	0.00	0.05	0.009	O	|	|	|	0.11
53.750	0.00	0.05	0.009	O	|	|	|	0.10
53.833	0.00	0.05	0.009	O	|	|	|	0.10
53.917	0.00	0.04	0.008	O	|	|	|	0.09
54.000	0.00	0.04	0.008	O	|	|	|	0.09
54.083	0.00	0.04	0.008	O	|	|	|	0.09
54.167	0.00	0.04	0.007	O	|	|	|	0.08
54.250	0.00	0.04	0.007	O	|	|	|	0.08
54.333	0.00	0.04	0.007	O	|	|	|	0.08
54.417	0.00	0.04	0.007	O	|	|	|	0.08
54.500	0.00	0.03	0.006	O	|	|	|	0.07
54.583	0.00	0.03	0.006	O	|	|	|	0.07
54.667	0.00	0.03	0.006	O	|	|	|	0.07
54.750	0.00	0.03	0.006	O	|	|	|	0.07
54.833	0.00	0.03	0.006	O	|	|	|	0.06
54.917	0.00	0.03	0.005	O	|	|	|	0.06
55.000	0.00	0.03	0.005	O	|	|	|	0.06
55.083	0.00	0.03	0.005	O	|	|	|	0.06
55.167	0.00	0.03	0.005	O	|	|	|	0.05
55.250	0.00	0.02	0.005	O	|	|	|	0.05
55.333	0.00	0.02	0.004	O	|	|	|	0.05
55.417	0.00	0.02	0.004	O	|	|	|	0.05
55.500	0.00	0.02	0.004	O	|	|	|	0.05
55.583	0.00	0.02	0.004	O	|	|	|	0.05
55.667	0.00	0.02	0.004	O	|	|	|	0.04
55.750	0.00	0.02	0.004	O	|	|	|	0.04
55.833	0.00	0.02	0.004	O	|	|	|	0.04
55.917	0.00	0.02	0.003	O	|	|	|	0.04
56.000	0.00	0.02	0.003	O	|	|	|	0.04
56.083	0.00	0.02	0.003	O	|	|	|	0.04
56.167	0.00	0.02	0.003	O	|	|	|	0.03
56.250	0.00	0.02	0.003	O	|	|	|	0.03
56.333	0.00	0.02	0.003	O	|	|	|	0.03
56.417	0.00	0.01	0.003	O	|	|	|	0.03
56.500	0.00	0.01	0.003	O	|	|	|	0.03
56.583	0.00	0.01	0.003	O	|	|	|	0.03
56.667	0.00	0.01	0.002	O	|	|	|	0.03
56.750	0.00	0.01	0.002	O	|	|	|	0.03
56.833	0.00	0.01	0.002	O	|	|	|	0.03
56.917	0.00	0.01	0.002	O	|	|	|	0.02
57.000	0.00	0.01	0.002	O	|	|	|	0.02
57.083	0.00	0.01	0.002	O	|	|	|	0.02
57.167	0.00	0.01	0.002	O	|	|	|	0.02
57.250	0.00	0.01	0.002	O	|	|	|	0.02
57.333	0.00	0.01	0.002	O	|	|	|	0.02
57.417	0.00	0.01	0.002	O	|	|	|	0.02
57.500	0.00	0.01	0.002	O	|	|	|	0.02
57.583	0.00	0.01	0.002	O	|	|	|	0.02
57.667	0.00	0.01	0.002	O	|	|	|	0.02
57.750	0.00	0.01	0.002	O	|	|	|	0.02
57.833	0.00	0.01	0.001	O	|	|	|	0.02
57.917	0.00	0.01	0.001	O	|	|	|	0.02
58.000	0.00	0.01	0.001	O	|	|	|	0.02
58.083	0.00	0.01	0.001	O	|	|	|	0.01
58.167	0.00	0.01	0.001	O	|	|	|	0.01
58.250	0.00	0.01	0.001	O	|	|	|	0.01
58.333	0.00	0.01	0.001	O	|	|	|	0.01
58.417	0.00	0.01	0.001	O	|	|	|	0.01
58.500	0.00	0.01	0.001	O	|	|	|	0.01
58.583	0.00	0.01	0.001	O	|	|	|	0.01
58.667	0.00	0.01	0.001	O	|	|	|	0.01
58.750	0.00	0.01	0.001	O	|	|	|	0.01
58.833	0.00	0.01	0.001	O	|	|	|	0.01
58.917	0.00	0.00	0.001	O	|	|	|	0.01
59.000	0.00	0.00	0.001	O	|	|	|	0.01
59.083	0.00	0.00	0.001	O	|	|	|	0.01
59.167	0.00	0.00	0.001	O	|	|	|	0.01
59.250	0.00	0.00	0.001	O	|	|	|	0.01
59.333	0.00	0.00	0.001	O	|	|	|	0.01
59.417	0.00	0.00	0.001	O	|	|	|	0.01

59.500	0.00	0.00	0.001	O	|	|	|	|	0.01
59.583	0.00	0.00	0.001	O	|	|	|	|	0.01
59.667	0.00	0.00	0.001	O	|	|	|	|	0.01
59.750	0.00	0.00	0.001	O	|	|	|	|	0.01
59.833	0.00	0.00	0.001	O	|	|	|	|	0.01
59.917	0.00	0.00	0.001	O	|	|	|	|	0.01
60.000	0.00	0.00	0.001	O	|	|	|	|	0.01
60.083	0.00	0.00	0.001	O	|	|	|	|	0.01
60.167	0.00	0.00	0.001	O	|	|	|	|	0.01
60.250	0.00	0.00	0.001	O	|	|	|	|	0.01
60.333	0.00	0.00	0.000	O	|	|	|	|	0.01
60.417	0.00	0.00	0.000	O	|	|	|	|	0.01
60.500	0.00	0.00	0.000	O	|	|	|	|	0.01
60.583	0.00	0.00	0.000	O	|	|	|	|	0.00
60.667	0.00	0.00	0.000	O	|	|	|	|	0.00
60.750	0.00	0.00	0.000	O	|	|	|	|	0.00
60.833	0.00	0.00	0.000	O	|	|	|	|	0.00
60.917	0.00	0.00	0.000	O	|	|	|	|	0.00
61.000	0.00	0.00	0.000	O	|	|	|	|	0.00
61.083	0.00	0.00	0.000	O	|	|	|	|	0.00
61.167	0.00	0.00	0.000	O	|	|	|	|	0.00
61.250	0.00	0.00	0.000	O	|	|	|	|	0.00
61.333	0.00	0.00	0.000	O	|	|	|	|	0.00
61.417	0.00	0.00	0.000	O	|	|	|	|	0.00
61.500	0.00	0.00	0.000	O	|	|	|	|	0.00
61.583	0.00	0.00	0.000	O	|	|	|	|	0.00
61.667	0.00	0.00	0.000	O	|	|	|	|	0.00
61.750	0.00	0.00	0.000	O	|	|	|	|	0.00
61.833	0.00	0.00	0.000	O	|	|	|	|	0.00
61.917	0.00	0.00	0.000	O	|	|	|	|	0.00
62.000	0.00	0.00	0.000	O	|	|	|	|	0.00
62.083	0.00	0.00	0.000	O	|	|	|	|	0.00
62.167	0.00	0.00	0.000	O	|	|	|	|	0.00
62.250	0.00	0.00	0.000	O	|	|	|	|	0.00
62.333	0.00	0.00	0.000	O	|	|	|	|	0.00
62.417	0.00	0.00	0.000	O	|	|	|	|	0.00
62.500	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 750
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.539 (CFS)
Total volume = 1.384 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
6-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA10610.rte
**********HYDROGRAPH DATA**********
Number of intervals = 74
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 5.954 (CFS)
Total volume = 0.722 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 74
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.5 2.98 4.47 5.95	Depth (Ft.)
0.083	0.30	0.01	0.001	OI	0.01
0.167	0.54	0.02	0.004	O I	0.04
0.250	0.61	0.04	0.008	O I	0.09
0.333	0.61	0.06	0.011	O I	0.13
0.417	0.61	0.08	0.015	O I	0.17
0.500	0.67	0.10	0.019	O I	0.22
0.583	0.71	0.12	0.023	O I	0.25
0.667	0.72	0.12	0.027	O I	0.27
0.750	0.72	0.13	0.031	O I	0.29
0.833	0.72	0.13	0.035	O I	0.31
0.917	0.72	0.14	0.039	O I	0.33
1.000	0.77	0.14	0.043	O I	0.35
1.083	0.81	0.14	0.048	O I	0.36
1.167	0.82	0.15	0.052	O I	0.38
1.250	0.82	0.15	0.057	O I	0.40
1.333	0.82	0.15	0.062	O I	0.42
1.417	0.82	0.16	0.066	O I	0.44
1.500	0.82	0.16	0.071	O I	0.46
1.583	0.82	0.16	0.075	O I	0.48
1.667	0.82	0.17	0.080	O I	0.50
1.750	0.82	0.17	0.084	O I	0.51
1.833	0.82	0.17	0.089	O I	0.53
1.917	0.82	0.17	0.093	O I	0.55
2.000	0.88	0.18	0.098	O I	0.57
2.083	0.86	0.18	0.103	O I	0.59
2.167	0.88	0.18	0.107	O I	0.61
2.250	0.91	0.18	0.112	O I	0.62
2.333	0.92	0.19	0.117	|O I	0.65
2.417	0.92	0.19	0.122	|O I	0.67
2.500	0.92	0.19	0.127	|O I	0.69
2.583	0.92	0.20	0.132	|O I	0.71
2.667	0.92	0.20	0.137	|O I	0.73
2.750	0.98	0.20	0.142	|O I	0.75
2.833	1.02	0.20	0.148	|O I	0.77
2.917	1.02	0.21	0.154	|O I	0.79
3.000	1.02	0.21	0.159	|O I	0.81
3.083	1.02	0.21	0.165	|O I	0.83
3.167	1.08	0.22	0.171	|O I	0.86
3.250	1.12	0.22	0.177	|O I	0.88
3.333	1.12	0.22	0.183	|O I	0.91
3.417	1.18	0.23	0.189	|O I	0.93
3.500	1.28	0.23	0.196	|O I	0.96
3.583	1.38	0.23	0.204	|O I	0.99
3.667	1.43	0.24	0.212	|O I	1.02
3.750	1.49	0.24	0.220	|O I	1.06
3.833	1.53	0.25	0.229	|O I	1.09
3.917	1.59	0.25	0.238	|O I	1.13
4.000	1.63	0.25	0.247	|O I	1.17
4.083	1.69	0.26	0.257	|O I	1.20
4.167	1.79	0.26	0.267	|O I	1.25
4.250	1.89	0.27	0.278	|O I	1.29
4.333	2.00	0.27	0.289	|O I	1.34
4.417	2.10	0.28	0.302	|O I	1.39
4.500	2.14	0.28	0.314	|O I	1.44
4.583	2.21	0.29	0.327	|O I	1.49
4.667	2.30	0.29	0.341	|O I	1.55
4.750	2.42	0.30	0.355	|O I	1.61
4.833	2.47	0.30	0.370	|O I	1.67
4.917	2.54	0.31	0.385	|O I	1.73
5.000	2.66	0.32	0.401	|O I	1.79
5.083	3.08	0.32	0.418	|O I	1.87
5.167	3.67	0.33	0.439	|O I	1.95
5.250	4.15	0.34	0.464	|O I	2.06
5.333	4.54	0.35	0.491	|O I	2.17
5.417	5.06	0.36	0.522	|O I	2.31

5.500	5.95	0.37	0.557	O			I	2.46
5.583	3.79	0.38	0.588	O		I		2.60
5.667	1.61	0.39	0.604	O	I			2.67
5.750	0.80	0.39	0.610	O I				2.70
5.833	0.57	0.39	0.612	OI				2.70
5.917	0.40	0.39	0.613	O				2.71
6.000	0.26	0.39	0.612	IO				2.71
6.083	0.09	0.39	0.611	I O				2.70
6.167	0.01	0.39	0.608	I O				2.69
6.250	0.00	0.39	0.606	I O				2.68
6.333	0.00	0.39	0.603	I O				2.66
6.417	0.00	0.38	0.601	I O				2.65
6.500	0.00	0.38	0.598	I O				2.64
6.583	0.00	0.38	0.595	I O				2.63
6.667	0.00	0.38	0.593	I O				2.62
6.750	0.00	0.38	0.590	I O				2.60
6.833	0.00	0.38	0.587	I O				2.59
6.917	0.00	0.38	0.585	I O				2.58
7.000	0.00	0.38	0.582	I O				2.57
7.083	0.00	0.38	0.580	I O				2.56
7.167	0.00	0.38	0.577	I O				2.55
7.250	0.00	0.38	0.574	I O				2.53
7.333	0.00	0.38	0.572	I O				2.52
7.417	0.00	0.37	0.569	I O				2.51
7.500	0.00	0.37	0.567	I O				2.50
7.583	0.00	0.37	0.564	I O				2.49
7.667	0.00	0.37	0.561	IO				2.48
7.750	0.00	0.37	0.559	IO				2.47
7.833	0.00	0.37	0.556	IO				2.45
7.917	0.00	0.37	0.554	IO				2.44
8.000	0.00	0.37	0.551	IO				2.43
8.083	0.00	0.37	0.549	IO				2.42
8.167	0.00	0.37	0.546	IO				2.41
8.250	0.00	0.37	0.544	IO				2.40
8.333	0.00	0.37	0.541	IO				2.39
8.417	0.00	0.36	0.539	IO				2.38
8.500	0.00	0.36	0.536	IO				2.37
8.583	0.00	0.36	0.534	IO				2.36
8.667	0.00	0.36	0.531	IO				2.35
8.750	0.00	0.36	0.529	IO				2.33
8.833	0.00	0.36	0.526	IO				2.32
8.917	0.00	0.36	0.524	IO				2.31
9.000	0.00	0.36	0.521	IO				2.30
9.083	0.00	0.36	0.519	IO				2.29
9.167	0.00	0.36	0.516	IO				2.28
9.250	0.00	0.36	0.514	IO				2.27
9.333	0.00	0.35	0.511	IO				2.26
9.417	0.00	0.35	0.509	IO				2.25
9.500	0.00	0.35	0.507	IO				2.24
9.583	0.00	0.35	0.504	IO				2.23
9.667	0.00	0.35	0.502	IO				2.22
9.750	0.00	0.35	0.499	IO				2.21
9.833	0.00	0.35	0.497	IO				2.20
9.917	0.00	0.35	0.494	IO				2.19
10.000	0.00	0.35	0.492	IO				2.18
10.083	0.00	0.35	0.490	IO				2.17
10.167	0.00	0.35	0.487	IO				2.16
10.250	0.00	0.35	0.485	IO				2.15
10.333	0.00	0.34	0.482	IO				2.14
10.417	0.00	0.34	0.480	IO				2.13
10.500	0.00	0.34	0.478	IO				2.12
10.583	0.00	0.34	0.475	IO				2.11
10.667	0.00	0.34	0.473	IO				2.09
10.750	0.00	0.34	0.471	IO				2.08
10.833	0.00	0.34	0.468	IO				2.07
10.917	0.00	0.34	0.466	IO				2.06
11.000	0.00	0.34	0.464	IO				2.05
11.083	0.00	0.34	0.461	IO				2.04
11.167	0.00	0.34	0.459	IO				2.03
11.250	0.00	0.34	0.457	IO				2.02
11.333	0.00	0.34	0.454	IO				2.01
11.417	0.00	0.33	0.452	IO				2.00

11.500	0.00	0.33	0.450	IO				2.00
11.583	0.00	0.33	0.447	IO				1.99
11.667	0.00	0.33	0.445	IO				1.98
11.750	0.00	0.33	0.443	IO				1.97
11.833	0.00	0.33	0.441	IO				1.96
11.917	0.00	0.33	0.438	IO				1.95
12.000	0.00	0.33	0.436	IO				1.94
12.083	0.00	0.33	0.434	IO				1.93
12.167	0.00	0.33	0.432	IO				1.92
12.250	0.00	0.33	0.429	IO				1.91
12.333	0.00	0.33	0.427	IO				1.90
12.417	0.00	0.32	0.425	IO				1.89
12.500	0.00	0.32	0.423	IO				1.88
12.583	0.00	0.32	0.420	IO				1.87
12.667	0.00	0.32	0.418	IO				1.87
12.750	0.00	0.32	0.416	IO				1.86
12.833	0.00	0.32	0.414	IO				1.85
12.917	0.00	0.32	0.412	IO				1.84
13.000	0.00	0.32	0.409	IO				1.83
13.083	0.00	0.32	0.407	IO				1.82
13.167	0.00	0.32	0.405	IO				1.81
13.250	0.00	0.32	0.403	IO				1.80
13.333	0.00	0.32	0.401	IO				1.79
13.417	0.00	0.31	0.398	IO				1.78
13.500	0.00	0.31	0.396	IO				1.78
13.583	0.00	0.31	0.394	IO				1.77
13.667	0.00	0.31	0.392	IO				1.76
13.750	0.00	0.31	0.390	IO				1.75
13.833	0.00	0.31	0.388	IO				1.74
13.917	0.00	0.31	0.386	IO				1.73
14.000	0.00	0.31	0.383	IO				1.72
14.083	0.00	0.31	0.381	IO				1.71
14.167	0.00	0.31	0.379	IO				1.71
14.250	0.00	0.31	0.377	IO				1.70
14.333	0.00	0.31	0.375	IO				1.69
14.417	0.00	0.31	0.373	IO				1.68
14.500	0.00	0.30	0.371	IO				1.67
14.583	0.00	0.30	0.369	IO				1.66
14.667	0.00	0.30	0.367	IO				1.65
14.750	0.00	0.30	0.364	IO				1.65
14.833	0.00	0.30	0.362	IO				1.64
14.917	0.00	0.30	0.360	IO				1.63
15.000	0.00	0.30	0.358	IO				1.62
15.083	0.00	0.30	0.356	IO				1.61
15.167	0.00	0.30	0.354	IO				1.60
15.250	0.00	0.30	0.352	IO				1.59
15.333	0.00	0.30	0.350	IO				1.59
15.417	0.00	0.30	0.348	IO				1.58
15.500	0.00	0.30	0.346	IO				1.57
15.583	0.00	0.29	0.344	IO				1.56
15.667	0.00	0.29	0.342	IO				1.55
15.750	0.00	0.29	0.340	IO				1.54
15.833	0.00	0.29	0.338	IO				1.54
15.917	0.00	0.29	0.336	IO				1.53
16.000	0.00	0.29	0.334	IO				1.52
16.083	0.00	0.29	0.332	IO				1.51
16.167	0.00	0.29	0.330	IO				1.50
16.250	0.00	0.29	0.328	IO				1.50
16.333	0.00	0.29	0.326	IO				1.49
16.417	0.00	0.29	0.324	IO				1.48
16.500	0.00	0.29	0.322	IO				1.47
16.583	0.00	0.29	0.320	IO				1.46
16.667	0.00	0.28	0.318	IO				1.45
16.750	0.00	0.28	0.316	IO				1.45
16.833	0.00	0.28	0.314	IO				1.44
16.917	0.00	0.28	0.312	IO				1.43
17.000	0.00	0.28	0.310	IO				1.42
17.083	0.00	0.28	0.308	IO				1.41
17.167	0.00	0.28	0.306	IO				1.41
17.250	0.00	0.28	0.304	IO				1.40
17.333	0.00	0.28	0.302	IO				1.39
17.417	0.00	0.28	0.301	IO				1.38

17.500	0.00	0.28	0.299	IO				1.37
17.583	0.00	0.28	0.297	IO				1.37
17.667	0.00	0.28	0.295	IO				1.36
17.750	0.00	0.27	0.293	IO				1.35
17.833	0.00	0.27	0.291	IO				1.34
17.917	0.00	0.27	0.289	IO				1.33
18.000	0.00	0.27	0.287	IO				1.33
18.083	0.00	0.27	0.285	IO				1.32
18.167	0.00	0.27	0.284	IO				1.31
18.250	0.00	0.27	0.282	IO				1.30
18.333	0.00	0.27	0.280	IO				1.30
18.417	0.00	0.27	0.278	IO				1.29
18.500	0.00	0.27	0.276	IO				1.28
18.583	0.00	0.27	0.274	IO				1.27
18.667	0.00	0.27	0.272	IO				1.27
18.750	0.00	0.26	0.271	IO				1.26
18.833	0.00	0.26	0.269	IO				1.25
18.917	0.00	0.26	0.267	IO				1.25
19.000	0.00	0.26	0.265	IO				1.24
19.083	0.00	0.26	0.263	IO				1.23
19.167	0.00	0.26	0.262	IO				1.22
19.250	0.00	0.26	0.260	IO				1.22
19.333	0.00	0.26	0.258	IO				1.21
19.417	0.00	0.26	0.256	IO				1.20
19.500	0.00	0.26	0.254	IO				1.19
19.583	0.00	0.26	0.253	IO				1.19
19.667	0.00	0.26	0.251	IO				1.18
19.750	0.00	0.26	0.249	IO				1.17
19.833	0.00	0.25	0.247	IO				1.17
19.917	0.00	0.25	0.246	IO				1.16
20.000	0.00	0.25	0.244	IO				1.15
20.083	0.00	0.25	0.242	IO				1.15
20.167	0.00	0.25	0.240	IO				1.14
20.250	0.00	0.25	0.239	IO				1.13
20.333	0.00	0.25	0.237	IO				1.12
20.417	0.00	0.25	0.235	IO				1.12
20.500	0.00	0.25	0.234	IO				1.11
20.583	0.00	0.25	0.232	IO				1.10
20.667	0.00	0.25	0.230	IO				1.10
20.750	0.00	0.25	0.228	IO				1.09
20.833	0.00	0.25	0.227	IO				1.08
20.917	0.00	0.24	0.225	IO				1.08
21.000	0.00	0.24	0.223	IO				1.07
21.083	0.00	0.24	0.222	IO				1.06
21.167	0.00	0.24	0.220	IO				1.06
21.250	0.00	0.24	0.218	IO				1.05
21.333	0.00	0.24	0.217	IO				1.04
21.417	0.00	0.24	0.215	IO				1.04
21.500	0.00	0.24	0.213	IO				1.03
21.583	0.00	0.24	0.212	IO				1.02
21.667	0.00	0.24	0.210	IO				1.02
21.750	0.00	0.24	0.208	IO				1.01
21.833	0.00	0.24	0.207	IO				1.00
21.917	0.00	0.24	0.205	IO				1.00
22.000	0.00	0.23	0.204	IO				0.99
22.083	0.00	0.23	0.202	IO				0.98
22.167	0.00	0.23	0.200	IO				0.98
22.250	0.00	0.23	0.199	IO				0.97
22.333	0.00	0.23	0.197	IO				0.96
22.417	0.00	0.23	0.196	IO				0.96
22.500	0.00	0.23	0.194	IO				0.95
22.583	0.00	0.23	0.192	IO				0.95
22.667	0.00	0.23	0.191	IO				0.94
22.750	0.00	0.23	0.189	IO				0.93
22.833	0.00	0.23	0.188	IO				0.93
22.917	0.00	0.23	0.186	IO				0.92
23.000	0.00	0.22	0.185	IO				0.91
23.083	0.00	0.22	0.183	IO				0.91
23.167	0.00	0.22	0.182	IO				0.90
23.250	0.00	0.22	0.180	IO				0.90
23.333	0.00	0.22	0.179	IO				0.89
23.417	0.00	0.22	0.177	IO				0.88

23.500	0.00	0.22	0.175	IO				0.88
23.583	0.00	0.22	0.174	IO				0.87
23.667	0.00	0.22	0.172	IO				0.87
23.750	0.00	0.22	0.171	IO				0.86
23.833	0.00	0.22	0.169	IO				0.85
23.917	0.00	0.22	0.168	IO				0.85
24.000	0.00	0.21	0.167	IO				0.84
24.083	0.00	0.21	0.165	IO				0.84
24.167	0.00	0.21	0.164	IO				0.83
24.250	0.00	0.21	0.162	IO				0.82
24.333	0.00	0.21	0.161	IO				0.82
24.417	0.00	0.21	0.159	IO				0.81
24.500	0.00	0.21	0.158	IO				0.81
24.583	0.00	0.21	0.156	IO				0.80
24.667	0.00	0.21	0.155	IO				0.80
24.750	0.00	0.21	0.153	IO				0.79
24.833	0.00	0.21	0.152	IO				0.78
24.917	0.00	0.21	0.151	IO				0.78
25.000	0.00	0.20	0.149	IO				0.77
25.083	0.00	0.20	0.148	IO				0.77
25.167	0.00	0.20	0.146	IO				0.76
25.250	0.00	0.20	0.145	IO				0.76
25.333	0.00	0.20	0.144	IO				0.75
25.417	0.00	0.20	0.142	IO				0.74
25.500	0.00	0.20	0.141	IO				0.74
25.583	0.00	0.20	0.139	IO				0.73
25.667	0.00	0.20	0.138	IO				0.73
25.750	0.00	0.20	0.137	IO				0.72
25.833	0.00	0.20	0.135	IO				0.72
25.917	0.00	0.20	0.134	IO				0.71
26.000	0.00	0.20	0.133	IO				0.71
26.083	0.00	0.19	0.131	IO				0.70
26.167	0.00	0.19	0.130	IO				0.70
26.250	0.00	0.19	0.129	IO				0.69
26.333	0.00	0.19	0.127	IO				0.69
26.417	0.00	0.19	0.126	IO				0.68
26.500	0.00	0.19	0.125	IO				0.67
26.583	0.00	0.19	0.123	IO				0.67
26.667	0.00	0.19	0.122	IO				0.66
26.750	0.00	0.19	0.121	IO				0.66
26.833	0.00	0.19	0.119	IO				0.65
26.917	0.00	0.19	0.118	IO				0.65
27.000	0.00	0.19	0.117	IO				0.64
27.083	0.00	0.19	0.116	IO				0.64
27.167	0.00	0.19	0.114	O				0.63
27.250	0.00	0.18	0.113	O				0.63
27.333	0.00	0.18	0.112	O				0.62
27.417	0.00	0.18	0.111	O				0.62
27.500	0.00	0.18	0.109	O				0.61
27.583	0.00	0.18	0.108	O				0.61
27.667	0.00	0.18	0.107	O				0.60
27.750	0.00	0.18	0.106	O				0.60
27.833	0.00	0.18	0.104	O				0.59
27.917	0.00	0.18	0.103	O				0.59
28.000	0.00	0.18	0.102	O				0.58
28.083	0.00	0.18	0.101	O				0.58
28.167	0.00	0.18	0.099	O				0.57
28.250	0.00	0.18	0.098	O				0.57
28.333	0.00	0.18	0.097	O				0.56
28.417	0.00	0.18	0.096	O				0.56
28.500	0.00	0.17	0.095	O				0.55
28.583	0.00	0.17	0.093	O				0.55
28.667	0.00	0.17	0.092	O				0.54
28.750	0.00	0.17	0.091	O				0.54
28.833	0.00	0.17	0.090	O				0.53
28.917	0.00	0.17	0.089	O				0.53
29.000	0.00	0.17	0.087	O				0.53
29.083	0.00	0.17	0.086	O				0.52
29.167	0.00	0.17	0.085	O				0.52
29.250	0.00	0.17	0.084	O				0.51
29.333	0.00	0.17	0.083	O				0.51
29.417	0.00	0.17	0.082	O				0.50

29.500	0.00	0.17	0.080	O	|	|	|	0.50
29.583	0.00	0.17	0.079	O	|	|	|	0.49
29.667	0.00	0.16	0.078	O	|	|	|	0.49
29.750	0.00	0.16	0.077	O	|	|	|	0.48
29.833	0.00	0.16	0.076	O	|	|	|	0.48
29.917	0.00	0.16	0.075	O	|	|	|	0.47
30.000	0.00	0.16	0.074	O	|	|	|	0.47
30.083	0.00	0.16	0.073	O	|	|	|	0.47
30.167	0.00	0.16	0.071	O	|	|	|	0.46
30.250	0.00	0.16	0.070	O	|	|	|	0.46
30.333	0.00	0.16	0.069	O	|	|	|	0.45
30.417	0.00	0.16	0.068	O	|	|	|	0.45
30.500	0.00	0.16	0.067	O	|	|	|	0.44
30.583	0.00	0.16	0.066	O	|	|	|	0.44
30.667	0.00	0.16	0.065	O	|	|	|	0.43
30.750	0.00	0.15	0.064	O	|	|	|	0.43
30.833	0.00	0.15	0.063	O	|	|	|	0.43
30.917	0.00	0.15	0.062	O	|	|	|	0.42
31.000	0.00	0.15	0.061	O	|	|	|	0.42
31.083	0.00	0.15	0.060	O	|	|	|	0.41
31.167	0.00	0.15	0.059	O	|	|	|	0.41
31.250	0.00	0.15	0.058	O	|	|	|	0.40
31.333	0.00	0.15	0.057	O	|	|	|	0.40
31.417	0.00	0.15	0.056	O	|	|	|	0.40
31.500	0.00	0.15	0.055	O	|	|	|	0.39
31.583	0.00	0.15	0.053	O	|	|	|	0.39
31.667	0.00	0.15	0.052	O	|	|	|	0.38
31.750	0.00	0.15	0.051	O	|	|	|	0.38
31.833	0.00	0.14	0.050	O	|	|	|	0.37
31.917	0.00	0.14	0.049	O	|	|	|	0.37
32.000	0.00	0.14	0.049	O	|	|	|	0.37
32.083	0.00	0.14	0.048	O	|	|	|	0.36
32.167	0.00	0.14	0.047	O	|	|	|	0.36
32.250	0.00	0.14	0.046	O	|	|	|	0.35
32.333	0.00	0.14	0.045	O	|	|	|	0.35
32.417	0.00	0.14	0.044	O	|	|	|	0.35
32.500	0.00	0.14	0.043	O	|	|	|	0.34
32.583	0.00	0.14	0.042	O	|	|	|	0.34
32.667	0.00	0.14	0.041	O	|	|	|	0.33
32.750	0.00	0.14	0.040	O	|	|	|	0.33
32.833	0.00	0.13	0.039	O	|	|	|	0.33
32.917	0.00	0.13	0.038	O	|	|	|	0.32
33.000	0.00	0.13	0.037	O	|	|	|	0.32
33.083	0.00	0.13	0.036	O	|	|	|	0.31
33.167	0.00	0.13	0.035	O	|	|	|	0.31
33.250	0.00	0.13	0.034	O	|	|	|	0.31
33.333	0.00	0.13	0.033	O	|	|	|	0.30
33.417	0.00	0.13	0.033	O	|	|	|	0.30
33.500	0.00	0.13	0.032	O	|	|	|	0.29
33.583	0.00	0.13	0.031	O	|	|	|	0.29
33.667	0.00	0.13	0.030	O	|	|	|	0.29
33.750	0.00	0.13	0.029	O	|	|	|	0.28
33.833	0.00	0.12	0.028	O	|	|	|	0.28
33.917	0.00	0.12	0.027	O	|	|	|	0.27
34.000	0.00	0.12	0.027	O	|	|	|	0.27
34.083	0.00	0.12	0.026	O	|	|	|	0.27
34.167	0.00	0.12	0.025	O	|	|	|	0.26
34.250	0.00	0.12	0.024	O	|	|	|	0.26
34.333	0.00	0.12	0.023	O	|	|	|	0.26
34.417	0.00	0.12	0.022	O	|	|	|	0.25
34.500	0.00	0.12	0.022	O	|	|	|	0.25
34.583	0.00	0.11	0.021	O	|	|	|	0.24
34.667	0.00	0.11	0.020	O	|	|	|	0.23
34.750	0.00	0.10	0.019	O	|	|	|	0.22
34.833	0.00	0.10	0.019	O	|	|	|	0.21
34.917	0.00	0.10	0.018	O	|	|	|	0.20
35.000	0.00	0.09	0.017	O	|	|	|	0.20
35.083	0.00	0.09	0.017	O	|	|	|	0.19
35.167	0.00	0.09	0.016	O	|	|	|	0.18
35.250	0.00	0.08	0.015	O	|	|	|	0.18
35.333	0.00	0.08	0.015	O	|	|	|	0.17
35.417	0.00	0.08	0.014	O	|	|	|	0.16

35.500	0.00	0.07	0.014	O	|	|	|	0.16
35.583	0.00	0.07	0.013	O	|	|	|	0.15
35.667	0.00	0.07	0.013	O	|	|	|	0.15
35.750	0.00	0.07	0.012	O	|	|	|	0.14
35.833	0.00	0.06	0.012	O	|	|	|	0.14
35.917	0.00	0.06	0.012	O	|	|	|	0.13
36.000	0.00	0.06	0.011	O	|	|	|	0.13
36.083	0.00	0.06	0.011	O	|	|	|	0.12
36.167	0.00	0.06	0.010	O	|	|	|	0.12
36.250	0.00	0.05	0.010	O	|	|	|	0.11
36.333	0.00	0.05	0.010	O	|	|	|	0.11
36.417	0.00	0.05	0.009	O	|	|	|	0.10
36.500	0.00	0.05	0.009	O	|	|	|	0.10
36.583	0.00	0.05	0.009	O	|	|	|	0.10
36.667	0.00	0.04	0.008	O	|	|	|	0.09
36.750	0.00	0.04	0.008	O	|	|	|	0.09
36.833	0.00	0.04	0.008	O	|	|	|	0.09
36.917	0.00	0.04	0.007	O	|	|	|	0.08
37.000	0.00	0.04	0.007	O	|	|	|	0.08
37.083	0.00	0.04	0.007	O	|	|	|	0.08
37.167	0.00	0.04	0.007	O	|	|	|	0.08
37.250	0.00	0.03	0.006	O	|	|	|	0.07
37.333	0.00	0.03	0.006	O	|	|	|	0.07
37.417	0.00	0.03	0.006	O	|	|	|	0.07
37.500	0.00	0.03	0.006	O	|	|	|	0.06
37.583	0.00	0.03	0.005	O	|	|	|	0.06
37.667	0.00	0.03	0.005	O	|	|	|	0.06
37.750	0.00	0.03	0.005	O	|	|	|	0.06
37.833	0.00	0.03	0.005	O	|	|	|	0.06
37.917	0.00	0.03	0.005	O	|	|	|	0.05
38.000	0.00	0.02	0.005	O	|	|	|	0.05
38.083	0.00	0.02	0.004	O	|	|	|	0.05
38.167	0.00	0.02	0.004	O	|	|	|	0.05
38.250	0.00	0.02	0.004	O	|	|	|	0.05
38.333	0.00	0.02	0.004	O	|	|	|	0.04
38.417	0.00	0.02	0.004	O	|	|	|	0.04
38.500	0.00	0.02	0.004	O	|	|	|	0.04
38.583	0.00	0.02	0.004	O	|	|	|	0.04
38.667	0.00	0.02	0.003	O	|	|	|	0.04
38.750	0.00	0.02	0.003	O	|	|	|	0.04
38.833	0.00	0.02	0.003	O	|	|	|	0.04
38.917	0.00	0.02	0.003	O	|	|	|	0.03
39.000	0.00	0.02	0.003	O	|	|	|	0.03
39.083	0.00	0.02	0.003	O	|	|	|	0.03
39.167	0.00	0.01	0.003	O	|	|	|	0.03
39.250	0.00	0.01	0.003	O	|	|	|	0.03
39.333	0.00	0.01	0.003	O	|	|	|	0.03
39.417	0.00	0.01	0.002	O	|	|	|	0.03
39.500	0.00	0.01	0.002	O	|	|	|	0.03
39.583	0.00	0.01	0.002	O	|	|	|	0.03
39.667	0.00	0.01	0.002	O	|	|	|	0.02
39.750	0.00	0.01	0.002	O	|	|	|	0.02
39.833	0.00	0.01	0.002	O	|	|	|	0.02
39.917	0.00	0.01	0.002	O	|	|	|	0.02
40.000	0.00	0.01	0.002	O	|	|	|	0.02
40.083	0.00	0.01	0.002	O	|	|	|	0.02
40.167	0.00	0.01	0.002	O	|	|	|	0.02
40.250	0.00	0.01	0.002	O	|	|	|	0.02
40.333	0.00	0.01	0.002	O	|	|	|	0.02
40.417	0.00	0.01	0.002	O	|	|	|	0.02
40.500	0.00	0.01	0.002	O	|	|	|	0.02
40.583	0.00	0.01	0.001	O	|	|	|	0.02
40.667	0.00	0.01	0.001	O	|	|	|	0.02
40.750	0.00	0.01	0.001	O	|	|	|	0.02
40.833	0.00	0.01	0.001	O	|	|	|	0.01
40.917	0.00	0.01	0.001	O	|	|	|	0.01
41.000	0.00	0.01	0.001	O	|	|	|	0.01
41.083	0.00	0.01	0.001	O	|	|	|	0.01
41.167	0.00	0.01	0.001	O	|	|	|	0.01
41.250	0.00	0.01	0.001	O	|	|	|	0.01
41.333	0.00	0.01	0.001	O	|	|	|	0.01
41.417	0.00	0.01	0.001	O	|	|	|	0.01

41.500	0.00	0.01	0.001	O	|	|	|	|	0.01
41.583	0.00	0.01	0.001	O	|	|	|	|	0.01
41.667	0.00	0.00	0.001	O	|	|	|	|	0.01
41.750	0.00	0.00	0.001	O	|	|	|	|	0.01
41.833	0.00	0.00	0.001	O	|	|	|	|	0.01
41.917	0.00	0.00	0.001	O	|	|	|	|	0.01
42.000	0.00	0.00	0.001	O	|	|	|	|	0.01
42.083	0.00	0.00	0.001	O	|	|	|	|	0.01
42.167	0.00	0.00	0.001	O	|	|	|	|	0.01
42.250	0.00	0.00	0.001	O	|	|	|	|	0.01
42.333	0.00	0.00	0.001	O	|	|	|	|	0.01
42.417	0.00	0.00	0.001	O	|	|	|	|	0.01
42.500	0.00	0.00	0.001	O	|	|	|	|	0.01
42.583	0.00	0.00	0.001	O	|	|	|	|	0.01
42.667	0.00	0.00	0.001	O	|	|	|	|	0.01
42.750	0.00	0.00	0.001	O	|	|	|	|	0.01
42.833	0.00	0.00	0.001	O	|	|	|	|	0.01
42.917	0.00	0.00	0.001	O	|	|	|	|	0.01
43.000	0.00	0.00	0.000	O	|	|	|	|	0.01
43.083	0.00	0.00	0.000	O	|	|	|	|	0.01
43.167	0.00	0.00	0.000	O	|	|	|	|	0.01
43.250	0.00	0.00	0.000	O	|	|	|	|	0.01
43.333	0.00	0.00	0.000	O	|	|	|	|	0.00
43.417	0.00	0.00	0.000	O	|	|	|	|	0.00
43.500	0.00	0.00	0.000	O	|	|	|	|	0.00
43.583	0.00	0.00	0.000	O	|	|	|	|	0.00
43.667	0.00	0.00	0.000	O	|	|	|	|	0.00
43.750	0.00	0.00	0.000	O	|	|	|	|	0.00
43.833	0.00	0.00	0.000	O	|	|	|	|	0.00
43.917	0.00	0.00	0.000	O	|	|	|	|	0.00
44.000	0.00	0.00	0.000	O	|	|	|	|	0.00
44.083	0.00	0.00	0.000	O	|	|	|	|	0.00
44.167	0.00	0.00	0.000	O	|	|	|	|	0.00
44.250	0.00	0.00	0.000	O	|	|	|	|	0.00
44.333	0.00	0.00	0.000	O	|	|	|	|	0.00
44.417	0.00	0.00	0.000	O	|	|	|	|	0.00
44.500	0.00	0.00	0.000	O	|	|	|	|	0.00
44.583	0.00	0.00	0.000	O	|	|	|	|	0.00
44.667	0.00	0.00	0.000	O	|	|	|	|	0.00
44.750	0.00	0.00	0.000	O	|	|	|	|	0.00
44.833	0.00	0.00	0.000	O	|	|	|	|	0.00
44.917	0.00	0.00	0.000	O	|	|	|	|	0.00
45.000	0.00	0.00	0.000	O	|	|	|	|	0.00
45.083	0.00	0.00	0.000	O	|	|	|	|	0.00
45.167	0.00	0.00	0.000	O	|	|	|	|	0.00
45.250	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 543
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.389 (CFS)
Total volume = 0.722 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
3-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA10310.rte
**********HYDROGRAPH DATA**********
Number of intervals = 38
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 6.973 (CFS)
Total volume = 0.567 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 38
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	1.7	3.49	5.23	6.97	Depth (Ft.)
0.083	0.59	0.01	0.002	O I	|	|	|	|	0.02
0.167	0.97	0.04	0.007	O I	|	|	|	|	0.08
0.250	0.93	0.07	0.013	O I	|	|	|	|	0.15
0.333	1.06	0.11	0.020	O I	|	|	|	|	0.22
0.417	1.16	0.12	0.026	O I	|	|	|	|	0.27
0.500	1.32	0.13	0.034	O I	|	|	|	|	0.30
0.583	1.27	0.14	0.042	O I	|	|	|	|	0.34
0.667	1.33	0.14	0.050	O I	|	|	|	|	0.37
0.750	1.41	0.15	0.059	O I	|	|	|	|	0.41
0.833	1.28	0.16	0.067	O I	|	|	|	|	0.44
0.917	1.24	0.16	0.074	O I	|	|	|	|	0.47
1.000	1.35	0.17	0.082	O I	|	|	|	|	0.50
1.083	1.59	0.17	0.091	O I	|	|	|	|	0.54
1.167	1.72	0.18	0.101	O I	|	|	|	|	0.58
1.250	1.73	0.18	0.112	O I	|	|	|	|	0.62
1.333	1.64	0.19	0.122	O I	|	|	|	|	0.67
1.417	1.86	0.20	0.133	O I	|	|	|	|	0.71
1.500	2.07	0.20	0.145	O I	|	|	|	|	0.76
1.583	1.99	0.21	0.158	O I	|	|	|	|	0.81
1.667	2.04	0.22	0.170	O I	|	|	|	|	0.86
1.750	2.42	0.22	0.184	O I	|	|	|	|	0.91
1.833	2.51	0.23	0.199	O I	|	|	|	|	0.97
1.917	2.37	0.24	0.215	O I	|	|	|	|	1.03
2.000	2.34	0.25	0.229	O I	|	|	|	|	1.09
2.083	2.42	0.25	0.244	O I	|	|	|	|	1.15
2.167	3.07	0.26	0.261	O |	I	|	|	|	1.22
2.250	3.90	0.27	0.283	O |	|	I	|	|	1.31
2.333	3.41	0.28	0.306	O |	|	I	|	|	1.41
2.417	4.76	0.29	0.333	O |	|	|	I	|	1.51
2.500	6.12	0.30	0.368	O |	|	|	|	I	1.66
2.583	6.97	0.32	0.411	O |	|	|	|	I	1.84
2.667	6.04	0.33	0.453	O |	|	|	I	|	2.01
2.750	3.21	0.35	0.483	O |	|	I	|	|	2.14
2.833	1.69	0.35	0.497	O |	I	|	|	|	2.20
2.917	1.43	0.35	0.506	O |	I	|	|	|	2.24
3.000	0.87	0.35	0.511	O I	|	|	|	|	2.26
3.083	0.25	0.36	0.513	O |	|	|	|	|	2.27
3.167	0.03	0.35	0.511	IO	|	|	|	|	2.26
3.250	0.00	0.35	0.509	IO	|	|	|	|	2.25
3.333	0.00	0.35	0.506	IO	|	|	|	|	2.24
3.417	0.00	0.35	0.504	IO	|	|	|	|	2.23
3.500	0.00	0.35	0.502	IO	|	|	|	|	2.22
3.583	0.00	0.35	0.499	IO	|	|	|	|	2.21
3.667	0.00	0.35	0.497	IO	|	|	|	|	2.20
3.750	0.00	0.35	0.494	IO	|	|	|	|	2.19
3.833	0.00	0.35	0.492	IO	|	|	|	|	2.18
3.917	0.00	0.35	0.490	IO	|	|	|	|	2.17
4.000	0.00	0.35	0.487	IO	|	|	|	|	2.16
4.083	0.00	0.35	0.485	IO	|	|	|	|	2.15
4.167	0.00	0.34	0.482	IO	|	|	|	|	2.14
4.250	0.00	0.34	0.480	IO	|	|	|	|	2.12
4.333	0.00	0.34	0.478	IO	|	|	|	|	2.11
4.417	0.00	0.34	0.475	IO	|	|	|	|	2.10
4.500	0.00	0.34	0.473	IO	|	|	|	|	2.09
4.583	0.00	0.34	0.471	IO	|	|	|	|	2.08
4.667	0.00	0.34	0.468	IO	|	|	|	|	2.07
4.750	0.00	0.34	0.466	IO	|	|	|	|	2.06
4.833	0.00	0.34	0.464	IO	|	|	|	|	2.05
4.917	0.00	0.34	0.461	IO	|	|	|	|	2.04
5.000	0.00	0.34	0.459	IO	|	|	|	|	2.03
5.083	0.00	0.34	0.457	IO	|	|	|	|	2.02
5.167	0.00	0.34	0.454	IO	|	|	|	|	2.01
5.250	0.00	0.33	0.452	IO	|	|	|	|	2.00
5.333	0.00	0.33	0.450	IO	|	|	|	|	1.99
5.417	0.00	0.33	0.447	IO	|	|	|	|	1.99

5.500	0.00	0.33	0.445	IO				1.98
5.583	0.00	0.33	0.443	IO				1.97
5.667	0.00	0.33	0.441	IO				1.96
5.750	0.00	0.33	0.438	IO				1.95
5.833	0.00	0.33	0.436	IO				1.94
5.917	0.00	0.33	0.434	IO				1.93
6.000	0.00	0.33	0.431	IO				1.92
6.083	0.00	0.33	0.429	IO				1.91
6.167	0.00	0.33	0.427	IO				1.90
6.250	0.00	0.32	0.425	IO				1.89
6.333	0.00	0.32	0.423	IO				1.88
6.417	0.00	0.32	0.420	IO				1.87
6.500	0.00	0.32	0.418	IO				1.87
6.583	0.00	0.32	0.416	IO				1.86
6.667	0.00	0.32	0.414	IO				1.85
6.750	0.00	0.32	0.411	IO				1.84
6.833	0.00	0.32	0.409	IO				1.83
6.917	0.00	0.32	0.407	IO				1.82
7.000	0.00	0.32	0.405	IO				1.81
7.083	0.00	0.32	0.403	IO				1.80
7.167	0.00	0.32	0.401	IO				1.79
7.250	0.00	0.31	0.398	IO				1.78
7.333	0.00	0.31	0.396	IO				1.78
7.417	0.00	0.31	0.394	IO				1.77
7.500	0.00	0.31	0.392	IO				1.76
7.583	0.00	0.31	0.390	IO				1.75
7.667	0.00	0.31	0.388	IO				1.74
7.750	0.00	0.31	0.385	IO				1.73
7.833	0.00	0.31	0.383	IO				1.72
7.917	0.00	0.31	0.381	IO				1.71
8.000	0.00	0.31	0.379	IO				1.71
8.083	0.00	0.31	0.377	IO				1.70
8.167	0.00	0.31	0.375	IO				1.69
8.250	0.00	0.31	0.373	IO				1.68
8.333	0.00	0.30	0.371	IO				1.67
8.417	0.00	0.30	0.369	IO				1.66
8.500	0.00	0.30	0.366	IO				1.65
8.583	0.00	0.30	0.364	IO				1.64
8.667	0.00	0.30	0.362	IO				1.64
8.750	0.00	0.30	0.360	IO				1.63
8.833	0.00	0.30	0.358	IO				1.62
8.917	0.00	0.30	0.356	IO				1.61
9.000	0.00	0.30	0.354	IO				1.60
9.083	0.00	0.30	0.352	IO				1.59
9.167	0.00	0.30	0.350	IO				1.59
9.250	0.00	0.30	0.348	IO				1.58
9.333	0.00	0.30	0.346	IO				1.57
9.417	0.00	0.29	0.344	IO				1.56
9.500	0.00	0.29	0.342	IO				1.55
9.583	0.00	0.29	0.340	IO				1.54
9.667	0.00	0.29	0.338	IO				1.54
9.750	0.00	0.29	0.336	IO				1.53
9.833	0.00	0.29	0.334	IO				1.52
9.917	0.00	0.29	0.332	IO				1.51
10.000	0.00	0.29	0.330	IO				1.50
10.083	0.00	0.29	0.328	IO				1.49
10.167	0.00	0.29	0.326	IO				1.49
10.250	0.00	0.29	0.324	IO				1.48
10.333	0.00	0.29	0.322	IO				1.47
10.417	0.00	0.29	0.320	IO				1.46
10.500	0.00	0.28	0.318	IO				1.45
10.583	0.00	0.28	0.316	IO				1.45
10.667	0.00	0.28	0.314	IO				1.44
10.750	0.00	0.28	0.312	IO				1.43
10.833	0.00	0.28	0.310	IO				1.42
10.917	0.00	0.28	0.308	IO				1.41
11.000	0.00	0.28	0.306	IO				1.41
11.083	0.00	0.28	0.304	IO				1.40
11.167	0.00	0.28	0.302	IO				1.39
11.250	0.00	0.28	0.300	IO				1.38
11.333	0.00	0.28	0.299	IO				1.37
11.417	0.00	0.28	0.297	IO				1.37

11.500	0.00	0.28	0.295	IO				1.36
11.583	0.00	0.27	0.293	IO				1.35
11.667	0.00	0.27	0.291	IO				1.34
11.750	0.00	0.27	0.289	IO				1.33
11.833	0.00	0.27	0.287	IO				1.33
11.917	0.00	0.27	0.285	IO				1.32
12.000	0.00	0.27	0.283	IO				1.31
12.083	0.00	0.27	0.282	IO				1.30
12.167	0.00	0.27	0.280	IO				1.30
12.250	0.00	0.27	0.278	IO				1.29
12.333	0.00	0.27	0.276	IO				1.28
12.417	0.00	0.27	0.274	IO				1.27
12.500	0.00	0.27	0.272	IO				1.27
12.583	0.00	0.26	0.271	IO				1.26
12.667	0.00	0.26	0.269	IO				1.25
12.750	0.00	0.26	0.267	IO				1.25
12.833	0.00	0.26	0.265	IO				1.24
12.917	0.00	0.26	0.263	IO				1.23
13.000	0.00	0.26	0.261	IO				1.22
13.083	0.00	0.26	0.260	IO				1.22
13.167	0.00	0.26	0.258	IO				1.21
13.250	0.00	0.26	0.256	IO				1.20
13.333	0.00	0.26	0.254	IO				1.19
13.417	0.00	0.26	0.253	IO				1.19
13.500	0.00	0.26	0.251	IO				1.18
13.583	0.00	0.26	0.249	IO				1.17
13.667	0.00	0.25	0.247	IO				1.17
13.750	0.00	0.25	0.246	IO				1.16
13.833	0.00	0.25	0.244	IO				1.15
13.917	0.00	0.25	0.242	IO				1.15
14.000	0.00	0.25	0.240	IO				1.14
14.083	0.00	0.25	0.239	IO				1.13
14.167	0.00	0.25	0.237	IO				1.12
14.250	0.00	0.25	0.235	IO				1.12
14.333	0.00	0.25	0.233	IO				1.11
14.417	0.00	0.25	0.232	IO				1.10
14.500	0.00	0.25	0.230	IO				1.10
14.583	0.00	0.25	0.228	IO				1.09
14.667	0.00	0.25	0.227	IO				1.08
14.750	0.00	0.24	0.225	IO				1.08
14.833	0.00	0.24	0.223	IO				1.07
14.917	0.00	0.24	0.222	IO				1.06
15.000	0.00	0.24	0.220	IO				1.06
15.083	0.00	0.24	0.218	IO				1.05
15.167	0.00	0.24	0.217	IO				1.04
15.250	0.00	0.24	0.215	IO				1.04
15.333	0.00	0.24	0.213	IO				1.03
15.417	0.00	0.24	0.212	IO				1.02
15.500	0.00	0.24	0.210	IO				1.02
15.583	0.00	0.24	0.208	IO				1.01
15.667	0.00	0.24	0.207	IO				1.00
15.750	0.00	0.24	0.205	IO				1.00
15.833	0.00	0.23	0.204	IO				0.99
15.917	0.00	0.23	0.202	IO				0.98
16.000	0.00	0.23	0.200	IO				0.98
16.083	0.00	0.23	0.199	IO				0.97
16.167	0.00	0.23	0.197	IO				0.96
16.250	0.00	0.23	0.196	IO				0.96
16.333	0.00	0.23	0.194	IO				0.95
16.417	0.00	0.23	0.192	IO				0.95
16.500	0.00	0.23	0.191	IO				0.94
16.583	0.00	0.23	0.189	IO				0.93
16.667	0.00	0.23	0.188	IO				0.93
16.750	0.00	0.23	0.186	IO				0.92
16.833	0.00	0.22	0.185	IO				0.91
16.917	0.00	0.22	0.183	IO				0.91
17.000	0.00	0.22	0.181	IO				0.90
17.083	0.00	0.22	0.180	IO				0.90
17.167	0.00	0.22	0.178	IO				0.89
17.250	0.00	0.22	0.177	IO				0.88
17.333	0.00	0.22	0.175	IO				0.88
17.417	0.00	0.22	0.174	IO				0.87

17.500	0.00	0.22	0.172	O	|	|	|	0.87
17.583	0.00	0.22	0.171	O	|	|	|	0.86
17.667	0.00	0.22	0.169	O	|	|	|	0.85
17.750	0.00	0.21	0.168	O	|	|	|	0.85
17.833	0.00	0.21	0.166	O	|	|	|	0.84
17.917	0.00	0.21	0.165	O	|	|	|	0.84
18.000	0.00	0.21	0.164	O	|	|	|	0.83
18.083	0.00	0.21	0.162	O	|	|	|	0.82
18.167	0.00	0.21	0.161	O	|	|	|	0.82
18.250	0.00	0.21	0.159	O	|	|	|	0.81
18.333	0.00	0.21	0.158	O	|	|	|	0.81
18.417	0.00	0.21	0.156	O	|	|	|	0.80
18.500	0.00	0.21	0.155	O	|	|	|	0.80
18.583	0.00	0.21	0.153	O	|	|	|	0.79
18.667	0.00	0.21	0.152	O	|	|	|	0.78
18.750	0.00	0.21	0.151	O	|	|	|	0.78
18.833	0.00	0.20	0.149	O	|	|	|	0.77
18.917	0.00	0.20	0.148	O	|	|	|	0.77
19.000	0.00	0.20	0.146	O	|	|	|	0.76
19.083	0.00	0.20	0.145	O	|	|	|	0.76
19.167	0.00	0.20	0.144	O	|	|	|	0.75
19.250	0.00	0.20	0.142	O	|	|	|	0.74
19.333	0.00	0.20	0.141	O	|	|	|	0.74
19.417	0.00	0.20	0.139	O	|	|	|	0.73
19.500	0.00	0.20	0.138	O	|	|	|	0.73
19.583	0.00	0.20	0.137	O	|	|	|	0.72
19.667	0.00	0.20	0.135	O	|	|	|	0.72
19.750	0.00	0.20	0.134	O	|	|	|	0.71
19.833	0.00	0.20	0.133	O	|	|	|	0.71
19.917	0.00	0.19	0.131	O	|	|	|	0.70
20.000	0.00	0.19	0.130	O	|	|	|	0.70
20.083	0.00	0.19	0.129	O	|	|	|	0.69
20.167	0.00	0.19	0.127	O	|	|	|	0.69
20.250	0.00	0.19	0.126	O	|	|	|	0.68
20.333	0.00	0.19	0.125	O	|	|	|	0.67
20.417	0.00	0.19	0.123	O	|	|	|	0.67
20.500	0.00	0.19	0.122	O	|	|	|	0.66
20.583	0.00	0.19	0.121	O	|	|	|	0.66
20.667	0.00	0.19	0.119	O	|	|	|	0.65
20.750	0.00	0.19	0.118	O	|	|	|	0.65
20.833	0.00	0.19	0.117	O	|	|	|	0.64
20.917	0.00	0.19	0.116	O	|	|	|	0.64
21.000	0.00	0.19	0.114	O	|	|	|	0.63
21.083	0.00	0.18	0.113	O	|	|	|	0.63
21.167	0.00	0.18	0.112	O	|	|	|	0.62
21.250	0.00	0.18	0.110	O	|	|	|	0.62
21.333	0.00	0.18	0.109	O	|	|	|	0.61
21.417	0.00	0.18	0.108	O	|	|	|	0.61
21.500	0.00	0.18	0.107	O	|	|	|	0.60
21.583	0.00	0.18	0.105	O	|	|	|	0.60
21.667	0.00	0.18	0.104	O	|	|	|	0.59
21.750	0.00	0.18	0.103	O	|	|	|	0.59
21.833	0.00	0.18	0.102	O	|	|	|	0.58
21.917	0.00	0.18	0.101	O	|	|	|	0.58
22.000	0.00	0.18	0.099	O	|	|	|	0.57
22.083	0.00	0.18	0.098	O	|	|	|	0.57
22.167	0.00	0.18	0.097	O	|	|	|	0.56
22.250	0.00	0.18	0.096	O	|	|	|	0.56
22.333	0.00	0.17	0.094	O	|	|	|	0.55
22.417	0.00	0.17	0.093	O	|	|	|	0.55
22.500	0.00	0.17	0.092	O	|	|	|	0.54
22.583	0.00	0.17	0.091	O	|	|	|	0.54
22.667	0.00	0.17	0.090	O	|	|	|	0.53
22.750	0.00	0.17	0.088	O	|	|	|	0.53
22.833	0.00	0.17	0.087	O	|	|	|	0.53
22.917	0.00	0.17	0.086	O	|	|	|	0.52
23.000	0.00	0.17	0.085	O	|	|	|	0.52
23.083	0.00	0.17	0.084	O	|	|	|	0.51
23.167	0.00	0.17	0.083	O	|	|	|	0.51
23.250	0.00	0.17	0.081	O	|	|	|	0.50
23.333	0.00	0.17	0.080	O	|	|	|	0.50
23.417	0.00	0.17	0.079	O	|	|	|	0.49

23.500	0.00	0.16	0.078	O	|	|	|	0.49
23.583	0.00	0.16	0.077	O	|	|	|	0.48
23.667	0.00	0.16	0.076	O	|	|	|	0.48
23.750	0.00	0.16	0.075	O	|	|	|	0.47
23.833	0.00	0.16	0.074	O	|	|	|	0.47
23.917	0.00	0.16	0.072	O	|	|	|	0.46
24.000	0.00	0.16	0.071	O	|	|	|	0.46
24.083	0.00	0.16	0.070	O	|	|	|	0.46
24.167	0.00	0.16	0.069	O	|	|	|	0.45
24.250	0.00	0.16	0.068	O	|	|	|	0.45
24.333	0.00	0.16	0.067	O	|	|	|	0.44
24.417	0.00	0.16	0.066	O	|	|	|	0.44
24.500	0.00	0.15	0.065	O	|	|	|	0.43
24.583	0.00	0.15	0.064	O	|	|	|	0.43
24.667	0.00	0.15	0.063	O	|	|	|	0.43
24.750	0.00	0.15	0.062	O	|	|	|	0.42
24.833	0.00	0.15	0.061	O	|	|	|	0.42
24.917	0.00	0.15	0.060	O	|	|	|	0.41
25.000	0.00	0.15	0.059	O	|	|	|	0.41
25.083	0.00	0.15	0.058	O	|	|	|	0.40
25.167	0.00	0.15	0.056	O	|	|	|	0.40
25.250	0.00	0.15	0.055	O	|	|	|	0.40
25.333	0.00	0.15	0.054	O	|	|	|	0.39
25.417	0.00	0.15	0.053	O	|	|	|	0.39
25.500	0.00	0.15	0.052	O	|	|	|	0.38
25.583	0.00	0.15	0.051	O	|	|	|	0.38
25.667	0.00	0.14	0.050	O	|	|	|	0.37
25.750	0.00	0.14	0.049	O	|	|	|	0.37
25.833	0.00	0.14	0.048	O	|	|	|	0.37
25.917	0.00	0.14	0.047	O	|	|	|	0.36
26.000	0.00	0.14	0.046	O	|	|	|	0.36
26.083	0.00	0.14	0.046	O	|	|	|	0.35
26.167	0.00	0.14	0.045	O	|	|	|	0.35
26.250	0.00	0.14	0.044	O	|	|	|	0.35
26.333	0.00	0.14	0.043	O	|	|	|	0.34
26.417	0.00	0.14	0.042	O	|	|	|	0.34
26.500	0.00	0.14	0.041	O	|	|	|	0.33
26.583	0.00	0.14	0.040	O	|	|	|	0.33
26.667	0.00	0.13	0.039	O	|	|	|	0.33
26.750	0.00	0.13	0.038	O	|	|	|	0.32
26.833	0.00	0.13	0.037	O	|	|	|	0.32
26.917	0.00	0.13	0.036	O	|	|	|	0.31
27.000	0.00	0.13	0.035	O	|	|	|	0.31
27.083	0.00	0.13	0.034	O	|	|	|	0.31
27.167	0.00	0.13	0.033	O	|	|	|	0.30
27.250	0.00	0.13	0.033	O	|	|	|	0.30
27.333	0.00	0.13	0.032	O	|	|	|	0.29
27.417	0.00	0.13	0.031	O	|	|	|	0.29
27.500	0.00	0.13	0.030	O	|	|	|	0.29
27.583	0.00	0.13	0.029	O	|	|	|	0.28
27.667	0.00	0.12	0.028	O	|	|	|	0.28
27.750	0.00	0.12	0.027	O	|	|	|	0.27
27.833	0.00	0.12	0.026	O	|	|	|	0.27
27.917	0.00	0.12	0.026	O	|	|	|	0.27
28.000	0.00	0.12	0.025	O	|	|	|	0.26
28.083	0.00	0.12	0.024	O	|	|	|	0.26
28.167	0.00	0.12	0.023	O	|	|	|	0.26
28.250	0.00	0.12	0.022	O	|	|	|	0.25
28.333	0.00	0.12	0.022	O	|	|	|	0.24
28.417	0.00	0.11	0.021	O	|	|	|	0.24
28.500	0.00	0.11	0.020	O	|	|	|	0.23
28.583	0.00	0.10	0.019	O	|	|	|	0.22
28.667	0.00	0.10	0.019	O	|	|	|	0.21
28.750	0.00	0.10	0.018	O	|	|	|	0.20
28.833	0.00	0.09	0.017	O	|	|	|	0.20
28.917	0.00	0.09	0.017	O	|	|	|	0.19
29.000	0.00	0.09	0.016	O	|	|	|	0.18
29.083	0.00	0.08	0.015	O	|	|	|	0.18
29.167	0.00	0.08	0.015	O	|	|	|	0.17
29.250	0.00	0.08	0.014	O	|	|	|	0.16
29.333	0.00	0.07	0.014	O	|	|	|	0.16
29.417	0.00	0.07	0.013	O	|	|	|	0.15

29.500	0.00	0.07	0.013	O	|	|	|	0.15
29.583	0.00	0.07	0.012	O	|	|	|	0.14
29.667	0.00	0.06	0.012	O	|	|	|	0.14
29.750	0.00	0.06	0.011	O	|	|	|	0.13
29.833	0.00	0.06	0.011	O	|	|	|	0.13
29.917	0.00	0.06	0.011	O	|	|	|	0.12
30.000	0.00	0.06	0.010	O	|	|	|	0.12
30.083	0.00	0.05	0.010	O	|	|	|	0.11
30.167	0.00	0.05	0.010	O	|	|	|	0.11
30.250	0.00	0.05	0.009	O	|	|	|	0.10
30.333	0.00	0.05	0.009	O	|	|	|	0.10
30.417	0.00	0.05	0.009	O	|	|	|	0.10
30.500	0.00	0.04	0.008	O	|	|	|	0.09
30.583	0.00	0.04	0.008	O	|	|	|	0.09
30.667	0.00	0.04	0.008	O	|	|	|	0.09
30.750	0.00	0.04	0.007	O	|	|	|	0.08
30.833	0.00	0.04	0.007	O	|	|	|	0.08
30.917	0.00	0.04	0.007	O	|	|	|	0.08
31.000	0.00	0.04	0.007	O	|	|	|	0.08
31.083	0.00	0.03	0.006	O	|	|	|	0.07
31.167	0.00	0.03	0.006	O	|	|	|	0.07
31.250	0.00	0.03	0.006	O	|	|	|	0.07
31.333	0.00	0.03	0.006	O	|	|	|	0.06
31.417	0.00	0.03	0.005	O	|	|	|	0.06
31.500	0.00	0.03	0.005	O	|	|	|	0.06
31.583	0.00	0.03	0.005	O	|	|	|	0.06
31.667	0.00	0.03	0.005	O	|	|	|	0.06
31.750	0.00	0.03	0.005	O	|	|	|	0.05
31.833	0.00	0.02	0.005	O	|	|	|	0.05
31.917	0.00	0.02	0.004	O	|	|	|	0.05
32.000	0.00	0.02	0.004	O	|	|	|	0.05
32.083	0.00	0.02	0.004	O	|	|	|	0.05
32.167	0.00	0.02	0.004	O	|	|	|	0.04
32.250	0.00	0.02	0.004	O	|	|	|	0.04
32.333	0.00	0.02	0.004	O	|	|	|	0.04
32.417	0.00	0.02	0.004	O	|	|	|	0.04
32.500	0.00	0.02	0.003	O	|	|	|	0.04
32.583	0.00	0.02	0.003	O	|	|	|	0.04
32.667	0.00	0.02	0.003	O	|	|	|	0.04
32.750	0.00	0.02	0.003	O	|	|	|	0.03
32.833	0.00	0.02	0.003	O	|	|	|	0.03
32.917	0.00	0.02	0.003	O	|	|	|	0.03
33.000	0.00	0.01	0.003	O	|	|	|	0.03
33.083	0.00	0.01	0.003	O	|	|	|	0.03
33.167	0.00	0.01	0.003	O	|	|	|	0.03
33.250	0.00	0.01	0.002	O	|	|	|	0.03
33.333	0.00	0.01	0.002	O	|	|	|	0.03
33.417	0.00	0.01	0.002	O	|	|	|	0.03
33.500	0.00	0.01	0.002	O	|	|	|	0.02
33.583	0.00	0.01	0.002	O	|	|	|	0.02
33.667	0.00	0.01	0.002	O	|	|	|	0.02
33.750	0.00	0.01	0.002	O	|	|	|	0.02
33.833	0.00	0.01	0.002	O	|	|	|	0.02
33.917	0.00	0.01	0.002	O	|	|	|	0.02
34.000	0.00	0.01	0.002	O	|	|	|	0.02
34.083	0.00	0.01	0.002	O	|	|	|	0.02
34.167	0.00	0.01	0.002	O	|	|	|	0.02
34.250	0.00	0.01	0.002	O	|	|	|	0.02
34.333	0.00	0.01	0.002	O	|	|	|	0.02
34.417	0.00	0.01	0.001	O	|	|	|	0.02
34.500	0.00	0.01	0.001	O	|	|	|	0.02
34.583	0.00	0.01	0.001	O	|	|	|	0.02
34.667	0.00	0.01	0.001	O	|	|	|	0.01
34.750	0.00	0.01	0.001	O	|	|	|	0.01
34.833	0.00	0.01	0.001	O	|	|	|	0.01
34.917	0.00	0.01	0.001	O	|	|	|	0.01
35.000	0.00	0.01	0.001	O	|	|	|	0.01
35.083	0.00	0.01	0.001	O	|	|	|	0.01
35.167	0.00	0.01	0.001	O	|	|	|	0.01
35.250	0.00	0.01	0.001	O	|	|	|	0.01
35.333	0.00	0.01	0.001	O	|	|	|	0.01
35.417	0.00	0.00	0.001	O	|	|	|	0.01

35.500	0.00	0.00	0.001	O	|	|	|	|	0.01
35.583	0.00	0.00	0.001	O	|	|	|	|	0.01
35.667	0.00	0.00	0.001	O	|	|	|	|	0.01
35.750	0.00	0.00	0.001	O	|	|	|	|	0.01
35.833	0.00	0.00	0.001	O	|	|	|	|	0.01
35.917	0.00	0.00	0.001	O	|	|	|	|	0.01
36.000	0.00	0.00	0.001	O	|	|	|	|	0.01
36.083	0.00	0.00	0.001	O	|	|	|	|	0.01
36.167	0.00	0.00	0.001	O	|	|	|	|	0.01
36.250	0.00	0.00	0.001	O	|	|	|	|	0.01
36.333	0.00	0.00	0.001	O	|	|	|	|	0.01
36.417	0.00	0.00	0.001	O	|	|	|	|	0.01
36.500	0.00	0.00	0.001	O	|	|	|	|	0.01
36.583	0.00	0.00	0.001	O	|	|	|	|	0.01
36.667	0.00	0.00	0.001	O	|	|	|	|	0.01
36.750	0.00	0.00	0.001	O	|	|	|	|	0.01
36.833	0.00	0.00	0.000	O	|	|	|	|	0.01
36.917	0.00	0.00	0.000	O	|	|	|	|	0.01
37.000	0.00	0.00	0.000	O	|	|	|	|	0.01
37.083	0.00	0.00	0.000	O	|	|	|	|	0.01
37.167	0.00	0.00	0.000	O	|	|	|	|	0.00
37.250	0.00	0.00	0.000	O	|	|	|	|	0.00
37.333	0.00	0.00	0.000	O	|	|	|	|	0.00
37.417	0.00	0.00	0.000	O	|	|	|	|	0.00
37.500	0.00	0.00	0.000	O	|	|	|	|	0.00
37.583	0.00	0.00	0.000	O	|	|	|	|	0.00
37.667	0.00	0.00	0.000	O	|	|	|	|	0.00
37.750	0.00	0.00	0.000	O	|	|	|	|	0.00
37.833	0.00	0.00	0.000	O	|	|	|	|	0.00
37.917	0.00	0.00	0.000	O	|	|	|	|	0.00
38.000	0.00	0.00	0.000	O	|	|	|	|	0.00
38.083	0.00	0.00	0.000	O	|	|	|	|	0.00
38.167	0.00	0.00	0.000	O	|	|	|	|	0.00
38.250	0.00	0.00	0.000	O	|	|	|	|	0.00
38.333	0.00	0.00	0.000	O	|	|	|	|	0.00
38.417	0.00	0.00	0.000	O	|	|	|	|	0.00
38.500	0.00	0.00	0.000	O	|	|	|	|	0.00
38.583	0.00	0.00	0.000	O	|	|	|	|	0.00
38.667	0.00	0.00	0.000	O	|	|	|	|	0.00
38.750	0.00	0.00	0.000	O	|	|	|	|	0.00
38.833	0.00	0.00	0.000	O	|	|	|	|	0.00
38.917	0.00	0.00	0.000	O	|	|	|	|	0.00
39.000	0.00	0.00	0.000	O	|	|	|	|	0.00
39.083	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 469
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.355 (CFS)
Total volume = 0.567 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/05/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 100-131
MITIGATION ANALYSIS
1-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PA10110.rte
**********HYDROGRAPH DATA**********
Number of intervals = 14
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 10.749 (CFS)
Total volume = 0.346 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 14
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.022	0.118	0.022	0.022
0.340	0.042	0.138	0.042	0.042
0.500	0.081	0.167	0.080	0.082
1.000	0.206	0.236	0.205	0.207
1.350	0.293	0.275	0.292	0.294
1.500	0.329	0.289	0.328	0.330
2.000	0.451	0.334	0.450	0.452
2.500	0.567	0.374	0.566	0.568
3.000	0.677	0.409	0.676	0.678
3.100	0.697	0.416	0.696	0.698
3.500	0.775	1.336	0.770	0.780
4.000	0.841	3.874	0.828	0.854
4.100	0.846	4.260	0.831	0.861
4.340	0.859	4.703	0.843	0.875

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	2.7	5.37	8.06	10.75	Depth (Ft.)
0.083	1.18	0.02	0.004	O I	|	|	|	|	0.05
0.167	1.95	0.08	0.014	O I	|	|	|	|	0.16
0.250	2.33	0.12	0.028	O I	|	|	|	|	0.28
0.333	2.50	0.14	0.044	O I	|	|	|	|	0.35
0.417	2.62	0.15	0.061	O I	|	|	|	|	0.42
0.500	2.91	0.17	0.079	O I	|	|	|	|	0.49
0.583	3.55	0.18	0.100	O I	|	|	|	|	0.58
0.667	4.28	0.19	0.126	O I	|	|	|	|	0.68
0.750	5.78	0.21	0.159	O I	|	I	|	|	0.81
0.833	10.75	0.24	0.214	O I	|	|	|	I	1.03
0.917	7.73	0.27	0.276	O I	|	|	I	|	1.28
1.000	3.53	0.28	0.313	O I	|	|	|	|	1.43
1.083	1.05	0.29	0.327	O I	|	|	|	|	1.49
1.167	0.13	0.29	0.329	O	|	|	|	|	1.50
1.250	0.00	0.29	0.327	O	|	|	|	|	1.49
1.333	0.00	0.29	0.325	O	|	|	|	|	1.48
1.417	0.00	0.29	0.323	O	|	|	|	|	1.48
1.500	0.00	0.29	0.321	O	|	|	|	|	1.47
1.583	0.00	0.29	0.319	O	|	|	|	|	1.46
1.667	0.00	0.28	0.317	O	|	|	|	|	1.45
1.750	0.00	0.28	0.315	O	|	|	|	|	1.44
1.833	0.00	0.28	0.314	O	|	|	|	|	1.44
1.917	0.00	0.28	0.312	O	|	|	|	|	1.43
2.000	0.00	0.28	0.310	O	|	|	|	|	1.42
2.083	0.00	0.28	0.308	O	|	|	|	|	1.41
2.167	0.00	0.28	0.306	O	|	|	|	|	1.40
2.250	0.00	0.28	0.304	O	|	|	|	|	1.40
2.333	0.00	0.28	0.302	O	|	|	|	|	1.39
2.417	0.00	0.28	0.300	O	|	|	|	|	1.38
2.500	0.00	0.28	0.298	O	|	|	|	|	1.37
2.583	0.00	0.28	0.296	O	|	|	|	|	1.36
2.667	0.00	0.28	0.294	O	|	|	|	|	1.36
2.750	0.00	0.27	0.292	O	|	|	|	|	1.35
2.833	0.00	0.27	0.290	O	|	|	|	|	1.34
2.917	0.00	0.27	0.289	O	|	|	|	|	1.33
3.000	0.00	0.27	0.287	O	|	|	|	|	1.32
3.083	0.00	0.27	0.285	O	|	|	|	|	1.32
3.167	0.00	0.27	0.283	O	|	|	|	|	1.31
3.250	0.00	0.27	0.281	O	|	|	|	|	1.30
3.333	0.00	0.27	0.279	O	|	|	|	|	1.29
3.417	0.00	0.27	0.277	O	|	|	|	|	1.29
3.500	0.00	0.27	0.276	O	|	|	|	|	1.28
3.583	0.00	0.27	0.274	O	|	|	|	|	1.27
3.667	0.00	0.27	0.272	O	|	|	|	|	1.27
3.750	0.00	0.26	0.270	O	|	|	|	|	1.26
3.833	0.00	0.26	0.268	O	|	|	|	|	1.25
3.917	0.00	0.26	0.266	O	|	|	|	|	1.24
4.000	0.00	0.26	0.265	O	|	|	|	|	1.24
4.083	0.00	0.26	0.263	O	|	|	|	|	1.23
4.167	0.00	0.26	0.261	O	|	|	|	|	1.22
4.250	0.00	0.26	0.259	O	|	|	|	|	1.21
4.333	0.00	0.26	0.257	O	|	|	|	|	1.21
4.417	0.00	0.26	0.256	O	|	|	|	|	1.20
4.500	0.00	0.26	0.254	O	|	|	|	|	1.19
4.583	0.00	0.26	0.252	O	|	|	|	|	1.19
4.667	0.00	0.26	0.250	O	|	|	|	|	1.18
4.750	0.00	0.26	0.249	O	|	|	|	|	1.17
4.833	0.00	0.25	0.247	O	|	|	|	|	1.16
4.917	0.00	0.25	0.245	O	|	|	|	|	1.16
5.000	0.00	0.25	0.243	O	|	|	|	|	1.15
5.083	0.00	0.25	0.242	O	|	|	|	|	1.14
5.167	0.00	0.25	0.240	O	|	|	|	|	1.14
5.250	0.00	0.25	0.238	O	|	|	|	|	1.13
5.333	0.00	0.25	0.236	O	|	|	|	|	1.12
5.417	0.00	0.25	0.235	O	|	|	|	|	1.12

5.500	0.00	0.25	0.233	O	|	|	|	1.11
5.583	0.00	0.25	0.231	O	|	|	|	1.10
5.667	0.00	0.25	0.230	O	|	|	|	1.10
5.750	0.00	0.25	0.228	O	|	|	|	1.09
5.833	0.00	0.25	0.226	O	|	|	|	1.08
5.917	0.00	0.24	0.225	O	|	|	|	1.07
6.000	0.00	0.24	0.223	O	|	|	|	1.07
6.083	0.00	0.24	0.221	O	|	|	|	1.06
6.167	0.00	0.24	0.220	O	|	|	|	1.05
6.250	0.00	0.24	0.218	O	|	|	|	1.05
6.333	0.00	0.24	0.216	O	|	|	|	1.04
6.417	0.00	0.24	0.215	O	|	|	|	1.03
6.500	0.00	0.24	0.213	O	|	|	|	1.03
6.583	0.00	0.24	0.211	O	|	|	|	1.02
6.667	0.00	0.24	0.210	O	|	|	|	1.01
6.750	0.00	0.24	0.208	O	|	|	|	1.01
6.833	0.00	0.24	0.206	O	|	|	|	1.00
6.917	0.00	0.24	0.205	O	|	|	|	0.99
7.000	0.00	0.23	0.203	O	|	|	|	0.99
7.083	0.00	0.23	0.201	O	|	|	|	0.98
7.167	0.00	0.23	0.200	O	|	|	|	0.98
7.250	0.00	0.23	0.198	O	|	|	|	0.97
7.333	0.00	0.23	0.197	O	|	|	|	0.96
7.417	0.00	0.23	0.195	O	|	|	|	0.96
7.500	0.00	0.23	0.194	O	|	|	|	0.95
7.583	0.00	0.23	0.192	O	|	|	|	0.94
7.667	0.00	0.23	0.190	O	|	|	|	0.94
7.750	0.00	0.23	0.189	O	|	|	|	0.93
7.833	0.00	0.23	0.187	O	|	|	|	0.93
7.917	0.00	0.22	0.186	O	|	|	|	0.92
8.000	0.00	0.22	0.184	O	|	|	|	0.91
8.083	0.00	0.22	0.183	O	|	|	|	0.91
8.167	0.00	0.22	0.181	O	|	|	|	0.90
8.250	0.00	0.22	0.180	O	|	|	|	0.89
8.333	0.00	0.22	0.178	O	|	|	|	0.89
8.417	0.00	0.22	0.177	O	|	|	|	0.88
8.500	0.00	0.22	0.175	O	|	|	|	0.88
8.583	0.00	0.22	0.174	O	|	|	|	0.87
8.667	0.00	0.22	0.172	O	|	|	|	0.86
8.750	0.00	0.22	0.171	O	|	|	|	0.86
8.833	0.00	0.22	0.169	O	|	|	|	0.85
8.917	0.00	0.21	0.168	O	|	|	|	0.85
9.000	0.00	0.21	0.166	O	|	|	|	0.84
9.083	0.00	0.21	0.165	O	|	|	|	0.83
9.167	0.00	0.21	0.163	O	|	|	|	0.83
9.250	0.00	0.21	0.162	O	|	|	|	0.82
9.333	0.00	0.21	0.160	O	|	|	|	0.82
9.417	0.00	0.21	0.159	O	|	|	|	0.81
9.500	0.00	0.21	0.157	O	|	|	|	0.81
9.583	0.00	0.21	0.156	O	|	|	|	0.80
9.667	0.00	0.21	0.154	O	|	|	|	0.79
9.750	0.00	0.21	0.153	O	|	|	|	0.79
9.833	0.00	0.21	0.152	O	|	|	|	0.78
9.917	0.00	0.21	0.150	O	|	|	|	0.78
10.000	0.00	0.20	0.149	O	|	|	|	0.77
10.083	0.00	0.20	0.147	O	|	|	|	0.77
10.167	0.00	0.20	0.146	O	|	|	|	0.76
10.250	0.00	0.20	0.145	O	|	|	|	0.75
10.333	0.00	0.20	0.143	O	|	|	|	0.75
10.417	0.00	0.20	0.142	O	|	|	|	0.74
10.500	0.00	0.20	0.140	O	|	|	|	0.74
10.583	0.00	0.20	0.139	O	|	|	|	0.73
10.667	0.00	0.20	0.138	O	|	|	|	0.73
10.750	0.00	0.20	0.136	O	|	|	|	0.72
10.833	0.00	0.20	0.135	O	|	|	|	0.72
10.917	0.00	0.20	0.134	O	|	|	|	0.71
11.000	0.00	0.20	0.132	O	|	|	|	0.71
11.083	0.00	0.19	0.131	O	|	|	|	0.70
11.167	0.00	0.19	0.130	O	|	|	|	0.69
11.250	0.00	0.19	0.128	O	|	|	|	0.69
11.333	0.00	0.19	0.127	O	|	|	|	0.68
11.417	0.00	0.19	0.126	O	|	|	|	0.68

11.500	0.00	0.19	0.124	O	|	|	|	0.67
11.583	0.00	0.19	0.123	O	|	|	|	0.67
11.667	0.00	0.19	0.122	O	|	|	|	0.66
11.750	0.00	0.19	0.120	O	|	|	|	0.66
11.833	0.00	0.19	0.119	O	|	|	|	0.65
11.917	0.00	0.19	0.118	O	|	|	|	0.65
12.000	0.00	0.19	0.116	O	|	|	|	0.64
12.083	0.00	0.19	0.115	O	|	|	|	0.64
12.167	0.00	0.19	0.114	O	|	|	|	0.63
12.250	0.00	0.18	0.113	O	|	|	|	0.63
12.333	0.00	0.18	0.111	O	|	|	|	0.62
12.417	0.00	0.18	0.110	O	|	|	|	0.62
12.500	0.00	0.18	0.109	O	|	|	|	0.61
12.583	0.00	0.18	0.108	O	|	|	|	0.61
12.667	0.00	0.18	0.106	O	|	|	|	0.60
12.750	0.00	0.18	0.105	O	|	|	|	0.60
12.833	0.00	0.18	0.104	O	|	|	|	0.59
12.917	0.00	0.18	0.103	O	|	|	|	0.59
13.000	0.00	0.18	0.101	O	|	|	|	0.58
13.083	0.00	0.18	0.100	O	|	|	|	0.58
13.167	0.00	0.18	0.099	O	|	|	|	0.57
13.250	0.00	0.18	0.098	O	|	|	|	0.57
13.333	0.00	0.18	0.097	O	|	|	|	0.56
13.417	0.00	0.17	0.095	O	|	|	|	0.56
13.500	0.00	0.17	0.094	O	|	|	|	0.55
13.583	0.00	0.17	0.093	O	|	|	|	0.55
13.667	0.00	0.17	0.092	O	|	|	|	0.54
13.750	0.00	0.17	0.091	O	|	|	|	0.54
13.833	0.00	0.17	0.089	O	|	|	|	0.53
13.917	0.00	0.17	0.088	O	|	|	|	0.53
14.000	0.00	0.17	0.087	O	|	|	|	0.52
14.083	0.00	0.17	0.086	O	|	|	|	0.52
14.167	0.00	0.17	0.085	O	|	|	|	0.51
14.250	0.00	0.17	0.084	O	|	|	|	0.51
14.333	0.00	0.17	0.082	O	|	|	|	0.51
14.417	0.00	0.17	0.081	O	|	|	|	0.50
14.500	0.00	0.17	0.080	O	|	|	|	0.50
14.583	0.00	0.17	0.079	O	|	|	|	0.49
14.667	0.00	0.16	0.078	O	|	|	|	0.49
14.750	0.00	0.16	0.077	O	|	|	|	0.48
14.833	0.00	0.16	0.076	O	|	|	|	0.48
14.917	0.00	0.16	0.074	O	|	|	|	0.47
15.000	0.00	0.16	0.073	O	|	|	|	0.47
15.083	0.00	0.16	0.072	O	|	|	|	0.46
15.167	0.00	0.16	0.071	O	|	|	|	0.46
15.250	0.00	0.16	0.070	O	|	|	|	0.45
15.333	0.00	0.16	0.069	O	|	|	|	0.45
15.417	0.00	0.16	0.068	O	|	|	|	0.45
15.500	0.00	0.16	0.067	O	|	|	|	0.44
15.583	0.00	0.16	0.066	O	|	|	|	0.44
15.667	0.00	0.15	0.065	O	|	|	|	0.43
15.750	0.00	0.15	0.064	O	|	|	|	0.43
15.833	0.00	0.15	0.062	O	|	|	|	0.42
15.917	0.00	0.15	0.061	O	|	|	|	0.42
16.000	0.00	0.15	0.060	O	|	|	|	0.42
16.083	0.00	0.15	0.059	O	|	|	|	0.41
16.167	0.00	0.15	0.058	O	|	|	|	0.41
16.250	0.00	0.15	0.057	O	|	|	|	0.40
16.333	0.00	0.15	0.056	O	|	|	|	0.40
16.417	0.00	0.15	0.055	O	|	|	|	0.39
16.500	0.00	0.15	0.054	O	|	|	|	0.39
16.583	0.00	0.15	0.053	O	|	|	|	0.39
16.667	0.00	0.15	0.052	O	|	|	|	0.38
16.750	0.00	0.14	0.051	O	|	|	|	0.38
16.833	0.00	0.14	0.050	O	|	|	|	0.37
16.917	0.00	0.14	0.049	O	|	|	|	0.37
17.000	0.00	0.14	0.048	O	|	|	|	0.37
17.083	0.00	0.14	0.047	O	|	|	|	0.36
17.167	0.00	0.14	0.046	O	|	|	|	0.36
17.250	0.00	0.14	0.045	O	|	|	|	0.35
17.333	0.00	0.14	0.044	O	|	|	|	0.35
17.417	0.00	0.14	0.043	O	|	|	|	0.35

17.500	0.00	0.14	0.042	O	|	|	|	0.34
17.583	0.00	0.14	0.041	O	|	|	|	0.34
17.667	0.00	0.14	0.041	O	|	|	|	0.33
17.750	0.00	0.14	0.040	O	|	|	|	0.33
17.833	0.00	0.13	0.039	O	|	|	|	0.32
17.917	0.00	0.13	0.038	O	|	|	|	0.32
18.000	0.00	0.13	0.037	O	|	|	|	0.32
18.083	0.00	0.13	0.036	O	|	|	|	0.31
18.167	0.00	0.13	0.035	O	|	|	|	0.31
18.250	0.00	0.13	0.034	O	|	|	|	0.30
18.333	0.00	0.13	0.033	O	|	|	|	0.30
18.417	0.00	0.13	0.032	O	|	|	|	0.30
18.500	0.00	0.13	0.031	O	|	|	|	0.29
18.583	0.00	0.13	0.031	O	|	|	|	0.29
18.667	0.00	0.13	0.030	O	|	|	|	0.28
18.750	0.00	0.12	0.029	O	|	|	|	0.28
18.833	0.00	0.12	0.028	O	|	|	|	0.28
18.917	0.00	0.12	0.027	O	|	|	|	0.27
19.000	0.00	0.12	0.026	O	|	|	|	0.27
19.083	0.00	0.12	0.025	O	|	|	|	0.27
19.167	0.00	0.12	0.025	O	|	|	|	0.26
19.250	0.00	0.12	0.024	O	|	|	|	0.26
19.333	0.00	0.12	0.023	O	|	|	|	0.25
19.417	0.00	0.12	0.022	O	|	|	|	0.25
19.500	0.00	0.11	0.021	O	|	|	|	0.24
19.583	0.00	0.11	0.021	O	|	|	|	0.23
19.667	0.00	0.11	0.020	O	|	|	|	0.23
19.750	0.00	0.10	0.019	O	|	|	|	0.22
19.833	0.00	0.10	0.018	O	|	|	|	0.21
19.917	0.00	0.10	0.018	O	|	|	|	0.20
20.000	0.00	0.09	0.017	O	|	|	|	0.19
20.083	0.00	0.09	0.016	O	|	|	|	0.19
20.167	0.00	0.09	0.016	O	|	|	|	0.18
20.250	0.00	0.08	0.015	O	|	|	|	0.17
20.333	0.00	0.08	0.015	O	|	|	|	0.17
20.417	0.00	0.08	0.014	O	|	|	|	0.16
20.500	0.00	0.07	0.014	O	|	|	|	0.16
20.583	0.00	0.07	0.013	O	|	|	|	0.15
20.667	0.00	0.07	0.013	O	|	|	|	0.14
20.750	0.00	0.07	0.012	O	|	|	|	0.14
20.833	0.00	0.06	0.012	O	|	|	|	0.13
20.917	0.00	0.06	0.011	O	|	|	|	0.13
21.000	0.00	0.06	0.011	O	|	|	|	0.12
21.083	0.00	0.06	0.011	O	|	|	|	0.12
21.167	0.00	0.05	0.010	O	|	|	|	0.12
21.250	0.00	0.05	0.010	O	|	|	|	0.11
21.333	0.00	0.05	0.009	O	|	|	|	0.11
21.417	0.00	0.05	0.009	O	|	|	|	0.10
21.500	0.00	0.05	0.009	O	|	|	|	0.10
21.583	0.00	0.05	0.008	O	|	|	|	0.10
21.667	0.00	0.04	0.008	O	|	|	|	0.09
21.750	0.00	0.04	0.008	O	|	|	|	0.09
21.833	0.00	0.04	0.008	O	|	|	|	0.09
21.917	0.00	0.04	0.007	O	|	|	|	0.08
22.000	0.00	0.04	0.007	O	|	|	|	0.08
22.083	0.00	0.04	0.007	O	|	|	|	0.08
22.167	0.00	0.04	0.007	O	|	|	|	0.07
22.250	0.00	0.03	0.006	O	|	|	|	0.07
22.333	0.00	0.03	0.006	O	|	|	|	0.07
22.417	0.00	0.03	0.006	O	|	|	|	0.07
22.500	0.00	0.03	0.006	O	|	|	|	0.06
22.583	0.00	0.03	0.005	O	|	|	|	0.06
22.667	0.00	0.03	0.005	O	|	|	|	0.06
22.750	0.00	0.03	0.005	O	|	|	|	0.06
22.833	0.00	0.03	0.005	O	|	|	|	0.06
22.917	0.00	0.03	0.005	O	|	|	|	0.05
23.000	0.00	0.02	0.005	O	|	|	|	0.05
23.083	0.00	0.02	0.004	O	|	|	|	0.05
23.167	0.00	0.02	0.004	O	|	|	|	0.05
23.250	0.00	0.02	0.004	O	|	|	|	0.05
23.333	0.00	0.02	0.004	O	|	|	|	0.04
23.417	0.00	0.02	0.004	O	|	|	|	0.04

23.500	0.00	0.02	0.004	O	|	|	|	0.04
23.583	0.00	0.02	0.003	O	|	|	|	0.04
23.667	0.00	0.02	0.003	O	|	|	|	0.04
23.750	0.00	0.02	0.003	O	|	|	|	0.04
23.833	0.00	0.02	0.003	O	|	|	|	0.04
23.917	0.00	0.02	0.003	O	|	|	|	0.03
24.000	0.00	0.02	0.003	O	|	|	|	0.03
24.083	0.00	0.01	0.003	O	|	|	|	0.03
24.167	0.00	0.01	0.003	O	|	|	|	0.03
24.250	0.00	0.01	0.003	O	|	|	|	0.03
24.333	0.00	0.01	0.003	O	|	|	|	0.03
24.417	0.00	0.01	0.002	O	|	|	|	0.03
24.500	0.00	0.01	0.002	O	|	|	|	0.03
24.583	0.00	0.01	0.002	O	|	|	|	0.03
24.667	0.00	0.01	0.002	O	|	|	|	0.02
24.750	0.00	0.01	0.002	O	|	|	|	0.02
24.833	0.00	0.01	0.002	O	|	|	|	0.02
24.917	0.00	0.01	0.002	O	|	|	|	0.02
25.000	0.00	0.01	0.002	O	|	|	|	0.02
25.083	0.00	0.01	0.002	O	|	|	|	0.02
25.167	0.00	0.01	0.002	O	|	|	|	0.02
25.250	0.00	0.01	0.002	O	|	|	|	0.02
25.333	0.00	0.01	0.002	O	|	|	|	0.02
25.417	0.00	0.01	0.002	O	|	|	|	0.02
25.500	0.00	0.01	0.001	O	|	|	|	0.02
25.583	0.00	0.01	0.001	O	|	|	|	0.02
25.667	0.00	0.01	0.001	O	|	|	|	0.02
25.750	0.00	0.01	0.001	O	|	|	|	0.02
25.833	0.00	0.01	0.001	O	|	|	|	0.01
25.917	0.00	0.01	0.001	O	|	|	|	0.01
26.000	0.00	0.01	0.001	O	|	|	|	0.01
26.083	0.00	0.01	0.001	O	|	|	|	0.01
26.167	0.00	0.01	0.001	O	|	|	|	0.01
26.250	0.00	0.01	0.001	O	|	|	|	0.01
26.333	0.00	0.01	0.001	O	|	|	|	0.01
26.417	0.00	0.01	0.001	O	|	|	|	0.01
26.500	0.00	0.01	0.001	O	|	|	|	0.01
26.583	0.00	0.00	0.001	O	|	|	|	0.01
26.667	0.00	0.00	0.001	O	|	|	|	0.01
26.750	0.00	0.00	0.001	O	|	|	|	0.01
26.833	0.00	0.00	0.001	O	|	|	|	0.01
26.917	0.00	0.00	0.001	O	|	|	|	0.01
27.000	0.00	0.00	0.001	O	|	|	|	0.01
27.083	0.00	0.00	0.001	O	|	|	|	0.01
27.167	0.00	0.00	0.001	O	|	|	|	0.01
27.250	0.00	0.00	0.001	O	|	|	|	0.01
27.333	0.00	0.00	0.001	O	|	|	|	0.01
27.417	0.00	0.00	0.001	O	|	|	|	0.01
27.500	0.00	0.00	0.001	O	|	|	|	0.01
27.583	0.00	0.00	0.001	O	|	|	|	0.01
27.667	0.00	0.00	0.001	O	|	|	|	0.01
27.750	0.00	0.00	0.001	O	|	|	|	0.01
27.833	0.00	0.00	0.001	O	|	|	|	0.01
27.917	0.00	0.00	0.001	O	|	|	|	0.01
28.000	0.00	0.00	0.000	O	|	|	|	0.01
28.083	0.00	0.00	0.000	O	|	|	|	0.01
28.167	0.00	0.00	0.000	O	|	|	|	0.01
28.250	0.00	0.00	0.000	O	|	|	|	0.01
28.333	0.00	0.00	0.000	O	|	|	|	0.00
28.417	0.00	0.00	0.000	O	|	|	|	0.00
28.500	0.00	0.00	0.000	O	|	|	|	0.00
28.583	0.00	0.00	0.000	O	|	|	|	0.00
28.667	0.00	0.00	0.000	O	|	|	|	0.00
28.750	0.00	0.00	0.000	O	|	|	|	0.00
28.833	0.00	0.00	0.000	O	|	|	|	0.00
28.917	0.00	0.00	0.000	O	|	|	|	0.00
29.000	0.00	0.00	0.000	O	|	|	|	0.00
29.083	0.00	0.00	0.000	O	|	|	|	0.00
29.167	0.00	0.00	0.000	O	|	|	|	0.00
29.250	0.00	0.00	0.000	O	|	|	|	0.00
29.333	0.00	0.00	0.000	O	|	|	|	0.00
29.417	0.00	0.00	0.000	O	|	|	|	0.00

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29.500    0.00    0.00      0.000  O       |       |       |       |     0.00
29.583    0.00    0.00      0.000  O       |       |       |       |     0.00
29.667    0.00    0.00      0.000  O       |       |       |       |     0.00
29.750    0.00    0.00      0.000  O       |       |       |       |     0.00
29.833    0.00    0.00      0.000  O       |       |       |       |     0.00
29.917    0.00    0.00      0.000  O       |       |       |       |     0.00
30.000    0.00    0.00      0.000  O       |       |       |       |     0.00
30.083    0.00    0.00      0.000  O       |       |       |       |     0.00
30.167    0.00    0.00      0.000  O       |       |       |       |     0.00
30.250    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =   363
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.289 (CFS)
                      Total volume =       0.346 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

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Temescal Canyon Self Storage - Riverside County
Underground Storage Analysis

East

Storage

Arch Span (ft)	Arch Rise (ft)	Number Rows (#)	Row Length (ft)	Row Slope (ft/ft)	Invert (D/S) (ft)	Invert U/S (ft)
16	5	1	600	0.0010	897.94	898.54

Low Flow Discharge

Orifice C ()	Number Outlets (#)	Outlet Diameter (in)	Outlet Invert (ft)	Outlet Soffit (ft)
0.60	1	3	897.94	898.19

High Flow Discharge

Orifice C ()	Number Outlets (#)	Outlet Diameter (in)	Outlet Invert (ft)	Outlet Soffit (ft)
0.60	1	12	901.84	902.84

Rating Curve

Elevation (ft)	Depth (ft)	Storage (cu-ft)	Storage (ac-ft)	Low Flow Discharge (cfs)	High Flow Discharge (cfs)	Total Discharge (cfs)
897.94	0.00	0	0.000	0.000	0.000	0.000
898.19	0.25	480	0.011	0.118	0.000	0.118
898.44	0.50	2,000	0.046	0.167	0.000	0.167
898.54	0.60	2,880	0.066	0.183	0.000	0.183
898.94	1.00	6,672	0.153	0.236	0.000	0.236
899.44	1.50	11,472	0.263	0.289	0.000	0.289
899.75	1.81	14,396	0.330	0.318	0.000	0.318
899.94	2.00	16,266	0.373	0.334	0.000	0.334
900.44	2.50	21,025	0.483	0.374	0.000	0.374
900.94	3.00	25,703	0.590	0.409	0.000	0.409
901.44	3.50	30,233	0.694	0.442	0.000	0.442
901.84	3.90	33,633	0.772	0.467	0.000	0.467
901.94	4.00	34,530	0.793	0.473	0.062	0.535
902.44	4.50	38,402	0.882	0.501	1.835	2.336
902.84	4.90	40,663	0.933	0.523	3.782	4.305
902.94	5.00	41,237	0.947	0.529	3.966	4.495
903.44	5.50	42,405	0.973	0.554	4.783	5.338
903.54	5.60	42,624	0.979	0.559	4.931	5.490

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
24-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD02242.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.365 (CFS)
Total volume = 0.830 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

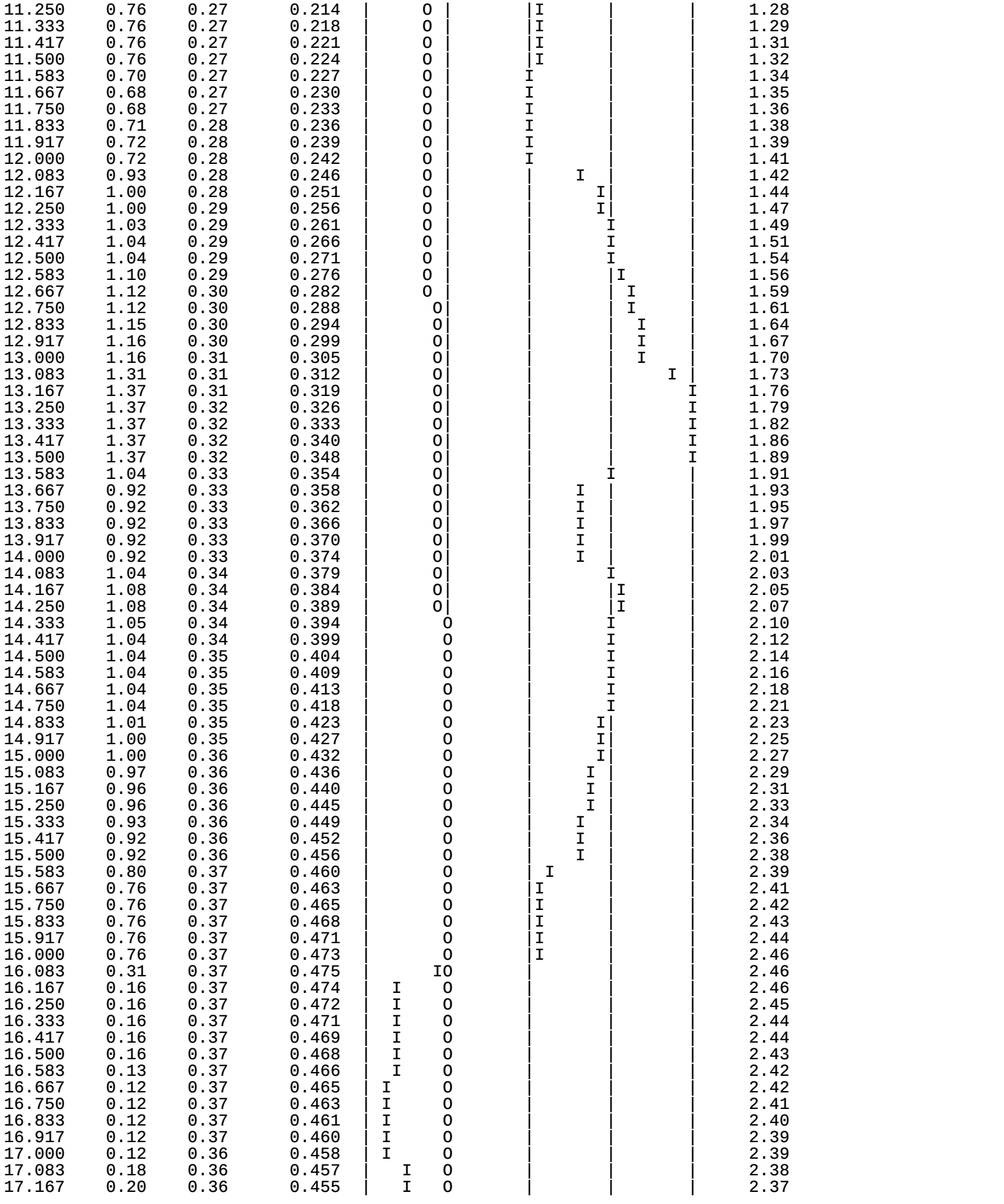
5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.3	0.68	1.02	1.37	Depth (Ft.)
0.083	0.06	0.00	0.000	OI					0.00
0.167	0.08	0.01	0.001	OI					0.01
0.250	0.08	0.01	0.001	OI					0.03
0.333	0.11	0.02	0.002	O I					0.04
0.417	0.12	0.03	0.002	O I					0.05
0.500	0.12	0.03	0.003	O I					0.07
0.583	0.12	0.04	0.004	O I					0.08
0.667	0.12	0.04	0.004	|OI					0.09
0.750	0.12	0.05	0.005	|OI					0.10
0.833	0.15	0.06	0.005	|O I					0.12
0.917	0.16	0.06	0.006	|O I					0.13
1.000	0.16	0.07	0.006	|O I					0.15
1.083	0.13	0.08	0.007	|O I					0.16
1.167	0.12	0.08	0.007	|OI					0.17
1.250	0.12	0.08	0.008	|OI					0.17
1.333	0.12	0.08	0.008	|OI					0.18
1.417	0.12	0.09	0.008	| O					0.18
1.500	0.12	0.09	0.008	| O					0.19
1.583	0.12	0.09	0.009	| O					0.19
1.667	0.12	0.09	0.009	| O					0.20
1.750	0.12	0.10	0.009	| O					0.20
1.833	0.15	0.10	0.009	| OI					0.21
1.917	0.16	0.10	0.010	| OI					0.22
2.000	0.16	0.11	0.010	| OI					0.23
2.083	0.16	0.11	0.010	| OI					0.23
2.167	0.16	0.11	0.011	| OI					0.24
2.250	0.16	0.12	0.011	| OI					0.25
2.333	0.16	0.12	0.011	| OI					0.25
2.417	0.16	0.12	0.012	| OI					0.25
2.500	0.16	0.12	0.012	| OI					0.26
2.583	0.19	0.12	0.012	| O I					0.26
2.667	0.20	0.12	0.013	| O I					0.26
2.750	0.20	0.12	0.013	| O I					0.27
2.833	0.20	0.12	0.014	| O I					0.27
2.917	0.20	0.12	0.014	| O I					0.27
3.000	0.20	0.12	0.015	| O I					0.28
3.083	0.20	0.12	0.015	| O I					0.28
3.167	0.20	0.12	0.016	| O I					0.29
3.250	0.20	0.13	0.016	| O I					0.29
3.333	0.20	0.13	0.017	| O I					0.29
3.417	0.20	0.13	0.017	| O I					0.30
3.500	0.20	0.13	0.018	| O I					0.30
3.583	0.20	0.13	0.018	| OI					0.30
3.667	0.20	0.13	0.019	| OI					0.31
3.750	0.20	0.13	0.019	| OI					0.31
3.833	0.23	0.13	0.020	| O I					0.31
3.917	0.24	0.13	0.021	| O I					0.32
4.000	0.24	0.13	0.022	| O I					0.33
4.083	0.24	0.13	0.022	| O I					0.33
4.167	0.24	0.13	0.023	| O I					0.34
4.250	0.24	0.14	0.024	| O I					0.34
4.333	0.27	0.14	0.025	| O I					0.35
4.417	0.28	0.14	0.026	| O I					0.35
4.500	0.28	0.14	0.026	| O I					0.36
4.583	0.28	0.14	0.027	| O I					0.37
4.667	0.28	0.14	0.028	| O I					0.37
4.750	0.28	0.14	0.029	| O I					0.38
4.833	0.31	0.15	0.030	| O I					0.39
4.917	0.32	0.15	0.032	| O I					0.40
5.000	0.32	0.15	0.033	| O I					0.41
5.083	0.26	0.15	0.034	| O I					0.41
5.167	0.24	0.15	0.034	| O I					0.42

5.250	0.24	0.15	0.035	O I				0.42
5.333	0.27	0.15	0.036	O I				0.43
5.417	0.28	0.15	0.037	O I				0.43
5.500	0.28	0.16	0.038	O I				0.44
5.583	0.31	0.16	0.038	O I				0.45
5.667	0.32	0.16	0.040	O I				0.45
5.750	0.32	0.16	0.041	O I				0.46
5.833	0.32	0.16	0.042	O I				0.47
5.917	0.32	0.16	0.043	O I				0.48
6.000	0.32	0.16	0.044	O I				0.49
6.083	0.35	0.17	0.045	O I				0.49
6.167	0.36	0.17	0.046	O I				0.50
6.250	0.36	0.17	0.048	O I				0.51
6.333	0.36	0.17	0.049	O I				0.52
6.417	0.36	0.17	0.050	O I				0.52
6.500	0.36	0.17	0.052	O I				0.53
6.583	0.39	0.17	0.053	O I				0.54
6.667	0.40	0.17	0.055	O I				0.54
6.750	0.40	0.18	0.056	O I				0.55
6.833	0.40	0.18	0.058	O I				0.56
6.917	0.40	0.18	0.059	O I				0.57
7.000	0.40	0.18	0.061	O I				0.57
7.083	0.40	0.18	0.062	O I				0.58
7.167	0.40	0.18	0.064	O I				0.59
7.250	0.40	0.18	0.065	O I				0.60
7.333	0.43	0.18	0.067	O I				0.60
7.417	0.44	0.18	0.069	O I				0.61
7.500	0.44	0.19	0.071	O I				0.62
7.583	0.47	0.19	0.072	O I				0.63
7.667	0.48	0.19	0.074	O I				0.64
7.750	0.48	0.19	0.076	O I				0.65
7.833	0.51	0.19	0.079	O I				0.66
7.917	0.52	0.19	0.081	O I				0.67
8.000	0.52	0.19	0.083	O I				0.68
8.083	0.58	0.19	0.086	O I				0.69
8.167	0.60	0.20	0.088	O I				0.70
8.250	0.60	0.20	0.091	O I				0.72
8.333	0.60	0.20	0.094	O I				0.73
8.417	0.60	0.20	0.097	O I				0.74
8.500	0.60	0.20	0.099	O I				0.75
8.583	0.63	0.21	0.102	O I				0.77
8.667	0.64	0.21	0.105	O I				0.78
8.750	0.64	0.21	0.108	O I				0.79
8.833	0.67	0.21	0.111	O I				0.81
8.917	0.68	0.21	0.114	O I				0.82
9.000	0.68	0.21	0.118	O I				0.84
9.083	0.74	0.22	0.121	O I				0.85
9.167	0.76	0.22	0.125	O I				0.87
9.250	0.76	0.22	0.129	O I				0.89
9.333	0.79	0.22	0.132	O I				0.90
9.417	0.80	0.23	0.136	O I				0.92
9.500	0.80	0.23	0.140	O I				0.94
9.583	0.83	0.23	0.144	O I				0.96
9.667	0.84	0.23	0.148	O I				0.98
9.750	0.84	0.24	0.153	O I				1.00
9.833	0.87	0.24	0.157	O I				1.02
9.917	0.88	0.24	0.161	O I				1.04
10.000	0.88	0.24	0.166	O I				1.06
10.083	0.67	0.24	0.169	O I				1.07
10.167	0.60	0.25	0.172	O I				1.09
10.250	0.60	0.25	0.175	O I				1.10
10.333	0.60	0.25	0.177	O I				1.11
10.417	0.60	0.25	0.180	O I				1.12
10.500	0.60	0.25	0.182	O I				1.13
10.583	0.75	0.25	0.185	O I				1.14
10.667	0.80	0.25	0.188	O I				1.16
10.750	0.80	0.25	0.192	O I				1.18
10.833	0.80	0.26	0.196	O I				1.20
10.917	0.80	0.26	0.200	O I				1.21
11.000	0.80	0.26	0.204	O I				1.23
11.083	0.77	0.26	0.207	O I				1.25
11.167	0.76	0.26	0.211	O I				1.26



11.250	0.76	0.27	0.214	O	I		1.28
11.333	0.76	0.27	0.218	O	I		1.29
11.417	0.76	0.27	0.221	O	I		1.31
11.500	0.76	0.27	0.224	O	I		1.32
11.583	0.70	0.27	0.227	O	I		1.34
11.667	0.68	0.27	0.230	O	I		1.35
11.750	0.68	0.27	0.233	O	I		1.36
11.833	0.71	0.28	0.236	O	I		1.38
11.917	0.72	0.28	0.239	O	I		1.39
12.000	0.72	0.28	0.242	O	I		1.41
12.083	0.93	0.28	0.246	O	I		1.42
12.167	1.00	0.28	0.251	O	I		1.44
12.250	1.00	0.29	0.256	O	I		1.47
12.333	1.03	0.29	0.261	O	I		1.49
12.417	1.04	0.29	0.266	O	I		1.51
12.500	1.04	0.29	0.271	O	I		1.54
12.583	1.10	0.29	0.276	O	I		1.56
12.667	1.12	0.30	0.282	O	I		1.59
12.750	1.12	0.30	0.288	O	I		1.61
12.833	1.15	0.30	0.294	O	I		1.64
12.917	1.16	0.30	0.299	O	I		1.67
13.000	1.16	0.31	0.305	O	I		1.70
13.083	1.31	0.31	0.312	O	I		1.73
13.167	1.37	0.31	0.319	O	I		1.76
13.250	1.37	0.32	0.326	O	I		1.79
13.333	1.37	0.32	0.333	O	I		1.82
13.417	1.37	0.32	0.340	O	I		1.86
13.500	1.37	0.32	0.348	O	I		1.89
13.583	1.04	0.33	0.354	O	I		1.91
13.667	0.92	0.33	0.358	O	I		1.93
13.750	0.92	0.33	0.362	O	I		1.95
13.833	0.92	0.33	0.366	O	I		1.97
13.917	0.92	0.33	0.370	O	I		1.99
14.000	0.92	0.33	0.374	O	I		2.01
14.083	1.04	0.34	0.379	O	I		2.03
14.167	1.08	0.34	0.384	O	I		2.05
14.250	1.08	0.34	0.389	O	I		2.07
14.333	1.05	0.34	0.394	O	I		2.10
14.417	1.04	0.34	0.399	O	I		2.12
14.500	1.04	0.35	0.404	O	I		2.14
14.583	1.04	0.35	0.409	O	I		2.16
14.667	1.04	0.35	0.413	O	I		2.18
14.750	1.04	0.35	0.418	O	I		2.21
14.833	1.01	0.35	0.423	O	I		2.23
14.917	1.00	0.35	0.427	O	I		2.25
15.000	1.00	0.36	0.432	O	I		2.27
15.083	0.97	0.36	0.436	O	I		2.29
15.167	0.96	0.36	0.440	O	I		2.31
15.250	0.96	0.36	0.445	O	I		2.33
15.333	0.93	0.36	0.449	O	I		2.34
15.417	0.92	0.36	0.452	O	I		2.36
15.500	0.92	0.36	0.456	O	I		2.38
15.583	0.80	0.37	0.460	O	I		2.39
15.667	0.76	0.37	0.463	O	I		2.41
15.750	0.76	0.37	0.465	O	I		2.42
15.833	0.76	0.37	0.468	O	I		2.43
15.917	0.76	0.37	0.471	O	I		2.44
16.000	0.76	0.37	0.473	O	I		2.46
16.083	0.31	0.37	0.475	IO			2.46
16.167	0.16	0.37	0.474	I O			2.46
16.250	0.16	0.37	0.472	I O			2.45
16.333	0.16	0.37	0.471	I O			2.44
16.417	0.16	0.37	0.469	I O			2.44
16.500	0.16	0.37	0.468	I O			2.43
16.583	0.13	0.37	0.466	I O			2.42
16.667	0.12	0.37	0.465	I O			2.42
16.750	0.12	0.37	0.463	I O			2.41
16.833	0.12	0.37	0.461	I O			2.40
16.917	0.12	0.37	0.460	I O			2.39
17.000	0.12	0.36	0.458	I O			2.39
17.083	0.18	0.36	0.457	I O			2.38
17.167	0.20	0.36	0.455	I O			2.37

17.250	0.20	0.36	0.454	| I O |	|	|	2.37
17.333	0.20	0.36	0.453	| I O |	|	|	2.36
17.417	0.20	0.36	0.452	| I O |	|	|	2.36
17.500	0.20	0.36	0.451	| I O |	|	|	2.35
17.583	0.20	0.36	0.450	| I O |	|	|	2.35
17.667	0.20	0.36	0.449	| I O |	|	|	2.34
17.750	0.20	0.36	0.448	| I O |	|	|	2.34
17.833	0.17	0.36	0.446	| I O |	|	|	2.33
17.917	0.16	0.36	0.445	| I O |	|	|	2.33
18.000	0.16	0.36	0.444	| I O |	|	|	2.32
18.083	0.16	0.36	0.442	| I O |	|	|	2.31
18.167	0.16	0.36	0.441	| I O |	|	|	2.31
18.250	0.16	0.36	0.440	| I O |	|	|	2.30
18.333	0.16	0.36	0.438	| I O |	|	|	2.30
18.417	0.16	0.36	0.437	| I O |	|	|	2.29
18.500	0.16	0.36	0.435	| I O |	|	|	2.28
18.583	0.13	0.36	0.434	| I O |	|	|	2.28
18.667	0.12	0.36	0.432	| I O |	|	|	2.27
18.750	0.12	0.36	0.431	| I O |	|	|	2.26
18.833	0.09	0.35	0.429	| I O |	|	|	2.25
18.917	0.08	0.35	0.427	|I O |	|	|	2.25
19.000	0.08	0.35	0.425	|I O |	|	|	2.24
19.083	0.11	0.35	0.424	| I O |	|	|	2.23
19.167	0.12	0.35	0.422	| I O |	|	|	2.22
19.250	0.12	0.35	0.420	| I O |	|	|	2.22
19.333	0.15	0.35	0.419	| I O |	|	|	2.21
19.417	0.16	0.35	0.418	| I O |	|	|	2.20
19.500	0.16	0.35	0.416	| I O |	|	|	2.20
19.583	0.13	0.35	0.415	| I O |	|	|	2.19
19.667	0.12	0.35	0.413	| I O |	|	|	2.18
19.750	0.12	0.35	0.412	| I O |	|	|	2.18
19.833	0.09	0.35	0.410	| I O |	|	|	2.17
19.917	0.08	0.35	0.408	|I O |	|	|	2.16
20.000	0.08	0.35	0.406	|I O |	|	|	2.15
20.083	0.11	0.35	0.405	| I O |	|	|	2.14
20.167	0.12	0.34	0.403	| I O |	|	|	2.14
20.250	0.12	0.34	0.402	| I O |	|	|	2.13
20.333	0.12	0.34	0.400	| I O |	|	|	2.12
20.417	0.12	0.34	0.398	| I O |	|	|	2.12
20.500	0.12	0.34	0.397	| I O |	|	|	2.11
20.583	0.12	0.34	0.395	| I O |	|	|	2.10
20.667	0.12	0.34	0.394	| I O |	|	|	2.09
20.750	0.12	0.34	0.392	| I O|	|	|	2.09
20.833	0.09	0.34	0.391	| I O|	|	|	2.08
20.917	0.08	0.34	0.389	|I O|	|	|	2.07
21.000	0.08	0.34	0.387	|I O|	|	|	2.06
21.083	0.11	0.34	0.386	| I O|	|	|	2.06
21.167	0.12	0.34	0.384	| I O|	|	|	2.05
21.250	0.12	0.34	0.382	| I O|	|	|	2.04
21.333	0.09	0.34	0.381	| I O|	|	|	2.04
21.417	0.08	0.34	0.379	|I O|	|	|	2.03
21.500	0.08	0.34	0.377	|I O|	|	|	2.02
21.583	0.11	0.33	0.376	| I O|	|	|	2.01
21.667	0.12	0.33	0.374	| I O|	|	|	2.01
21.750	0.12	0.33	0.373	| I O|	|	|	2.00
21.833	0.09	0.33	0.371	| I O|	|	|	1.99
21.917	0.08	0.33	0.369	|I O|	|	|	1.98
22.000	0.08	0.33	0.368	|I O|	|	|	1.98
22.083	0.11	0.33	0.366	| I O|	|	|	1.97
22.167	0.12	0.33	0.365	| I O|	|	|	1.96
22.250	0.12	0.33	0.363	| I O|	|	|	1.96
22.333	0.09	0.33	0.362	| I O|	|	|	1.95
22.417	0.08	0.33	0.360	|I O|	|	|	1.94
22.500	0.08	0.33	0.358	|I O|	|	|	1.93
22.583	0.08	0.33	0.357	|I O|	|	|	1.93
22.667	0.08	0.33	0.355	|I O|	|	|	1.92
22.750	0.08	0.33	0.353	|I O|	|	|	1.91
22.833	0.08	0.33	0.351	|I O|	|	|	1.90
22.917	0.08	0.33	0.350	|I O|	|	|	1.90
23.000	0.08	0.32	0.348	|I O|	|	|	1.89
23.083	0.08	0.32	0.346	|I O|	|	|	1.88
23.167	0.08	0.32	0.345	|I O|	|	|	1.88

23.250	0.08	0.32	0.343	|I O|				1.87
23.333	0.08	0.32	0.341	|I O|				1.86
23.417	0.08	0.32	0.340	|I O|				1.85
23.500	0.08	0.32	0.338	|I O|				1.85
23.583	0.08	0.32	0.336	|I O|				1.84
23.667	0.08	0.32	0.335	|I O|				1.83
23.750	0.08	0.32	0.333	|I O|				1.82
23.833	0.08	0.32	0.331	|I O|				1.82
23.917	0.08	0.32	0.330	|I O|				1.81
24.000	0.08	0.32	0.328	|I O|				1.80
24.083	0.02	0.32	0.326	I O|				1.79
24.167	0.00	0.32	0.324	I O|				1.78
24.250	0.00	0.31	0.322	I O|				1.77
24.333	0.00	0.31	0.320	I O|				1.76
24.417	0.00	0.31	0.318	I O|				1.75
24.500	0.00	0.31	0.316	I O|				1.74
24.583	0.00	0.31	0.313	I O|				1.73
24.667	0.00	0.31	0.311	I O|				1.72
24.750	0.00	0.31	0.309	I O|				1.71
24.833	0.00	0.31	0.307	I O|				1.70
24.917	0.00	0.31	0.305	I O|				1.69
25.000	0.00	0.31	0.303	I O|				1.68
25.083	0.00	0.31	0.301	I O|				1.67
25.167	0.00	0.30	0.299	I O|				1.66
25.250	0.00	0.30	0.297	I O|				1.66
25.333	0.00	0.30	0.294	I O|				1.65
25.417	0.00	0.30	0.292	I O|				1.64
25.500	0.00	0.30	0.290	I O|				1.63
25.583	0.00	0.30	0.288	I O|				1.62
25.667	0.00	0.30	0.286	I O|				1.61
25.750	0.00	0.30	0.284	I O |				1.60
25.833	0.00	0.30	0.282	I O |				1.59
25.917	0.00	0.30	0.280	I O |				1.58
26.000	0.00	0.30	0.278	I O |				1.57
26.083	0.00	0.29	0.276	I O |				1.56
26.167	0.00	0.29	0.274	I O |				1.55
26.250	0.00	0.29	0.272	I O |				1.54
26.333	0.00	0.29	0.270	I O |				1.53
26.417	0.00	0.29	0.268	I O |				1.52
26.500	0.00	0.29	0.266	I O |				1.51
26.583	0.00	0.29	0.264	I O |				1.50
26.667	0.00	0.29	0.262	I O |				1.49
26.750	0.00	0.29	0.260	I O |				1.49
26.833	0.00	0.29	0.258	I O |				1.48
26.917	0.00	0.29	0.256	I O |				1.47
27.000	0.00	0.28	0.254	I O |				1.46
27.083	0.00	0.28	0.252	I O |				1.45
27.167	0.00	0.28	0.250	I O |				1.44
27.250	0.00	0.28	0.248	I O |				1.43
27.333	0.00	0.28	0.246	I O |				1.42
27.417	0.00	0.28	0.244	I O |				1.41
27.500	0.00	0.28	0.242	I O |				1.41
27.583	0.00	0.28	0.240	I O |				1.40
27.667	0.00	0.28	0.239	I O |				1.39
27.750	0.00	0.28	0.237	I O |				1.38
27.833	0.00	0.28	0.235	I O |				1.37
27.917	0.00	0.27	0.233	I O |				1.36
28.000	0.00	0.27	0.231	I O |				1.35
28.083	0.00	0.27	0.229	I O |				1.35
28.167	0.00	0.27	0.227	I O |				1.34
28.250	0.00	0.27	0.225	I O |				1.33
28.333	0.00	0.27	0.223	I O |				1.32
28.417	0.00	0.27	0.222	I O |				1.31
28.500	0.00	0.27	0.220	I O |				1.30
28.583	0.00	0.27	0.218	I O |				1.29
28.667	0.00	0.27	0.216	I O |				1.29
28.750	0.00	0.27	0.214	I O |				1.28
28.833	0.00	0.26	0.212	I O |				1.27
28.917	0.00	0.26	0.211	I O |				1.26
29.000	0.00	0.26	0.209	I O |				1.25
29.083	0.00	0.26	0.207	I O |				1.25
29.167	0.00	0.26	0.205	I O |				1.24

29.250	0.00	0.26	0.203	I	O	|	|	|	1.23
29.333	0.00	0.26	0.202	I	O	|	|	|	1.22
29.417	0.00	0.26	0.200	I	O	|	|	|	1.21
29.500	0.00	0.26	0.198	I	O	|	|	|	1.20
29.583	0.00	0.26	0.196	I	O	|	|	|	1.20
29.667	0.00	0.26	0.194	I	O	|	|	|	1.19
29.750	0.00	0.26	0.193	I	O	|	|	|	1.18
29.833	0.00	0.25	0.191	I	O	|	|	|	1.17
29.917	0.00	0.25	0.189	I	O	|	|	|	1.16
30.000	0.00	0.25	0.187	I	O	|	|	|	1.16
30.083	0.00	0.25	0.186	I	O	|	|	|	1.15
30.167	0.00	0.25	0.184	I	O	|	|	|	1.14
30.250	0.00	0.25	0.182	I	O	|	|	|	1.13
30.333	0.00	0.25	0.181	I	O	|	|	|	1.13
30.417	0.00	0.25	0.179	I	O	|	|	|	1.12
30.500	0.00	0.25	0.177	I	O	|	|	|	1.11
30.583	0.00	0.25	0.175	I	O	|	|	|	1.10
30.667	0.00	0.25	0.174	I	O	|	|	|	1.09
30.750	0.00	0.25	0.172	I	O	|	|	|	1.09
30.833	0.00	0.24	0.170	I	O	|	|	|	1.08
30.917	0.00	0.24	0.169	I	O	|	|	|	1.07
31.000	0.00	0.24	0.167	I	O	|	|	|	1.06
31.083	0.00	0.24	0.165	I	O	|	|	|	1.06
31.167	0.00	0.24	0.164	I	O	|	|	|	1.05
31.250	0.00	0.24	0.162	I	O	|	|	|	1.04
31.333	0.00	0.24	0.160	I	O	|	|	|	1.03
31.417	0.00	0.24	0.159	I	O	|	|	|	1.03
31.500	0.00	0.24	0.157	I	O	|	|	|	1.02
31.583	0.00	0.24	0.155	I	O	|	|	|	1.01
31.667	0.00	0.24	0.154	I	O	|	|	|	1.00
31.750	0.00	0.24	0.152	I	O	|	|	|	1.00
31.833	0.00	0.23	0.151	I	O	|	|	|	0.99
31.917	0.00	0.23	0.149	I	O	|	|	|	0.98
32.000	0.00	0.23	0.147	I	O	|	|	|	0.97
32.083	0.00	0.23	0.146	I	O	|	|	|	0.97
32.167	0.00	0.23	0.144	I	O	|	|	|	0.96
32.250	0.00	0.23	0.143	I	O	|	|	|	0.95
32.333	0.00	0.23	0.141	I	O	|	|	|	0.94
32.417	0.00	0.23	0.139	I	O	|	|	|	0.94
32.500	0.00	0.23	0.138	I	O	|	|	|	0.93
32.583	0.00	0.23	0.136	I	O	|	|	|	0.92
32.667	0.00	0.22	0.135	I	O	|	|	|	0.92
32.750	0.00	0.22	0.133	I	O	|	|	|	0.91
32.833	0.00	0.22	0.132	I	O	|	|	|	0.90
32.917	0.00	0.22	0.130	I	O	|	|	|	0.89
33.000	0.00	0.22	0.129	I	O	|	|	|	0.89
33.083	0.00	0.22	0.127	I	O	|	|	|	0.88
33.167	0.00	0.22	0.126	I	O	|	|	|	0.87
33.250	0.00	0.22	0.124	I	O	|	|	|	0.87
33.333	0.00	0.22	0.123	I	O	|	|	|	0.86
33.417	0.00	0.22	0.121	I	O	|	|	|	0.85
33.500	0.00	0.22	0.120	I	O	|	|	|	0.85
33.583	0.00	0.21	0.118	I	O	|	|	|	0.84
33.667	0.00	0.21	0.117	I	O	|	|	|	0.83
33.750	0.00	0.21	0.115	I	O	|	|	|	0.83
33.833	0.00	0.21	0.114	I	O	|	|	|	0.82
33.917	0.00	0.21	0.112	I	O	|	|	|	0.81
34.000	0.00	0.21	0.111	I	O	|	|	|	0.81
34.083	0.00	0.21	0.109	I	O	|	|	|	0.80
34.167	0.00	0.21	0.108	I	O	|	|	|	0.79
34.250	0.00	0.21	0.106	I	O	|	|	|	0.79
34.333	0.00	0.21	0.105	I	O	|	|	|	0.78
34.417	0.00	0.21	0.104	I	O	|	|	|	0.77
34.500	0.00	0.21	0.102	I	O	|	|	|	0.77
34.583	0.00	0.20	0.101	I	O	|	|	|	0.76
34.667	0.00	0.20	0.099	I	O	|	|	|	0.75
34.750	0.00	0.20	0.098	I	O	|	|	|	0.75
34.833	0.00	0.20	0.097	I	O	|	|	|	0.74
34.917	0.00	0.20	0.095	I	O	|	|	|	0.73
35.000	0.00	0.20	0.094	I	O	|	|	|	0.73
35.083	0.00	0.20	0.092	I	O	|	|	|	0.72
35.167	0.00	0.20	0.091	I	O	|	|	|	0.72

35.250	0.00	0.20	0.090	I	O	|	|	|	0.71
35.333	0.00	0.20	0.088	I	O	|	|	|	0.70
35.417	0.00	0.20	0.087	I	O	|	|	|	0.70
35.500	0.00	0.19	0.086	I	O	|	|	|	0.69
35.583	0.00	0.19	0.084	I	O	|	|	|	0.68
35.667	0.00	0.19	0.083	I	O	|	|	|	0.68
35.750	0.00	0.19	0.082	I	O	|	|	|	0.67
35.833	0.00	0.19	0.080	I	O	|	|	|	0.67
35.917	0.00	0.19	0.079	I	O	|	|	|	0.66
36.000	0.00	0.19	0.078	I	O	|	|	|	0.65
36.083	0.00	0.19	0.076	I	O	|	|	|	0.65
36.167	0.00	0.19	0.075	I	O	|	|	|	0.64
36.250	0.00	0.19	0.074	I	O	|	|	|	0.64
36.333	0.00	0.19	0.073	I	O	|	|	|	0.63
36.417	0.00	0.19	0.071	I	O	|	|	|	0.62
36.500	0.00	0.19	0.070	I	O	|	|	|	0.62
36.583	0.00	0.18	0.069	I	O	|	|	|	0.61
36.667	0.00	0.18	0.067	I	O	|	|	|	0.61
36.750	0.00	0.18	0.066	I	O	|	|	|	0.60
36.833	0.00	0.18	0.065	I	O	|	|	|	0.59
36.917	0.00	0.18	0.064	I	O	|	|	|	0.59
37.000	0.00	0.18	0.062	I	O	|	|	|	0.58
37.083	0.00	0.18	0.061	I	O	|	|	|	0.58
37.167	0.00	0.18	0.060	I	O	|	|	|	0.57
37.250	0.00	0.18	0.059	I	O	|	|	|	0.56
37.333	0.00	0.18	0.057	I	O	|	|	|	0.56
37.417	0.00	0.18	0.056	I	O	|	|	|	0.55
37.500	0.00	0.17	0.055	I	O	|	|	|	0.55
37.583	0.00	0.17	0.054	I	O	|	|	|	0.54
37.667	0.00	0.17	0.053	I	O	|	|	|	0.53
37.750	0.00	0.17	0.051	I	O	|	|	|	0.53
37.833	0.00	0.17	0.050	I	O	|	|	|	0.52
37.917	0.00	0.17	0.049	I	O	|	|	|	0.52
38.000	0.00	0.17	0.048	I	O	|	|	|	0.51
38.083	0.00	0.17	0.047	I	O	|	|	|	0.50
38.167	0.00	0.17	0.046	I	O	|	|	|	0.50
38.250	0.00	0.16	0.045	I	O	|	|	|	0.49
38.333	0.00	0.16	0.043	I	O	|	|	|	0.48
38.417	0.00	0.16	0.042	I	O	|	|	|	0.47
38.500	0.00	0.16	0.041	I	O	|	|	|	0.47
38.583	0.00	0.16	0.040	I	O	|	|	|	0.46
38.667	0.00	0.16	0.039	I	O	|	|	|	0.45
38.750	0.00	0.16	0.038	I	O	|	|	|	0.44
38.833	0.00	0.15	0.037	I	O	|	|	|	0.43
38.917	0.00	0.15	0.036	I	O	|	|	|	0.43
39.000	0.00	0.15	0.035	I	O	|	|	|	0.42
39.083	0.00	0.15	0.034	I	O	|	|	|	0.41
39.167	0.00	0.15	0.033	I	O	|	|	|	0.40
39.250	0.00	0.15	0.032	I	O	|	|	|	0.40
39.333	0.00	0.15	0.031	I	O	|	|	|	0.39
39.417	0.00	0.14	0.030	I	O	|	|	|	0.38
39.500	0.00	0.14	0.029	I	O	|	|	|	0.38
39.583	0.00	0.14	0.028	I	O	|	|	|	0.37
39.667	0.00	0.14	0.027	I	O	|	|	|	0.36
39.750	0.00	0.14	0.026	I	O	|	|	|	0.36
39.833	0.00	0.14	0.025	I	O	|	|	|	0.35
39.917	0.00	0.14	0.024	I	O	|	|	|	0.34
40.000	0.00	0.13	0.023	I	O	|	|	|	0.34
40.083	0.00	0.13	0.022	I	O	|	|	|	0.33
40.167	0.00	0.13	0.021	I	O	|	|	|	0.32
40.250	0.00	0.13	0.020	I	O	|	|	|	0.32
40.333	0.00	0.13	0.019	I	O	|	|	|	0.31
40.417	0.00	0.13	0.018	I	O	|	|	|	0.30
40.500	0.00	0.13	0.018	I	O	|	|	|	0.30
40.583	0.00	0.13	0.017	I	O	|	|	|	0.29
40.667	0.00	0.12	0.016	I	O	|	|	|	0.28
40.750	0.00	0.12	0.015	I	O	|	|	|	0.28
40.833	0.00	0.12	0.014	I	O	|	|	|	0.27
40.917	0.00	0.12	0.013	I	O	|	|	|	0.27
41.000	0.00	0.12	0.012	I	O	|	|	|	0.26
41.083	0.00	0.12	0.012	I	O	|	|	|	0.25
41.167	0.00	0.12	0.011	I	O	|	|	|	0.25

41.250	0.00	0.11	0.010	I O	|	|	|	0.23
41.333	0.00	0.10	0.009	I O	|	|	|	0.21
41.417	0.00	0.09	0.009	I O	|	|	|	0.20
41.500	0.00	0.09	0.008	I O	|	|	|	0.18
41.583	0.00	0.08	0.007	IO	|	|	|	0.17
41.667	0.00	0.07	0.007	IO	|	|	|	0.16
41.750	0.00	0.07	0.006	IO	|	|	|	0.15
41.833	0.00	0.06	0.006	IO	|	|	|	0.14
41.917	0.00	0.06	0.006	IO	|	|	|	0.13
42.000	0.00	0.06	0.005	IO	|	|	|	0.12
42.083	0.00	0.05	0.005	IO	|	|	|	0.11
42.167	0.00	0.05	0.004	IO	|	|	|	0.10
42.250	0.00	0.04	0.004	IO	|	|	|	0.09
42.333	0.00	0.04	0.004	O	|	|	|	0.09
42.417	0.00	0.04	0.004	O	|	|	|	0.08
42.500	0.00	0.04	0.003	O	|	|	|	0.08
42.583	0.00	0.03	0.003	O	|	|	|	0.07
42.667	0.00	0.03	0.003	O	|	|	|	0.06
42.750	0.00	0.03	0.003	O	|	|	|	0.06
42.833	0.00	0.03	0.002	O	|	|	|	0.06
42.917	0.00	0.02	0.002	O	|	|	|	0.05
43.000	0.00	0.02	0.002	O	|	|	|	0.05
43.083	0.00	0.02	0.002	O	|	|	|	0.04
43.167	0.00	0.02	0.002	O	|	|	|	0.04
43.250	0.00	0.02	0.002	O	|	|	|	0.04
43.333	0.00	0.02	0.002	O	|	|	|	0.04
43.417	0.00	0.02	0.001	O	|	|	|	0.03
43.500	0.00	0.01	0.001	O	|	|	|	0.03
43.583	0.00	0.01	0.001	O	|	|	|	0.03
43.667	0.00	0.01	0.001	O	|	|	|	0.03
43.750	0.00	0.01	0.001	O	|	|	|	0.02
43.833	0.00	0.01	0.001	O	|	|	|	0.02
43.917	0.00	0.01	0.001	O	|	|	|	0.02
44.000	0.00	0.01	0.001	O	|	|	|	0.02
44.083	0.00	0.01	0.001	O	|	|	|	0.02
44.167	0.00	0.01	0.001	O	|	|	|	0.02
44.250	0.00	0.01	0.001	O	|	|	|	0.02
44.333	0.00	0.01	0.001	O	|	|	|	0.01
44.417	0.00	0.01	0.001	O	|	|	|	0.01
44.500	0.00	0.01	0.001	O	|	|	|	0.01
44.583	0.00	0.01	0.001	O	|	|	|	0.01
44.667	0.00	0.01	0.000	O	|	|	|	0.01
44.750	0.00	0.00	0.000	O	|	|	|	0.01
44.833	0.00	0.00	0.000	O	|	|	|	0.01
44.917	0.00	0.00	0.000	O	|	|	|	0.01
45.000	0.00	0.00	0.000	O	|	|	|	0.01
45.083	0.00	0.00	0.000	O	|	|	|	0.01
45.167	0.00	0.00	0.000	O	|	|	|	0.01
45.250	0.00	0.00	0.000	O	|	|	|	0.01
45.333	0.00	0.00	0.000	O	|	|	|	0.01
45.417	0.00	0.00	0.000	O	|	|	|	0.01
45.500	0.00	0.00	0.000	O	|	|	|	0.01
45.583	0.00	0.00	0.000	O	|	|	|	0.00
45.667	0.00	0.00	0.000	O	|	|	|	0.00
45.750	0.00	0.00	0.000	O	|	|	|	0.00
45.833	0.00	0.00	0.000	O	|	|	|	0.00
45.917	0.00	0.00	0.000	O	|	|	|	0.00
46.000	0.00	0.00	0.000	O	|	|	|	0.00
46.083	0.00	0.00	0.000	O	|	|	|	0.00
46.167	0.00	0.00	0.000	O	|	|	|	0.00
46.250	0.00	0.00	0.000	O	|	|	|	0.00
46.333	0.00	0.00	0.000	O	|	|	|	0.00
46.417	0.00	0.00	0.000	O	|	|	|	0.00
46.500	0.00	0.00	0.000	O	|	|	|	0.00
46.583	0.00	0.00	0.000	O	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 559
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.371 (CFS)
Total volume = 0.829 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
6-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD0262.rte
**********HYDROGRAPH DATA**********
Number of intervals = 73
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.932 (CFS)
Total volume = 0.498 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 73
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.0 1.97 2.95 3.93	Depth (Ft.)
0.083	0.27	0.01	0.001	O I	0.02
0.167	0.42	0.03	0.003	O I	0.07
0.250	0.43	0.06	0.006	O I	0.13
0.333	0.43	0.09	0.008	O I	0.19
0.417	0.43	0.11	0.010	O I	0.24
0.500	0.49	0.12	0.013	O I	0.26
0.583	0.51	0.12	0.015	O I	0.28
0.667	0.51	0.13	0.018	O I	0.30
0.750	0.51	0.13	0.021	O I	0.32
0.833	0.51	0.14	0.023	O I	0.34
0.917	0.51	0.14	0.026	O I	0.36
1.000	0.56	0.14	0.028	O I	0.37
1.083	0.58	0.15	0.031	O I	0.40
1.167	0.58	0.15	0.034	O I	0.42
1.250	0.58	0.15	0.037	O I	0.44
1.333	0.58	0.16	0.040	O I	0.46
1.417	0.58	0.16	0.043	O I	0.48
1.500	0.58	0.17	0.046	O I	0.50
1.583	0.58	0.17	0.049	O I	0.51
1.667	0.58	0.17	0.052	O I	0.53
1.750	0.58	0.17	0.054	O I	0.54
1.833	0.58	0.18	0.057	O I	0.56
1.917	0.58	0.18	0.060	O I	0.57
2.000	0.63	0.18	0.063	O I	0.58
2.083	0.60	0.18	0.066	O I	0.60
2.167	0.63	0.18	0.069	O I	0.61
2.250	0.65	0.19	0.072	O I	0.63
2.333	0.65	0.19	0.075	O I	0.64
2.417	0.65	0.19	0.078	O I	0.66
2.500	0.65	0.19	0.081	O I	0.67
2.583	0.65	0.19	0.085	O I	0.69
2.667	0.65	0.20	0.088	O I	0.70
2.750	0.70	0.20	0.091	O I	0.71
2.833	0.72	0.20	0.095	O I	0.73
2.917	0.72	0.20	0.098	O I	0.75
3.000	0.72	0.20	0.102	O I	0.76
3.083	0.72	0.21	0.105	O I	0.78
3.167	0.78	0.21	0.109	O I	0.80
3.250	0.79	0.21	0.113	O I	0.82
3.333	0.79	0.21	0.117	O I	0.83
3.417	0.85	0.22	0.121	O I	0.85
3.500	0.92	0.22	0.126	O I	0.87
3.583	0.99	0.22	0.131	O I	0.90
3.667	1.01	0.23	0.136	O I	0.92
3.750	1.07	0.23	0.142	O I	0.95
3.833	1.08	0.23	0.148	O I	0.97
3.917	1.14	0.24	0.154	O I	1.00
4.000	1.16	0.24	0.160	O I	1.03
4.083	1.21	0.24	0.166	O I	1.06
4.167	1.28	0.25	0.173	O I	1.09
4.250	1.35	0.25	0.181	O I	1.13
4.333	1.43	0.25	0.188	O I	1.16
4.417	1.50	0.26	0.197	O I	1.20
4.500	1.52	0.26	0.205	O I	1.24
4.583	1.57	0.27	0.214	O I	1.28
4.667	1.64	0.27	0.223	O I	1.32
4.750	1.72	0.27	0.233	O I	1.36
4.833	1.73	0.28	0.243	O I	1.41
4.917	1.79	0.28	0.253	O I	1.46
5.000	1.86	0.29	0.264	O I	1.50
5.083	2.15	0.29	0.276	O I	1.56
5.167	2.51	0.30	0.290	O I	1.62

5.250	2.76	0.31	0.306	O			I		1.70
5.333	2.98	0.32	0.323	O			I		1.78
5.417	3.30	0.32	0.343	O			I		1.87
5.500	3.93	0.33	0.365	O				I	1.97
5.583	2.07	0.34	0.384	O		I			2.05
5.667	0.83	0.34	0.392	O I					2.08
5.750	0.49	0.34	0.394	OI					2.09
5.833	0.38	0.34	0.394	OI					2.10
5.917	0.25	0.34	0.394	O					2.10
6.000	0.16	0.34	0.393	IO					2.09
6.083	0.04	0.34	0.392	I O					2.08
6.167	0.00	0.34	0.389	I O					2.07
6.250	0.00	0.34	0.387	I O					2.06
6.333	0.00	0.34	0.385	I O					2.05
6.417	0.00	0.34	0.382	I O					2.04
6.500	0.00	0.34	0.380	I O					2.03
6.583	0.00	0.34	0.378	I O					2.02
6.667	0.00	0.33	0.375	I O					2.01
6.750	0.00	0.33	0.373	I O					2.00
6.833	0.00	0.33	0.371	I O					1.99
6.917	0.00	0.33	0.369	I O					1.98
7.000	0.00	0.33	0.366	I O					1.97
7.083	0.00	0.33	0.364	I O					1.96
7.167	0.00	0.33	0.362	I O					1.95
7.250	0.00	0.33	0.359	I O					1.94
7.333	0.00	0.33	0.357	I O					1.93
7.417	0.00	0.33	0.355	I O					1.92
7.500	0.00	0.33	0.353	I O					1.91
7.583	0.00	0.33	0.350	I O					1.90
7.667	0.00	0.32	0.348	I O					1.89
7.750	0.00	0.32	0.346	I O					1.88
7.833	0.00	0.32	0.344	I O					1.87
7.917	0.00	0.32	0.342	I O					1.86
8.000	0.00	0.32	0.339	I O					1.85
8.083	0.00	0.32	0.337	I O					1.84
8.167	0.00	0.32	0.335	I O					1.83
8.250	0.00	0.32	0.333	I O					1.82
8.333	0.00	0.32	0.330	I O					1.81
8.417	0.00	0.32	0.328	I O					1.80
8.500	0.00	0.32	0.326	I O					1.79
8.583	0.00	0.32	0.324	I O					1.78
8.667	0.00	0.31	0.322	I O					1.77
8.750	0.00	0.31	0.320	I O					1.76
8.833	0.00	0.31	0.317	I O					1.75
8.917	0.00	0.31	0.315	I O					1.74
9.000	0.00	0.31	0.313	I O					1.73
9.083	0.00	0.31	0.311	I O					1.72
9.167	0.00	0.31	0.309	I O					1.71
9.250	0.00	0.31	0.307	I O					1.70
9.333	0.00	0.31	0.305	I O					1.69
9.417	0.00	0.31	0.303	I O					1.68
9.500	0.00	0.31	0.300	I O					1.67
9.583	0.00	0.30	0.298	I O					1.66
9.667	0.00	0.30	0.296	I O					1.65
9.750	0.00	0.30	0.294	I O					1.64
9.833	0.00	0.30	0.292	I O					1.63
9.917	0.00	0.30	0.290	I O					1.62
10.000	0.00	0.30	0.288	I O					1.62
10.083	0.00	0.30	0.286	I O					1.61
10.167	0.00	0.30	0.284	I O					1.60
10.250	0.00	0.30	0.282	I O					1.59
10.333	0.00	0.30	0.280	I O					1.58
10.417	0.00	0.30	0.278	I O					1.57
10.500	0.00	0.29	0.276	I O					1.56
10.583	0.00	0.29	0.274	I O					1.55
10.667	0.00	0.29	0.272	I O					1.54
10.750	0.00	0.29	0.270	I O					1.53
10.833	0.00	0.29	0.268	I O					1.52
10.917	0.00	0.29	0.266	I O					1.51
11.000	0.00	0.29	0.264	I O					1.50
11.083	0.00	0.29	0.262	I O					1.49
11.167	0.00	0.29	0.260	I O					1.48

11.250	0.00	0.29	0.258	I O	|	|	|	1.48
11.333	0.00	0.29	0.256	I O	|	|	|	1.47
11.417	0.00	0.28	0.254	I O	|	|	|	1.46
11.500	0.00	0.28	0.252	I O	|	|	|	1.45
11.583	0.00	0.28	0.250	I O	|	|	|	1.44
11.667	0.00	0.28	0.248	I O	|	|	|	1.43
11.750	0.00	0.28	0.246	I O	|	|	|	1.42
11.833	0.00	0.28	0.244	I O	|	|	|	1.41
11.917	0.00	0.28	0.242	I O	|	|	|	1.40
12.000	0.00	0.28	0.240	I O	|	|	|	1.40
12.083	0.00	0.28	0.238	I O	|	|	|	1.39
12.167	0.00	0.28	0.236	I O	|	|	|	1.38
12.250	0.00	0.28	0.234	I O	|	|	|	1.37
12.333	0.00	0.27	0.233	I O	|	|	|	1.36
12.417	0.00	0.27	0.231	I O	|	|	|	1.35
12.500	0.00	0.27	0.229	I O	|	|	|	1.34
12.583	0.00	0.27	0.227	I O	|	|	|	1.34
12.667	0.00	0.27	0.225	I O	|	|	|	1.33
12.750	0.00	0.27	0.223	I O	|	|	|	1.32
12.833	0.00	0.27	0.221	I O	|	|	|	1.31
12.917	0.00	0.27	0.219	I O	|	|	|	1.30
13.000	0.00	0.27	0.218	I O	|	|	|	1.29
13.083	0.00	0.27	0.216	I O	|	|	|	1.29
13.167	0.00	0.27	0.214	I O	|	|	|	1.28
13.250	0.00	0.26	0.212	I O	|	|	|	1.27
13.333	0.00	0.26	0.210	I O	|	|	|	1.26
13.417	0.00	0.26	0.209	I O	|	|	|	1.25
13.500	0.00	0.26	0.207	I O	|	|	|	1.24
13.583	0.00	0.26	0.205	I O	|	|	|	1.24
13.667	0.00	0.26	0.203	I O	|	|	|	1.23
13.750	0.00	0.26	0.201	I O	|	|	|	1.22
13.833	0.00	0.26	0.200	I O	|	|	|	1.21
13.917	0.00	0.26	0.198	I O	|	|	|	1.20
14.000	0.00	0.26	0.196	I O	|	|	|	1.20
14.083	0.00	0.26	0.194	I O	|	|	|	1.19
14.167	0.00	0.26	0.192	I O	|	|	|	1.18
14.250	0.00	0.25	0.191	I O	|	|	|	1.17
14.333	0.00	0.25	0.189	I O	|	|	|	1.16
14.417	0.00	0.25	0.187	I O	|	|	|	1.16
14.500	0.00	0.25	0.185	I O	|	|	|	1.15
14.583	0.00	0.25	0.184	I O	|	|	|	1.14
14.667	0.00	0.25	0.182	I O	|	|	|	1.13
14.750	0.00	0.25	0.180	I O	|	|	|	1.12
14.833	0.00	0.25	0.179	I O	|	|	|	1.12
14.917	0.00	0.25	0.177	I O	|	|	|	1.11
15.000	0.00	0.25	0.175	I O	|	|	|	1.10
15.083	0.00	0.25	0.173	I O	|	|	|	1.09
15.167	0.00	0.25	0.172	IO	|	|	|	1.09
15.250	0.00	0.24	0.170	IO	|	|	|	1.08
15.333	0.00	0.24	0.168	IO	|	|	|	1.07
15.417	0.00	0.24	0.167	IO	|	|	|	1.06
15.500	0.00	0.24	0.165	IO	|	|	|	1.05
15.583	0.00	0.24	0.163	IO	|	|	|	1.05
15.667	0.00	0.24	0.162	IO	|	|	|	1.04
15.750	0.00	0.24	0.160	IO	|	|	|	1.03
15.833	0.00	0.24	0.158	IO	|	|	|	1.02
15.917	0.00	0.24	0.157	IO	|	|	|	1.02
16.000	0.00	0.24	0.155	IO	|	|	|	1.01
16.083	0.00	0.24	0.154	IO	|	|	|	1.00
16.167	0.00	0.24	0.152	IO	|	|	|	1.00
16.250	0.00	0.23	0.150	IO	|	|	|	0.99
16.333	0.00	0.23	0.149	IO	|	|	|	0.98
16.417	0.00	0.23	0.147	IO	|	|	|	0.97
16.500	0.00	0.23	0.146	IO	|	|	|	0.97
16.583	0.00	0.23	0.144	IO	|	|	|	0.96
16.667	0.00	0.23	0.142	IO	|	|	|	0.95
16.750	0.00	0.23	0.141	IO	|	|	|	0.94
16.833	0.00	0.23	0.139	IO	|	|	|	0.94
16.917	0.00	0.23	0.138	IO	|	|	|	0.93
17.000	0.00	0.23	0.136	IO	|	|	|	0.92
17.083	0.00	0.22	0.135	IO	|	|	|	0.92
17.167	0.00	0.22	0.133	IO	|	|	|	0.91

17.250	0.00	0.22	0.131	IO				0.90
17.333	0.00	0.22	0.130	IO				0.89
17.417	0.00	0.22	0.128	IO				0.89
17.500	0.00	0.22	0.127	IO				0.88
17.583	0.00	0.22	0.125	IO				0.87
17.667	0.00	0.22	0.124	IO				0.87
17.750	0.00	0.22	0.122	IO				0.86
17.833	0.00	0.22	0.121	IO				0.85
17.917	0.00	0.22	0.119	IO				0.85
18.000	0.00	0.21	0.118	IO				0.84
18.083	0.00	0.21	0.116	IO				0.83
18.167	0.00	0.21	0.115	IO				0.83
18.250	0.00	0.21	0.113	IO				0.82
18.333	0.00	0.21	0.112	IO				0.81
18.417	0.00	0.21	0.111	IO				0.80
18.500	0.00	0.21	0.109	IO				0.80
18.583	0.00	0.21	0.108	IO				0.79
18.667	0.00	0.21	0.106	IO				0.79
18.750	0.00	0.21	0.105	IO				0.78
18.833	0.00	0.21	0.103	IO				0.77
18.917	0.00	0.20	0.102	IO				0.77
19.000	0.00	0.20	0.101	IO				0.76
19.083	0.00	0.20	0.099	IO				0.75
19.167	0.00	0.20	0.098	IO				0.75
19.250	0.00	0.20	0.096	IO				0.74
19.333	0.00	0.20	0.095	IO				0.73
19.417	0.00	0.20	0.094	IO				0.73
19.500	0.00	0.20	0.092	IO				0.72
19.583	0.00	0.20	0.091	IO				0.71
19.667	0.00	0.20	0.090	IO				0.71
19.750	0.00	0.20	0.088	IO				0.70
19.833	0.00	0.20	0.087	IO				0.70
19.917	0.00	0.19	0.085	IO				0.69
20.000	0.00	0.19	0.084	IO				0.68
20.083	0.00	0.19	0.083	IO				0.68
20.167	0.00	0.19	0.081	IO				0.67
20.250	0.00	0.19	0.080	IO				0.67
20.333	0.00	0.19	0.079	IO				0.66
20.417	0.00	0.19	0.078	IO				0.65
20.500	0.00	0.19	0.076	IO				0.65
20.583	0.00	0.19	0.075	IO				0.64
20.667	0.00	0.19	0.074	IO				0.64
20.750	0.00	0.19	0.072	IO				0.63
20.833	0.00	0.19	0.071	IO				0.62
20.917	0.00	0.19	0.070	IO				0.62
21.000	0.00	0.18	0.068	IO				0.61
21.083	0.00	0.18	0.067	IO				0.61
21.167	0.00	0.18	0.066	IO				0.60
21.250	0.00	0.18	0.065	IO				0.59
21.333	0.00	0.18	0.063	IO				0.59
21.417	0.00	0.18	0.062	IO				0.58
21.500	0.00	0.18	0.061	IO				0.57
21.583	0.00	0.18	0.060	IO				0.57
21.667	0.00	0.18	0.059	IO				0.56
21.750	0.00	0.18	0.057	IO				0.56
21.833	0.00	0.18	0.056	IO				0.55
21.917	0.00	0.17	0.055	IO				0.54
22.000	0.00	0.17	0.054	IO				0.54
22.083	0.00	0.17	0.053	IO				0.53
22.167	0.00	0.17	0.051	IO				0.53
22.250	0.00	0.17	0.050	IO				0.52
22.333	0.00	0.17	0.049	IO				0.51
22.417	0.00	0.17	0.048	IO				0.51
22.500	0.00	0.17	0.047	IO				0.50
22.583	0.00	0.17	0.046	IO				0.50
22.667	0.00	0.16	0.044	IO				0.49
22.750	0.00	0.16	0.043	IO				0.48
22.833	0.00	0.16	0.042	IO				0.47
22.917	0.00	0.16	0.041	IO				0.46
23.000	0.00	0.16	0.040	IO				0.46
23.083	0.00	0.16	0.039	IO				0.45
23.167	0.00	0.16	0.038	IO				0.44

23.250	0.00	0.15	0.037	IO				0.43
23.333	0.00	0.15	0.036	IO				0.43
23.417	0.00	0.15	0.035	IO				0.42
23.500	0.00	0.15	0.034	IO				0.41
23.583	0.00	0.15	0.033	IO				0.40
23.667	0.00	0.15	0.032	IO				0.40
23.750	0.00	0.15	0.031	IO				0.39
23.833	0.00	0.14	0.030	IO				0.38
23.917	0.00	0.14	0.029	IO				0.38
24.000	0.00	0.14	0.028	IO				0.37
24.083	0.00	0.14	0.027	IO				0.36
24.167	0.00	0.14	0.026	IO				0.35
24.250	0.00	0.14	0.025	IO				0.35
24.333	0.00	0.14	0.024	IO				0.34
24.417	0.00	0.13	0.023	IO				0.33
24.500	0.00	0.13	0.022	IO				0.33
24.583	0.00	0.13	0.021	IO				0.32
24.667	0.00	0.13	0.020	IO				0.31
24.750	0.00	0.13	0.019	IO				0.31
24.833	0.00	0.13	0.018	IO				0.30
24.917	0.00	0.13	0.017	IO				0.30
25.000	0.00	0.13	0.017	IO				0.29
25.083	0.00	0.12	0.016	IO				0.28
25.167	0.00	0.12	0.015	IO				0.28
25.250	0.00	0.12	0.014	O				0.27
25.333	0.00	0.12	0.013	O				0.27
25.417	0.00	0.12	0.012	O				0.26
25.500	0.00	0.12	0.011	O				0.25
25.583	0.00	0.11	0.011	O				0.24
25.667	0.00	0.11	0.010	O				0.23
25.750	0.00	0.10	0.009	O				0.21
25.833	0.00	0.09	0.009	O				0.19
25.917	0.00	0.09	0.008	O				0.18
26.000	0.00	0.08	0.007	O				0.17
26.083	0.00	0.07	0.007	O				0.16
26.167	0.00	0.07	0.006	O				0.14
26.250	0.00	0.06	0.006	O				0.13
26.333	0.00	0.06	0.005	O				0.12
26.417	0.00	0.05	0.005	O				0.12
26.500	0.00	0.05	0.005	O				0.11
26.583	0.00	0.05	0.004	O				0.10
26.667	0.00	0.04	0.004	O				0.09
26.750	0.00	0.04	0.004	O				0.09
26.833	0.00	0.04	0.004	O				0.08
26.917	0.00	0.04	0.003	O				0.07
27.000	0.00	0.03	0.003	O				0.07
27.083	0.00	0.03	0.003	O				0.06
27.167	0.00	0.03	0.003	O				0.06
27.250	0.00	0.03	0.002	O				0.06
27.333	0.00	0.02	0.002	O				0.05
27.417	0.00	0.02	0.002	O				0.05
27.500	0.00	0.02	0.002	O				0.04
27.583	0.00	0.02	0.002	O				0.04
27.667	0.00	0.02	0.002	O				0.04
27.750	0.00	0.02	0.002	O				0.04
27.833	0.00	0.02	0.001	O				0.03
27.917	0.00	0.01	0.001	O				0.03
28.000	0.00	0.01	0.001	O				0.03
28.083	0.00	0.01	0.001	O				0.03
28.167	0.00	0.01	0.001	O				0.02
28.250	0.00	0.01	0.001	O				0.02
28.333	0.00	0.01	0.001	O				0.02
28.417	0.00	0.01	0.001	O				0.02
28.500	0.00	0.01	0.001	O				0.02
28.583	0.00	0.01	0.001	O				0.02
28.667	0.00	0.01	0.001	O				0.02
28.750	0.00	0.01	0.001	O				0.01
28.833	0.00	0.01	0.001	O				0.01
28.917	0.00	0.01	0.001	O				0.01
29.000	0.00	0.01	0.001	O				0.01
29.083	0.00	0.01	0.000	O				0.01
29.167	0.00	0.00	0.000	O				0.01

29.250	0.00	0.00	0.000	O	|	|	|	|	0.01
29.333	0.00	0.00	0.000	O	|	|	|	|	0.01
29.417	0.00	0.00	0.000	O	|	|	|	|	0.01
29.500	0.00	0.00	0.000	O	|	|	|	|	0.01
29.583	0.00	0.00	0.000	O	|	|	|	|	0.01
29.667	0.00	0.00	0.000	O	|	|	|	|	0.01
29.750	0.00	0.00	0.000	O	|	|	|	|	0.01
29.833	0.00	0.00	0.000	O	|	|	|	|	0.01
29.917	0.00	0.00	0.000	O	|	|	|	|	0.01
30.000	0.00	0.00	0.000	O	|	|	|	|	0.00
30.083	0.00	0.00	0.000	O	|	|	|	|	0.00
30.167	0.00	0.00	0.000	O	|	|	|	|	0.00
30.250	0.00	0.00	0.000	O	|	|	|	|	0.00
30.333	0.00	0.00	0.000	O	|	|	|	|	0.00
30.417	0.00	0.00	0.000	O	|	|	|	|	0.00
30.500	0.00	0.00	0.000	O	|	|	|	|	0.00
30.583	0.00	0.00	0.000	O	|	|	|	|	0.00
30.667	0.00	0.00	0.000	O	|	|	|	|	0.00
30.750	0.00	0.00	0.000	O	|	|	|	|	0.00
30.833	0.00	0.00	0.000	O	|	|	|	|	0.00
30.917	0.00	0.00	0.000	O	|	|	|	|	0.00
31.000	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 372
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.342 (CFS)
Total volume = 0.498 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
3-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD0232.rte
**********HYDROGRAPH DATA**********
Number of intervals = 37
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 4.448 (CFS)
Total volume = 0.375 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 37
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.1 2.22 3.34 4.45	Depth (Ft.)
0.083	0.53	0.02	0.002	O I | | | |	0.04
0.167	0.70	0.06	0.006	O I | | | |	0.13
0.250	0.62	0.10	0.010	O I | | | |	0.22
0.333	0.76	0.12	0.014	O I | | | |	0.27
0.417	0.81	0.13	0.018	O I | | | |	0.30
0.500	0.93	0.14	0.023	O I | | | |	0.34
0.583	0.85	0.14	0.029	|O I | | | |	0.38
0.667	0.93	0.15	0.034	|O I | | | |	0.41
0.750	0.98	0.16	0.039	|O I| | | |	0.45
0.833	0.85	0.16	0.044	|O I | | | |	0.49
0.917	0.85	0.17	0.049	|O I | | | |	0.52
1.000	0.95	0.17	0.054	|O I | | | |	0.54
1.083	1.14	0.18	0.060	|O I | | | |	0.57
1.167	1.19	0.18	0.067	|O I | | | |	0.60
1.250	1.19	0.19	0.074	|O I | | | |	0.64
1.333	1.11	0.19	0.080	|O I| | | |	0.67
1.417	1.33	0.20	0.088	|O |I | | |	0.70
1.500	1.45	0.20	0.096	|O | I | | |	0.74
1.583	1.34	0.21	0.104	|O |I | | |	0.77
1.667	1.42	0.21	0.112	|O | I | | |	0.81
1.750	1.71	0.22	0.121	|O | I | | |	0.85
1.833	1.71	0.22	0.132	|O | I | | |	0.90
1.917	1.60	0.23	0.141	|O | I | | |	0.95
2.000	1.61	0.23	0.151	|O | I | | |	0.99
2.083	1.67	0.24	0.161	|O | I | | |	1.03
2.167	2.12	0.25	0.172	|O | | I| | |	1.09
2.250	2.60	0.25	0.186	|O | | | I | |	1.15
2.333	2.10	0.26	0.201	|O | | I| | |	1.22
2.417	3.23	0.27	0.217	|O | | | I| |	1.29
2.500	3.92	0.28	0.240	| O | | | | I |	1.40
2.583	4.45	0.29	0.267	| O | | | | | I	1.52
2.667	3.55	0.30	0.293	| O | | | I | |	1.64
2.750	1.62	0.31	0.308	| O | I | | | |	1.71
2.833	1.00	0.31	0.315	| O I| | | | |	1.74
2.917	0.98	0.31	0.320	| O I| | | | |	1.76
3.000	0.49	0.31	0.323	| OI | | | | |	1.78
3.083	0.08	0.31	0.323	I O | | | | |	1.78
3.167	0.00	0.31	0.321	I O | | | | |	1.77
3.250	0.00	0.31	0.319	I O | | | | |	1.76
3.333	0.00	0.31	0.316	I O | | | | |	1.75
3.417	0.00	0.31	0.314	I O | | | | |	1.74
3.500	0.00	0.31	0.312	I O | | | | |	1.73
3.583	0.00	0.31	0.310	I O | | | | |	1.72
3.667	0.00	0.31	0.308	I O | | | | |	1.71
3.750	0.00	0.31	0.306	I O | | | | |	1.70
3.833	0.00	0.31	0.304	I O | | | | |	1.69
3.917	0.00	0.31	0.301	I O | | | | |	1.68
4.000	0.00	0.30	0.299	I O | | | | |	1.67
4.083	0.00	0.30	0.297	I O | | | | |	1.66
4.167	0.00	0.30	0.295	I O | | | | |	1.65
4.250	0.00	0.30	0.293	I O | | | | |	1.64
4.333	0.00	0.30	0.291	I O | | | | |	1.63
4.417	0.00	0.30	0.289	I O | | | | |	1.62
4.500	0.00	0.30	0.287	I O | | | | |	1.61
4.583	0.00	0.30	0.285	I O | | | | |	1.60
4.667	0.00	0.30	0.283	I O | | | | |	1.59
4.750	0.00	0.30	0.281	I O | | | | |	1.58
4.833	0.00	0.30	0.279	I O | | | | |	1.57
4.917	0.00	0.29	0.277	I O | | | | |	1.56
5.000	0.00	0.29	0.275	I O | | | | |	1.55
5.083	0.00	0.29	0.273	I O | | | | |	1.54
5.167	0.00	0.29	0.271	I O | | | | |	1.54

5.250	0.00	0.29	0.269	I O				1.53
5.333	0.00	0.29	0.267	I O				1.52
5.417	0.00	0.29	0.265	I O				1.51
5.500	0.00	0.29	0.263	I O				1.50
5.583	0.00	0.29	0.261	I O				1.49
5.667	0.00	0.29	0.259	I O				1.48
5.750	0.00	0.29	0.257	I O				1.47
5.833	0.00	0.29	0.255	I O				1.46
5.917	0.00	0.28	0.253	I O				1.45
6.000	0.00	0.28	0.251	I O				1.44
6.083	0.00	0.28	0.249	I O				1.44
6.167	0.00	0.28	0.247	I O				1.43
6.250	0.00	0.28	0.245	I O				1.42
6.333	0.00	0.28	0.243	I O				1.41
6.417	0.00	0.28	0.241	I O				1.40
6.500	0.00	0.28	0.239	IO				1.39
6.583	0.00	0.28	0.237	IO				1.38
6.667	0.00	0.28	0.235	IO				1.37
6.750	0.00	0.27	0.233	IO				1.37
6.833	0.00	0.27	0.232	IO				1.36
6.917	0.00	0.27	0.230	IO				1.35
7.000	0.00	0.27	0.228	IO				1.34
7.083	0.00	0.27	0.226	IO				1.33
7.167	0.00	0.27	0.224	IO				1.32
7.250	0.00	0.27	0.222	IO				1.31
7.333	0.00	0.27	0.220	IO				1.31
7.417	0.00	0.27	0.219	IO				1.30
7.500	0.00	0.27	0.217	IO				1.29
7.583	0.00	0.27	0.215	IO				1.28
7.667	0.00	0.26	0.213	IO				1.27
7.750	0.00	0.26	0.211	IO				1.26
7.833	0.00	0.26	0.209	IO				1.26
7.917	0.00	0.26	0.208	IO				1.25
8.000	0.00	0.26	0.206	IO				1.24
8.083	0.00	0.26	0.204	IO				1.23
8.167	0.00	0.26	0.202	IO				1.22
8.250	0.00	0.26	0.200	IO				1.22
8.333	0.00	0.26	0.199	IO				1.21
8.417	0.00	0.26	0.197	IO				1.20
8.500	0.00	0.26	0.195	IO				1.19
8.583	0.00	0.26	0.193	IO				1.18
8.667	0.00	0.25	0.192	IO				1.18
8.750	0.00	0.25	0.190	IO				1.17
8.833	0.00	0.25	0.188	IO				1.16
8.917	0.00	0.25	0.186	IO				1.15
9.000	0.00	0.25	0.185	IO				1.14
9.083	0.00	0.25	0.183	IO				1.14
9.167	0.00	0.25	0.181	IO				1.13
9.250	0.00	0.25	0.179	IO				1.12
9.333	0.00	0.25	0.178	IO				1.11
9.417	0.00	0.25	0.176	IO				1.10
9.500	0.00	0.25	0.174	IO				1.10
9.583	0.00	0.25	0.173	IO				1.09
9.667	0.00	0.24	0.171	IO				1.08
9.750	0.00	0.24	0.169	IO				1.07
9.833	0.00	0.24	0.168	IO				1.07
9.917	0.00	0.24	0.166	IO				1.06
10.000	0.00	0.24	0.164	IO				1.05
10.083	0.00	0.24	0.163	IO				1.04
10.167	0.00	0.24	0.161	IO				1.04
10.250	0.00	0.24	0.159	IO				1.03
10.333	0.00	0.24	0.158	IO				1.02
10.417	0.00	0.24	0.156	IO				1.01
10.500	0.00	0.24	0.154	IO				1.01
10.583	0.00	0.24	0.153	IO				1.00
10.667	0.00	0.23	0.151	IO				0.99
10.750	0.00	0.23	0.150	IO				0.98
10.833	0.00	0.23	0.148	IO				0.98
10.917	0.00	0.23	0.146	IO				0.97
11.000	0.00	0.23	0.145	IO				0.96
11.083	0.00	0.23	0.143	IO				0.95
11.167	0.00	0.23	0.142	IO				0.95

11.250	0.00	0.23	0.140	IO				0.94
11.333	0.00	0.23	0.138	IO				0.93
11.417	0.00	0.23	0.137	IO				0.93
11.500	0.00	0.23	0.135	IO				0.92
11.583	0.00	0.22	0.134	IO				0.91
11.667	0.00	0.22	0.132	IO				0.90
11.750	0.00	0.22	0.131	IO				0.90
11.833	0.00	0.22	0.129	IO				0.89
11.917	0.00	0.22	0.128	IO				0.88
12.000	0.00	0.22	0.126	IO				0.88
12.083	0.00	0.22	0.125	IO				0.87
12.167	0.00	0.22	0.123	IO				0.86
12.250	0.00	0.22	0.122	IO				0.86
12.333	0.00	0.22	0.120	IO				0.85
12.417	0.00	0.22	0.119	IO				0.84
12.500	0.00	0.21	0.117	IO				0.84
12.583	0.00	0.21	0.116	IO				0.83
12.667	0.00	0.21	0.114	IO				0.82
12.750	0.00	0.21	0.113	IO				0.81
12.833	0.00	0.21	0.111	IO				0.81
12.917	0.00	0.21	0.110	IO				0.80
13.000	0.00	0.21	0.108	IO				0.79
13.083	0.00	0.21	0.107	IO				0.79
13.167	0.00	0.21	0.106	IO				0.78
13.250	0.00	0.21	0.104	IO				0.78
13.333	0.00	0.21	0.103	IO				0.77
13.417	0.00	0.20	0.101	IO				0.76
13.500	0.00	0.20	0.100	IO				0.76
13.583	0.00	0.20	0.098	IO				0.75
13.667	0.00	0.20	0.097	IO				0.74
13.750	0.00	0.20	0.096	IO				0.74
13.833	0.00	0.20	0.094	IO				0.73
13.917	0.00	0.20	0.093	IO				0.72
14.000	0.00	0.20	0.092	IO				0.72
14.083	0.00	0.20	0.090	IO				0.71
14.167	0.00	0.20	0.089	IO				0.71
14.250	0.00	0.20	0.088	IO				0.70
14.333	0.00	0.20	0.086	IO				0.69
14.417	0.00	0.19	0.085	IO				0.69
14.500	0.00	0.19	0.083	IO				0.68
14.583	0.00	0.19	0.082	IO				0.67
14.667	0.00	0.19	0.081	IO				0.67
14.750	0.00	0.19	0.079	IO				0.66
14.833	0.00	0.19	0.078	IO				0.66
14.917	0.00	0.19	0.077	IO				0.65
15.000	0.00	0.19	0.076	IO				0.64
15.083	0.00	0.19	0.074	IO				0.64
15.167	0.00	0.19	0.073	IO				0.63
15.250	0.00	0.19	0.072	IO				0.63
15.333	0.00	0.19	0.070	IO				0.62
15.417	0.00	0.18	0.069	IO				0.61
15.500	0.00	0.18	0.068	IO				0.61
15.583	0.00	0.18	0.067	IO				0.60
15.667	0.00	0.18	0.065	IO				0.60
15.750	0.00	0.18	0.064	IO				0.59
15.833	0.00	0.18	0.063	IO				0.58
15.917	0.00	0.18	0.062	IO				0.58
16.000	0.00	0.18	0.060	IO				0.57
16.083	0.00	0.18	0.059	IO				0.57
16.167	0.00	0.18	0.058	IO				0.56
16.250	0.00	0.18	0.057	IO				0.55
16.333	0.00	0.17	0.056	IO				0.55
16.417	0.00	0.17	0.054	IO				0.54
16.500	0.00	0.17	0.053	IO				0.54
16.583	0.00	0.17	0.052	IO				0.53
16.667	0.00	0.17	0.051	IO				0.52
16.750	0.00	0.17	0.050	IO				0.52
16.833	0.00	0.17	0.048	IO				0.51
16.917	0.00	0.17	0.047	IO				0.51
17.000	0.00	0.17	0.046	IO				0.50
17.083	0.00	0.17	0.045	IO				0.49
17.167	0.00	0.16	0.044	IO				0.48

17.250	0.00	0.16	0.043	IO				0.48
17.333	0.00	0.16	0.042	IO				0.47
17.417	0.00	0.16	0.040	IO				0.46
17.500	0.00	0.16	0.039	IO				0.45
17.583	0.00	0.16	0.038	IO				0.45
17.667	0.00	0.15	0.037	IO				0.44
17.750	0.00	0.15	0.036	IO				0.43
17.833	0.00	0.15	0.035	IO				0.42
17.917	0.00	0.15	0.034	IO				0.41
18.000	0.00	0.15	0.033	IO				0.41
18.083	0.00	0.15	0.032	IO				0.40
18.167	0.00	0.15	0.031	IO				0.39
18.250	0.00	0.14	0.030	IO				0.39
18.333	0.00	0.14	0.029	IO				0.38
18.417	0.00	0.14	0.028	IO				0.37
18.500	0.00	0.14	0.027	IO				0.36
18.583	0.00	0.14	0.026	IO				0.36
18.667	0.00	0.14	0.025	O				0.35
18.750	0.00	0.14	0.024	O				0.34
18.833	0.00	0.14	0.023	O				0.34
18.917	0.00	0.13	0.022	O				0.33
19.000	0.00	0.13	0.021	O				0.32
19.083	0.00	0.13	0.021	O				0.32
19.167	0.00	0.13	0.020	O				0.31
19.250	0.00	0.13	0.019	O				0.31
19.333	0.00	0.13	0.018	O				0.30
19.417	0.00	0.13	0.017	O				0.29
19.500	0.00	0.13	0.016	O				0.29
19.583	0.00	0.12	0.015	O				0.28
19.667	0.00	0.12	0.014	O				0.27
19.750	0.00	0.12	0.014	O				0.27
19.833	0.00	0.12	0.013	O				0.26
19.917	0.00	0.12	0.012	O				0.26
20.000	0.00	0.12	0.011	O				0.25
20.083	0.00	0.11	0.010	O				0.23
20.167	0.00	0.10	0.010	O				0.22
20.250	0.00	0.10	0.009	O				0.20
20.333	0.00	0.09	0.008	O				0.19
20.417	0.00	0.08	0.008	O				0.17
20.500	0.00	0.08	0.007	O				0.16
20.583	0.00	0.07	0.007	O				0.15
20.667	0.00	0.07	0.006	O				0.14
20.750	0.00	0.06	0.006	O				0.13
20.833	0.00	0.06	0.005	O				0.12
20.917	0.00	0.05	0.005	O				0.11
21.000	0.00	0.05	0.005	O				0.10
21.083	0.00	0.05	0.004	O				0.10
21.167	0.00	0.04	0.004	O				0.09
21.250	0.00	0.04	0.004	O				0.08
21.333	0.00	0.04	0.003	O				0.08
21.417	0.00	0.03	0.003	O				0.07
21.500	0.00	0.03	0.003	O				0.07
21.583	0.00	0.03	0.003	O				0.06
21.667	0.00	0.03	0.003	O				0.06
21.750	0.00	0.03	0.002	O				0.05
21.833	0.00	0.02	0.002	O				0.05
21.917	0.00	0.02	0.002	O				0.05
22.000	0.00	0.02	0.002	O				0.04
22.083	0.00	0.02	0.002	O				0.04
22.167	0.00	0.02	0.002	O				0.04
22.250	0.00	0.02	0.002	O				0.03
22.333	0.00	0.02	0.001	O				0.03
22.417	0.00	0.01	0.001	O				0.03
22.500	0.00	0.01	0.001	O				0.03
22.583	0.00	0.01	0.001	O				0.03
22.667	0.00	0.01	0.001	O				0.02
22.750	0.00	0.01	0.001	O				0.02
22.833	0.00	0.01	0.001	O				0.02
22.917	0.00	0.01	0.001	O				0.02
23.000	0.00	0.01	0.001	O				0.02
23.083	0.00	0.01	0.001	O				0.02
23.167	0.00	0.01	0.001	O				0.02

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23.250    0.00    0.01      0.001  O       |       |       |       |     0.01
23.333    0.00    0.01      0.001  O       |       |       |       |     0.01
23.417    0.00    0.01      0.001  O       |       |       |       |     0.01
23.500    0.00    0.01      0.000  O       |       |       |       |     0.01
23.583    0.00    0.00      0.000  O       |       |       |       |     0.01
23.667    0.00    0.00      0.000  O       |       |       |       |     0.01
23.750    0.00    0.00      0.000  O       |       |       |       |     0.01
23.833    0.00    0.00      0.000  O       |       |       |       |     0.01
23.917    0.00    0.00      0.000  O       |       |       |       |     0.01
24.000    0.00    0.00      0.000  O       |       |       |       |     0.01
24.083    0.00    0.00      0.000  O       |       |       |       |     0.01
24.167    0.00    0.00      0.000  O       |       |       |       |     0.01
24.250    0.00    0.00      0.000  O       |       |       |       |     0.01
24.333    0.00    0.00      0.000  O       |       |       |       |     0.01
24.417    0.00    0.00      0.000  O       |       |       |       |     0.01
24.500    0.00    0.00      0.000  O       |       |       |       |     0.00
24.583    0.00    0.00      0.000  O       |       |       |       |     0.00
24.667    0.00    0.00      0.000  O       |       |       |       |     0.00
24.750    0.00    0.00      0.000  O       |       |       |       |     0.00
24.833    0.00    0.00      0.000  O       |       |       |       |     0.00
24.917    0.00    0.00      0.000  O       |       |       |       |     0.00
25.000    0.00    0.00      0.000  O       |       |       |       |     0.00
25.083    0.00    0.00      0.000  O       |       |       |       |     0.00
25.167    0.00    0.00      0.000  O       |       |       |       |     0.00
25.250    0.00    0.00      0.000  O       |       |       |       |     0.00
25.333    0.00    0.00      0.000  O       |       |       |       |     0.00
25.417    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =   305
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.315 (CFS)
                      Total volume =       0.375 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
1-HOUR - 2-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD0212.rte
**********HYDROGRAPH DATA**********
Number of intervals = 13
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 8.041 (CFS)
Total volume = 0.232 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 13
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991	
5.600	0.979	5.490	0.960	0.998	

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 2.0 4.02 6.03 8.04	Depth (Ft.)
0.083	1.07	0.04	0.004	O I | | | |	0.08
0.167	1.46	0.12	0.012	O I | | | |	0.25
0.250	1.68	0.13	0.022	O I | | | |	0.33
0.333	1.76	0.15	0.032	O I | | | |	0.40
0.417	1.83	0.16	0.044	O I| | | |	0.48
0.500	2.02	0.17	0.056	O I | | |	0.55
0.583	2.45	0.19	0.070	O |I | | |	0.62
0.667	2.86	0.20	0.087	O | I | | |	0.70
0.750	3.93	0.21	0.109	O | I| | |	0.80
0.833	8.04	0.23	0.149	O | | | I	0.98
0.917	4.29	0.25	0.189	|O | I | |	1.17
1.000	1.84	0.26	0.209	|O I| | |	1.25
1.083	0.41	0.27	0.215	|O | | |	1.28
1.167	0.00	0.27	0.214	IO | | | |	1.28
1.250	0.00	0.26	0.212	IO | | | |	1.27
1.333	0.00	0.26	0.211	IO | | | |	1.26
1.417	0.00	0.26	0.209	IO | | | |	1.25
1.500	0.00	0.26	0.207	IO | | | |	1.25
1.583	0.00	0.26	0.205	IO | | | |	1.24
1.667	0.00	0.26	0.203	IO | | | |	1.23
1.750	0.00	0.26	0.202	IO | | | |	1.22
1.833	0.00	0.26	0.200	IO | | | |	1.21
1.917	0.00	0.26	0.198	IO | | | |	1.20
2.000	0.00	0.26	0.196	IO | | | |	1.20
2.083	0.00	0.26	0.194	IO | | | |	1.19
2.167	0.00	0.26	0.193	IO | | | |	1.18
2.250	0.00	0.25	0.191	IO | | | |	1.17
2.333	0.00	0.25	0.189	IO | | | |	1.16
2.417	0.00	0.25	0.187	IO | | | |	1.16
2.500	0.00	0.25	0.186	IO | | | |	1.15
2.583	0.00	0.25	0.184	O | | | |	1.14
2.667	0.00	0.25	0.182	O | | | |	1.13
2.750	0.00	0.25	0.181	O | | | |	1.13
2.833	0.00	0.25	0.179	O | | | |	1.12
2.917	0.00	0.25	0.177	O | | | |	1.11
3.000	0.00	0.25	0.175	O | | | |	1.10
3.083	0.00	0.25	0.174	O | | | |	1.09
3.167	0.00	0.25	0.172	O | | | |	1.09
3.250	0.00	0.24	0.170	O | | | |	1.08
3.333	0.00	0.24	0.169	O | | | |	1.07
3.417	0.00	0.24	0.167	O | | | |	1.06
3.500	0.00	0.24	0.165	O | | | |	1.06
3.583	0.00	0.24	0.164	O | | | |	1.05
3.667	0.00	0.24	0.162	O | | | |	1.04
3.750	0.00	0.24	0.160	O | | | |	1.03
3.833	0.00	0.24	0.159	O | | | |	1.03
3.917	0.00	0.24	0.157	O | | | |	1.02
4.000	0.00	0.24	0.155	O | | | |	1.01
4.083	0.00	0.24	0.154	O | | | |	1.00
4.167	0.00	0.24	0.152	O | | | |	1.00
4.250	0.00	0.23	0.151	O | | | |	0.99
4.333	0.00	0.23	0.149	O | | | |	0.98
4.417	0.00	0.23	0.147	O | | | |	0.97
4.500	0.00	0.23	0.146	O | | | |	0.97
4.583	0.00	0.23	0.144	O | | | |	0.96
4.667	0.00	0.23	0.143	O | | | |	0.95
4.750	0.00	0.23	0.141	O | | | |	0.94
4.833	0.00	0.23	0.139	O | | | |	0.94
4.917	0.00	0.23	0.138	O | | | |	0.93
5.000	0.00	0.23	0.136	O | | | |	0.92
5.083	0.00	0.22	0.135	O | | | |	0.92
5.167	0.00	0.22	0.133	O | | | |	0.91

5.250	0.00	0.22	0.132	O	|	|	|	0.90
5.333	0.00	0.22	0.130	O	|	|	|	0.89
5.417	0.00	0.22	0.129	O	|	|	|	0.89
5.500	0.00	0.22	0.127	O	|	|	|	0.88
5.583	0.00	0.22	0.126	O	|	|	|	0.87
5.667	0.00	0.22	0.124	O	|	|	|	0.87
5.750	0.00	0.22	0.123	O	|	|	|	0.86
5.833	0.00	0.22	0.121	O	|	|	|	0.85
5.917	0.00	0.22	0.120	O	|	|	|	0.85
6.000	0.00	0.21	0.118	O	|	|	|	0.84
6.083	0.00	0.21	0.117	O	|	|	|	0.83
6.167	0.00	0.21	0.115	O	|	|	|	0.83
6.250	0.00	0.21	0.114	O	|	|	|	0.82
6.333	0.00	0.21	0.112	O	|	|	|	0.81
6.417	0.00	0.21	0.111	O	|	|	|	0.81
6.500	0.00	0.21	0.109	O	|	|	|	0.80
6.583	0.00	0.21	0.108	O	|	|	|	0.79
6.667	0.00	0.21	0.106	O	|	|	|	0.79
6.750	0.00	0.21	0.105	O	|	|	|	0.78
6.833	0.00	0.21	0.104	O	|	|	|	0.77
6.917	0.00	0.21	0.102	O	|	|	|	0.77
7.000	0.00	0.20	0.101	O	|	|	|	0.76
7.083	0.00	0.20	0.099	O	|	|	|	0.75
7.167	0.00	0.20	0.098	O	|	|	|	0.75
7.250	0.00	0.20	0.097	O	|	|	|	0.74
7.333	0.00	0.20	0.095	O	|	|	|	0.73
7.417	0.00	0.20	0.094	O	|	|	|	0.73
7.500	0.00	0.20	0.092	O	|	|	|	0.72
7.583	0.00	0.20	0.091	O	|	|	|	0.72
7.667	0.00	0.20	0.090	O	|	|	|	0.71
7.750	0.00	0.20	0.088	O	|	|	|	0.70
7.833	0.00	0.20	0.087	O	|	|	|	0.70
7.917	0.00	0.19	0.086	O	|	|	|	0.69
8.000	0.00	0.19	0.084	O	|	|	|	0.68
8.083	0.00	0.19	0.083	O	|	|	|	0.68
8.167	0.00	0.19	0.082	O	|	|	|	0.67
8.250	0.00	0.19	0.080	O	|	|	|	0.67
8.333	0.00	0.19	0.079	O	|	|	|	0.66
8.417	0.00	0.19	0.078	O	|	|	|	0.65
8.500	0.00	0.19	0.076	O	|	|	|	0.65
8.583	0.00	0.19	0.075	O	|	|	|	0.64
8.667	0.00	0.19	0.074	O	|	|	|	0.64
8.750	0.00	0.19	0.073	O	|	|	|	0.63
8.833	0.00	0.19	0.071	O	|	|	|	0.62
8.917	0.00	0.19	0.070	O	|	|	|	0.62
9.000	0.00	0.18	0.069	O	|	|	|	0.61
9.083	0.00	0.18	0.067	O	|	|	|	0.61
9.167	0.00	0.18	0.066	O	|	|	|	0.60
9.250	0.00	0.18	0.065	O	|	|	|	0.59
9.333	0.00	0.18	0.064	O	|	|	|	0.59
9.417	0.00	0.18	0.062	O	|	|	|	0.58
9.500	0.00	0.18	0.061	O	|	|	|	0.58
9.583	0.00	0.18	0.060	O	|	|	|	0.57
9.667	0.00	0.18	0.059	O	|	|	|	0.56
9.750	0.00	0.18	0.057	O	|	|	|	0.56
9.833	0.00	0.18	0.056	O	|	|	|	0.55
9.917	0.00	0.17	0.055	O	|	|	|	0.55
10.000	0.00	0.17	0.054	O	|	|	|	0.54
10.083	0.00	0.17	0.053	O	|	|	|	0.53
10.167	0.00	0.17	0.051	O	|	|	|	0.53
10.250	0.00	0.17	0.050	O	|	|	|	0.52
10.333	0.00	0.17	0.049	O	|	|	|	0.52
10.417	0.00	0.17	0.048	O	|	|	|	0.51
10.500	0.00	0.17	0.047	O	|	|	|	0.50
10.583	0.00	0.17	0.046	O	|	|	|	0.50
10.667	0.00	0.16	0.045	O	|	|	|	0.49
10.750	0.00	0.16	0.043	O	|	|	|	0.48
10.833	0.00	0.16	0.042	O	|	|	|	0.47
10.917	0.00	0.16	0.041	O	|	|	|	0.47
11.000	0.00	0.16	0.040	O	|	|	|	0.46
11.083	0.00	0.16	0.039	O	|	|	|	0.45
11.167	0.00	0.16	0.038	O	|	|	|	0.44

11.250	0.00	0.15	0.037	O	|	|	|	0.43
11.333	0.00	0.15	0.036	O	|	|	|	0.43
11.417	0.00	0.15	0.035	O	|	|	|	0.42
11.500	0.00	0.15	0.034	O	|	|	|	0.41
11.583	0.00	0.15	0.033	O	|	|	|	0.40
11.667	0.00	0.15	0.032	O	|	|	|	0.40
11.750	0.00	0.15	0.031	O	|	|	|	0.39
11.833	0.00	0.14	0.030	O	|	|	|	0.38
11.917	0.00	0.14	0.029	O	|	|	|	0.38
12.000	0.00	0.14	0.028	O	|	|	|	0.37
12.083	0.00	0.14	0.027	O	|	|	|	0.36
12.167	0.00	0.14	0.026	O	|	|	|	0.36
12.250	0.00	0.14	0.025	O	|	|	|	0.35
12.333	0.00	0.14	0.024	O	|	|	|	0.34
12.417	0.00	0.13	0.023	O	|	|	|	0.34
12.500	0.00	0.13	0.022	O	|	|	|	0.33
12.583	0.00	0.13	0.021	O	|	|	|	0.32
12.667	0.00	0.13	0.020	O	|	|	|	0.32
12.750	0.00	0.13	0.019	O	|	|	|	0.31
12.833	0.00	0.13	0.018	O	|	|	|	0.30
12.917	0.00	0.13	0.018	O	|	|	|	0.30
13.000	0.00	0.13	0.017	O	|	|	|	0.29
13.083	0.00	0.12	0.016	O	|	|	|	0.28
13.167	0.00	0.12	0.015	O	|	|	|	0.28
13.250	0.00	0.12	0.014	O	|	|	|	0.27
13.333	0.00	0.12	0.013	O	|	|	|	0.27
13.417	0.00	0.12	0.012	O	|	|	|	0.26
13.500	0.00	0.12	0.012	O	|	|	|	0.25
13.583	0.00	0.12	0.011	O	|	|	|	0.25
13.667	0.00	0.11	0.010	O	|	|	|	0.23
13.750	0.00	0.10	0.009	O	|	|	|	0.21
13.833	0.00	0.09	0.009	O	|	|	|	0.20
13.917	0.00	0.09	0.008	O	|	|	|	0.18
14.000	0.00	0.08	0.007	O	|	|	|	0.17
14.083	0.00	0.07	0.007	O	|	|	|	0.16
14.167	0.00	0.07	0.006	O	|	|	|	0.15
14.250	0.00	0.06	0.006	O	|	|	|	0.14
14.333	0.00	0.06	0.006	O	|	|	|	0.13
14.417	0.00	0.06	0.005	O	|	|	|	0.12
14.500	0.00	0.05	0.005	O	|	|	|	0.11
14.583	0.00	0.05	0.004	O	|	|	|	0.10
14.667	0.00	0.04	0.004	O	|	|	|	0.09
14.750	0.00	0.04	0.004	O	|	|	|	0.09
14.833	0.00	0.04	0.004	O	|	|	|	0.08
14.917	0.00	0.04	0.003	O	|	|	|	0.08
15.000	0.00	0.03	0.003	O	|	|	|	0.07
15.083	0.00	0.03	0.003	O	|	|	|	0.06
15.167	0.00	0.03	0.003	O	|	|	|	0.06
15.250	0.00	0.03	0.002	O	|	|	|	0.06
15.333	0.00	0.02	0.002	O	|	|	|	0.05
15.417	0.00	0.02	0.002	O	|	|	|	0.05
15.500	0.00	0.02	0.002	O	|	|	|	0.04
15.583	0.00	0.02	0.002	O	|	|	|	0.04
15.667	0.00	0.02	0.002	O	|	|	|	0.04
15.750	0.00	0.02	0.002	O	|	|	|	0.04
15.833	0.00	0.02	0.001	O	|	|	|	0.03
15.917	0.00	0.01	0.001	O	|	|	|	0.03
16.000	0.00	0.01	0.001	O	|	|	|	0.03
16.083	0.00	0.01	0.001	O	|	|	|	0.03
16.167	0.00	0.01	0.001	O	|	|	|	0.02
16.250	0.00	0.01	0.001	O	|	|	|	0.02
16.333	0.00	0.01	0.001	O	|	|	|	0.02
16.417	0.00	0.01	0.001	O	|	|	|	0.02
16.500	0.00	0.01	0.001	O	|	|	|	0.02
16.583	0.00	0.01	0.001	O	|	|	|	0.02
16.667	0.00	0.01	0.001	O	|	|	|	0.02
16.750	0.00	0.01	0.001	O	|	|	|	0.01
16.833	0.00	0.01	0.001	O	|	|	|	0.01
16.917	0.00	0.01	0.001	O	|	|	|	0.01
17.000	0.00	0.01	0.001	O	|	|	|	0.01
17.083	0.00	0.01	0.000	O	|	|	|	0.01
17.167	0.00	0.00	0.000	O	|	|	|	0.01

17.250	0.00	0.00	0.000	O	|	|	|	|	0.01
17.333	0.00	0.00	0.000	O	|	|	|	|	0.01
17.417	0.00	0.00	0.000	O	|	|	|	|	0.01
17.500	0.00	0.00	0.000	O	|	|	|	|	0.01
17.583	0.00	0.00	0.000	O	|	|	|	|	0.01
17.667	0.00	0.00	0.000	O	|	|	|	|	0.01
17.750	0.00	0.00	0.000	O	|	|	|	|	0.01
17.833	0.00	0.00	0.000	O	|	|	|	|	0.01
17.917	0.00	0.00	0.000	O	|	|	|	|	0.01
18.000	0.00	0.00	0.000	O	|	|	|	|	0.00
18.083	0.00	0.00	0.000	O	|	|	|	|	0.00
18.167	0.00	0.00	0.000	O	|	|	|	|	0.00
18.250	0.00	0.00	0.000	O	|	|	|	|	0.00
18.333	0.00	0.00	0.000	O	|	|	|	|	0.00
18.417	0.00	0.00	0.000	O	|	|	|	|	0.00
18.500	0.00	0.00	0.000	O	|	|	|	|	0.00
18.583	0.00	0.00	0.000	O	|	|	|	|	0.00
18.667	0.00	0.00	0.000	O	|	|	|	|	0.00
18.750	0.00	0.00	0.000	O	|	|	|	|	0.00
18.833	0.00	0.00	0.000	O	|	|	|	|	0.00
18.917	0.00	0.00	0.000	O	|	|	|	|	0.00
19.000	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 228
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.266 (CFS)
Total volume = 0.231 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
24-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD05245.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.069 (CFS)
Total volume = 1.257 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

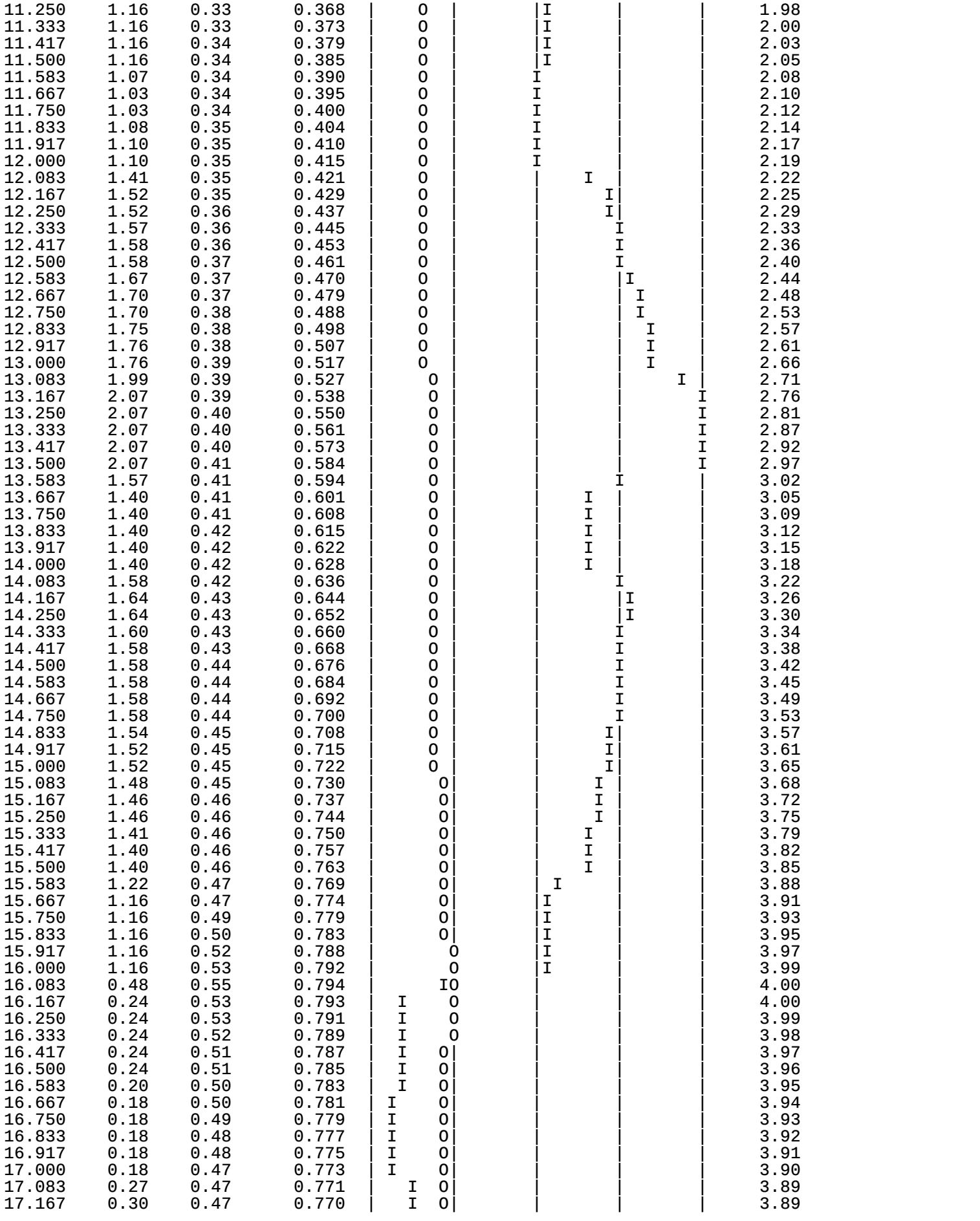
5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.5 1.03 1.55 2.07	Depth (Ft.)
0.083	0.09	0.00	0.000	OI	0.01
0.167	0.12	0.01	0.001	OI	0.02
0.250	0.12	0.02	0.002	OI	0.04
0.333	0.17	0.03	0.003	O I	0.06
0.417	0.18	0.04	0.004	O I	0.08
0.500	0.18	0.05	0.004	O I	0.10
0.583	0.18	0.06	0.005	O I	0.12
0.667	0.18	0.07	0.006	|OI	0.14
0.750	0.18	0.07	0.007	|OI	0.16
0.833	0.23	0.08	0.008	|O I	0.18
0.917	0.24	0.10	0.009	|O I	0.20
1.000	0.24	0.11	0.010	|O I	0.22
1.083	0.20	0.11	0.011	|O I	0.24
1.167	0.18	0.12	0.011	|OI	0.25
1.250	0.18	0.12	0.012	|OI	0.25
1.333	0.18	0.12	0.012	|OI	0.26
1.417	0.18	0.12	0.012	|OI	0.26
1.500	0.18	0.12	0.013	|OI	0.26
1.583	0.18	0.12	0.013	|OI	0.27
1.667	0.18	0.12	0.014	|OI	0.27
1.750	0.18	0.12	0.014	|OI	0.27
1.833	0.23	0.12	0.015	|O I	0.28
1.917	0.24	0.12	0.015	|O I	0.28
2.000	0.24	0.13	0.016	|O I	0.29
2.083	0.24	0.13	0.017	|O I	0.29
2.167	0.24	0.13	0.018	|O I	0.30
2.250	0.24	0.13	0.019	|O I	0.30
2.333	0.24	0.13	0.019	| OI	0.31
2.417	0.24	0.13	0.020	| OI	0.32
2.500	0.24	0.13	0.021	| OI	0.32
2.583	0.29	0.13	0.022	| O I	0.33
2.667	0.30	0.13	0.023	| O I	0.34
2.750	0.30	0.14	0.024	| O I	0.34
2.833	0.30	0.14	0.025	| O I	0.35
2.917	0.30	0.14	0.026	| O I	0.36
3.000	0.30	0.14	0.028	| O I	0.37
3.083	0.30	0.14	0.029	| O I	0.38
3.167	0.30	0.14	0.030	| O I	0.38
3.250	0.30	0.15	0.031	| O I	0.39
3.333	0.30	0.15	0.032	| O I	0.40
3.417	0.30	0.15	0.033	| O I	0.41
3.500	0.30	0.15	0.034	| O I	0.42
3.583	0.30	0.15	0.035	| O I	0.42
3.667	0.30	0.15	0.036	| O I	0.43
3.750	0.30	0.15	0.037	| O I	0.44
3.833	0.35	0.16	0.038	| O I	0.45
3.917	0.37	0.16	0.040	| O I	0.46
4.000	0.37	0.16	0.041	| O I	0.47
4.083	0.37	0.16	0.043	| O I	0.48
4.167	0.37	0.16	0.044	| O I	0.49
4.250	0.37	0.17	0.045	| O I	0.50
4.333	0.41	0.17	0.047	| O I	0.50
4.417	0.43	0.17	0.049	| O I	0.51
4.500	0.43	0.17	0.050	| O I	0.52
4.583	0.43	0.17	0.052	| O I	0.53
4.667	0.43	0.17	0.054	| O I	0.54
4.750	0.43	0.17	0.056	| O I	0.55
4.833	0.47	0.18	0.058	| O I|	0.56
4.917	0.49	0.18	0.060	| O I|	0.57
5.000	0.49	0.18	0.062	| O I|	0.58
5.083	0.40	0.18	0.064	| O I |	0.59
5.167	0.37	0.18	0.065	| O I |	0.59

5.250	0.37	0.18	0.066	O I				0.60
5.333	0.41	0.18	0.068	O I				0.61
5.417	0.43	0.18	0.069	O I				0.61
5.500	0.43	0.19	0.071	O I				0.62
5.583	0.47	0.19	0.073	O I				0.63
5.667	0.49	0.19	0.075	O I				0.64
5.750	0.49	0.19	0.077	O I				0.65
5.833	0.49	0.19	0.079	O I				0.66
5.917	0.49	0.19	0.081	O I				0.67
6.000	0.49	0.19	0.083	O I				0.68
6.083	0.53	0.19	0.085	O I				0.69
6.167	0.55	0.20	0.087	O I				0.70
6.250	0.55	0.20	0.090	O I				0.71
6.333	0.55	0.20	0.092	O I				0.72
6.417	0.55	0.20	0.095	O I				0.73
6.500	0.55	0.20	0.097	O I				0.74
6.583	0.59	0.20	0.099	O I				0.75
6.667	0.61	0.21	0.102	O I				0.77
6.750	0.61	0.21	0.105	O I				0.78
6.833	0.61	0.21	0.108	O I				0.79
6.917	0.61	0.21	0.111	O I				0.80
7.000	0.61	0.21	0.113	O I				0.82
7.083	0.61	0.21	0.116	O I				0.83
7.167	0.61	0.22	0.119	O I				0.84
7.250	0.61	0.22	0.121	O I				0.85
7.333	0.65	0.22	0.124	O I				0.87
7.417	0.67	0.22	0.127	O I				0.88
7.500	0.67	0.22	0.130	O I				0.90
7.583	0.71	0.22	0.134	O I				0.91
7.667	0.73	0.23	0.137	O I				0.93
7.750	0.73	0.23	0.140	O I				0.94
7.833	0.78	0.23	0.144	O I				0.96
7.917	0.79	0.23	0.148	O I				0.98
8.000	0.79	0.24	0.152	O I				0.99
8.083	0.88	0.24	0.156	O I				1.01
8.167	0.91	0.24	0.160	O I				1.03
8.250	0.91	0.24	0.165	O I				1.05
8.333	0.91	0.24	0.170	O I				1.08
8.417	0.91	0.25	0.174	O I				1.10
8.500	0.91	0.25	0.179	O I				1.12
8.583	0.96	0.25	0.184	O I				1.14
8.667	0.97	0.25	0.188	O I				1.16
8.750	0.97	0.26	0.193	O I				1.18
8.833	1.02	0.26	0.198	O I				1.21
8.917	1.03	0.26	0.204	O I				1.23
9.000	1.03	0.26	0.209	O I				1.25
9.083	1.13	0.27	0.215	O I				1.28
9.167	1.16	0.27	0.221	O I				1.31
9.250	1.16	0.27	0.227	O I				1.34
9.333	1.20	0.27	0.233	O I				1.36
9.417	1.22	0.28	0.239	O I				1.39
9.500	1.22	0.28	0.246	O I				1.42
9.583	1.26	0.28	0.253	O I				1.45
9.667	1.28	0.29	0.259	O I				1.48
9.750	1.28	0.29	0.266	O I				1.51
9.833	1.32	0.29	0.273	O I				1.55
9.917	1.34	0.30	0.280	O I				1.58
10.000	1.34	0.30	0.287	O I				1.61
10.083	1.02	0.30	0.293	O I				1.64
10.167	0.91	0.30	0.298	O I				1.66
10.250	0.91	0.31	0.302	O I				1.68
10.333	0.91	0.31	0.306	O I				1.70
10.417	0.91	0.31	0.311	O I				1.72
10.500	0.91	0.31	0.315	O I				1.74
10.583	1.14	0.31	0.320	O I				1.76
10.667	1.22	0.32	0.326	O I				1.79
10.750	1.22	0.32	0.332	O I				1.82
10.833	1.22	0.32	0.338	O I				1.84
10.917	1.22	0.32	0.344	O I				1.87
11.000	1.22	0.33	0.350	O I				1.90
11.083	1.17	0.33	0.356	O I				1.93
11.167	1.16	0.33	0.362	O I				1.95



11.250	1.16	0.33	0.368		O		I		1.98
11.333	1.16	0.33	0.373		O		I		2.00
11.417	1.16	0.34	0.379		O		I		2.03
11.500	1.16	0.34	0.385		O		I		2.05
11.583	1.07	0.34	0.390		O		I		2.08
11.667	1.03	0.34	0.395		O		I		2.10
11.750	1.03	0.34	0.400		O		I		2.12
11.833	1.08	0.35	0.404		O		I		2.14
11.917	1.10	0.35	0.410		O		I		2.17
12.000	1.10	0.35	0.415		O		I		2.19
12.083	1.41	0.35	0.421		O		I		2.22
12.167	1.52	0.35	0.429		O		I		2.25
12.250	1.52	0.36	0.437		O		I		2.29
12.333	1.57	0.36	0.445		O		I		2.33
12.417	1.58	0.36	0.453		O		I		2.36
12.500	1.58	0.37	0.461		O		I		2.40
12.583	1.67	0.37	0.470		O		I		2.44
12.667	1.70	0.37	0.479		O		I		2.48
12.750	1.70	0.38	0.488		O		I		2.53
12.833	1.75	0.38	0.498		O		I		2.57
12.917	1.76	0.38	0.507		O		I		2.61
13.000	1.76	0.39	0.517		O		I		2.66
13.083	1.99	0.39	0.527		O		I		2.71
13.167	2.07	0.39	0.538		O		I		2.76
13.250	2.07	0.40	0.550		O		I		2.81
13.333	2.07	0.40	0.561		O		I		2.87
13.417	2.07	0.40	0.573		O		I		2.92
13.500	2.07	0.41	0.584		O		I		2.97
13.583	1.57	0.41	0.594		O		I		3.02
13.667	1.40	0.41	0.601		O		I		3.05
13.750	1.40	0.41	0.608		O		I		3.09
13.833	1.40	0.42	0.615		O		I		3.12
13.917	1.40	0.42	0.622		O		I		3.15
14.000	1.40	0.42	0.628		O		I		3.18
14.083	1.58	0.42	0.636		O		I		3.22
14.167	1.64	0.43	0.644		O		I		3.26
14.250	1.64	0.43	0.652		O		I		3.30
14.333	1.60	0.43	0.660		O		I		3.34
14.417	1.58	0.43	0.668		O		I		3.38
14.500	1.58	0.44	0.676		O		I		3.42
14.583	1.58	0.44	0.684		O		I		3.45
14.667	1.58	0.44	0.692		O		I		3.49
14.750	1.58	0.44	0.700		O		I		3.53
14.833	1.54	0.45	0.708		O		I		3.57
14.917	1.52	0.45	0.715		O		I		3.61
15.000	1.52	0.45	0.722		O		I		3.65
15.083	1.48	0.45	0.730		O		I		3.68
15.167	1.46	0.46	0.737		O		I		3.72
15.250	1.46	0.46	0.744		O		I		3.75
15.333	1.41	0.46	0.750		O		I		3.79
15.417	1.40	0.46	0.757		O		I		3.82
15.500	1.40	0.46	0.763		O		I		3.85
15.583	1.22	0.47	0.769		O		I		3.88
15.667	1.16	0.47	0.774		O		I		3.91
15.750	1.16	0.49	0.779		O		I		3.93
15.833	1.16	0.50	0.783		O		I		3.95
15.917	1.16	0.52	0.788		O		I		3.97
16.000	1.16	0.53	0.792		O		I		3.99
16.083	0.48	0.55	0.794		IO				4.00
16.167	0.24	0.53	0.793	I	O				4.00
16.250	0.24	0.53	0.791	I	O				3.99
16.333	0.24	0.52	0.789	I	O				3.98
16.417	0.24	0.51	0.787	I	O				3.97
16.500	0.24	0.51	0.785	I	O				3.96
16.583	0.20	0.50	0.783	I	O				3.95
16.667	0.18	0.50	0.781	I	O				3.94
16.750	0.18	0.49	0.779	I	O				3.93
16.833	0.18	0.48	0.777	I	O				3.92
16.917	0.18	0.48	0.775	I	O				3.91
17.000	0.18	0.47	0.773	I	O				3.90
17.083	0.27	0.47	0.771	I	O				3.89
17.167	0.30	0.47	0.770	I	O				3.89

17.250	0.30	0.47	0.769	| I O|	|	|	|	3.88
17.333	0.30	0.47	0.767	| I O|	|	|	|	3.88
17.417	0.30	0.47	0.766	| I O|	|	|	|	3.87
17.500	0.30	0.46	0.765	| I O|	|	|	|	3.87
17.583	0.30	0.46	0.764	| I O|	|	|	|	3.86
17.667	0.30	0.46	0.763	| I O|	|	|	|	3.85
17.750	0.30	0.46	0.762	| I O|	|	|	|	3.85
17.833	0.26	0.46	0.761	| I O|	|	|	|	3.84
17.917	0.24	0.46	0.759	| I O|	|	|	|	3.83
18.000	0.24	0.46	0.758	| I O|	|	|	|	3.83
18.083	0.24	0.46	0.756	| I O|	|	|	|	3.82
18.167	0.24	0.46	0.755	| I O|	|	|	|	3.81
18.250	0.24	0.46	0.753	| I O|	|	|	|	3.80
18.333	0.24	0.46	0.752	| I O|	|	|	|	3.80
18.417	0.24	0.46	0.750	| I O|	|	|	|	3.79
18.500	0.24	0.46	0.749	| I O|	|	|	|	3.78
18.583	0.20	0.46	0.747	| I O|	|	|	|	3.77
18.667	0.18	0.46	0.745	| I O|	|	|	|	3.76
18.750	0.18	0.46	0.743	| I O|	|	|	|	3.75
18.833	0.14	0.46	0.741	| I O|	|	|	|	3.74
18.917	0.12	0.46	0.739	|I O|	|	|	|	3.73
19.000	0.12	0.46	0.737	|I O|	|	|	|	3.72
19.083	0.17	0.46	0.735	| I O|	|	|	|	3.71
19.167	0.18	0.45	0.733	| I O|	|	|	|	3.70
19.250	0.18	0.45	0.731	| I O|	|	|	|	3.69
19.333	0.23	0.45	0.729	| I O|	|	|	|	3.68
19.417	0.24	0.45	0.728	| I O|	|	|	|	3.67
19.500	0.24	0.45	0.726	| I O |	|	|	|	3.66
19.583	0.20	0.45	0.725	| I O |	|	|	|	3.66
19.667	0.18	0.45	0.723	| I O |	|	|	|	3.65
19.750	0.18	0.45	0.721	| I O |	|	|	|	3.64
19.833	0.14	0.45	0.719	| I O |	|	|	|	3.63
19.917	0.12	0.45	0.717	|I O |	|	|	|	3.62
20.000	0.12	0.45	0.714	|I O |	|	|	|	3.60
20.083	0.17	0.45	0.712	| I O |	|	|	|	3.59
20.167	0.18	0.45	0.710	| I O |	|	|	|	3.58
20.250	0.18	0.45	0.709	| I O |	|	|	|	3.58
20.333	0.18	0.45	0.707	| I O |	|	|	|	3.57
20.417	0.18	0.45	0.705	| I O |	|	|	|	3.56
20.500	0.18	0.44	0.703	| I O |	|	|	|	3.55
20.583	0.18	0.44	0.701	| I O |	|	|	|	3.54
20.667	0.18	0.44	0.700	| I O |	|	|	|	3.53
20.750	0.18	0.44	0.698	| I O |	|	|	|	3.52
20.833	0.14	0.44	0.696	| I O |	|	|	|	3.51
20.917	0.12	0.44	0.694	|I O |	|	|	|	3.50
21.000	0.12	0.44	0.692	|I O |	|	|	|	3.49
21.083	0.17	0.44	0.689	| I O |	|	|	|	3.48
21.167	0.18	0.44	0.688	| I O |	|	|	|	3.47
21.250	0.18	0.44	0.686	| I O |	|	|	|	3.46
21.333	0.14	0.44	0.684	| I O |	|	|	|	3.45
21.417	0.12	0.44	0.682	|I O |	|	|	|	3.44
21.500	0.12	0.44	0.680	|I O |	|	|	|	3.43
21.583	0.17	0.44	0.678	| I O |	|	|	|	3.42
21.667	0.18	0.44	0.676	| I O |	|	|	|	3.41
21.750	0.18	0.44	0.674	| I O |	|	|	|	3.40
21.833	0.14	0.44	0.672	| I O |	|	|	|	3.40
21.917	0.12	0.43	0.670	|I O |	|	|	|	3.38
22.000	0.12	0.43	0.668	|I O |	|	|	|	3.37
22.083	0.17	0.43	0.666	| I O |	|	|	|	3.37
22.167	0.18	0.43	0.664	| I O |	|	|	|	3.36
22.250	0.18	0.43	0.662	| I O |	|	|	|	3.35
22.333	0.14	0.43	0.661	| I O |	|	|	|	3.34
22.417	0.12	0.43	0.658	|I O |	|	|	|	3.33
22.500	0.12	0.43	0.656	|I O |	|	|	|	3.32
22.583	0.12	0.43	0.654	|I O |	|	|	|	3.31
22.667	0.12	0.43	0.652	|I O |	|	|	|	3.30
22.750	0.12	0.43	0.650	|I O |	|	|	|	3.29
22.833	0.12	0.43	0.648	|I O |	|	|	|	3.28
22.917	0.12	0.43	0.646	|I O |	|	|	|	3.27
23.000	0.12	0.43	0.644	|I O |	|	|	|	3.26
23.083	0.12	0.43	0.642	|I O |	|	|	|	3.25
23.167	0.12	0.42	0.640	|I O |	|	|	|	3.24

23.250	0.12	0.42	0.637	I	O				3.23
23.333	0.12	0.42	0.635	I	O				3.22
23.417	0.12	0.42	0.633	I	O				3.21
23.500	0.12	0.42	0.631	I	O				3.20
23.583	0.12	0.42	0.629	I	O				3.19
23.667	0.12	0.42	0.627	I	O				3.18
23.750	0.12	0.42	0.625	I	O				3.17
23.833	0.12	0.42	0.623	I	O				3.16
23.917	0.12	0.42	0.621	I	O				3.15
24.000	0.12	0.42	0.619	I	O				3.14
24.083	0.03	0.42	0.617	I	O				3.13
24.167	0.00	0.42	0.614	I	O				3.11
24.250	0.00	0.42	0.611	I	O				3.10
24.333	0.00	0.41	0.608	I	O				3.09
24.417	0.00	0.41	0.605	I	O				3.07
24.500	0.00	0.41	0.602	I	O				3.06
24.583	0.00	0.41	0.599	I	O				3.05
24.667	0.00	0.41	0.597	I	O				3.03
24.750	0.00	0.41	0.594	I	O				3.02
24.833	0.00	0.41	0.591	I	O				3.00
24.917	0.00	0.41	0.588	I	O				2.99
25.000	0.00	0.41	0.585	I	O				2.98
25.083	0.00	0.41	0.583	I	O				2.97
25.167	0.00	0.41	0.580	I	O				2.95
25.250	0.00	0.40	0.577	I	O				2.94
25.333	0.00	0.40	0.574	I	O				2.93
25.417	0.00	0.40	0.571	I	O				2.91
25.500	0.00	0.40	0.569	I	O				2.90
25.583	0.00	0.40	0.566	I	O				2.89
25.667	0.00	0.40	0.563	I	O				2.87
25.750	0.00	0.40	0.560	I	O				2.86
25.833	0.00	0.40	0.558	I	O				2.85
25.917	0.00	0.40	0.555	I	O				2.84
26.000	0.00	0.40	0.552	I	O				2.82
26.083	0.00	0.40	0.549	I	O				2.81
26.167	0.00	0.39	0.547	I	O				2.80
26.250	0.00	0.39	0.544	I	O				2.78
26.333	0.00	0.39	0.541	I	O				2.77
26.417	0.00	0.39	0.539	I	O				2.76
26.500	0.00	0.39	0.536	I	O				2.75
26.583	0.00	0.39	0.533	I	O				2.73
26.667	0.00	0.39	0.530	I	O				2.72
26.750	0.00	0.39	0.528	I	O				2.71
26.833	0.00	0.39	0.525	I	O				2.70
26.917	0.00	0.39	0.522	I	O				2.68
27.000	0.00	0.39	0.520	I	O				2.67
27.083	0.00	0.39	0.517	I	O				2.66
27.167	0.00	0.38	0.515	I	O				2.65
27.250	0.00	0.38	0.512	I	O				2.63
27.333	0.00	0.38	0.509	I	O				2.62
27.417	0.00	0.38	0.507	I	O				2.61
27.500	0.00	0.38	0.504	I	O				2.60
27.583	0.00	0.38	0.501	I	O				2.59
27.667	0.00	0.38	0.499	I	O				2.57
27.750	0.00	0.38	0.496	I	O				2.56
27.833	0.00	0.38	0.494	I	O				2.55
27.917	0.00	0.38	0.491	I	O				2.54
28.000	0.00	0.38	0.488	I	O				2.52
28.083	0.00	0.37	0.486	I	O				2.51
28.167	0.00	0.37	0.483	I	O				2.50
28.250	0.00	0.37	0.481	I	O				2.49
28.333	0.00	0.37	0.478	I	O				2.48
28.417	0.00	0.37	0.475	I	O				2.47
28.500	0.00	0.37	0.473	I	O				2.45
28.583	0.00	0.37	0.470	I	O				2.44
28.667	0.00	0.37	0.468	I	O				2.43
28.750	0.00	0.37	0.465	I	O				2.42
28.833	0.00	0.37	0.463	I	O				2.41
28.917	0.00	0.37	0.460	I	O				2.40
29.000	0.00	0.36	0.458	I	O				2.39
29.083	0.00	0.36	0.455	I	O				2.37
29.167	0.00	0.36	0.453	I	O				2.36

29.250	0.00	0.36	0.450	I	O	|	|	|	2.35
29.333	0.00	0.36	0.448	I	O	|	|	|	2.34
29.417	0.00	0.36	0.445	I	O	|	|	|	2.33
29.500	0.00	0.36	0.443	I	O	|	|	|	2.32
29.583	0.00	0.36	0.440	I	O	|	|	|	2.31
29.667	0.00	0.36	0.438	I	O	|	|	|	2.29
29.750	0.00	0.36	0.435	I	O	|	|	|	2.28
29.833	0.00	0.36	0.433	I	O	|	|	|	2.27
29.917	0.00	0.35	0.430	I	O	|	|	|	2.26
30.000	0.00	0.35	0.428	I	O	|	|	|	2.25
30.083	0.00	0.35	0.426	I	O	|	|	|	2.24
30.167	0.00	0.35	0.423	I	O	|	|	|	2.23
30.250	0.00	0.35	0.421	I	O	|	|	|	2.22
30.333	0.00	0.35	0.418	I	O	|	|	|	2.21
30.417	0.00	0.35	0.416	I	O	|	|	|	2.20
30.500	0.00	0.35	0.414	I	O	|	|	|	2.18
30.583	0.00	0.35	0.411	I	O	|	|	|	2.17
30.667	0.00	0.35	0.409	I	O	|	|	|	2.16
30.750	0.00	0.35	0.406	I	O	|	|	|	2.15
30.833	0.00	0.35	0.404	I	O	|	|	|	2.14
30.917	0.00	0.34	0.402	I	O	|	|	|	2.13
31.000	0.00	0.34	0.399	I	O	|	|	|	2.12
31.083	0.00	0.34	0.397	I	O	|	|	|	2.11
31.167	0.00	0.34	0.394	I	O	|	|	|	2.10
31.250	0.00	0.34	0.392	I	O	|	|	|	2.09
31.333	0.00	0.34	0.390	I	O	|	|	|	2.08
31.417	0.00	0.34	0.387	I	O	|	|	|	2.07
31.500	0.00	0.34	0.385	I	O	|	|	|	2.06
31.583	0.00	0.34	0.383	I	O	|	|	|	2.04
31.667	0.00	0.34	0.380	I	O	|	|	|	2.03
31.750	0.00	0.34	0.378	I	O	|	|	|	2.02
31.833	0.00	0.34	0.376	I	O	|	|	|	2.01
31.917	0.00	0.33	0.374	I	O	|	|	|	2.00
32.000	0.00	0.33	0.371	I	O	|	|	|	1.99
32.083	0.00	0.33	0.369	I	O	|	|	|	1.98
32.167	0.00	0.33	0.367	I	O	|	|	|	1.97
32.250	0.00	0.33	0.364	I	O	|	|	|	1.96
32.333	0.00	0.33	0.362	I	O	|	|	|	1.95
32.417	0.00	0.33	0.360	I	O	|	|	|	1.94
32.500	0.00	0.33	0.358	I	O	|	|	|	1.93
32.583	0.00	0.33	0.355	I	O	|	|	|	1.92
32.667	0.00	0.33	0.353	I	O	|	|	|	1.91
32.750	0.00	0.33	0.351	I	O	|	|	|	1.90
32.833	0.00	0.32	0.349	I	O	|	|	|	1.89
32.917	0.00	0.32	0.346	I	O	|	|	|	1.88
33.000	0.00	0.32	0.344	I	O	|	|	|	1.87
33.083	0.00	0.32	0.342	I	O	|	|	|	1.86
33.167	0.00	0.32	0.340	I	O	|	|	|	1.85
33.250	0.00	0.32	0.337	I	O	|	|	|	1.84
33.333	0.00	0.32	0.335	I	O	|	|	|	1.83
33.417	0.00	0.32	0.333	I	O	|	|	|	1.82
33.500	0.00	0.32	0.331	I	O	|	|	|	1.81
33.583	0.00	0.32	0.329	I	O	|	|	|	1.80
33.667	0.00	0.32	0.326	I	O	|	|	|	1.79
33.750	0.00	0.32	0.324	I	O	|	|	|	1.78
33.833	0.00	0.31	0.322	I	O	|	|	|	1.77
33.917	0.00	0.31	0.320	I	O	|	|	|	1.76
34.000	0.00	0.31	0.318	I	O	|	|	|	1.75
34.083	0.00	0.31	0.316	I	O	|	|	|	1.74
34.167	0.00	0.31	0.314	I	O	|	|	|	1.73
34.250	0.00	0.31	0.311	I	O	|	|	|	1.72
34.333	0.00	0.31	0.309	I	O	|	|	|	1.71
34.417	0.00	0.31	0.307	I	O	|	|	|	1.70
34.500	0.00	0.31	0.305	I	O	|	|	|	1.69
34.583	0.00	0.31	0.303	I	O	|	|	|	1.68
34.667	0.00	0.31	0.301	I	O	|	|	|	1.67
34.750	0.00	0.30	0.299	I	O	|	|	|	1.67
34.833	0.00	0.30	0.297	I	O	|	|	|	1.66
34.917	0.00	0.30	0.295	I	O	|	|	|	1.65
35.000	0.00	0.30	0.292	I	O	|	|	|	1.64
35.083	0.00	0.30	0.290	I	O	|	|	|	1.63
35.167	0.00	0.30	0.288	I	O	|	|	|	1.62

35.250	0.00	0.30	0.286	I	O	|	|	|	1.61
35.333	0.00	0.30	0.284	I	O	|	|	|	1.60
35.417	0.00	0.30	0.282	I	O	|	|	|	1.59
35.500	0.00	0.30	0.280	I	O	|	|	|	1.58
35.583	0.00	0.30	0.278	I	O	|	|	|	1.57
35.667	0.00	0.29	0.276	I	O	|	|	|	1.56
35.750	0.00	0.29	0.274	I	O	|	|	|	1.55
35.833	0.00	0.29	0.272	I	O	|	|	|	1.54
35.917	0.00	0.29	0.270	I	O	|	|	|	1.53
36.000	0.00	0.29	0.268	I	O	|	|	|	1.52
36.083	0.00	0.29	0.266	I	O	|	|	|	1.51
36.167	0.00	0.29	0.264	I	O	|	|	|	1.50
36.250	0.00	0.29	0.262	I	O	|	|	|	1.50
36.333	0.00	0.29	0.260	I	O	|	|	|	1.49
36.417	0.00	0.29	0.258	I	O	|	|	|	1.48
36.500	0.00	0.29	0.256	I	O	|	|	|	1.47
36.583	0.00	0.28	0.254	I	O	|	|	|	1.46
36.667	0.00	0.28	0.252	I	O	|	|	|	1.45
36.750	0.00	0.28	0.250	I	O	|	|	|	1.44
36.833	0.00	0.28	0.248	I	O	|	|	|	1.43
36.917	0.00	0.28	0.246	I	O	|	|	|	1.42
37.000	0.00	0.28	0.244	I	O	|	|	|	1.42
37.083	0.00	0.28	0.242	I	O	|	|	|	1.41
37.167	0.00	0.28	0.240	I	O	|	|	|	1.40
37.250	0.00	0.28	0.239	I	O	|	|	|	1.39
37.333	0.00	0.28	0.237	I	O	|	|	|	1.38
37.417	0.00	0.28	0.235	I	O	|	|	|	1.37
37.500	0.00	0.27	0.233	I	O	|	|	|	1.36
37.583	0.00	0.27	0.231	I	O	|	|	|	1.35
37.667	0.00	0.27	0.229	I	O	|	|	|	1.35
37.750	0.00	0.27	0.227	I	O	|	|	|	1.34
37.833	0.00	0.27	0.225	I	O	|	|	|	1.33
37.917	0.00	0.27	0.223	I	O	|	|	|	1.32
38.000	0.00	0.27	0.222	I	O	|	|	|	1.31
38.083	0.00	0.27	0.220	I	O	|	|	|	1.30
38.167	0.00	0.27	0.218	I	O	|	|	|	1.30
38.250	0.00	0.27	0.216	I	O	|	|	|	1.29
38.333	0.00	0.27	0.214	I	O	|	|	|	1.28
38.417	0.00	0.26	0.212	I	O	|	|	|	1.27
38.500	0.00	0.26	0.211	I	O	|	|	|	1.26
38.583	0.00	0.26	0.209	I	O	|	|	|	1.25
38.667	0.00	0.26	0.207	I	O	|	|	|	1.25
38.750	0.00	0.26	0.205	I	O	|	|	|	1.24
38.833	0.00	0.26	0.203	I	O	|	|	|	1.23
38.917	0.00	0.26	0.202	I	O	|	|	|	1.22
39.000	0.00	0.26	0.200	I	O	|	|	|	1.21
39.083	0.00	0.26	0.198	I	O	|	|	|	1.20
39.167	0.00	0.26	0.196	I	O	|	|	|	1.20
39.250	0.00	0.26	0.195	I	O	|	|	|	1.19
39.333	0.00	0.26	0.193	I	O	|	|	|	1.18
39.417	0.00	0.25	0.191	I	O	|	|	|	1.17
39.500	0.00	0.25	0.189	I	O	|	|	|	1.16
39.583	0.00	0.25	0.188	I	O	|	|	|	1.16
39.667	0.00	0.25	0.186	I	O	|	|	|	1.15
39.750	0.00	0.25	0.184	I	O	|	|	|	1.14
39.833	0.00	0.25	0.182	I	O	|	|	|	1.13
39.917	0.00	0.25	0.181	I	O	|	|	|	1.13
40.000	0.00	0.25	0.179	I	O	|	|	|	1.12
40.083	0.00	0.25	0.177	I	O	|	|	|	1.11
40.167	0.00	0.25	0.175	I	O	|	|	|	1.10
40.250	0.00	0.25	0.174	I	O	|	|	|	1.09
40.333	0.00	0.25	0.172	I	O	|	|	|	1.09
40.417	0.00	0.24	0.170	I	O	|	|	|	1.08
40.500	0.00	0.24	0.169	I	O	|	|	|	1.07
40.583	0.00	0.24	0.167	I	O	|	|	|	1.06
40.667	0.00	0.24	0.165	I	O	|	|	|	1.06
40.750	0.00	0.24	0.164	I	O	|	|	|	1.05
40.833	0.00	0.24	0.162	I	O	|	|	|	1.04
40.917	0.00	0.24	0.160	I	O	|	|	|	1.03
41.000	0.00	0.24	0.159	I	O	|	|	|	1.03
41.083	0.00	0.24	0.157	I	O	|	|	|	1.02
41.167	0.00	0.24	0.155	I	O	|	|	|	1.01

41.250	0.00	0.24	0.154	I	O	|	|	|	1.00
41.333	0.00	0.24	0.152	I	O	|	|	|	1.00
41.417	0.00	0.23	0.151	I	O	|	|	|	0.99
41.500	0.00	0.23	0.149	I	O	|	|	|	0.98
41.583	0.00	0.23	0.147	I	O	|	|	|	0.97
41.667	0.00	0.23	0.146	I	O	|	|	|	0.97
41.750	0.00	0.23	0.144	I	O	|	|	|	0.96
41.833	0.00	0.23	0.143	I	O	|	|	|	0.95
41.917	0.00	0.23	0.141	I	O	|	|	|	0.94
42.000	0.00	0.23	0.139	I	O	|	|	|	0.94
42.083	0.00	0.23	0.138	I	O	|	|	|	0.93
42.167	0.00	0.23	0.136	I	O	|	|	|	0.92
42.250	0.00	0.22	0.135	I	O	|	|	|	0.92
42.333	0.00	0.22	0.133	I	O	|	|	|	0.91
42.417	0.00	0.22	0.132	I	O	|	|	|	0.90
42.500	0.00	0.22	0.130	I	O	|	|	|	0.90
42.583	0.00	0.22	0.129	I	O	|	|	|	0.89
42.667	0.00	0.22	0.127	I	O	|	|	|	0.88
42.750	0.00	0.22	0.126	I	O	|	|	|	0.87
42.833	0.00	0.22	0.124	I	O	|	|	|	0.87
42.917	0.00	0.22	0.123	I	O	|	|	|	0.86
43.000	0.00	0.22	0.121	I	O	|	|	|	0.85
43.083	0.00	0.22	0.120	I	O	|	|	|	0.85
43.167	0.00	0.21	0.118	I	O	|	|	|	0.84
43.250	0.00	0.21	0.117	I	O	|	|	|	0.83
43.333	0.00	0.21	0.115	I	O	|	|	|	0.83
43.417	0.00	0.21	0.114	I	O	|	|	|	0.82
43.500	0.00	0.21	0.112	I	O	|	|	|	0.81
43.583	0.00	0.21	0.111	I	O	|	|	|	0.81
43.667	0.00	0.21	0.109	I	O	|	|	|	0.80
43.750	0.00	0.21	0.108	I	O	|	|	|	0.79
43.833	0.00	0.21	0.106	I	O	|	|	|	0.79
43.917	0.00	0.21	0.105	I	O	|	|	|	0.78
44.000	0.00	0.21	0.104	I	O	|	|	|	0.77
44.083	0.00	0.21	0.102	I	O	|	|	|	0.77
44.167	0.00	0.20	0.101	I	O	|	|	|	0.76
44.250	0.00	0.20	0.099	I	O	|	|	|	0.75
44.333	0.00	0.20	0.098	I	O	|	|	|	0.75
44.417	0.00	0.20	0.097	I	O	|	|	|	0.74
44.500	0.00	0.20	0.095	I	O	|	|	|	0.73
44.583	0.00	0.20	0.094	I	O	|	|	|	0.73
44.667	0.00	0.20	0.092	I	O	|	|	|	0.72
44.750	0.00	0.20	0.091	I	O	|	|	|	0.72
44.833	0.00	0.20	0.090	I	O	|	|	|	0.71
44.917	0.00	0.20	0.088	I	O	|	|	|	0.70
45.000	0.00	0.20	0.087	I	O	|	|	|	0.70
45.083	0.00	0.20	0.086	I	O	|	|	|	0.69
45.167	0.00	0.19	0.084	I	O	|	|	|	0.68
45.250	0.00	0.19	0.083	I	O	|	|	|	0.68
45.333	0.00	0.19	0.082	I	O	|	|	|	0.67
45.417	0.00	0.19	0.080	I	O	|	|	|	0.67
45.500	0.00	0.19	0.079	I	O	|	|	|	0.66
45.583	0.00	0.19	0.078	I	O	|	|	|	0.65
45.667	0.00	0.19	0.076	I	O	|	|	|	0.65
45.750	0.00	0.19	0.075	I	O	|	|	|	0.64
45.833	0.00	0.19	0.074	I	O	|	|	|	0.64
45.917	0.00	0.19	0.073	I	O	|	|	|	0.63
46.000	0.00	0.19	0.071	I	O	|	|	|	0.62
46.083	0.00	0.19	0.070	I	O	|	|	|	0.62
46.167	0.00	0.18	0.069	I	O	|	|	|	0.61
46.250	0.00	0.18	0.067	I	O	|	|	|	0.61
46.333	0.00	0.18	0.066	I	O	|	|	|	0.60
46.417	0.00	0.18	0.065	I	O	|	|	|	0.59
46.500	0.00	0.18	0.064	I	O	|	|	|	0.59
46.583	0.00	0.18	0.062	I	O	|	|	|	0.58
46.667	0.00	0.18	0.061	I	O	|	|	|	0.58
46.750	0.00	0.18	0.060	I	O	|	|	|	0.57
46.833	0.00	0.18	0.059	I	O	|	|	|	0.56
46.917	0.00	0.18	0.058	I	O	|	|	|	0.56
47.000	0.00	0.18	0.056	I	O	|	|	|	0.55
47.083	0.00	0.17	0.055	I	O	|	|	|	0.55
47.167	0.00	0.17	0.054	I	O	|	|	|	0.54

47.250	0.00	0.17	0.053	I O	|	|	|	0.53
47.333	0.00	0.17	0.052	I O	|	|	|	0.53
47.417	0.00	0.17	0.050	I O	|	|	|	0.52
47.500	0.00	0.17	0.049	I O	|	|	|	0.52
47.583	0.00	0.17	0.048	I O	|	|	|	0.51
47.667	0.00	0.17	0.047	I O	|	|	|	0.50
47.750	0.00	0.17	0.046	I O	|	|	|	0.50
47.833	0.00	0.16	0.045	I O	|	|	|	0.49
47.917	0.00	0.16	0.043	I O	|	|	|	0.48
48.000	0.00	0.16	0.042	I O	|	|	|	0.47
48.083	0.00	0.16	0.041	I O	|	|	|	0.47
48.167	0.00	0.16	0.040	I O	|	|	|	0.46
48.250	0.00	0.16	0.039	I O	|	|	|	0.45
48.333	0.00	0.16	0.038	I O	|	|	|	0.44
48.417	0.00	0.15	0.037	I O	|	|	|	0.43
48.500	0.00	0.15	0.036	I O	|	|	|	0.43
48.583	0.00	0.15	0.035	I O	|	|	|	0.42
48.667	0.00	0.15	0.034	I O	|	|	|	0.41
48.750	0.00	0.15	0.033	I O	|	|	|	0.41
48.833	0.00	0.15	0.032	I O	|	|	|	0.40
48.917	0.00	0.15	0.031	I O	|	|	|	0.39
49.000	0.00	0.14	0.030	I O	|	|	|	0.38
49.083	0.00	0.14	0.029	I O	|	|	|	0.38
49.167	0.00	0.14	0.028	I O	|	|	|	0.37
49.250	0.00	0.14	0.027	I O	|	|	|	0.36
49.333	0.00	0.14	0.026	I O	|	|	|	0.36
49.417	0.00	0.14	0.025	I O	|	|	|	0.35
49.500	0.00	0.14	0.024	I O	|	|	|	0.34
49.583	0.00	0.13	0.023	I O	|	|	|	0.34
49.667	0.00	0.13	0.022	I O	|	|	|	0.33
49.750	0.00	0.13	0.021	I O	|	|	|	0.32
49.833	0.00	0.13	0.020	I O	|	|	|	0.32
49.917	0.00	0.13	0.019	I O	|	|	|	0.31
50.000	0.00	0.13	0.018	IO	|	|	|	0.30
50.083	0.00	0.13	0.018	IO	|	|	|	0.30
50.167	0.00	0.13	0.017	IO	|	|	|	0.29
50.250	0.00	0.12	0.016	IO	|	|	|	0.28
50.333	0.00	0.12	0.015	IO	|	|	|	0.28
50.417	0.00	0.12	0.014	IO	|	|	|	0.27
50.500	0.00	0.12	0.013	IO	|	|	|	0.27
50.583	0.00	0.12	0.012	IO	|	|	|	0.26
50.667	0.00	0.12	0.012	IO	|	|	|	0.25
50.750	0.00	0.12	0.011	IO	|	|	|	0.25
50.833	0.00	0.11	0.010	IO	|	|	|	0.23
50.917	0.00	0.10	0.009	IO	|	|	|	0.21
51.000	0.00	0.09	0.009	IO	|	|	|	0.20
51.083	0.00	0.09	0.008	IO	|	|	|	0.18
51.167	0.00	0.08	0.007	IO	|	|	|	0.17
51.250	0.00	0.07	0.007	IO	|	|	|	0.16
51.333	0.00	0.07	0.006	IO	|	|	|	0.15
51.417	0.00	0.06	0.006	O	|	|	|	0.14
51.500	0.00	0.06	0.006	O	|	|	|	0.13
51.583	0.00	0.06	0.005	O	|	|	|	0.12
51.667	0.00	0.05	0.005	O	|	|	|	0.11
51.750	0.00	0.05	0.004	O	|	|	|	0.10
51.833	0.00	0.04	0.004	O	|	|	|	0.09
51.917	0.00	0.04	0.004	O	|	|	|	0.09
52.000	0.00	0.04	0.004	O	|	|	|	0.08
52.083	0.00	0.04	0.003	O	|	|	|	0.08
52.167	0.00	0.03	0.003	O	|	|	|	0.07
52.250	0.00	0.03	0.003	O	|	|	|	0.07
52.333	0.00	0.03	0.003	O	|	|	|	0.06
52.417	0.00	0.03	0.002	O	|	|	|	0.06
52.500	0.00	0.02	0.002	O	|	|	|	0.05
52.583	0.00	0.02	0.002	O	|	|	|	0.05
52.667	0.00	0.02	0.002	O	|	|	|	0.04
52.750	0.00	0.02	0.002	O	|	|	|	0.04
52.833	0.00	0.02	0.002	O	|	|	|	0.04
52.917	0.00	0.02	0.002	O	|	|	|	0.04
53.000	0.00	0.02	0.001	O	|	|	|	0.03
53.083	0.00	0.01	0.001	O	|	|	|	0.03
53.167	0.00	0.01	0.001	O	|	|	|	0.03

53.250	0.00	0.01	0.001	O	|	|	|	|	0.03
53.333	0.00	0.01	0.001	O	|	|	|	|	0.02
53.417	0.00	0.01	0.001	O	|	|	|	|	0.02
53.500	0.00	0.01	0.001	O	|	|	|	|	0.02
53.583	0.00	0.01	0.001	O	|	|	|	|	0.02
53.667	0.00	0.01	0.001	O	|	|	|	|	0.02
53.750	0.00	0.01	0.001	O	|	|	|	|	0.02
53.833	0.00	0.01	0.001	O	|	|	|	|	0.02
53.917	0.00	0.01	0.001	O	|	|	|	|	0.01
54.000	0.00	0.01	0.001	O	|	|	|	|	0.01
54.083	0.00	0.01	0.001	O	|	|	|	|	0.01
54.167	0.00	0.01	0.001	O	|	|	|	|	0.01
54.250	0.00	0.01	0.000	O	|	|	|	|	0.01
54.333	0.00	0.00	0.000	O	|	|	|	|	0.01
54.417	0.00	0.00	0.000	O	|	|	|	|	0.01
54.500	0.00	0.00	0.000	O	|	|	|	|	0.01
54.583	0.00	0.00	0.000	O	|	|	|	|	0.01
54.667	0.00	0.00	0.000	O	|	|	|	|	0.01
54.750	0.00	0.00	0.000	O	|	|	|	|	0.01
54.833	0.00	0.00	0.000	O	|	|	|	|	0.01
54.917	0.00	0.00	0.000	O	|	|	|	|	0.01
55.000	0.00	0.00	0.000	O	|	|	|	|	0.01
55.083	0.00	0.00	0.000	O	|	|	|	|	0.01
55.167	0.00	0.00	0.000	O	|	|	|	|	0.00
55.250	0.00	0.00	0.000	O	|	|	|	|	0.00
55.333	0.00	0.00	0.000	O	|	|	|	|	0.00
55.417	0.00	0.00	0.000	O	|	|	|	|	0.00
55.500	0.00	0.00	0.000	O	|	|	|	|	0.00
55.583	0.00	0.00	0.000	O	|	|	|	|	0.00
55.667	0.00	0.00	0.000	O	|	|	|	|	0.00
55.750	0.00	0.00	0.000	O	|	|	|	|	0.00
55.833	0.00	0.00	0.000	O	|	|	|	|	0.00
55.917	0.00	0.00	0.000	O	|	|	|	|	0.00
56.000	0.00	0.00	0.000	O	|	|	|	|	0.00
56.083	0.00	0.00	0.000	O	|	|	|	|	0.00
56.167	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 674
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.552 (CFS)
Total volume = 1.257 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
6-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD0565.rte
**********HYDROGRAPH DATA**********
Number of intervals = 73
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 5.576 (CFS)
Total volume = 0.677 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 73
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991	
5.600	0.979	5.490	0.960	0.998	

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.4 2.79 4.18 5.58	Depth (Ft.)
0.083	0.36	0.01	0.001	O I	0.03
0.167	0.56	0.05	0.004	O I	0.10
0.250	0.59	0.08	0.008	O I	0.18
0.333	0.59	0.12	0.011	O I	0.25
0.417	0.59	0.12	0.014	O I	0.27
0.500	0.66	0.13	0.018	O I	0.30
0.583	0.68	0.13	0.021	O I	0.32
0.667	0.68	0.14	0.025	O I	0.35
0.750	0.68	0.14	0.029	O I	0.38
0.833	0.68	0.15	0.033	O I	0.40
0.917	0.68	0.15	0.036	O I	0.43
1.000	0.76	0.16	0.040	O I	0.46
1.083	0.78	0.16	0.044	O I	0.49
1.167	0.78	0.17	0.049	O I	0.51
1.250	0.78	0.17	0.053	O I	0.53
1.333	0.78	0.18	0.057	O I	0.55
1.417	0.78	0.18	0.061	O I	0.58
1.500	0.78	0.18	0.065	O I	0.60
1.583	0.78	0.19	0.069	O I	0.62
1.667	0.78	0.19	0.073	O I	0.63
1.750	0.78	0.19	0.078	O I	0.65
1.833	0.78	0.19	0.082	O I	0.67
1.917	0.78	0.19	0.086	O I	0.69
2.000	0.85	0.20	0.090	O I	0.71
2.083	0.81	0.20	0.094	O I	0.73
2.167	0.85	0.20	0.099	O I	0.75
2.250	0.88	0.21	0.103	O I	0.77
2.333	0.88	0.21	0.108	O I	0.79
2.417	0.88	0.21	0.112	O I	0.81
2.500	0.88	0.21	0.117	O I	0.83
2.583	0.88	0.22	0.122	O I	0.86
2.667	0.88	0.22	0.126	O I	0.88
2.750	0.95	0.22	0.131	O I	0.90
2.833	0.98	0.23	0.136	O I	0.92
2.917	0.98	0.23	0.141	O I	0.95
3.000	0.98	0.23	0.146	O I	0.97
3.083	0.98	0.24	0.151	O I	0.99
3.167	1.05	0.24	0.157	O I	1.02
3.250	1.07	0.24	0.162	O I	1.04
3.333	1.07	0.24	0.168	O I	1.07
3.417	1.15	0.25	0.174	O I	1.10
3.500	1.24	0.25	0.181	O I	1.13
3.583	1.34	0.25	0.188	O I	1.16
3.667	1.37	0.26	0.195	O I	1.19
3.750	1.44	0.26	0.203	O I	1.23
3.833	1.46	0.26	0.212	O I	1.27
3.917	1.54	0.27	0.220	O I	1.30
4.000	1.56	0.27	0.229	O I	1.34
4.083	1.64	0.28	0.238	O I	1.39
4.167	1.73	0.28	0.248	O I	1.43
4.250	1.83	0.29	0.258	O I	1.48
4.333	1.93	0.29	0.269	O I	1.53
4.417	2.03	0.30	0.281	O I	1.58
4.500	2.05	0.30	0.292	O I	1.64
4.583	2.12	0.31	0.305	O I	1.69
4.667	2.22	0.31	0.318	O I	1.75
4.750	2.32	0.32	0.331	O I	1.81
4.833	2.34	0.32	0.345	O I	1.88
4.917	2.42	0.33	0.359	O I	1.94
5.000	2.51	0.33	0.374	O I	2.00
5.083	2.90	0.34	0.390	O I	2.08
5.167	3.39	0.35	0.409	O I	2.17

5.250	3.75	0.36	0.432	| O	|	|	| I |	|	2.27
5.333	4.09	0.36	0.456	| O	|	|	| I|	|	2.38
5.417	4.63	0.37	0.484	| O	|	|	| | I	|	2.50
5.500	5.58	0.38	0.516	| O	|	|	| |	| I	2.65
5.583	2.87	0.39	0.542	| O	|	I	| |	|	2.78
5.667	1.13	0.40	0.553	| O I	|	|	| |	|	2.83
5.750	0.66	0.40	0.557	| OI	|	|	| |	|	2.85
5.833	0.51	0.40	0.558	| O	|	|	| |	|	2.85
5.917	0.34	0.40	0.558	|IO	|	|	| |	|	2.85
6.000	0.22	0.40	0.558	|IO	|	|	| |	|	2.85
6.083	0.05	0.40	0.556	I O	|	|	| |	|	2.84
6.167	0.00	0.40	0.553	I O	|	|	| |	|	2.83
6.250	0.00	0.40	0.550	I O	|	|	| |	|	2.82
6.333	0.00	0.40	0.548	I O	|	|	| |	|	2.80
6.417	0.00	0.39	0.545	I O	|	|	| |	|	2.79
6.500	0.00	0.39	0.542	I O	|	|	| |	|	2.78
6.583	0.00	0.39	0.540	I O	|	|	| |	|	2.76
6.667	0.00	0.39	0.537	I O	|	|	| |	|	2.75
6.750	0.00	0.39	0.534	I O	|	|	| |	|	2.74
6.833	0.00	0.39	0.532	I O	|	|	| |	|	2.73
6.917	0.00	0.39	0.529	I O	|	|	| |	|	2.71
7.000	0.00	0.39	0.526	I O	|	|	| |	|	2.70
7.083	0.00	0.39	0.524	I O	|	|	| |	|	2.69
7.167	0.00	0.39	0.521	I O	|	|	| |	|	2.68
7.250	0.00	0.39	0.518	I O	|	|	| |	|	2.66
7.333	0.00	0.38	0.516	I O	|	|	| |	|	2.65
7.417	0.00	0.38	0.513	I O	|	|	| |	|	2.64
7.500	0.00	0.38	0.510	I O	|	|	| |	|	2.63
7.583	0.00	0.38	0.508	I O	|	|	| |	|	2.62
7.667	0.00	0.38	0.505	I O	|	|	| |	|	2.60
7.750	0.00	0.38	0.502	I O	|	|	| |	|	2.59
7.833	0.00	0.38	0.500	I O	|	|	| |	|	2.58
7.917	0.00	0.38	0.497	I O	|	|	| |	|	2.57
8.000	0.00	0.38	0.495	I O	|	|	| |	|	2.55
8.083	0.00	0.38	0.492	I O	|	|	| |	|	2.54
8.167	0.00	0.38	0.489	I O	|	|	| |	|	2.53
8.250	0.00	0.38	0.487	I O	|	|	| |	|	2.52
8.333	0.00	0.37	0.484	I O	|	|	| |	|	2.51
8.417	0.00	0.37	0.482	I O	|	|	| |	|	2.49
8.500	0.00	0.37	0.479	I O	|	|	| |	|	2.48
8.583	0.00	0.37	0.476	I O	|	|	| |	|	2.47
8.667	0.00	0.37	0.474	I O	|	|	| |	|	2.46
8.750	0.00	0.37	0.471	I O	|	|	| |	|	2.45
8.833	0.00	0.37	0.469	I O	|	|	| |	|	2.44
8.917	0.00	0.37	0.466	I O	|	|	| |	|	2.42
9.000	0.00	0.37	0.464	I O	|	|	| |	|	2.41
9.083	0.00	0.37	0.461	I O	|	|	| |	|	2.40
9.167	0.00	0.37	0.459	I O	|	|	| |	|	2.39
9.250	0.00	0.36	0.456	I O	|	|	| |	|	2.38
9.333	0.00	0.36	0.454	I O	|	|	| |	|	2.37
9.417	0.00	0.36	0.451	I O	|	|	| |	|	2.36
9.500	0.00	0.36	0.449	I O	|	|	| |	|	2.34
9.583	0.00	0.36	0.446	I O	|	|	| |	|	2.33
9.667	0.00	0.36	0.444	I O	|	|	| |	|	2.32
9.750	0.00	0.36	0.441	I O	|	|	| |	|	2.31
9.833	0.00	0.36	0.439	I O	|	|	| |	|	2.30
9.917	0.00	0.36	0.436	I O	|	|	| |	|	2.29
10.000	0.00	0.36	0.434	I O	|	|	| |	|	2.28
10.083	0.00	0.36	0.431	I O	|	|	| |	|	2.27
10.167	0.00	0.35	0.429	I O	|	|	| |	|	2.25
10.250	0.00	0.35	0.427	I O	|	|	| |	|	2.24
10.333	0.00	0.35	0.424	I O	|	|	| |	|	2.23
10.417	0.00	0.35	0.422	I O	|	|	| |	|	2.22
10.500	0.00	0.35	0.419	I O	|	|	| |	|	2.21
10.583	0.00	0.35	0.417	I O	|	|	| |	|	2.20
10.667	0.00	0.35	0.414	I O	|	|	| |	|	2.19
10.750	0.00	0.35	0.412	IO	|	|	| |	|	2.18
10.833	0.00	0.35	0.410	IO	|	|	| |	|	2.17
10.917	0.00	0.35	0.407	IO	|	|	| |	|	2.16
11.000	0.00	0.35	0.405	IO	|	|	| |	|	2.14
11.083	0.00	0.34	0.402	IO	|	|	| |	|	2.13
11.167	0.00	0.34	0.400	IO	|	|	| |	|	2.12

11.250	0.00	0.34	0.398	IO				2.11
11.333	0.00	0.34	0.395	IO				2.10
11.417	0.00	0.34	0.393	IO				2.09
11.500	0.00	0.34	0.391	IO				2.08
11.583	0.00	0.34	0.388	IO				2.07
11.667	0.00	0.34	0.386	IO				2.06
11.750	0.00	0.34	0.384	IO				2.05
11.833	0.00	0.34	0.381	IO				2.04
11.917	0.00	0.34	0.379	IO				2.03
12.000	0.00	0.34	0.377	IO				2.02
12.083	0.00	0.33	0.374	IO				2.01
12.167	0.00	0.33	0.372	IO				2.00
12.250	0.00	0.33	0.370	IO				1.99
12.333	0.00	0.33	0.368	IO				1.98
12.417	0.00	0.33	0.365	IO				1.97
12.500	0.00	0.33	0.363	IO				1.96
12.583	0.00	0.33	0.361	IO				1.95
12.667	0.00	0.33	0.358	IO				1.94
12.750	0.00	0.33	0.356	IO				1.93
12.833	0.00	0.33	0.354	IO				1.92
12.917	0.00	0.33	0.352	IO				1.91
13.000	0.00	0.33	0.349	IO				1.90
13.083	0.00	0.32	0.347	IO				1.89
13.167	0.00	0.32	0.345	IO				1.88
13.250	0.00	0.32	0.343	IO				1.87
13.333	0.00	0.32	0.341	IO				1.86
13.417	0.00	0.32	0.338	IO				1.85
13.500	0.00	0.32	0.336	IO				1.84
13.583	0.00	0.32	0.334	IO				1.83
13.667	0.00	0.32	0.332	IO				1.82
13.750	0.00	0.32	0.330	IO				1.81
13.833	0.00	0.32	0.327	IO				1.80
13.917	0.00	0.32	0.325	IO				1.79
14.000	0.00	0.31	0.323	IO				1.78
14.083	0.00	0.31	0.321	IO				1.77
14.167	0.00	0.31	0.319	IO				1.76
14.250	0.00	0.31	0.317	IO				1.75
14.333	0.00	0.31	0.314	IO				1.74
14.417	0.00	0.31	0.312	IO				1.73
14.500	0.00	0.31	0.310	IO				1.72
14.583	0.00	0.31	0.308	IO				1.71
14.667	0.00	0.31	0.306	IO				1.70
14.750	0.00	0.31	0.304	IO				1.69
14.833	0.00	0.31	0.302	IO				1.68
14.917	0.00	0.30	0.300	IO				1.67
15.000	0.00	0.30	0.297	IO				1.66
15.083	0.00	0.30	0.295	IO				1.65
15.167	0.00	0.30	0.293	IO				1.64
15.250	0.00	0.30	0.291	IO				1.63
15.333	0.00	0.30	0.289	IO				1.62
15.417	0.00	0.30	0.287	IO				1.61
15.500	0.00	0.30	0.285	IO				1.60
15.583	0.00	0.30	0.283	IO				1.59
15.667	0.00	0.30	0.281	IO				1.58
15.750	0.00	0.30	0.279	IO				1.57
15.833	0.00	0.29	0.277	IO				1.56
15.917	0.00	0.29	0.275	IO				1.55
16.000	0.00	0.29	0.273	IO				1.55
16.083	0.00	0.29	0.271	IO				1.54
16.167	0.00	0.29	0.269	IO				1.53
16.250	0.00	0.29	0.267	IO				1.52
16.333	0.00	0.29	0.265	IO				1.51
16.417	0.00	0.29	0.263	IO				1.50
16.500	0.00	0.29	0.261	IO				1.49
16.583	0.00	0.29	0.259	IO				1.48
16.667	0.00	0.29	0.257	IO				1.47
16.750	0.00	0.29	0.255	IO				1.46
16.833	0.00	0.28	0.253	IO				1.45
16.917	0.00	0.28	0.251	IO				1.44
17.000	0.00	0.28	0.249	IO				1.44
17.083	0.00	0.28	0.247	IO				1.43
17.167	0.00	0.28	0.245	IO				1.42

17.250	0.00	0.28	0.243	IO				1.41
17.333	0.00	0.28	0.241	IO				1.40
17.417	0.00	0.28	0.239	IO				1.39
17.500	0.00	0.28	0.237	IO				1.38
17.583	0.00	0.28	0.236	IO				1.38
17.667	0.00	0.27	0.234	IO				1.37
17.750	0.00	0.27	0.232	IO				1.36
17.833	0.00	0.27	0.230	IO				1.35
17.917	0.00	0.27	0.228	IO				1.34
18.000	0.00	0.27	0.226	IO				1.33
18.083	0.00	0.27	0.224	IO				1.32
18.167	0.00	0.27	0.222	IO				1.32
18.250	0.00	0.27	0.221	IO				1.31
18.333	0.00	0.27	0.219	IO				1.30
18.417	0.00	0.27	0.217	IO				1.29
18.500	0.00	0.27	0.215	IO				1.28
18.583	0.00	0.26	0.213	IO				1.27
18.667	0.00	0.26	0.211	IO				1.27
18.750	0.00	0.26	0.210	IO				1.26
18.833	0.00	0.26	0.208	IO				1.25
18.917	0.00	0.26	0.206	IO				1.24
19.000	0.00	0.26	0.204	IO				1.23
19.083	0.00	0.26	0.202	IO				1.22
19.167	0.00	0.26	0.201	IO				1.22
19.250	0.00	0.26	0.199	IO				1.21
19.333	0.00	0.26	0.197	IO				1.20
19.417	0.00	0.26	0.195	IO				1.19
19.500	0.00	0.26	0.193	IO				1.18
19.583	0.00	0.25	0.192	IO				1.18
19.667	0.00	0.25	0.190	IO				1.17
19.750	0.00	0.25	0.188	IO				1.16
19.833	0.00	0.25	0.186	IO				1.15
19.917	0.00	0.25	0.185	IO				1.14
20.000	0.00	0.25	0.183	IO				1.14
20.083	0.00	0.25	0.181	IO				1.13
20.167	0.00	0.25	0.180	IO				1.12
20.250	0.00	0.25	0.178	IO				1.11
20.333	0.00	0.25	0.176	IO				1.11
20.417	0.00	0.25	0.174	IO				1.10
20.500	0.00	0.25	0.173	IO				1.09
20.583	0.00	0.24	0.171	IO				1.08
20.667	0.00	0.24	0.169	IO				1.07
20.750	0.00	0.24	0.168	IO				1.07
20.833	0.00	0.24	0.166	IO				1.06
20.917	0.00	0.24	0.164	IO				1.05
21.000	0.00	0.24	0.163	IO				1.04
21.083	0.00	0.24	0.161	IO				1.04
21.167	0.00	0.24	0.159	IO				1.03
21.250	0.00	0.24	0.158	IO				1.02
21.333	0.00	0.24	0.156	IO				1.01
21.417	0.00	0.24	0.154	IO				1.01
21.500	0.00	0.24	0.153	IO				1.00
21.583	0.00	0.23	0.151	IO				0.99
21.667	0.00	0.23	0.150	IO				0.98
21.750	0.00	0.23	0.148	IO				0.98
21.833	0.00	0.23	0.146	IO				0.97
21.917	0.00	0.23	0.145	IO				0.96
22.000	0.00	0.23	0.143	IO				0.96
22.083	0.00	0.23	0.142	IO				0.95
22.167	0.00	0.23	0.140	IO				0.94
22.250	0.00	0.23	0.139	IO				0.93
22.333	0.00	0.23	0.137	IO				0.93
22.417	0.00	0.23	0.135	IO				0.92
22.500	0.00	0.22	0.134	IO				0.91
22.583	0.00	0.22	0.132	IO				0.90
22.667	0.00	0.22	0.131	IO				0.90
22.750	0.00	0.22	0.129	IO				0.89
22.833	0.00	0.22	0.128	IO				0.88
22.917	0.00	0.22	0.126	IO				0.88
23.000	0.00	0.22	0.125	IO				0.87
23.083	0.00	0.22	0.123	IO				0.86
23.167	0.00	0.22	0.122	IO				0.86

23.250	0.00	0.22	0.120	IO				0.85
23.333	0.00	0.22	0.119	IO				0.84
23.417	0.00	0.21	0.117	IO				0.84
23.500	0.00	0.21	0.116	IO				0.83
23.583	0.00	0.21	0.114	IO				0.82
23.667	0.00	0.21	0.113	IO				0.82
23.750	0.00	0.21	0.111	IO				0.81
23.833	0.00	0.21	0.110	IO				0.80
23.917	0.00	0.21	0.108	IO				0.80
24.000	0.00	0.21	0.107	IO				0.79
24.083	0.00	0.21	0.106	IO				0.78
24.167	0.00	0.21	0.104	IO				0.78
24.250	0.00	0.21	0.103	IO				0.77
24.333	0.00	0.20	0.101	IO				0.76
24.417	0.00	0.20	0.100	IO				0.76
24.500	0.00	0.20	0.099	IO				0.75
24.583	0.00	0.20	0.097	IO				0.74
24.667	0.00	0.20	0.096	IO				0.74
24.750	0.00	0.20	0.094	IO				0.73
24.833	0.00	0.20	0.093	IO				0.72
24.917	0.00	0.20	0.092	IO				0.72
25.000	0.00	0.20	0.090	IO				0.71
25.083	0.00	0.20	0.089	IO				0.71
25.167	0.00	0.20	0.088	IO				0.70
25.250	0.00	0.20	0.086	IO				0.69
25.333	0.00	0.19	0.085	IO				0.69
25.417	0.00	0.19	0.084	IO				0.68
25.500	0.00	0.19	0.082	IO				0.67
25.583	0.00	0.19	0.081	IO				0.67
25.667	0.00	0.19	0.080	IO				0.66
25.750	0.00	0.19	0.078	IO				0.66
25.833	0.00	0.19	0.077	IO				0.65
25.917	0.00	0.19	0.076	IO				0.64
26.000	0.00	0.19	0.074	IO				0.64
26.083	0.00	0.19	0.073	IO				0.63
26.167	0.00	0.19	0.072	IO				0.63
26.250	0.00	0.19	0.070	IO				0.62
26.333	0.00	0.18	0.069	IO				0.61
26.417	0.00	0.18	0.068	IO				0.61
26.500	0.00	0.18	0.067	IO				0.60
26.583	0.00	0.18	0.065	IO				0.60
26.667	0.00	0.18	0.064	IO				0.59
26.750	0.00	0.18	0.063	IO				0.58
26.833	0.00	0.18	0.062	IO				0.58
26.917	0.00	0.18	0.060	IO				0.57
27.000	0.00	0.18	0.059	IO				0.57
27.083	0.00	0.18	0.058	IO				0.56
27.167	0.00	0.18	0.057	IO				0.55
27.250	0.00	0.17	0.056	IO				0.55
27.333	0.00	0.17	0.054	O				0.54
27.417	0.00	0.17	0.053	O				0.54
27.500	0.00	0.17	0.052	O				0.53
27.583	0.00	0.17	0.051	O				0.52
27.667	0.00	0.17	0.050	O				0.52
27.750	0.00	0.17	0.048	O				0.51
27.833	0.00	0.17	0.047	O				0.51
27.917	0.00	0.17	0.046	O				0.50
28.000	0.00	0.17	0.045	O				0.49
28.083	0.00	0.16	0.044	O				0.48
28.167	0.00	0.16	0.043	O				0.48
28.250	0.00	0.16	0.042	O				0.47
28.333	0.00	0.16	0.041	O				0.46
28.417	0.00	0.16	0.039	O				0.45
28.500	0.00	0.16	0.038	O				0.45
28.583	0.00	0.15	0.037	O				0.44
28.667	0.00	0.15	0.036	O				0.43
28.750	0.00	0.15	0.035	O				0.42
28.833	0.00	0.15	0.034	O				0.42
28.917	0.00	0.15	0.033	O				0.41
29.000	0.00	0.15	0.032	O				0.40
29.083	0.00	0.15	0.031	O				0.39
29.167	0.00	0.14	0.030	O				0.39

29.250	0.00	0.14	0.029	O	|	|	|	0.38
29.333	0.00	0.14	0.028	O	|	|	|	0.37
29.417	0.00	0.14	0.027	O	|	|	|	0.37
29.500	0.00	0.14	0.026	O	|	|	|	0.36
29.583	0.00	0.14	0.025	O	|	|	|	0.35
29.667	0.00	0.14	0.024	O	|	|	|	0.34
29.750	0.00	0.14	0.023	O	|	|	|	0.34
29.833	0.00	0.13	0.022	O	|	|	|	0.33
29.917	0.00	0.13	0.021	O	|	|	|	0.32
30.000	0.00	0.13	0.021	O	|	|	|	0.32
30.083	0.00	0.13	0.020	O	|	|	|	0.31
30.167	0.00	0.13	0.019	O	|	|	|	0.31
30.250	0.00	0.13	0.018	O	|	|	|	0.30
30.333	0.00	0.13	0.017	O	|	|	|	0.29
30.417	0.00	0.13	0.016	O	|	|	|	0.29
30.500	0.00	0.12	0.015	O	|	|	|	0.28
30.583	0.00	0.12	0.014	O	|	|	|	0.27
30.667	0.00	0.12	0.014	O	|	|	|	0.27
30.750	0.00	0.12	0.013	O	|	|	|	0.26
30.833	0.00	0.12	0.012	O	|	|	|	0.26
30.917	0.00	0.12	0.011	O	|	|	|	0.25
31.000	0.00	0.11	0.010	O	|	|	|	0.24
31.083	0.00	0.10	0.010	O	|	|	|	0.22
31.167	0.00	0.10	0.009	O	|	|	|	0.20
31.250	0.00	0.09	0.008	O	|	|	|	0.19
31.333	0.00	0.08	0.008	O	|	|	|	0.17
31.417	0.00	0.08	0.007	O	|	|	|	0.16
31.500	0.00	0.07	0.007	O	|	|	|	0.15
31.583	0.00	0.07	0.006	O	|	|	|	0.14
31.667	0.00	0.06	0.006	O	|	|	|	0.13
31.750	0.00	0.06	0.005	O	|	|	|	0.12
31.833	0.00	0.05	0.005	O	|	|	|	0.11
31.917	0.00	0.05	0.005	O	|	|	|	0.10
32.000	0.00	0.05	0.004	O	|	|	|	0.10
32.083	0.00	0.04	0.004	O	|	|	|	0.09
32.167	0.00	0.04	0.004	O	|	|	|	0.08
32.250	0.00	0.04	0.003	O	|	|	|	0.08
32.333	0.00	0.03	0.003	O	|	|	|	0.07
32.417	0.00	0.03	0.003	O	|	|	|	0.07
32.500	0.00	0.03	0.003	O	|	|	|	0.06
32.583	0.00	0.03	0.003	O	|	|	|	0.06
32.667	0.00	0.03	0.002	O	|	|	|	0.05
32.750	0.00	0.02	0.002	O	|	|	|	0.05
32.833	0.00	0.02	0.002	O	|	|	|	0.05
32.917	0.00	0.02	0.002	O	|	|	|	0.04
33.000	0.00	0.02	0.002	O	|	|	|	0.04
33.083	0.00	0.02	0.002	O	|	|	|	0.04
33.167	0.00	0.02	0.002	O	|	|	|	0.03
33.250	0.00	0.02	0.001	O	|	|	|	0.03
33.333	0.00	0.01	0.001	O	|	|	|	0.03
33.417	0.00	0.01	0.001	O	|	|	|	0.03
33.500	0.00	0.01	0.001	O	|	|	|	0.03
33.583	0.00	0.01	0.001	O	|	|	|	0.02
33.667	0.00	0.01	0.001	O	|	|	|	0.02
33.750	0.00	0.01	0.001	O	|	|	|	0.02
33.833	0.00	0.01	0.001	O	|	|	|	0.02
33.917	0.00	0.01	0.001	O	|	|	|	0.02
34.000	0.00	0.01	0.001	O	|	|	|	0.02
34.083	0.00	0.01	0.001	O	|	|	|	0.02
34.167	0.00	0.01	0.001	O	|	|	|	0.01
34.250	0.00	0.01	0.001	O	|	|	|	0.01
34.333	0.00	0.01	0.001	O	|	|	|	0.01
34.417	0.00	0.01	0.000	O	|	|	|	0.01
34.500	0.00	0.00	0.000	O	|	|	|	0.01
34.583	0.00	0.00	0.000	O	|	|	|	0.01
34.667	0.00	0.00	0.000	O	|	|	|	0.01
34.750	0.00	0.00	0.000	O	|	|	|	0.01
34.833	0.00	0.00	0.000	O	|	|	|	0.01
34.917	0.00	0.00	0.000	O	|	|	|	0.01
35.000	0.00	0.00	0.000	O	|	|	|	0.01
35.083	0.00	0.00	0.000	O	|	|	|	0.01
35.167	0.00	0.00	0.000	O	|	|	|	0.01

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35.250    0.00    0.00      0.000  O       |       |       |       |     0.01
35.333    0.00    0.00      0.000  O       |       |       |       |     0.01
35.417    0.00    0.00      0.000  O       |       |       |       |     0.00
35.500    0.00    0.00      0.000  O       |       |       |       |     0.00
35.583    0.00    0.00      0.000  O       |       |       |       |     0.00
35.667    0.00    0.00      0.000  O       |       |       |       |     0.00
35.750    0.00    0.00      0.000  O       |       |       |       |     0.00
35.833    0.00    0.00      0.000  O       |       |       |       |     0.00
35.917    0.00    0.00      0.000  O       |       |       |       |     0.00
36.000    0.00    0.00      0.000  O       |       |       |       |     0.00
36.083    0.00    0.00      0.000  O       |       |       |       |     0.00
36.167    0.00    0.00      0.000  O       |       |       |       |     0.00
36.250    0.00    0.00      0.000  O       |       |       |       |     0.00
36.333    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                       Number of intervals =   436
                       Time interval =    5.0 (Min.)
                       Maximum/Peak flow rate =        0.399 (CFS)
                       Total volume =       0.677 (Ac.Ft)
               Status of hydrographs being held in storage
                          Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
               Peak (CFS)      0.000     0.000     0.000     0.000     0.000
               Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
3-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD0535.rte
**********HYDROGRAPH DATA**********
Number of intervals = 37
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 6.436 (CFS)
Total volume = 0.523 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 37
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991	
5.600	0.979	5.490	0.960	0.998	

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.6 3.22 4.83 6.44	Depth (Ft.)
0.083	0.72	0.03	0.002	O I | | | | |	0.05
0.167	0.97	0.08	0.008	O I | | | | |	0.18
0.250	0.86	0.12	0.013	O I | | | | |	0.27
0.333	1.04	0.13	0.019	O I | | | | |	0.31
0.417	1.12	0.14	0.026	O I | | | | |	0.35
0.500	1.29	0.15	0.033	O I | | | | |	0.41
0.583	1.18	0.16	0.040	O I | | | | |	0.46
0.667	1.29	0.17	0.048	O I | | | | |	0.51
0.750	1.34	0.17	0.056	O I | | | | |	0.55
0.833	1.18	0.18	0.063	O I | | | | |	0.59
0.917	1.18	0.19	0.070	O I | | | | |	0.62
1.000	1.31	0.19	0.077	O I | | | | |	0.65
1.083	1.57	0.20	0.086	O I | | | | |	0.69
1.167	1.64	0.20	0.095	O I | | | | |	0.74
1.250	1.64	0.21	0.105	|O I | | | |	0.78
1.333	1.53	0.21	0.115	|O I | | | |	0.82
1.417	1.83	0.22	0.125	|O I | | | |	0.87
1.500	2.00	0.23	0.137	|O I | | | |	0.92
1.583	1.85	0.23	0.148	|O I | | | |	0.98
1.667	1.96	0.24	0.160	|O I | | | |	1.03
1.750	2.35	0.25	0.173	|O | I | | |	1.09
1.833	2.35	0.25	0.187	|O | I | | |	1.16
1.917	2.20	0.26	0.201	|O | I | | |	1.22
2.000	2.22	0.27	0.215	|O | I | | |	1.28
2.083	2.30	0.27	0.228	|O | I | | |	1.34
2.167	2.93	0.28	0.244	|O | | I | |	1.42
2.250	3.58	0.29	0.265	|O | | | I |	1.51
2.333	2.90	0.30	0.285	|O | | I | |	1.60
2.417	4.67	0.31	0.309	|O | | | I |	1.71
2.500	5.71	0.32	0.343	|O | | | | I	1.87
2.583	6.44	0.34	0.382	|O | | | | | I	2.04
2.667	5.08	0.35	0.420	|O | | | I |	2.21
2.750	2.27	0.36	0.442	|O | I | | |	2.32
2.833	1.38	0.36	0.453	|O I | | | |	2.36
2.917	1.34	0.37	0.459	|O I | | | |	2.39
3.000	0.68	0.37	0.464	|O I | | | |	2.41
3.083	0.11	0.37	0.464	IO | | | |	2.41
3.167	0.00	0.37	0.462	IO | | | |	2.40
3.250	0.00	0.37	0.459	IO | | | |	2.39
3.333	0.00	0.36	0.457	IO | | | |	2.38
3.417	0.00	0.36	0.454	IO | | | |	2.37
3.500	0.00	0.36	0.452	IO | | | |	2.36
3.583	0.00	0.36	0.449	IO | | | |	2.35
3.667	0.00	0.36	0.447	IO | | | |	2.34
3.750	0.00	0.36	0.444	IO | | | |	2.32
3.833	0.00	0.36	0.442	IO | | | |	2.31
3.917	0.00	0.36	0.439	IO | | | |	2.30
4.000	0.00	0.36	0.437	IO | | | |	2.29
4.083	0.00	0.36	0.435	IO | | | |	2.28
4.167	0.00	0.36	0.432	IO | | | |	2.27
4.250	0.00	0.35	0.430	IO | | | |	2.26
4.333	0.00	0.35	0.427	IO | | | |	2.25
4.417	0.00	0.35	0.425	IO | | | |	2.24
4.500	0.00	0.35	0.422	IO | | | |	2.22
4.583	0.00	0.35	0.420	IO | | | |	2.21
4.667	0.00	0.35	0.417	IO | | | |	2.20
4.750	0.00	0.35	0.415	IO | | | |	2.19
4.833	0.00	0.35	0.413	IO | | | |	2.18
4.917	0.00	0.35	0.410	IO | | | |	2.17
5.000	0.00	0.35	0.408	IO | | | |	2.16
5.083	0.00	0.35	0.405	IO | | | |	2.15
5.167	0.00	0.34	0.403	IO | | | |	2.14

5.250	0.00	0.34	0.401	IO				2.13
5.333	0.00	0.34	0.398	IO				2.12
5.417	0.00	0.34	0.396	IO				2.10
5.500	0.00	0.34	0.394	IO				2.09
5.583	0.00	0.34	0.391	IO				2.08
5.667	0.00	0.34	0.389	IO				2.07
5.750	0.00	0.34	0.387	IO				2.06
5.833	0.00	0.34	0.384	IO				2.05
5.917	0.00	0.34	0.382	IO				2.04
6.000	0.00	0.34	0.380	IO				2.03
6.083	0.00	0.34	0.377	IO				2.02
6.167	0.00	0.33	0.375	IO				2.01
6.250	0.00	0.33	0.373	IO				2.00
6.333	0.00	0.33	0.370	IO				1.99
6.417	0.00	0.33	0.368	IO				1.98
6.500	0.00	0.33	0.366	IO				1.97
6.583	0.00	0.33	0.364	IO				1.96
6.667	0.00	0.33	0.361	IO				1.95
6.750	0.00	0.33	0.359	IO				1.94
6.833	0.00	0.33	0.357	IO				1.93
6.917	0.00	0.33	0.355	IO				1.92
7.000	0.00	0.33	0.352	IO				1.91
7.083	0.00	0.33	0.350	IO				1.90
7.167	0.00	0.32	0.348	IO				1.89
7.250	0.00	0.32	0.346	IO				1.88
7.333	0.00	0.32	0.343	IO				1.87
7.417	0.00	0.32	0.341	IO				1.86
7.500	0.00	0.32	0.339	IO				1.85
7.583	0.00	0.32	0.337	IO				1.84
7.667	0.00	0.32	0.334	IO				1.83
7.750	0.00	0.32	0.332	IO				1.82
7.833	0.00	0.32	0.330	IO				1.81
7.917	0.00	0.32	0.328	IO				1.80
8.000	0.00	0.32	0.326	IO				1.79
8.083	0.00	0.32	0.324	IO				1.78
8.167	0.00	0.31	0.321	IO				1.77
8.250	0.00	0.31	0.319	IO				1.76
8.333	0.00	0.31	0.317	IO				1.75
8.417	0.00	0.31	0.315	IO				1.74
8.500	0.00	0.31	0.313	IO				1.73
8.583	0.00	0.31	0.311	IO				1.72
8.667	0.00	0.31	0.309	IO				1.71
8.750	0.00	0.31	0.306	IO				1.70
8.833	0.00	0.31	0.304	IO				1.69
8.917	0.00	0.31	0.302	IO				1.68
9.000	0.00	0.31	0.300	IO				1.67
9.083	0.00	0.30	0.298	IO				1.66
9.167	0.00	0.30	0.296	IO				1.65
9.250	0.00	0.30	0.294	IO				1.64
9.333	0.00	0.30	0.292	IO				1.63
9.417	0.00	0.30	0.290	IO				1.62
9.500	0.00	0.30	0.288	IO				1.61
9.583	0.00	0.30	0.286	IO				1.60
9.667	0.00	0.30	0.283	IO				1.59
9.750	0.00	0.30	0.281	IO				1.59
9.833	0.00	0.30	0.279	IO				1.58
9.917	0.00	0.30	0.277	IO				1.57
10.000	0.00	0.29	0.275	IO				1.56
10.083	0.00	0.29	0.273	IO				1.55
10.167	0.00	0.29	0.271	IO				1.54
10.250	0.00	0.29	0.269	IO				1.53
10.333	0.00	0.29	0.267	IO				1.52
10.417	0.00	0.29	0.265	IO				1.51
10.500	0.00	0.29	0.263	IO				1.50
10.583	0.00	0.29	0.261	IO				1.49
10.667	0.00	0.29	0.259	IO				1.48
10.750	0.00	0.29	0.257	IO				1.47
10.833	0.00	0.29	0.255	IO				1.47
10.917	0.00	0.28	0.253	IO				1.46
11.000	0.00	0.28	0.251	IO				1.45
11.083	0.00	0.28	0.249	IO				1.44
11.167	0.00	0.28	0.248	IO				1.43

11.250	0.00	0.28	0.246	IO				1.42
11.333	0.00	0.28	0.244	IO				1.41
11.417	0.00	0.28	0.242	IO				1.40
11.500	0.00	0.28	0.240	IO				1.39
11.583	0.00	0.28	0.238	IO				1.39
11.667	0.00	0.28	0.236	IO				1.38
11.750	0.00	0.28	0.234	IO				1.37
11.833	0.00	0.27	0.232	IO				1.36
11.917	0.00	0.27	0.230	IO				1.35
12.000	0.00	0.27	0.228	IO				1.34
12.083	0.00	0.27	0.227	IO				1.33
12.167	0.00	0.27	0.225	IO				1.33
12.250	0.00	0.27	0.223	IO				1.32
12.333	0.00	0.27	0.221	IO				1.31
12.417	0.00	0.27	0.219	IO				1.30
12.500	0.00	0.27	0.217	IO				1.29
12.583	0.00	0.27	0.215	IO				1.28
12.667	0.00	0.27	0.214	IO				1.28
12.750	0.00	0.26	0.212	IO				1.27
12.833	0.00	0.26	0.210	IO				1.26
12.917	0.00	0.26	0.208	IO				1.25
13.000	0.00	0.26	0.206	IO				1.24
13.083	0.00	0.26	0.205	IO				1.23
13.167	0.00	0.26	0.203	IO				1.23
13.250	0.00	0.26	0.201	IO				1.22
13.333	0.00	0.26	0.199	IO				1.21
13.417	0.00	0.26	0.197	IO				1.20
13.500	0.00	0.26	0.196	IO				1.19
13.583	0.00	0.26	0.194	IO				1.19
13.667	0.00	0.25	0.192	IO				1.18
13.750	0.00	0.25	0.190	IO				1.17
13.833	0.00	0.25	0.189	IO				1.16
13.917	0.00	0.25	0.187	IO				1.15
14.000	0.00	0.25	0.185	IO				1.15
14.083	0.00	0.25	0.183	IO				1.14
14.167	0.00	0.25	0.182	IO				1.13
14.250	0.00	0.25	0.180	IO				1.12
14.333	0.00	0.25	0.178	IO				1.11
14.417	0.00	0.25	0.177	IO				1.11
14.500	0.00	0.25	0.175	IO				1.10
14.583	0.00	0.25	0.173	IO				1.09
14.667	0.00	0.24	0.172	IO				1.08
14.750	0.00	0.24	0.170	IO				1.08
14.833	0.00	0.24	0.168	IO				1.07
14.917	0.00	0.24	0.166	IO				1.06
15.000	0.00	0.24	0.165	IO				1.05
15.083	0.00	0.24	0.163	IO				1.05
15.167	0.00	0.24	0.161	IO				1.04
15.250	0.00	0.24	0.160	IO				1.03
15.333	0.00	0.24	0.158	IO				1.02
15.417	0.00	0.24	0.157	IO				1.02
15.500	0.00	0.24	0.155	IO				1.01
15.583	0.00	0.24	0.153	IO				1.00
15.667	0.00	0.24	0.152	IO				0.99
15.750	0.00	0.23	0.150	IO				0.99
15.833	0.00	0.23	0.148	IO				0.98
15.917	0.00	0.23	0.147	IO				0.97
16.000	0.00	0.23	0.145	IO				0.96
16.083	0.00	0.23	0.144	IO				0.96
16.167	0.00	0.23	0.142	IO				0.95
16.250	0.00	0.23	0.140	IO				0.94
16.333	0.00	0.23	0.139	IO				0.94
16.417	0.00	0.23	0.137	IO				0.93
16.500	0.00	0.23	0.136	IO				0.92
16.583	0.00	0.22	0.134	IO				0.91
16.667	0.00	0.22	0.133	IO				0.91
16.750	0.00	0.22	0.131	IO				0.90
16.833	0.00	0.22	0.130	IO				0.89
16.917	0.00	0.22	0.128	IO				0.89
17.000	0.00	0.22	0.127	IO				0.88
17.083	0.00	0.22	0.125	IO				0.87
17.167	0.00	0.22	0.124	IO				0.86

17.250	0.00	0.22	0.122	IO				0.86
17.333	0.00	0.22	0.121	IO				0.85
17.417	0.00	0.22	0.119	IO				0.84
17.500	0.00	0.21	0.118	IO				0.84
17.583	0.00	0.21	0.116	IO				0.83
17.667	0.00	0.21	0.115	IO				0.82
17.750	0.00	0.21	0.113	IO				0.82
17.833	0.00	0.21	0.112	IO				0.81
17.917	0.00	0.21	0.110	IO				0.80
18.000	0.00	0.21	0.109	IO				0.80
18.083	0.00	0.21	0.107	IO				0.79
18.167	0.00	0.21	0.106	IO				0.78
18.250	0.00	0.21	0.105	IO				0.78
18.333	0.00	0.21	0.103	IO				0.77
18.417	0.00	0.20	0.102	IO				0.76
18.500	0.00	0.20	0.100	IO				0.76
18.583	0.00	0.20	0.099	IO				0.75
18.667	0.00	0.20	0.098	IO				0.75
18.750	0.00	0.20	0.096	IO				0.74
18.833	0.00	0.20	0.095	O				0.73
18.917	0.00	0.20	0.093	O				0.73
19.000	0.00	0.20	0.092	O				0.72
19.083	0.00	0.20	0.091	O				0.71
19.167	0.00	0.20	0.089	O				0.71
19.250	0.00	0.20	0.088	O				0.70
19.333	0.00	0.20	0.087	O				0.69
19.417	0.00	0.19	0.085	O				0.69
19.500	0.00	0.19	0.084	O				0.68
19.583	0.00	0.19	0.083	O				0.68
19.667	0.00	0.19	0.081	O				0.67
19.750	0.00	0.19	0.080	O				0.66
19.833	0.00	0.19	0.079	O				0.66
19.917	0.00	0.19	0.077	O				0.65
20.000	0.00	0.19	0.076	O				0.65
20.083	0.00	0.19	0.075	O				0.64
20.167	0.00	0.19	0.073	O				0.63
20.250	0.00	0.19	0.072	O				0.63
20.333	0.00	0.19	0.071	O				0.62
20.417	0.00	0.19	0.070	O				0.62
20.500	0.00	0.18	0.068	O				0.61
20.583	0.00	0.18	0.067	O				0.60
20.667	0.00	0.18	0.066	O				0.60
20.750	0.00	0.18	0.064	O				0.59
20.833	0.00	0.18	0.063	O				0.59
20.917	0.00	0.18	0.062	O				0.58
21.000	0.00	0.18	0.061	O				0.57
21.083	0.00	0.18	0.060	O				0.57
21.167	0.00	0.18	0.058	O				0.56
21.250	0.00	0.18	0.057	O				0.56
21.333	0.00	0.17	0.056	O				0.55
21.417	0.00	0.17	0.055	O				0.54
21.500	0.00	0.17	0.053	O				0.54
21.583	0.00	0.17	0.052	O				0.53
21.667	0.00	0.17	0.051	O				0.53
21.750	0.00	0.17	0.050	O				0.52
21.833	0.00	0.17	0.049	O				0.51
21.917	0.00	0.17	0.048	O				0.51
22.000	0.00	0.17	0.046	O				0.50
22.083	0.00	0.17	0.045	O				0.50
22.167	0.00	0.16	0.044	O				0.49
22.250	0.00	0.16	0.043	O				0.48
22.333	0.00	0.16	0.042	O				0.47
22.417	0.00	0.16	0.041	O				0.46
22.500	0.00	0.16	0.040	O				0.46
22.583	0.00	0.16	0.039	O				0.45
22.667	0.00	0.16	0.038	O				0.44
22.750	0.00	0.15	0.037	O				0.43
22.833	0.00	0.15	0.035	O				0.42
22.917	0.00	0.15	0.034	O				0.42
23.000	0.00	0.15	0.033	O				0.41
23.083	0.00	0.15	0.032	O				0.40
23.167	0.00	0.15	0.031	O				0.40

23.250	0.00	0.15	0.030	O	|	|	|	0.39
23.333	0.00	0.14	0.029	O	|	|	|	0.38
23.417	0.00	0.14	0.028	O	|	|	|	0.37
23.500	0.00	0.14	0.027	O	|	|	|	0.37
23.583	0.00	0.14	0.026	O	|	|	|	0.36
23.667	0.00	0.14	0.025	O	|	|	|	0.35
23.750	0.00	0.14	0.025	O	|	|	|	0.35
23.833	0.00	0.14	0.024	O	|	|	|	0.34
23.917	0.00	0.13	0.023	O	|	|	|	0.33
24.000	0.00	0.13	0.022	O	|	|	|	0.33
24.083	0.00	0.13	0.021	O	|	|	|	0.32
24.167	0.00	0.13	0.020	O	|	|	|	0.31
24.250	0.00	0.13	0.019	O	|	|	|	0.31
24.333	0.00	0.13	0.018	O	|	|	|	0.30
24.417	0.00	0.13	0.017	O	|	|	|	0.29
24.500	0.00	0.13	0.016	O	|	|	|	0.29
24.583	0.00	0.12	0.016	O	|	|	|	0.28
24.667	0.00	0.12	0.015	O	|	|	|	0.28
24.750	0.00	0.12	0.014	O	|	|	|	0.27
24.833	0.00	0.12	0.013	O	|	|	|	0.26
24.917	0.00	0.12	0.012	O	|	|	|	0.26
25.000	0.00	0.12	0.011	O	|	|	|	0.25
25.083	0.00	0.11	0.011	O	|	|	|	0.24
25.167	0.00	0.11	0.010	O	|	|	|	0.22
25.250	0.00	0.10	0.009	O	|	|	|	0.21
25.333	0.00	0.09	0.008	O	|	|	|	0.19
25.417	0.00	0.08	0.008	O	|	|	|	0.18
25.500	0.00	0.08	0.007	O	|	|	|	0.17
25.583	0.00	0.07	0.007	O	|	|	|	0.15
25.667	0.00	0.07	0.006	O	|	|	|	0.14
25.750	0.00	0.06	0.006	O	|	|	|	0.13
25.833	0.00	0.06	0.005	O	|	|	|	0.12
25.917	0.00	0.05	0.005	O	|	|	|	0.11
26.000	0.00	0.05	0.005	O	|	|	|	0.11
26.083	0.00	0.05	0.004	O	|	|	|	0.10
26.167	0.00	0.04	0.004	O	|	|	|	0.09
26.250	0.00	0.04	0.004	O	|	|	|	0.09
26.333	0.00	0.04	0.003	O	|	|	|	0.08
26.417	0.00	0.03	0.003	O	|	|	|	0.07
26.500	0.00	0.03	0.003	O	|	|	|	0.07
26.583	0.00	0.03	0.003	O	|	|	|	0.06
26.667	0.00	0.03	0.003	O	|	|	|	0.06
26.750	0.00	0.03	0.002	O	|	|	|	0.05
26.833	0.00	0.02	0.002	O	|	|	|	0.05
26.917	0.00	0.02	0.002	O	|	|	|	0.05
27.000	0.00	0.02	0.002	O	|	|	|	0.04
27.083	0.00	0.02	0.002	O	|	|	|	0.04
27.167	0.00	0.02	0.002	O	|	|	|	0.04
27.250	0.00	0.02	0.002	O	|	|	|	0.04
27.333	0.00	0.02	0.001	O	|	|	|	0.03
27.417	0.00	0.01	0.001	O	|	|	|	0.03
27.500	0.00	0.01	0.001	O	|	|	|	0.03
27.583	0.00	0.01	0.001	O	|	|	|	0.03
27.667	0.00	0.01	0.001	O	|	|	|	0.02
27.750	0.00	0.01	0.001	O	|	|	|	0.02
27.833	0.00	0.01	0.001	O	|	|	|	0.02
27.917	0.00	0.01	0.001	O	|	|	|	0.02
28.000	0.00	0.01	0.001	O	|	|	|	0.02
28.083	0.00	0.01	0.001	O	|	|	|	0.02
28.167	0.00	0.01	0.001	O	|	|	|	0.02
28.250	0.00	0.01	0.001	O	|	|	|	0.01
28.333	0.00	0.01	0.001	O	|	|	|	0.01
28.417	0.00	0.01	0.001	O	|	|	|	0.01
28.500	0.00	0.01	0.001	O	|	|	|	0.01
28.583	0.00	0.01	0.000	O	|	|	|	0.01
28.667	0.00	0.00	0.000	O	|	|	|	0.01
28.750	0.00	0.00	0.000	O	|	|	|	0.01
28.833	0.00	0.00	0.000	O	|	|	|	0.01
28.917	0.00	0.00	0.000	O	|	|	|	0.01
29.000	0.00	0.00	0.000	O	|	|	|	0.01
29.083	0.00	0.00	0.000	O	|	|	|	0.01
29.167	0.00	0.00	0.000	O	|	|	|	0.01

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29.250    0.00    0.00      0.000  O       |       |       |       |     0.01
29.333    0.00    0.00      0.000  O       |       |       |       |     0.01
29.417    0.00    0.00      0.000  O       |       |       |       |     0.01
29.500    0.00    0.00      0.000  O       |       |       |       |     0.00
29.583    0.00    0.00      0.000  O       |       |       |       |     0.00
29.667    0.00    0.00      0.000  O       |       |       |       |     0.00
29.750    0.00    0.00      0.000  O       |       |       |       |     0.00
29.833    0.00    0.00      0.000  O       |       |       |       |     0.00
29.917    0.00    0.00      0.000  O       |       |       |       |     0.00
30.000    0.00    0.00      0.000  O       |       |       |       |     0.00
30.083    0.00    0.00      0.000  O       |       |       |       |     0.00
30.167    0.00    0.00      0.000  O       |       |       |       |     0.00
30.250    0.00    0.00      0.000  O       |       |       |       |     0.00
30.333    0.00    0.00      0.000  O       |       |       |       |     0.00
30.417    0.00    0.00      0.000  O       |       |       |       |     0.00

        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =   365
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.367 (CFS)
                      Total volume =       0.523 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
1-HOUR - 5-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD0515.rte
**********HYDROGRAPH DATA**********
Number of intervals = 13
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 11.192 (CFS)
Total volume = 0.318 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 13
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	2.8	5.60	8.39	11.19	Depth (Ft.)
0.083	1.45	0.05	0.005	O I	|	|	|	|	0.11
0.167	1.97	0.12	0.016	O I	|	|	|	|	0.29
0.250	2.28	0.14	0.030	O I	|	|	|	|	0.38
0.333	2.38	0.17	0.045	O I	|	|	|	|	0.49
0.417	2.48	0.18	0.060	O I	|	|	|	|	0.57
0.500	2.74	0.19	0.077	O I	|	|	|	|	0.65
0.583	3.31	0.20	0.096	O	I	|	|	|	0.74
0.667	3.92	0.22	0.120	O	I	|	|	|	0.85
0.750	5.55	0.23	0.151	O	|	I	|	|	0.99
0.833	11.19	0.26	0.207	O	|	|	|	I	1.25
0.917	5.89	0.29	0.264	O	|	I	|	|	1.50
1.000	2.50	0.30	0.291	O I	|	|	|	|	1.63
1.083	0.55	0.30	0.299	OI	|	|	|	|	1.67
1.167	0.00	0.30	0.299	O	|	|	|	|	1.67
1.250	0.00	0.30	0.297	O	|	|	|	|	1.66
1.333	0.00	0.30	0.295	O	|	|	|	|	1.65
1.417	0.00	0.30	0.293	O	|	|	|	|	1.64
1.500	0.00	0.30	0.291	O	|	|	|	|	1.63
1.583	0.00	0.30	0.289	O	|	|	|	|	1.62
1.667	0.00	0.30	0.286	O	|	|	|	|	1.61
1.750	0.00	0.30	0.284	O	|	|	|	|	1.60
1.833	0.00	0.30	0.282	O	|	|	|	|	1.59
1.917	0.00	0.30	0.280	O	|	|	|	|	1.58
2.000	0.00	0.30	0.278	O	|	|	|	|	1.57
2.083	0.00	0.29	0.276	O	|	|	|	|	1.56
2.167	0.00	0.29	0.274	O	|	|	|	|	1.55
2.250	0.00	0.29	0.272	O	|	|	|	|	1.54
2.333	0.00	0.29	0.270	O	|	|	|	|	1.53
2.417	0.00	0.29	0.268	O	|	|	|	|	1.52
2.500	0.00	0.29	0.266	O	|	|	|	|	1.51
2.583	0.00	0.29	0.264	O	|	|	|	|	1.51
2.667	0.00	0.29	0.262	O	|	|	|	|	1.50
2.750	0.00	0.29	0.260	O	|	|	|	|	1.49
2.833	0.00	0.29	0.258	O	|	|	|	|	1.48
2.917	0.00	0.29	0.256	O	|	|	|	|	1.47
3.000	0.00	0.28	0.254	O	|	|	|	|	1.46
3.083	0.00	0.28	0.252	O	|	|	|	|	1.45
3.167	0.00	0.28	0.250	O	|	|	|	|	1.44
3.250	0.00	0.28	0.248	O	|	|	|	|	1.43
3.333	0.00	0.28	0.246	O	|	|	|	|	1.42
3.417	0.00	0.28	0.245	O	|	|	|	|	1.42
3.500	0.00	0.28	0.243	O	|	|	|	|	1.41
3.583	0.00	0.28	0.241	O	|	|	|	|	1.40
3.667	0.00	0.28	0.239	O	|	|	|	|	1.39
3.750	0.00	0.28	0.237	O	|	|	|	|	1.38
3.833	0.00	0.28	0.235	O	|	|	|	|	1.37
3.917	0.00	0.27	0.233	O	|	|	|	|	1.36
4.000	0.00	0.27	0.231	O	|	|	|	|	1.36
4.083	0.00	0.27	0.229	O	|	|	|	|	1.35
4.167	0.00	0.27	0.227	O	|	|	|	|	1.34
4.250	0.00	0.27	0.226	O	|	|	|	|	1.33
4.333	0.00	0.27	0.224	O	|	|	|	|	1.32
4.417	0.00	0.27	0.222	O	|	|	|	|	1.31
4.500	0.00	0.27	0.220	O	|	|	|	|	1.30
4.583	0.00	0.27	0.218	O	|	|	|	|	1.30
4.667	0.00	0.27	0.216	O	|	|	|	|	1.29
4.750	0.00	0.27	0.214	O	|	|	|	|	1.28
4.833	0.00	0.26	0.213	O	|	|	|	|	1.27
4.917	0.00	0.26	0.211	O	|	|	|	|	1.26
5.000	0.00	0.26	0.209	O	|	|	|	|	1.25
5.083	0.00	0.26	0.207	O	|	|	|	|	1.25
5.167	0.00	0.26	0.205	O	|	|	|	|	1.24

5.250	0.00	0.26	0.204	O	|	|	|	1.23
5.333	0.00	0.26	0.202	O	|	|	|	1.22
5.417	0.00	0.26	0.200	O	|	|	|	1.21
5.500	0.00	0.26	0.198	O	|	|	|	1.21
5.583	0.00	0.26	0.196	O	|	|	|	1.20
5.667	0.00	0.26	0.195	O	|	|	|	1.19
5.750	0.00	0.26	0.193	O	|	|	|	1.18
5.833	0.00	0.25	0.191	O	|	|	|	1.17
5.917	0.00	0.25	0.189	O	|	|	|	1.17
6.000	0.00	0.25	0.188	O	|	|	|	1.16
6.083	0.00	0.25	0.186	O	|	|	|	1.15
6.167	0.00	0.25	0.184	O	|	|	|	1.14
6.250	0.00	0.25	0.183	O	|	|	|	1.13
6.333	0.00	0.25	0.181	O	|	|	|	1.13
6.417	0.00	0.25	0.179	O	|	|	|	1.12
6.500	0.00	0.25	0.177	O	|	|	|	1.11
6.583	0.00	0.25	0.176	O	|	|	|	1.10
6.667	0.00	0.25	0.174	O	|	|	|	1.10
6.750	0.00	0.25	0.172	O	|	|	|	1.09
6.833	0.00	0.24	0.171	O	|	|	|	1.08
6.917	0.00	0.24	0.169	O	|	|	|	1.07
7.000	0.00	0.24	0.167	O	|	|	|	1.06
7.083	0.00	0.24	0.166	O	|	|	|	1.06
7.167	0.00	0.24	0.164	O	|	|	|	1.05
7.250	0.00	0.24	0.162	O	|	|	|	1.04
7.333	0.00	0.24	0.161	O	|	|	|	1.03
7.417	0.00	0.24	0.159	O	|	|	|	1.03
7.500	0.00	0.24	0.157	O	|	|	|	1.02
7.583	0.00	0.24	0.156	O	|	|	|	1.01
7.667	0.00	0.24	0.154	O	|	|	|	1.00
7.750	0.00	0.24	0.152	O	|	|	|	1.00
7.833	0.00	0.23	0.151	O	|	|	|	0.99
7.917	0.00	0.23	0.149	O	|	|	|	0.98
8.000	0.00	0.23	0.148	O	|	|	|	0.98
8.083	0.00	0.23	0.146	O	|	|	|	0.97
8.167	0.00	0.23	0.144	O	|	|	|	0.96
8.250	0.00	0.23	0.143	O	|	|	|	0.95
8.333	0.00	0.23	0.141	O	|	|	|	0.95
8.417	0.00	0.23	0.140	O	|	|	|	0.94
8.500	0.00	0.23	0.138	O	|	|	|	0.93
8.583	0.00	0.23	0.137	O	|	|	|	0.92
8.667	0.00	0.23	0.135	O	|	|	|	0.92
8.750	0.00	0.22	0.133	O	|	|	|	0.91
8.833	0.00	0.22	0.132	O	|	|	|	0.90
8.917	0.00	0.22	0.130	O	|	|	|	0.90
9.000	0.00	0.22	0.129	O	|	|	|	0.89
9.083	0.00	0.22	0.127	O	|	|	|	0.88
9.167	0.00	0.22	0.126	O	|	|	|	0.87
9.250	0.00	0.22	0.124	O	|	|	|	0.87
9.333	0.00	0.22	0.123	O	|	|	|	0.86
9.417	0.00	0.22	0.121	O	|	|	|	0.85
9.500	0.00	0.22	0.120	O	|	|	|	0.85
9.583	0.00	0.21	0.118	O	|	|	|	0.84
9.667	0.00	0.21	0.117	O	|	|	|	0.83
9.750	0.00	0.21	0.115	O	|	|	|	0.83
9.833	0.00	0.21	0.114	O	|	|	|	0.82
9.917	0.00	0.21	0.112	O	|	|	|	0.81
10.000	0.00	0.21	0.111	O	|	|	|	0.81
10.083	0.00	0.21	0.110	O	|	|	|	0.80
10.167	0.00	0.21	0.108	O	|	|	|	0.79
10.250	0.00	0.21	0.107	O	|	|	|	0.79
10.333	0.00	0.21	0.105	O	|	|	|	0.78
10.417	0.00	0.21	0.104	O	|	|	|	0.77
10.500	0.00	0.21	0.102	O	|	|	|	0.77
10.583	0.00	0.20	0.101	O	|	|	|	0.76
10.667	0.00	0.20	0.100	O	|	|	|	0.75
10.750	0.00	0.20	0.098	O	|	|	|	0.75
10.833	0.00	0.20	0.097	O	|	|	|	0.74
10.917	0.00	0.20	0.095	O	|	|	|	0.74
11.000	0.00	0.20	0.094	O	|	|	|	0.73
11.083	0.00	0.20	0.093	O	|	|	|	0.72
11.167	0.00	0.20	0.091	O	|	|	|	0.72

11.250	0.00	0.20	0.090	O	|	|	|	0.71
11.333	0.00	0.20	0.089	O	|	|	|	0.70
11.417	0.00	0.20	0.087	O	|	|	|	0.70
11.500	0.00	0.20	0.086	O	|	|	|	0.69
11.583	0.00	0.19	0.085	O	|	|	|	0.69
11.667	0.00	0.19	0.083	O	|	|	|	0.68
11.750	0.00	0.19	0.082	O	|	|	|	0.67
11.833	0.00	0.19	0.081	O	|	|	|	0.67
11.917	0.00	0.19	0.079	O	|	|	|	0.66
12.000	0.00	0.19	0.078	O	|	|	|	0.65
12.083	0.00	0.19	0.077	O	|	|	|	0.65
12.167	0.00	0.19	0.075	O	|	|	|	0.64
12.250	0.00	0.19	0.074	O	|	|	|	0.64
12.333	0.00	0.19	0.073	O	|	|	|	0.63
12.417	0.00	0.19	0.071	O	|	|	|	0.62
12.500	0.00	0.19	0.070	O	|	|	|	0.62
12.583	0.00	0.18	0.069	O	|	|	|	0.61
12.667	0.00	0.18	0.068	O	|	|	|	0.61
12.750	0.00	0.18	0.066	O	|	|	|	0.60
12.833	0.00	0.18	0.065	O	|	|	|	0.60
12.917	0.00	0.18	0.064	O	|	|	|	0.59
13.000	0.00	0.18	0.063	O	|	|	|	0.58
13.083	0.00	0.18	0.061	O	|	|	|	0.58
13.167	0.00	0.18	0.060	O	|	|	|	0.57
13.250	0.00	0.18	0.059	O	|	|	|	0.56
13.333	0.00	0.18	0.058	O	|	|	|	0.56
13.417	0.00	0.18	0.056	O	|	|	|	0.55
13.500	0.00	0.17	0.055	O	|	|	|	0.55
13.583	0.00	0.17	0.054	O	|	|	|	0.54
13.667	0.00	0.17	0.053	O	|	|	|	0.53
13.750	0.00	0.17	0.052	O	|	|	|	0.53
13.833	0.00	0.17	0.050	O	|	|	|	0.52
13.917	0.00	0.17	0.049	O	|	|	|	0.52
14.000	0.00	0.17	0.048	O	|	|	|	0.51
14.083	0.00	0.17	0.047	O	|	|	|	0.51
14.167	0.00	0.17	0.046	O	|	|	|	0.50
14.250	0.00	0.17	0.045	O	|	|	|	0.49
14.333	0.00	0.16	0.044	O	|	|	|	0.48
14.417	0.00	0.16	0.042	O	|	|	|	0.47
14.500	0.00	0.16	0.041	O	|	|	|	0.47
14.583	0.00	0.16	0.040	O	|	|	|	0.46
14.667	0.00	0.16	0.039	O	|	|	|	0.45
14.750	0.00	0.16	0.038	O	|	|	|	0.44
14.833	0.00	0.15	0.037	O	|	|	|	0.44
14.917	0.00	0.15	0.036	O	|	|	|	0.43
15.000	0.00	0.15	0.035	O	|	|	|	0.42
15.083	0.00	0.15	0.034	O	|	|	|	0.41
15.167	0.00	0.15	0.033	O	|	|	|	0.41
15.250	0.00	0.15	0.032	O	|	|	|	0.40
15.333	0.00	0.15	0.031	O	|	|	|	0.39
15.417	0.00	0.14	0.030	O	|	|	|	0.38
15.500	0.00	0.14	0.029	O	|	|	|	0.38
15.583	0.00	0.14	0.028	O	|	|	|	0.37
15.667	0.00	0.14	0.027	O	|	|	|	0.36
15.750	0.00	0.14	0.026	O	|	|	|	0.36
15.833	0.00	0.14	0.025	O	|	|	|	0.35
15.917	0.00	0.14	0.024	O	|	|	|	0.34
16.000	0.00	0.13	0.023	O	|	|	|	0.34
16.083	0.00	0.13	0.022	O	|	|	|	0.33
16.167	0.00	0.13	0.021	O	|	|	|	0.32
16.250	0.00	0.13	0.020	O	|	|	|	0.32
16.333	0.00	0.13	0.019	O	|	|	|	0.31
16.417	0.00	0.13	0.019	O	|	|	|	0.30
16.500	0.00	0.13	0.018	O	|	|	|	0.30
16.583	0.00	0.13	0.017	O	|	|	|	0.29
16.667	0.00	0.12	0.016	O	|	|	|	0.29
16.750	0.00	0.12	0.015	O	|	|	|	0.28
16.833	0.00	0.12	0.014	O	|	|	|	0.27
16.917	0.00	0.12	0.013	O	|	|	|	0.27
17.000	0.00	0.12	0.013	O	|	|	|	0.26
17.083	0.00	0.12	0.012	O	|	|	|	0.26
17.167	0.00	0.12	0.011	O	|	|	|	0.25

17.250	0.00	0.11	0.010	O	|	|	|	|	0.23
17.333	0.00	0.10	0.009	O	|	|	|	|	0.21
17.417	0.00	0.09	0.009	O	|	|	|	|	0.20
17.500	0.00	0.09	0.008	O	|	|	|	|	0.18
17.583	0.00	0.08	0.008	O	|	|	|	|	0.17
17.667	0.00	0.08	0.007	O	|	|	|	|	0.16
17.750	0.00	0.07	0.007	O	|	|	|	|	0.15
17.833	0.00	0.06	0.006	O	|	|	|	|	0.14
17.917	0.00	0.06	0.006	O	|	|	|	|	0.13
18.000	0.00	0.06	0.005	O	|	|	|	|	0.12
18.083	0.00	0.05	0.005	O	|	|	|	|	0.11
18.167	0.00	0.05	0.004	O	|	|	|	|	0.10
18.250	0.00	0.04	0.004	O	|	|	|	|	0.09
18.333	0.00	0.04	0.004	O	|	|	|	|	0.09
18.417	0.00	0.04	0.004	O	|	|	|	|	0.08
18.500	0.00	0.04	0.003	O	|	|	|	|	0.08
18.583	0.00	0.03	0.003	O	|	|	|	|	0.07
18.667	0.00	0.03	0.003	O	|	|	|	|	0.07
18.750	0.00	0.03	0.003	O	|	|	|	|	0.06
18.833	0.00	0.03	0.002	O	|	|	|	|	0.06
18.917	0.00	0.02	0.002	O	|	|	|	|	0.05
19.000	0.00	0.02	0.002	O	|	|	|	|	0.05
19.083	0.00	0.02	0.002	O	|	|	|	|	0.05
19.167	0.00	0.02	0.002	O	|	|	|	|	0.04
19.250	0.00	0.02	0.002	O	|	|	|	|	0.04
19.333	0.00	0.02	0.002	O	|	|	|	|	0.04
19.417	0.00	0.02	0.001	O	|	|	|	|	0.03
19.500	0.00	0.01	0.001	O	|	|	|	|	0.03
19.583	0.00	0.01	0.001	O	|	|	|	|	0.03
19.667	0.00	0.01	0.001	O	|	|	|	|	0.03
19.750	0.00	0.01	0.001	O	|	|	|	|	0.03
19.833	0.00	0.01	0.001	O	|	|	|	|	0.02
19.917	0.00	0.01	0.001	O	|	|	|	|	0.02
20.000	0.00	0.01	0.001	O	|	|	|	|	0.02
20.083	0.00	0.01	0.001	O	|	|	|	|	0.02
20.167	0.00	0.01	0.001	O	|	|	|	|	0.02
20.250	0.00	0.01	0.001	O	|	|	|	|	0.02
20.333	0.00	0.01	0.001	O	|	|	|	|	0.01
20.417	0.00	0.01	0.001	O	|	|	|	|	0.01
20.500	0.00	0.01	0.001	O	|	|	|	|	0.01
20.583	0.00	0.01	0.001	O	|	|	|	|	0.01
20.667	0.00	0.01	0.000	O	|	|	|	|	0.01
20.750	0.00	0.00	0.000	O	|	|	|	|	0.01
20.833	0.00	0.00	0.000	O	|	|	|	|	0.01
20.917	0.00	0.00	0.000	O	|	|	|	|	0.01
21.000	0.00	0.00	0.000	O	|	|	|	|	0.01
21.083	0.00	0.00	0.000	O	|	|	|	|	0.01
21.167	0.00	0.00	0.000	O	|	|	|	|	0.01
21.250	0.00	0.00	0.000	O	|	|	|	|	0.01
21.333	0.00	0.00	0.000	O	|	|	|	|	0.01
21.417	0.00	0.00	0.000	O	|	|	|	|	0.01
21.500	0.00	0.00	0.000	O	|	|	|	|	0.01
21.583	0.00	0.00	0.000	O	|	|	|	|	0.00
21.667	0.00	0.00	0.000	O	|	|	|	|	0.00
21.750	0.00	0.00	0.000	O	|	|	|	|	0.00
21.833	0.00	0.00	0.000	O	|	|	|	|	0.00
21.917	0.00	0.00	0.000	O	|	|	|	|	0.00
22.000	0.00	0.00	0.000	O	|	|	|	|	0.00
22.083	0.00	0.00	0.000	O	|	|	|	|	0.00
22.167	0.00	0.00	0.000	O	|	|	|	|	0.00
22.250	0.00	0.00	0.000	O	|	|	|	|	0.00
22.333	0.00	0.00	0.000	O	|	|	|	|	0.00
22.417	0.00	0.00	0.000	O	|	|	|	|	0.00
22.500	0.00	0.00	0.000	O	|	|	|	|	0.00
22.583	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 271
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.305 (CFS)
Total volume = 0.318 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
24-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD102410.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.662 (CFS)
Total volume = 1.583 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

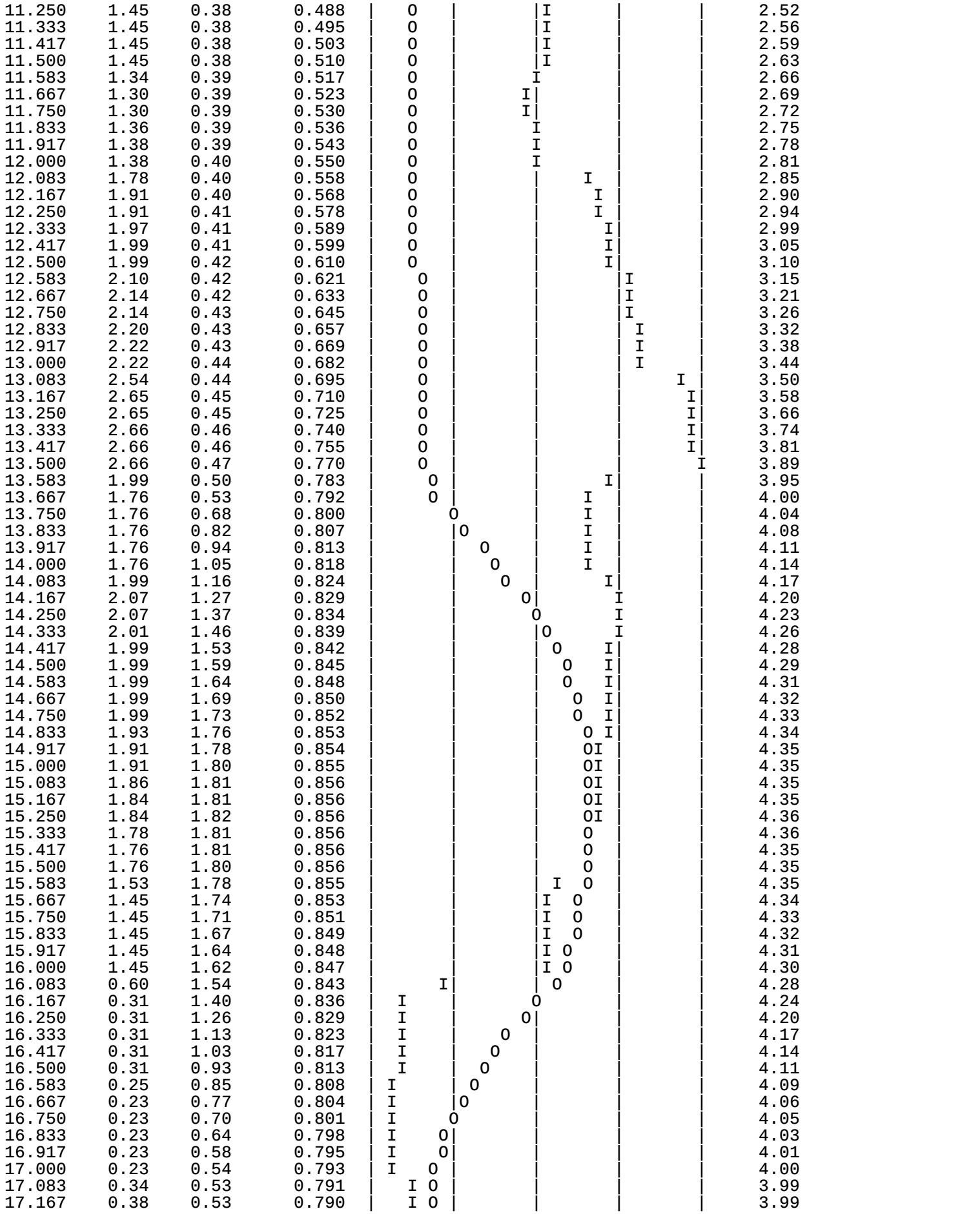
5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.7 1.33 2.00 2.66	Depth (Ft.)
0.083	0.11	0.00	0.000	OI	0.01
0.167	0.15	0.01	0.001	OI	0.03
0.250	0.15	0.02	0.002	OI	0.05
0.333	0.21	0.03	0.003	O I	0.07
0.417	0.23	0.05	0.004	O I	0.10
0.500	0.23	0.06	0.006	O I	0.13
0.583	0.23	0.07	0.007	O I	0.15
0.667	0.23	0.08	0.008	|OI	0.18
0.750	0.23	0.09	0.009	|OI	0.20
0.833	0.29	0.11	0.010	|O I	0.22
0.917	0.31	0.12	0.011	|O I	0.25
1.000	0.31	0.12	0.012	|O I	0.26
1.083	0.25	0.12	0.014	|OI	0.27
1.167	0.23	0.12	0.014	|OI	0.27
1.250	0.23	0.12	0.015	|OI	0.28
1.333	0.23	0.12	0.016	|OI	0.28
1.417	0.23	0.13	0.016	|OI	0.29
1.500	0.23	0.13	0.017	|OI	0.29
1.583	0.23	0.13	0.018	|OI	0.30
1.667	0.23	0.13	0.019	|OI	0.30
1.750	0.23	0.13	0.019	|OI	0.31
1.833	0.29	0.13	0.020	|O I	0.32
1.917	0.31	0.13	0.021	|O I	0.32
2.000	0.31	0.13	0.022	|O I	0.33
2.083	0.31	0.14	0.024	|O I	0.34
2.167	0.31	0.14	0.025	|O I	0.35
2.250	0.31	0.14	0.026	|O I	0.36
2.333	0.31	0.14	0.027	|O I	0.37
2.417	0.31	0.14	0.028	|O I	0.37
2.500	0.31	0.14	0.029	|O I	0.38
2.583	0.36	0.15	0.031	|O I	0.39
2.667	0.38	0.15	0.032	|O I	0.40
2.750	0.38	0.15	0.034	|O I	0.41
2.833	0.38	0.15	0.035	|O I	0.42
2.917	0.38	0.15	0.037	|O I	0.44
3.000	0.38	0.16	0.039	|O I	0.45
3.083	0.38	0.16	0.040	|O I	0.46
3.167	0.38	0.16	0.042	|O I	0.47
3.250	0.38	0.16	0.043	|O I	0.48
3.333	0.38	0.17	0.045	|O I	0.49
3.417	0.38	0.17	0.046	| O I	0.50
3.500	0.38	0.17	0.048	| O I	0.51
3.583	0.38	0.17	0.049	| O I	0.52
3.667	0.38	0.17	0.051	| O I	0.52
3.750	0.38	0.17	0.052	| O I	0.53
3.833	0.44	0.17	0.054	| O I	0.54
3.917	0.46	0.17	0.056	| O I	0.55
4.000	0.46	0.18	0.058	| O I	0.56
4.083	0.46	0.18	0.059	| O I	0.57
4.167	0.46	0.18	0.061	| O I	0.58
4.250	0.46	0.18	0.063	| O I	0.59
4.333	0.52	0.18	0.065	| O I	0.60
4.417	0.54	0.18	0.068	| O I	0.61
4.500	0.54	0.19	0.070	| O I	0.62
4.583	0.54	0.19	0.073	| O I	0.63
4.667	0.54	0.19	0.075	| O I	0.64
4.750	0.54	0.19	0.077	| O I	0.65
4.833	0.59	0.19	0.080	| O I	0.66
4.917	0.61	0.19	0.083	| O I	0.68
5.000	0.61	0.19	0.086	| O I	0.69
5.083	0.50	0.20	0.088	| O I	0.70
5.167	0.46	0.20	0.090	| O I	0.71

5.250	0.46	0.20	0.092	O I				0.72
5.333	0.52	0.20	0.094	O I				0.73
5.417	0.54	0.20	0.096	O I				0.74
5.500	0.54	0.20	0.098	O I				0.75
5.583	0.59	0.20	0.101	O I				0.76
5.667	0.61	0.21	0.104	O I				0.77
5.750	0.61	0.21	0.106	O I				0.79
5.833	0.61	0.21	0.109	O I				0.80
5.917	0.61	0.21	0.112	O I				0.81
6.000	0.61	0.21	0.115	O I				0.82
6.083	0.67	0.21	0.118	O I				0.84
6.167	0.69	0.22	0.121	O I				0.85
6.250	0.69	0.22	0.124	O I				0.87
6.333	0.69	0.22	0.127	O I				0.88
6.417	0.69	0.22	0.131	O I				0.90
6.500	0.69	0.22	0.134	O I				0.91
6.583	0.75	0.23	0.137	O I				0.93
6.667	0.76	0.23	0.141	O I				0.94
6.750	0.76	0.23	0.144	O I				0.96
6.833	0.76	0.23	0.148	O I				0.98
6.917	0.76	0.24	0.152	O I				0.99
7.000	0.76	0.24	0.155	O I				1.01
7.083	0.76	0.24	0.159	O I				1.03
7.167	0.76	0.24	0.163	O I				1.04
7.250	0.76	0.24	0.166	O I				1.06
7.333	0.82	0.24	0.170	O I				1.08
7.417	0.84	0.25	0.174	O I				1.10
7.500	0.84	0.25	0.178	O I				1.11
7.583	0.90	0.25	0.182	O I				1.13
7.667	0.92	0.25	0.187	O I				1.15
7.750	0.92	0.25	0.192	O I				1.18
7.833	0.97	0.26	0.196	O I				1.20
7.917	0.99	0.26	0.201	O I				1.22
8.000	0.99	0.26	0.206	O I				1.24
8.083	1.11	0.26	0.212	O I				1.27
8.167	1.15	0.27	0.218	O I				1.29
8.250	1.15	0.27	0.224	O I				1.32
8.333	1.15	0.27	0.230	O I				1.35
8.417	1.15	0.28	0.236	O I				1.38
8.500	1.15	0.28	0.242	O I				1.40
8.583	1.20	0.28	0.248	O I				1.43
8.667	1.22	0.28	0.254	O I				1.46
8.750	1.22	0.29	0.261	O I				1.49
8.833	1.28	0.29	0.267	O I				1.52
8.917	1.30	0.29	0.274	O I				1.55
9.000	1.30	0.30	0.281	O I				1.58
9.083	1.41	0.30	0.289	O	I			1.62
9.167	1.45	0.30	0.296	O	I			1.65
9.250	1.45	0.31	0.304	O	I			1.69
9.333	1.51	0.31	0.312	O	I			1.73
9.417	1.53	0.31	0.321	O	I			1.77
9.500	1.53	0.32	0.329	O	I			1.81
9.583	1.59	0.32	0.338	O	I			1.84
9.667	1.61	0.32	0.346	O	I			1.88
9.750	1.61	0.33	0.355	O	I			1.92
9.833	1.66	0.33	0.364	O	I			1.96
9.917	1.68	0.33	0.373	O	I			2.00
10.000	1.68	0.34	0.383	O	I			2.04
10.083	1.28	0.34	0.391	O	I			2.08
10.167	1.15	0.34	0.397	O	I			2.11
10.250	1.15	0.34	0.402	O	I			2.13
10.333	1.15	0.35	0.408	O	I			2.16
10.417	1.15	0.35	0.413	O	I			2.18
10.500	1.15	0.35	0.419	O	I			2.21
10.583	1.43	0.35	0.425	O	I			2.24
10.667	1.53	0.36	0.433	O	I			2.27
10.750	1.53	0.36	0.441	O	I			2.31
10.833	1.53	0.36	0.449	O	I			2.35
10.917	1.53	0.36	0.457	O	I			2.38
11.000	1.53	0.37	0.465	O	I			2.42
11.083	1.47	0.37	0.473	O	I			2.45
11.167	1.45	0.37	0.480	O	I			2.49



11.250	1.45	0.38	0.488	O	I				2.52
11.333	1.45	0.38	0.495	O	I				2.56
11.417	1.45	0.38	0.503	O	I				2.59
11.500	1.45	0.38	0.510	O	I				2.63
11.583	1.34	0.39	0.517	O	I				2.66
11.667	1.30	0.39	0.523	O	I				2.69
11.750	1.30	0.39	0.530	O	I				2.72
11.833	1.36	0.39	0.536	O	I				2.75
11.917	1.38	0.39	0.543	O	I				2.78
12.000	1.38	0.40	0.550	O	I				2.81
12.083	1.78	0.40	0.558	O	I				2.85
12.167	1.91	0.40	0.568	O	I				2.90
12.250	1.91	0.41	0.578	O	I				2.94
12.333	1.97	0.41	0.589	O	I				2.99
12.417	1.99	0.41	0.599	O	I				3.05
12.500	1.99	0.42	0.610	O	I				3.10
12.583	2.10	0.42	0.621	O	I				3.15
12.667	2.14	0.42	0.633	O	I				3.21
12.750	2.14	0.43	0.645	O	I				3.26
12.833	2.20	0.43	0.657	O	I				3.32
12.917	2.22	0.43	0.669	O	I				3.38
13.000	2.22	0.44	0.682	O	I				3.44
13.083	2.54	0.44	0.695	O	I				3.50
13.167	2.65	0.45	0.710	O	I				3.58
13.250	2.65	0.45	0.725	O	I				3.66
13.333	2.66	0.46	0.740	O	I				3.74
13.417	2.66	0.46	0.755	O	I				3.81
13.500	2.66	0.47	0.770	O	I				3.89
13.583	1.99	0.50	0.783	O	I				3.95
13.667	1.76	0.53	0.792	O	I				4.00
13.750	1.76	0.68	0.800	O	I				4.04
13.833	1.76	0.82	0.807	O	I				4.08
13.917	1.76	0.94	0.813	O	I				4.11
14.000	1.76	1.05	0.818	O	I				4.14
14.083	1.99	1.16	0.824	O	I				4.17
14.167	2.07	1.27	0.829	O	I				4.20
14.250	2.07	1.37	0.834	O	I				4.23
14.333	2.01	1.46	0.839	O	I				4.26
14.417	1.99	1.53	0.842	O	I				4.28
14.500	1.99	1.59	0.845	O	I				4.29
14.583	1.99	1.64	0.848	O	I				4.31
14.667	1.99	1.69	0.850	O	I				4.32
14.750	1.99	1.73	0.852	O	I				4.33
14.833	1.93	1.76	0.853	O	I				4.34
14.917	1.91	1.78	0.854	O	I				4.35
15.000	1.91	1.80	0.855	O	I				4.35
15.083	1.86	1.81	0.856	O	I				4.35
15.167	1.84	1.81	0.856	O	I				4.35
15.250	1.84	1.82	0.856	O	I				4.36
15.333	1.78	1.81	0.856	O					4.36
15.417	1.76	1.81	0.856	O					4.35
15.500	1.76	1.80	0.856	O					4.35
15.583	1.53	1.78	0.855	O	I				4.35
15.667	1.45	1.74	0.853	O	I				4.34
15.750	1.45	1.71	0.851	O	I				4.33
15.833	1.45	1.67	0.849	O	I				4.32
15.917	1.45	1.64	0.848	O	I				4.31
16.000	1.45	1.62	0.847	O	I				4.30
16.083	0.60	1.54	0.843	O	I				4.28
16.167	0.31	1.40	0.836	O	I				4.24
16.250	0.31	1.26	0.829	O	I				4.20
16.333	0.31	1.13	0.823	O	I				4.17
16.417	0.31	1.03	0.817	O	I				4.14
16.500	0.31	0.93	0.813	O	I				4.11
16.583	0.25	0.85	0.808	O	I				4.09
16.667	0.23	0.77	0.804	O	I				4.06
16.750	0.23	0.70	0.801	O	I				4.05
16.833	0.23	0.64	0.798	O	I				4.03
16.917	0.23	0.58	0.795	O	I				4.01
17.000	0.23	0.54	0.793	O	I				4.00
17.083	0.34	0.53	0.791	O	I				3.99
17.167	0.38	0.53	0.790	O	I				3.99

17.250	0.38	0.52	0.789	I O				3.98
17.333	0.38	0.52	0.788	I O				3.98
17.417	0.38	0.52	0.787	I O				3.97
17.500	0.38	0.51	0.786	I O				3.97
17.583	0.38	0.51	0.786	I O				3.96
17.667	0.38	0.51	0.785	I O				3.96
17.750	0.38	0.51	0.784	I O				3.96
17.833	0.33	0.50	0.783	I O				3.95
17.917	0.31	0.50	0.782	I O				3.95
18.000	0.31	0.49	0.780	I O				3.94
18.083	0.31	0.49	0.779	I O				3.93
18.167	0.31	0.49	0.778	I O				3.93
18.250	0.31	0.48	0.777	I O				3.92
18.333	0.31	0.48	0.775	I O				3.92
18.417	0.31	0.47	0.774	I O				3.91
18.500	0.31	0.47	0.773	I O				3.90
18.583	0.25	0.47	0.772	I O				3.90
18.667	0.23	0.47	0.770	I O				3.89
18.750	0.23	0.47	0.768	I O				3.88
18.833	0.17	0.47	0.767	I O				3.87
18.917	0.15	0.46	0.765	I O				3.86
19.000	0.15	0.46	0.762	I O				3.85
19.083	0.21	0.46	0.760	I O				3.84
19.167	0.23	0.46	0.759	I O				3.83
19.250	0.23	0.46	0.757	I O				3.82
19.333	0.29	0.46	0.756	I O				3.82
19.417	0.31	0.46	0.755	I O				3.81
19.500	0.31	0.46	0.754	I O				3.81
19.583	0.25	0.46	0.752	I O				3.80
19.667	0.23	0.46	0.751	I O				3.79
19.750	0.23	0.46	0.749	I O				3.78
19.833	0.17	0.46	0.747	I O				3.77
19.917	0.15	0.46	0.745	I O				3.76
20.000	0.15	0.46	0.743	I O				3.75
20.083	0.21	0.46	0.741	I O				3.74
20.167	0.23	0.46	0.740	I O				3.73
20.250	0.23	0.46	0.738	I O				3.73
20.333	0.23	0.46	0.737	I O				3.72
20.417	0.23	0.46	0.735	I O				3.71
20.500	0.23	0.45	0.734	I O				3.70
20.583	0.23	0.45	0.732	I O				3.69
20.667	0.23	0.45	0.730	I O				3.69
20.750	0.23	0.45	0.729	I O				3.68
20.833	0.17	0.45	0.727	I O				3.67
20.917	0.15	0.45	0.725	I O				3.66
21.000	0.15	0.45	0.723	I O				3.65
21.083	0.21	0.45	0.721	I O				3.64
21.167	0.23	0.45	0.720	I O				3.63
21.250	0.23	0.45	0.718	I O				3.62
21.333	0.17	0.45	0.716	I O				3.62
21.417	0.15	0.45	0.714	I O				3.60
21.500	0.15	0.45	0.712	I O				3.59
21.583	0.21	0.45	0.711	I O				3.59
21.667	0.23	0.45	0.709	I O				3.58
21.750	0.23	0.45	0.708	I O				3.57
21.833	0.17	0.45	0.706	I O				3.56
21.917	0.15	0.45	0.704	I O				3.55
22.000	0.15	0.44	0.702	I O				3.54
22.083	0.21	0.44	0.700	I O				3.53
22.167	0.23	0.44	0.699	I O				3.52
22.250	0.23	0.44	0.697	I O				3.52
22.333	0.17	0.44	0.695	I O				3.51
22.417	0.15	0.44	0.693	I O				3.50
22.500	0.15	0.44	0.691	I O				3.49
22.583	0.15	0.44	0.690	I O				3.48
22.667	0.15	0.44	0.688	I O				3.47
22.750	0.15	0.44	0.686	I O				3.46
22.833	0.15	0.44	0.684	I O				3.45
22.917	0.15	0.44	0.682	I O				3.44
23.000	0.15	0.44	0.680	I O				3.43
23.083	0.15	0.44	0.678	I O				3.42
23.167	0.15	0.44	0.676	I O				3.41

23.250	0.15	0.44	0.674	|I	O	|	|	|	3.40
23.333	0.15	0.43	0.672	|I	O	|	|	|	3.39
23.417	0.15	0.43	0.670	|I	O	|	|	|	3.38
23.500	0.15	0.43	0.668	|I	O	|	|	|	3.37
23.583	0.15	0.43	0.666	|I	O	|	|	|	3.37
23.667	0.15	0.43	0.664	|I	O	|	|	|	3.36
23.750	0.15	0.43	0.662	|I	O	|	|	|	3.35
23.833	0.15	0.43	0.660	|I	O	|	|	|	3.34
23.917	0.15	0.43	0.658	|I	O	|	|	|	3.33
24.000	0.15	0.43	0.656	|I	O	|	|	|	3.32
24.083	0.04	0.43	0.654	I	O	|	|	|	3.31
24.167	0.00	0.43	0.651	I	O	|	|	|	3.29
24.250	0.00	0.43	0.648	I	O	|	|	|	3.28
24.333	0.00	0.43	0.645	I	O	|	|	|	3.27
24.417	0.00	0.43	0.643	I	O	|	|	|	3.25
24.500	0.00	0.42	0.640	I	O	|	|	|	3.24
24.583	0.00	0.42	0.637	I	O	|	|	|	3.22
24.667	0.00	0.42	0.634	I	O	|	|	|	3.21
24.750	0.00	0.42	0.631	I	O	|	|	|	3.20
24.833	0.00	0.42	0.628	I	O	|	|	|	3.18
24.917	0.00	0.42	0.625	I	O	|	|	|	3.17
25.000	0.00	0.42	0.622	I	O	|	|	|	3.15
25.083	0.00	0.42	0.619	I	O	|	|	|	3.14
25.167	0.00	0.42	0.616	I	O	|	|	|	3.13
25.250	0.00	0.42	0.614	I	O	|	|	|	3.11
25.333	0.00	0.42	0.611	I	O	|	|	|	3.10
25.417	0.00	0.41	0.608	I	O	|	|	|	3.09
25.500	0.00	0.41	0.605	I	O	|	|	|	3.07
25.583	0.00	0.41	0.602	I	O	|	|	|	3.06
25.667	0.00	0.41	0.599	I	O	|	|	|	3.04
25.750	0.00	0.41	0.596	I	O	|	|	|	3.03
25.833	0.00	0.41	0.594	I	O	|	|	|	3.02
25.917	0.00	0.41	0.591	I	O	|	|	|	3.00
26.000	0.00	0.41	0.588	I	O	|	|	|	2.99
26.083	0.00	0.41	0.585	I	O	|	|	|	2.98
26.167	0.00	0.41	0.582	I	O	|	|	|	2.96
26.250	0.00	0.41	0.580	I	O	|	|	|	2.95
26.333	0.00	0.40	0.577	I	O	|	|	|	2.94
26.417	0.00	0.40	0.574	I	O	|	|	|	2.93
26.500	0.00	0.40	0.571	I	O	|	|	|	2.91
26.583	0.00	0.40	0.568	I	O	|	|	|	2.90
26.667	0.00	0.40	0.566	I	O	|	|	|	2.89
26.750	0.00	0.40	0.563	I	O	|	|	|	2.87
26.833	0.00	0.40	0.560	I	O	|	|	|	2.86
26.917	0.00	0.40	0.557	I	O	|	|	|	2.85
27.000	0.00	0.40	0.555	I	O	|	|	|	2.83
27.083	0.00	0.40	0.552	I	O	|	|	|	2.82
27.167	0.00	0.40	0.549	I	O	|	|	|	2.81
27.250	0.00	0.39	0.546	I	O	|	|	|	2.80
27.333	0.00	0.39	0.544	I	O	|	|	|	2.78
27.417	0.00	0.39	0.541	I	O	|	|	|	2.77
27.500	0.00	0.39	0.538	I	O	|	|	|	2.76
27.583	0.00	0.39	0.536	I	O	|	|	|	2.75
27.667	0.00	0.39	0.533	I	O	|	|	|	2.73
27.750	0.00	0.39	0.530	I	O	|	|	|	2.72
27.833	0.00	0.39	0.528	I	O	|	|	|	2.71
27.917	0.00	0.39	0.525	I	O	|	|	|	2.70
28.000	0.00	0.39	0.522	I	O	|	|	|	2.68
28.083	0.00	0.39	0.520	I	O	|	|	|	2.67
28.167	0.00	0.39	0.517	I	O	|	|	|	2.66
28.250	0.00	0.38	0.514	I	O	|	|	|	2.65
28.333	0.00	0.38	0.512	I	O	|	|	|	2.63
28.417	0.00	0.38	0.509	I	O	|	|	|	2.62
28.500	0.00	0.38	0.506	I	O	|	|	|	2.61
28.583	0.00	0.38	0.504	I	O	|	|	|	2.60
28.667	0.00	0.38	0.501	I	O	|	|	|	2.58
28.750	0.00	0.38	0.499	I	O	|	|	|	2.57
28.833	0.00	0.38	0.496	I	O	|	|	|	2.56
28.917	0.00	0.38	0.493	I	O	|	|	|	2.55
29.000	0.00	0.38	0.491	I	O	|	|	|	2.54
29.083	0.00	0.38	0.488	I	O	|	|	|	2.52
29.167	0.00	0.37	0.486	I	O	|	|	|	2.51

29.250	0.00	0.37	0.483	I	O	|	|	|	2.50
29.333	0.00	0.37	0.480	I	O	|	|	|	2.49
29.417	0.00	0.37	0.478	I	O	|	|	|	2.48
29.500	0.00	0.37	0.475	I	O	|	|	|	2.46
29.583	0.00	0.37	0.473	I	O	|	|	|	2.45
29.667	0.00	0.37	0.470	I	O	|	|	|	2.44
29.750	0.00	0.37	0.468	I	O	|	|	|	2.43
29.833	0.00	0.37	0.465	I	O	|	|	|	2.42
29.917	0.00	0.37	0.463	I	O	|	|	|	2.41
30.000	0.00	0.37	0.460	I	O	|	|	|	2.40
30.083	0.00	0.36	0.458	I	O	|	|	|	2.38
30.167	0.00	0.36	0.455	I	O	|	|	|	2.37
30.250	0.00	0.36	0.453	I	O	|	|	|	2.36
30.333	0.00	0.36	0.450	I	O	|	|	|	2.35
30.417	0.00	0.36	0.448	I	O	|	|	|	2.34
30.500	0.00	0.36	0.445	I	O	|	|	|	2.33
30.583	0.00	0.36	0.443	I	O	|	|	|	2.32
30.667	0.00	0.36	0.440	I	O	|	|	|	2.30
30.750	0.00	0.36	0.438	I	O	|	|	|	2.29
30.833	0.00	0.36	0.435	I	O	|	|	|	2.28
30.917	0.00	0.36	0.433	I	O	|	|	|	2.27
31.000	0.00	0.35	0.430	I	O	|	|	|	2.26
31.083	0.00	0.35	0.428	I	O	|	|	|	2.25
31.167	0.00	0.35	0.425	I	O	|	|	|	2.24
31.250	0.00	0.35	0.423	I	O	|	|	|	2.23
31.333	0.00	0.35	0.421	I	O	|	|	|	2.22
31.417	0.00	0.35	0.418	I	O	|	|	|	2.21
31.500	0.00	0.35	0.416	I	O	|	|	|	2.19
31.583	0.00	0.35	0.413	I	O	|	|	|	2.18
31.667	0.00	0.35	0.411	I	O	|	|	|	2.17
31.750	0.00	0.35	0.409	I	O	|	|	|	2.16
31.833	0.00	0.35	0.406	I	O	|	|	|	2.15
31.917	0.00	0.35	0.404	I	O	|	|	|	2.14
32.000	0.00	0.34	0.401	I	O	|	|	|	2.13
32.083	0.00	0.34	0.399	I	O	|	|	|	2.12
32.167	0.00	0.34	0.397	I	O	|	|	|	2.11
32.250	0.00	0.34	0.394	I	O	|	|	|	2.10
32.333	0.00	0.34	0.392	I	O	|	|	|	2.09
32.417	0.00	0.34	0.390	I	O	|	|	|	2.08
32.500	0.00	0.34	0.387	I	O	|	|	|	2.06
32.583	0.00	0.34	0.385	I	O	|	|	|	2.05
32.667	0.00	0.34	0.383	I	O	|	|	|	2.04
32.750	0.00	0.34	0.380	I	O	|	|	|	2.03
32.833	0.00	0.34	0.378	I	O	|	|	|	2.02
32.917	0.00	0.33	0.376	I	O	|	|	|	2.01
33.000	0.00	0.33	0.373	I	O	|	|	|	2.00
33.083	0.00	0.33	0.371	I	O	|	|	|	1.99
33.167	0.00	0.33	0.369	I	O	|	|	|	1.98
33.250	0.00	0.33	0.366	I	O	|	|	|	1.97
33.333	0.00	0.33	0.364	I	O	|	|	|	1.96
33.417	0.00	0.33	0.362	I	O	|	|	|	1.95
33.500	0.00	0.33	0.360	I	O	|	|	|	1.94
33.583	0.00	0.33	0.357	I	O	|	|	|	1.93
33.667	0.00	0.33	0.355	I	O	|	|	|	1.92
33.750	0.00	0.33	0.353	I	O	|	|	|	1.91
33.833	0.00	0.33	0.351	I	O	|	|	|	1.90
33.917	0.00	0.32	0.348	I	O	|	|	|	1.89
34.000	0.00	0.32	0.346	I	O	|	|	|	1.88
34.083	0.00	0.32	0.344	I	O	|	|	|	1.87
34.167	0.00	0.32	0.342	I	O	|	|	|	1.86
34.250	0.00	0.32	0.339	I	O	|	|	|	1.85
34.333	0.00	0.32	0.337	I	O	|	|	|	1.84
34.417	0.00	0.32	0.335	I	O	|	|	|	1.83
34.500	0.00	0.32	0.333	I	O	|	|	|	1.82
34.583	0.00	0.32	0.331	I	O	|	|	|	1.81
34.667	0.00	0.32	0.328	I	O	|	|	|	1.80
34.750	0.00	0.32	0.326	I	O	|	|	|	1.79
34.833	0.00	0.32	0.324	I	O	|	|	|	1.78
34.917	0.00	0.31	0.322	I	O	|	|	|	1.77
35.000	0.00	0.31	0.320	I	O	|	|	|	1.76
35.083	0.00	0.31	0.318	I	O	|	|	|	1.75
35.167	0.00	0.31	0.315	I	O	|	|	|	1.74

35.250	0.00	0.31	0.313	I	O	|	|	|	1.73
35.333	0.00	0.31	0.311	I	O	|	|	|	1.72
35.417	0.00	0.31	0.309	I	O	|	|	|	1.71
35.500	0.00	0.31	0.307	I	O	|	|	|	1.70
35.583	0.00	0.31	0.305	I	O	|	|	|	1.69
35.667	0.00	0.31	0.303	I	O	|	|	|	1.68
35.750	0.00	0.31	0.301	I	O	|	|	|	1.67
35.833	0.00	0.30	0.299	I	O	|	|	|	1.66
35.917	0.00	0.30	0.296	I	O	|	|	|	1.65
36.000	0.00	0.30	0.294	I	O	|	|	|	1.64
36.083	0.00	0.30	0.292	I	O	|	|	|	1.64
36.167	0.00	0.30	0.290	I	O	|	|	|	1.63
36.250	0.00	0.30	0.288	I	O	|	|	|	1.62
36.333	0.00	0.30	0.286	I	O	|	|	|	1.61
36.417	0.00	0.30	0.284	I	O	|	|	|	1.60
36.500	0.00	0.30	0.282	I	O	|	|	|	1.59
36.583	0.00	0.30	0.280	I	O	|	|	|	1.58
36.667	0.00	0.30	0.278	I	O	|	|	|	1.57
36.750	0.00	0.29	0.276	I	O	|	|	|	1.56
36.833	0.00	0.29	0.274	I	O	|	|	|	1.55
36.917	0.00	0.29	0.272	I	O	|	|	|	1.54
37.000	0.00	0.29	0.270	I	O	|	|	|	1.53
37.083	0.00	0.29	0.268	I	O	|	|	|	1.52
37.167	0.00	0.29	0.266	I	O	|	|	|	1.51
37.250	0.00	0.29	0.264	I	O	|	|	|	1.50
37.333	0.00	0.29	0.262	I	O	|	|	|	1.49
37.417	0.00	0.29	0.260	I	O	|	|	|	1.49
37.500	0.00	0.29	0.258	I	O	|	|	|	1.48
37.583	0.00	0.29	0.256	I	O	|	|	|	1.47
37.667	0.00	0.28	0.254	I	O	|	|	|	1.46
37.750	0.00	0.28	0.252	I	O	|	|	|	1.45
37.833	0.00	0.28	0.250	I	O	|	|	|	1.44
37.917	0.00	0.28	0.248	I	O	|	|	|	1.43
38.000	0.00	0.28	0.246	I	O	|	|	|	1.42
38.083	0.00	0.28	0.244	I	O	|	|	|	1.41
38.167	0.00	0.28	0.242	I	O	|	|	|	1.41
38.250	0.00	0.28	0.240	I	O	|	|	|	1.40
38.333	0.00	0.28	0.238	I	O	|	|	|	1.39
38.417	0.00	0.28	0.237	I	O	|	|	|	1.38
38.500	0.00	0.28	0.235	I	O	|	|	|	1.37
38.583	0.00	0.27	0.233	I	O	|	|	|	1.36
38.667	0.00	0.27	0.231	I	O	|	|	|	1.35
38.750	0.00	0.27	0.229	I	O	|	|	|	1.35
38.833	0.00	0.27	0.227	I	O	|	|	|	1.34
38.917	0.00	0.27	0.225	I	O	|	|	|	1.33
39.000	0.00	0.27	0.223	I	O	|	|	|	1.32
39.083	0.00	0.27	0.221	I	O	|	|	|	1.31
39.167	0.00	0.27	0.220	I	O	|	|	|	1.30
39.250	0.00	0.27	0.218	I	O	|	|	|	1.29
39.333	0.00	0.27	0.216	I	O	|	|	|	1.29
39.417	0.00	0.27	0.214	I	O	|	|	|	1.28
39.500	0.00	0.26	0.212	I	O	|	|	|	1.27
39.583	0.00	0.26	0.210	I	O	|	|	|	1.26
39.667	0.00	0.26	0.209	I	O	|	|	|	1.25
39.750	0.00	0.26	0.207	I	O	|	|	|	1.24
39.833	0.00	0.26	0.205	I	O	|	|	|	1.24
39.917	0.00	0.26	0.203	I	O	|	|	|	1.23
40.000	0.00	0.26	0.201	I	O	|	|	|	1.22
40.083	0.00	0.26	0.200	I	O	|	|	|	1.21
40.167	0.00	0.26	0.198	I	O	|	|	|	1.20
40.250	0.00	0.26	0.196	I	O	|	|	|	1.20
40.333	0.00	0.26	0.194	I	O	|	|	|	1.19
40.417	0.00	0.26	0.193	I	O	|	|	|	1.18
40.500	0.00	0.25	0.191	I	O	|	|	|	1.17
40.583	0.00	0.25	0.189	I	O	|	|	|	1.16
40.667	0.00	0.25	0.187	I	O	|	|	|	1.16
40.750	0.00	0.25	0.186	I	O	|	|	|	1.15
40.833	0.00	0.25	0.184	I	O	|	|	|	1.14
40.917	0.00	0.25	0.182	I	O	|	|	|	1.13
41.000	0.00	0.25	0.180	I	O	|	|	|	1.12
41.083	0.00	0.25	0.179	I	O	|	|	|	1.12
41.167	0.00	0.25	0.177	I	O	|	|	|	1.11

41.250	0.00	0.25	0.175	I O	|	|	|	1.10
41.333	0.00	0.25	0.174	I O	|	|	|	1.09
41.417	0.00	0.25	0.172	I O	|	|	|	1.09
41.500	0.00	0.24	0.170	I O	|	|	|	1.08
41.583	0.00	0.24	0.169	I O	|	|	|	1.07
41.667	0.00	0.24	0.167	I O	|	|	|	1.06
41.750	0.00	0.24	0.165	I O	|	|	|	1.06
41.833	0.00	0.24	0.164	I O	|	|	|	1.05
41.917	0.00	0.24	0.162	I O	|	|	|	1.04
42.000	0.00	0.24	0.160	I O	|	|	|	1.03
42.083	0.00	0.24	0.159	I O	|	|	|	1.03
42.167	0.00	0.24	0.157	I O	|	|	|	1.02
42.250	0.00	0.24	0.155	I O	|	|	|	1.01
42.333	0.00	0.24	0.154	I O	|	|	|	1.00
42.417	0.00	0.24	0.152	I O	|	|	|	1.00
42.500	0.00	0.23	0.150	I O	|	|	|	0.99
42.583	0.00	0.23	0.149	I O	|	|	|	0.98
42.667	0.00	0.23	0.147	I O	|	|	|	0.97
42.750	0.00	0.23	0.146	I O	|	|	|	0.97
42.833	0.00	0.23	0.144	I O	|	|	|	0.96
42.917	0.00	0.23	0.142	I O	|	|	|	0.95
43.000	0.00	0.23	0.141	I O	|	|	|	0.94
43.083	0.00	0.23	0.139	I O	|	|	|	0.94
43.167	0.00	0.23	0.138	I O	|	|	|	0.93
43.250	0.00	0.23	0.136	I O	|	|	|	0.92
43.333	0.00	0.22	0.135	I O	|	|	|	0.92
43.417	0.00	0.22	0.133	I O	|	|	|	0.91
43.500	0.00	0.22	0.132	I O	|	|	|	0.90
43.583	0.00	0.22	0.130	I O	|	|	|	0.89
43.667	0.00	0.22	0.129	I O	|	|	|	0.89
43.750	0.00	0.22	0.127	I O	|	|	|	0.88
43.833	0.00	0.22	0.125	I O	|	|	|	0.87
43.917	0.00	0.22	0.124	I O	|	|	|	0.87
44.000	0.00	0.22	0.122	I O	|	|	|	0.86
44.083	0.00	0.22	0.121	I O	|	|	|	0.85
44.167	0.00	0.22	0.119	I O	|	|	|	0.85
44.250	0.00	0.21	0.118	I O	|	|	|	0.84
44.333	0.00	0.21	0.117	I O	|	|	|	0.83
44.417	0.00	0.21	0.115	I O	|	|	|	0.83
44.500	0.00	0.21	0.114	I O	|	|	|	0.82
44.583	0.00	0.21	0.112	I O	|	|	|	0.81
44.667	0.00	0.21	0.111	I O	|	|	|	0.81
44.750	0.00	0.21	0.109	I O	|	|	|	0.80
44.833	0.00	0.21	0.108	I O	|	|	|	0.79
44.917	0.00	0.21	0.106	I O	|	|	|	0.79
45.000	0.00	0.21	0.105	I O	|	|	|	0.78
45.083	0.00	0.21	0.104	I O	|	|	|	0.77
45.167	0.00	0.21	0.102	I O	|	|	|	0.77
45.250	0.00	0.20	0.101	I O	|	|	|	0.76
45.333	0.00	0.20	0.099	I O	|	|	|	0.75
45.417	0.00	0.20	0.098	I O	|	|	|	0.75
45.500	0.00	0.20	0.097	I O	|	|	|	0.74
45.583	0.00	0.20	0.095	I O	|	|	|	0.73
45.667	0.00	0.20	0.094	I O	|	|	|	0.73
45.750	0.00	0.20	0.092	I O	|	|	|	0.72
45.833	0.00	0.20	0.091	I O	|	|	|	0.71
45.917	0.00	0.20	0.090	I O	|	|	|	0.71
46.000	0.00	0.20	0.088	I O	|	|	|	0.70
46.083	0.00	0.20	0.087	I O	|	|	|	0.70
46.167	0.00	0.19	0.086	I O	|	|	|	0.69
46.250	0.00	0.19	0.084	I O	|	|	|	0.68
46.333	0.00	0.19	0.083	I O	|	|	|	0.68
46.417	0.00	0.19	0.082	I O	|	|	|	0.67
46.500	0.00	0.19	0.080	I O	|	|	|	0.67
46.583	0.00	0.19	0.079	I O	|	|	|	0.66
46.667	0.00	0.19	0.078	I O	|	|	|	0.65
46.750	0.00	0.19	0.076	I O	|	|	|	0.65
46.833	0.00	0.19	0.075	I O	|	|	|	0.64
46.917	0.00	0.19	0.074	I O	|	|	|	0.64
47.000	0.00	0.19	0.072	I O	|	|	|	0.63
47.083	0.00	0.19	0.071	I O	|	|	|	0.62
47.167	0.00	0.19	0.070	I O	|	|	|	0.62

47.250	0.00	0.18	0.069	I O	|	|	|	0.61
47.333	0.00	0.18	0.067	I O	|	|	|	0.61
47.417	0.00	0.18	0.066	I O	|	|	|	0.60
47.500	0.00	0.18	0.065	I O	|	|	|	0.59
47.583	0.00	0.18	0.064	I O	|	|	|	0.59
47.667	0.00	0.18	0.062	I O	|	|	|	0.58
47.750	0.00	0.18	0.061	I O	|	|	|	0.58
47.833	0.00	0.18	0.060	I O	|	|	|	0.57
47.917	0.00	0.18	0.059	I O	|	|	|	0.56
48.000	0.00	0.18	0.057	I O	|	|	|	0.56
48.083	0.00	0.18	0.056	I O	|	|	|	0.55
48.167	0.00	0.17	0.055	I O	|	|	|	0.55
48.250	0.00	0.17	0.054	I O	|	|	|	0.54
48.333	0.00	0.17	0.053	I O	|	|	|	0.53
48.417	0.00	0.17	0.051	I O	|	|	|	0.53
48.500	0.00	0.17	0.050	I O	|	|	|	0.52
48.583	0.00	0.17	0.049	I O	|	|	|	0.52
48.667	0.00	0.17	0.048	I O	|	|	|	0.51
48.750	0.00	0.17	0.047	I O	|	|	|	0.50
48.833	0.00	0.17	0.046	I O	|	|	|	0.50
48.917	0.00	0.16	0.044	IO	|	|	|	0.49
49.000	0.00	0.16	0.043	IO	|	|	|	0.48
49.083	0.00	0.16	0.042	IO	|	|	|	0.47
49.167	0.00	0.16	0.041	IO	|	|	|	0.47
49.250	0.00	0.16	0.040	IO	|	|	|	0.46
49.333	0.00	0.16	0.039	IO	|	|	|	0.45
49.417	0.00	0.16	0.038	IO	|	|	|	0.44
49.500	0.00	0.15	0.037	IO	|	|	|	0.43
49.583	0.00	0.15	0.036	IO	|	|	|	0.43
49.667	0.00	0.15	0.035	IO	|	|	|	0.42
49.750	0.00	0.15	0.034	IO	|	|	|	0.41
49.833	0.00	0.15	0.033	IO	|	|	|	0.40
49.917	0.00	0.15	0.032	IO	|	|	|	0.40
50.000	0.00	0.15	0.031	IO	|	|	|	0.39
50.083	0.00	0.14	0.030	IO	|	|	|	0.38
50.167	0.00	0.14	0.029	IO	|	|	|	0.38
50.250	0.00	0.14	0.028	IO	|	|	|	0.37
50.333	0.00	0.14	0.027	IO	|	|	|	0.36
50.417	0.00	0.14	0.026	IO	|	|	|	0.36
50.500	0.00	0.14	0.025	IO	|	|	|	0.35
50.583	0.00	0.14	0.024	IO	|	|	|	0.34
50.667	0.00	0.13	0.023	IO	|	|	|	0.33
50.750	0.00	0.13	0.022	IO	|	|	|	0.33
50.833	0.00	0.13	0.021	IO	|	|	|	0.32
50.917	0.00	0.13	0.020	IO	|	|	|	0.32
51.000	0.00	0.13	0.019	IO	|	|	|	0.31
51.083	0.00	0.13	0.018	IO	|	|	|	0.30
51.167	0.00	0.13	0.017	IO	|	|	|	0.30
51.250	0.00	0.13	0.017	IO	|	|	|	0.29
51.333	0.00	0.12	0.016	IO	|	|	|	0.28
51.417	0.00	0.12	0.015	IO	|	|	|	0.28
51.500	0.00	0.12	0.014	IO	|	|	|	0.27
51.583	0.00	0.12	0.013	IO	|	|	|	0.27
51.667	0.00	0.12	0.012	IO	|	|	|	0.26
51.750	0.00	0.12	0.012	IO	|	|	|	0.25
51.833	0.00	0.12	0.011	IO	|	|	|	0.24
51.917	0.00	0.11	0.010	IO	|	|	|	0.23
52.000	0.00	0.10	0.009	IO	|	|	|	0.21
52.083	0.00	0.09	0.009	IO	|	|	|	0.20
52.167	0.00	0.09	0.008	IO	|	|	|	0.18
52.250	0.00	0.08	0.007	O	|	|	|	0.17
52.333	0.00	0.07	0.007	O	|	|	|	0.16
52.417	0.00	0.07	0.006	O	|	|	|	0.15
52.500	0.00	0.06	0.006	O	|	|	|	0.14
52.583	0.00	0.06	0.006	O	|	|	|	0.13
52.667	0.00	0.06	0.005	O	|	|	|	0.12
52.750	0.00	0.05	0.005	O	|	|	|	0.11
52.833	0.00	0.05	0.004	O	|	|	|	0.10
52.917	0.00	0.04	0.004	O	|	|	|	0.09
53.000	0.00	0.04	0.004	O	|	|	|	0.09
53.083	0.00	0.04	0.004	O	|	|	|	0.08
53.167	0.00	0.04	0.003	O	|	|	|	0.07

53.250	0.00	0.03	0.003	O	|	|	|	0.07
53.333	0.00	0.03	0.003	O	|	|	|	0.06
53.417	0.00	0.03	0.003	O	|	|	|	0.06
53.500	0.00	0.03	0.002	O	|	|	|	0.06
53.583	0.00	0.02	0.002	O	|	|	|	0.05
53.667	0.00	0.02	0.002	O	|	|	|	0.05
53.750	0.00	0.02	0.002	O	|	|	|	0.04
53.833	0.00	0.02	0.002	O	|	|	|	0.04
53.917	0.00	0.02	0.002	O	|	|	|	0.04
54.000	0.00	0.02	0.002	O	|	|	|	0.04
54.083	0.00	0.02	0.001	O	|	|	|	0.03
54.167	0.00	0.01	0.001	O	|	|	|	0.03
54.250	0.00	0.01	0.001	O	|	|	|	0.03
54.333	0.00	0.01	0.001	O	|	|	|	0.03
54.417	0.00	0.01	0.001	O	|	|	|	0.02
54.500	0.00	0.01	0.001	O	|	|	|	0.02
54.583	0.00	0.01	0.001	O	|	|	|	0.02
54.667	0.00	0.01	0.001	O	|	|	|	0.02
54.750	0.00	0.01	0.001	O	|	|	|	0.02
54.833	0.00	0.01	0.001	O	|	|	|	0.02
54.917	0.00	0.01	0.001	O	|	|	|	0.02
55.000	0.00	0.01	0.001	O	|	|	|	0.01
55.083	0.00	0.01	0.001	O	|	|	|	0.01
55.167	0.00	0.01	0.001	O	|	|	|	0.01
55.250	0.00	0.01	0.001	O	|	|	|	0.01
55.333	0.00	0.01	0.000	O	|	|	|	0.01
55.417	0.00	0.00	0.000	O	|	|	|	0.01
55.500	0.00	0.00	0.000	O	|	|	|	0.01
55.583	0.00	0.00	0.000	O	|	|	|	0.01
55.667	0.00	0.00	0.000	O	|	|	|	0.01
55.750	0.00	0.00	0.000	O	|	|	|	0.01
55.833	0.00	0.00	0.000	O	|	|	|	0.01
55.917	0.00	0.00	0.000	O	|	|	|	0.01
56.000	0.00	0.00	0.000	O	|	|	|	0.01
56.083	0.00	0.00	0.000	O	|	|	|	0.01
56.167	0.00	0.00	0.000	O	|	|	|	0.01
56.250	0.00	0.00	0.000	O	|	|	|	0.00
56.333	0.00	0.00	0.000	O	|	|	|	0.00
56.417	0.00	0.00	0.000	O	|	|	|	0.00
56.500	0.00	0.00	0.000	O	|	|	|	0.00
56.583	0.00	0.00	0.000	O	|	|	|	0.00
56.667	0.00	0.00	0.000	O	|	|	|	0.00
56.750	0.00	0.00	0.000	O	|	|	|	0.00
56.833	0.00	0.00	0.000	O	|	|	|	0.00
56.917	0.00	0.00	0.000	O	|	|	|	0.00
57.000	0.00	0.00	0.000	O	|	|	|	0.00
57.083	0.00	0.00	0.000	O	|	|	|	0.00
57.167	0.00	0.00	0.000	O	|	|	|	0.00
57.250	0.00	0.00	0.000	O	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 687
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.815 (CFS)
Total volume = 1.583 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
6-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD10610.rte
**********HYDROGRAPH DATA**********
Number of intervals = 73
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 7.061 (CFS)
Total volume = 0.826 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 73
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991	
5.600	0.979	5.490	0.960	0.998	

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.8 3.53 5.30 7.06	Depth (Ft.)
0.083	0.44	0.02	0.001	OI | | | |	0.03
0.167	0.67	0.05	0.005	O I | | | |	0.11
0.250	0.70	0.10	0.009	O I | | | |	0.21
0.333	0.70	0.12	0.013	O I | | | |	0.27
0.417	0.70	0.13	0.017	O I | | | |	0.29
0.500	0.79	0.13	0.022	O I | | | |	0.33
0.583	0.82	0.14	0.026	O I | | | |	0.36
0.667	0.82	0.15	0.031	O I | | | |	0.39
0.750	0.82	0.15	0.035	O I | | | |	0.42
0.833	0.82	0.16	0.040	O I | | | |	0.46
0.917	0.82	0.16	0.044	O I | | | |	0.49
1.000	0.91	0.17	0.049	O I | | | |	0.52
1.083	0.93	0.17	0.054	O I | | | |	0.54
1.167	0.93	0.18	0.060	O I | | | |	0.57
1.250	0.93	0.18	0.065	O I | | | |	0.59
1.333	0.93	0.19	0.070	O I | | | |	0.62
1.417	0.93	0.19	0.075	O I | | | |	0.64
1.500	0.93	0.19	0.080	O I | | | |	0.67
1.583	0.93	0.19	0.085	O I | | | |	0.69
1.667	0.93	0.20	0.090	O I | | | |	0.71
1.750	0.93	0.20	0.096	O I | | | |	0.74
1.833	0.93	0.20	0.101	O I | | | |	0.76
1.917	0.93	0.21	0.106	O I | | | |	0.78
2.000	1.02	0.21	0.111	O I | | | |	0.81
2.083	0.96	0.21	0.116	O I | | | |	0.83
2.167	1.02	0.22	0.122	O I | | | |	0.86
2.250	1.05	0.22	0.127	O I | | | |	0.88
2.333	1.05	0.22	0.133	|O I | | | |	0.91
2.417	1.05	0.23	0.139	|O I | | | |	0.93
2.500	1.05	0.23	0.144	|O I | | | |	0.96
2.583	1.05	0.23	0.150	|O I | | | |	0.99
2.667	1.05	0.24	0.156	|O I | | | |	1.01
2.750	1.14	0.24	0.162	|O I | | | |	1.04
2.833	1.17	0.24	0.168	|O I | | | |	1.07
2.917	1.17	0.25	0.174	|O I | | | |	1.10
3.000	1.17	0.25	0.180	|O I | | | |	1.12
3.083	1.17	0.25	0.187	|O I | | | |	1.15
3.167	1.26	0.26	0.193	|O I | | | |	1.18
3.250	1.29	0.26	0.200	|O I | | | |	1.22
3.333	1.29	0.26	0.207	|O I | | | |	1.25
3.417	1.37	0.27	0.215	|O I | | | |	1.28
3.500	1.49	0.27	0.223	|O I | | | |	1.32
3.583	1.61	0.27	0.232	|O I| | | |	1.36
3.667	1.64	0.28	0.241	|O I| | | |	1.40
3.750	1.72	0.28	0.250	|O I| | | |	1.44
3.833	1.75	0.29	0.261	|O I| | | |	1.49
3.917	1.84	0.29	0.271	|O I | | |	1.54
4.000	1.87	0.30	0.282	|O I | | |	1.59
4.083	1.96	0.30	0.293	|O I | | |	1.64
4.167	2.07	0.31	0.305	|O |I | | |	1.69
4.250	2.19	0.31	0.317	|O |I | | |	1.75
4.333	2.31	0.32	0.330	|O | I | | |	1.81
4.417	2.42	0.32	0.344	|O | I | | |	1.87
4.500	2.45	0.33	0.359	|O | I | | |	1.94
4.583	2.54	0.33	0.374	|O | I | | |	2.00
4.667	2.66	0.34	0.390	|O | I | | |	2.08
4.750	2.79	0.35	0.406	|O | I | | |	2.15
4.833	2.83	0.35	0.423	|O | I | | |	2.23
4.917	2.93	0.36	0.440	|O | I | | |	2.31
5.000	3.08	0.37	0.458	|O | I | | |	2.39
5.083	3.64	0.37	0.479	|O | | I | |	2.48
5.167	4.36	0.38	0.504	|O | | | I |	2.60

5.250	4.86	0.39	0.533	O		I		2.73
5.333	5.28	0.40	0.565	O		I		2.88
5.417	5.92	0.41	0.601	O		I		3.05
5.500	7.06	0.43	0.643	O		I		3.25
5.583	3.53	0.44	0.676	O	I			3.42
5.667	1.35	0.44	0.690	O I				3.48
5.750	0.79	0.44	0.695	OI				3.50
5.833	0.61	0.44	0.696	O				3.51
5.917	0.41	0.44	0.697	IO				3.51
6.000	0.26	0.44	0.696	IO				3.51
6.083	0.06	0.44	0.694	I O				3.50
6.167	0.00	0.44	0.691	IO				3.49
6.250	0.00	0.44	0.688	IO				3.47
6.333	0.00	0.44	0.685	IO				3.46
6.417	0.00	0.44	0.682	IO				3.44
6.500	0.00	0.44	0.679	IO				3.43
6.583	0.00	0.44	0.676	IO				3.41
6.667	0.00	0.44	0.673	IO				3.40
6.750	0.00	0.43	0.670	IO				3.39
6.833	0.00	0.43	0.667	IO				3.37
6.917	0.00	0.43	0.664	IO				3.36
7.000	0.00	0.43	0.661	IO				3.34
7.083	0.00	0.43	0.658	IO				3.33
7.167	0.00	0.43	0.655	IO				3.31
7.250	0.00	0.43	0.652	IO				3.30
7.333	0.00	0.43	0.649	IO				3.29
7.417	0.00	0.43	0.646	IO				3.27
7.500	0.00	0.43	0.644	IO				3.26
7.583	0.00	0.43	0.641	IO				3.24
7.667	0.00	0.42	0.638	IO				3.23
7.750	0.00	0.42	0.635	IO				3.22
7.833	0.00	0.42	0.632	IO				3.20
7.917	0.00	0.42	0.629	IO				3.19
8.000	0.00	0.42	0.626	IO				3.17
8.083	0.00	0.42	0.623	IO				3.16
8.167	0.00	0.42	0.620	IO				3.15
8.250	0.00	0.42	0.617	IO				3.13
8.333	0.00	0.42	0.614	IO				3.12
8.417	0.00	0.42	0.612	IO				3.10
8.500	0.00	0.41	0.609	IO				3.09
8.583	0.00	0.41	0.606	IO				3.08
8.667	0.00	0.41	0.603	IO				3.06
8.750	0.00	0.41	0.600	IO				3.05
8.833	0.00	0.41	0.597	IO				3.04
8.917	0.00	0.41	0.595	IO				3.02
9.000	0.00	0.41	0.592	IO				3.01
9.083	0.00	0.41	0.589	IO				2.99
9.167	0.00	0.41	0.586	IO				2.98
9.250	0.00	0.41	0.583	IO				2.97
9.333	0.00	0.41	0.580	IO				2.96
9.417	0.00	0.40	0.578	IO				2.94
9.500	0.00	0.40	0.575	IO				2.93
9.583	0.00	0.40	0.572	IO				2.92
9.667	0.00	0.40	0.569	IO				2.90
9.750	0.00	0.40	0.567	IO				2.89
9.833	0.00	0.40	0.564	IO				2.88
9.917	0.00	0.40	0.561	IO				2.86
10.000	0.00	0.40	0.558	IO				2.85
10.083	0.00	0.40	0.556	IO				2.84
10.167	0.00	0.40	0.553	IO				2.83
10.250	0.00	0.40	0.550	IO				2.81
10.333	0.00	0.40	0.547	IO				2.80
10.417	0.00	0.39	0.545	IO				2.79
10.500	0.00	0.39	0.542	IO				2.78
10.583	0.00	0.39	0.539	IO				2.76
10.667	0.00	0.39	0.537	IO				2.75
10.750	0.00	0.39	0.534	IO				2.74
10.833	0.00	0.39	0.531	IO				2.73
10.917	0.00	0.39	0.529	IO				2.71
11.000	0.00	0.39	0.526	IO				2.70
11.083	0.00	0.39	0.523	IO				2.69
11.167	0.00	0.39	0.520	IO				2.68

11.250	0.00	0.39	0.518	IO				2.66
11.333	0.00	0.38	0.515	IO				2.65
11.417	0.00	0.38	0.513	IO				2.64
11.500	0.00	0.38	0.510	IO				2.63
11.583	0.00	0.38	0.507	IO				2.61
11.667	0.00	0.38	0.505	IO				2.60
11.750	0.00	0.38	0.502	IO				2.59
11.833	0.00	0.38	0.499	IO				2.58
11.917	0.00	0.38	0.497	IO				2.56
12.000	0.00	0.38	0.494	IO				2.55
12.083	0.00	0.38	0.492	IO				2.54
12.167	0.00	0.38	0.489	IO				2.53
12.250	0.00	0.38	0.486	IO				2.52
12.333	0.00	0.37	0.484	IO				2.50
12.417	0.00	0.37	0.481	IO				2.49
12.500	0.00	0.37	0.479	IO				2.48
12.583	0.00	0.37	0.476	IO				2.47
12.667	0.00	0.37	0.474	IO				2.46
12.750	0.00	0.37	0.471	IO				2.45
12.833	0.00	0.37	0.468	IO				2.43
12.917	0.00	0.37	0.466	IO				2.42
13.000	0.00	0.37	0.463	IO				2.41
13.083	0.00	0.37	0.461	IO				2.40
13.167	0.00	0.37	0.458	IO				2.39
13.250	0.00	0.36	0.456	IO				2.38
13.333	0.00	0.36	0.453	IO				2.37
13.417	0.00	0.36	0.451	IO				2.35
13.500	0.00	0.36	0.448	IO				2.34
13.583	0.00	0.36	0.446	IO				2.33
13.667	0.00	0.36	0.443	IO				2.32
13.750	0.00	0.36	0.441	IO				2.31
13.833	0.00	0.36	0.438	IO				2.30
13.917	0.00	0.36	0.436	IO				2.29
14.000	0.00	0.36	0.434	IO				2.28
14.083	0.00	0.36	0.431	IO				2.26
14.167	0.00	0.35	0.429	IO				2.25
14.250	0.00	0.35	0.426	IO				2.24
14.333	0.00	0.35	0.424	IO				2.23
14.417	0.00	0.35	0.421	IO				2.22
14.500	0.00	0.35	0.419	IO				2.21
14.583	0.00	0.35	0.417	IO				2.20
14.667	0.00	0.35	0.414	IO				2.19
14.750	0.00	0.35	0.412	IO				2.18
14.833	0.00	0.35	0.409	IO				2.17
14.917	0.00	0.35	0.407	IO				2.15
15.000	0.00	0.35	0.405	IO				2.14
15.083	0.00	0.34	0.402	IO				2.13
15.167	0.00	0.34	0.400	IO				2.12
15.250	0.00	0.34	0.397	IO				2.11
15.333	0.00	0.34	0.395	IO				2.10
15.417	0.00	0.34	0.393	IO				2.09
15.500	0.00	0.34	0.390	IO				2.08
15.583	0.00	0.34	0.388	IO				2.07
15.667	0.00	0.34	0.386	IO				2.06
15.750	0.00	0.34	0.383	IO				2.05
15.833	0.00	0.34	0.381	IO				2.04
15.917	0.00	0.34	0.379	IO				2.03
16.000	0.00	0.34	0.376	IO				2.02
16.083	0.00	0.33	0.374	IO				2.01
16.167	0.00	0.33	0.372	IO				1.99
16.250	0.00	0.33	0.370	IO				1.98
16.333	0.00	0.33	0.367	IO				1.97
16.417	0.00	0.33	0.365	IO				1.96
16.500	0.00	0.33	0.363	IO				1.95
16.583	0.00	0.33	0.360	IO				1.94
16.667	0.00	0.33	0.358	IO				1.93
16.750	0.00	0.33	0.356	IO				1.92
16.833	0.00	0.33	0.354	IO				1.91
16.917	0.00	0.33	0.351	IO				1.90
17.000	0.00	0.33	0.349	IO				1.89
17.083	0.00	0.32	0.347	IO				1.88
17.167	0.00	0.32	0.345	IO				1.87

17.250	0.00	0.32	0.342	IO				1.87
17.333	0.00	0.32	0.340	IO				1.86
17.417	0.00	0.32	0.338	IO				1.85
17.500	0.00	0.32	0.336	IO				1.84
17.583	0.00	0.32	0.334	IO				1.83
17.667	0.00	0.32	0.331	IO				1.82
17.750	0.00	0.32	0.329	IO				1.81
17.833	0.00	0.32	0.327	IO				1.80
17.917	0.00	0.32	0.325	IO				1.79
18.000	0.00	0.31	0.323	IO				1.78
18.083	0.00	0.31	0.321	IO				1.77
18.167	0.00	0.31	0.318	IO				1.76
18.250	0.00	0.31	0.316	IO				1.75
18.333	0.00	0.31	0.314	IO				1.74
18.417	0.00	0.31	0.312	IO				1.73
18.500	0.00	0.31	0.310	IO				1.72
18.583	0.00	0.31	0.308	IO				1.71
18.667	0.00	0.31	0.306	IO				1.70
18.750	0.00	0.31	0.303	IO				1.69
18.833	0.00	0.31	0.301	IO				1.68
18.917	0.00	0.30	0.299	IO				1.67
19.000	0.00	0.30	0.297	IO				1.66
19.083	0.00	0.30	0.295	IO				1.65
19.167	0.00	0.30	0.293	IO				1.64
19.250	0.00	0.30	0.291	IO				1.63
19.333	0.00	0.30	0.289	IO				1.62
19.417	0.00	0.30	0.287	IO				1.61
19.500	0.00	0.30	0.285	IO				1.60
19.583	0.00	0.30	0.283	IO				1.59
19.667	0.00	0.30	0.281	IO				1.58
19.750	0.00	0.30	0.279	IO				1.57
19.833	0.00	0.29	0.277	IO				1.56
19.917	0.00	0.29	0.274	IO				1.55
20.000	0.00	0.29	0.272	IO				1.54
20.083	0.00	0.29	0.270	IO				1.53
20.167	0.00	0.29	0.268	IO				1.53
20.250	0.00	0.29	0.266	IO				1.52
20.333	0.00	0.29	0.264	IO				1.51
20.417	0.00	0.29	0.262	IO				1.50
20.500	0.00	0.29	0.260	IO				1.49
20.583	0.00	0.29	0.258	IO				1.48
20.667	0.00	0.29	0.257	IO				1.47
20.750	0.00	0.28	0.255	IO				1.46
20.833	0.00	0.28	0.253	IO				1.45
20.917	0.00	0.28	0.251	IO				1.44
21.000	0.00	0.28	0.249	IO				1.43
21.083	0.00	0.28	0.247	IO				1.43
21.167	0.00	0.28	0.245	IO				1.42
21.250	0.00	0.28	0.243	IO				1.41
21.333	0.00	0.28	0.241	IO				1.40
21.417	0.00	0.28	0.239	IO				1.39
21.500	0.00	0.28	0.237	IO				1.38
21.583	0.00	0.28	0.235	IO				1.37
21.667	0.00	0.27	0.233	IO				1.37
21.750	0.00	0.27	0.231	IO				1.36
21.833	0.00	0.27	0.230	IO				1.35
21.917	0.00	0.27	0.228	IO				1.34
22.000	0.00	0.27	0.226	IO				1.33
22.083	0.00	0.27	0.224	IO				1.32
22.167	0.00	0.27	0.222	IO				1.31
22.250	0.00	0.27	0.220	IO				1.31
22.333	0.00	0.27	0.218	IO				1.30
22.417	0.00	0.27	0.217	IO				1.29
22.500	0.00	0.27	0.215	IO				1.28
22.583	0.00	0.26	0.213	IO				1.27
22.667	0.00	0.26	0.211	IO				1.26
22.750	0.00	0.26	0.209	IO				1.26
22.833	0.00	0.26	0.207	IO				1.25
22.917	0.00	0.26	0.206	IO				1.24
23.000	0.00	0.26	0.204	IO				1.23
23.083	0.00	0.26	0.202	IO				1.22
23.167	0.00	0.26	0.200	IO				1.21

23.250	0.00	0.26	0.199	IO				1.21
23.333	0.00	0.26	0.197	IO				1.20
23.417	0.00	0.26	0.195	IO				1.19
23.500	0.00	0.26	0.193	IO				1.18
23.583	0.00	0.25	0.191	IO				1.17
23.667	0.00	0.25	0.190	IO				1.17
23.750	0.00	0.25	0.188	IO				1.16
23.833	0.00	0.25	0.186	IO				1.15
23.917	0.00	0.25	0.184	IO				1.14
24.000	0.00	0.25	0.183	IO				1.14
24.083	0.00	0.25	0.181	IO				1.13
24.167	0.00	0.25	0.179	IO				1.12
24.250	0.00	0.25	0.178	IO				1.11
24.333	0.00	0.25	0.176	IO				1.10
24.417	0.00	0.25	0.174	IO				1.10
24.500	0.00	0.25	0.173	IO				1.09
24.583	0.00	0.24	0.171	IO				1.08
24.667	0.00	0.24	0.169	IO				1.07
24.750	0.00	0.24	0.167	IO				1.07
24.833	0.00	0.24	0.166	IO				1.06
24.917	0.00	0.24	0.164	IO				1.05
25.000	0.00	0.24	0.162	IO				1.04
25.083	0.00	0.24	0.161	IO				1.04
25.167	0.00	0.24	0.159	IO				1.03
25.250	0.00	0.24	0.158	IO				1.02
25.333	0.00	0.24	0.156	IO				1.01
25.417	0.00	0.24	0.154	IO				1.01
25.500	0.00	0.24	0.153	IO				1.00
25.583	0.00	0.23	0.151	IO				0.99
25.667	0.00	0.23	0.149	IO				0.98
25.750	0.00	0.23	0.148	IO				0.98
25.833	0.00	0.23	0.146	IO				0.97
25.917	0.00	0.23	0.145	IO				0.96
26.000	0.00	0.23	0.143	IO				0.95
26.083	0.00	0.23	0.141	IO				0.95
26.167	0.00	0.23	0.140	IO				0.94
26.250	0.00	0.23	0.138	IO				0.93
26.333	0.00	0.23	0.137	IO				0.93
26.417	0.00	0.23	0.135	IO				0.92
26.500	0.00	0.22	0.134	IO				0.91
26.583	0.00	0.22	0.132	IO				0.90
26.667	0.00	0.22	0.131	IO				0.90
26.750	0.00	0.22	0.129	IO				0.89
26.833	0.00	0.22	0.128	O				0.88
26.917	0.00	0.22	0.126	O				0.88
27.000	0.00	0.22	0.124	O				0.87
27.083	0.00	0.22	0.123	O				0.86
27.167	0.00	0.22	0.121	O				0.86
27.250	0.00	0.22	0.120	O				0.85
27.333	0.00	0.21	0.119	O				0.84
27.417	0.00	0.21	0.117	O				0.83
27.500	0.00	0.21	0.116	O				0.83
27.583	0.00	0.21	0.114	O				0.82
27.667	0.00	0.21	0.113	O				0.81
27.750	0.00	0.21	0.111	O				0.81
27.833	0.00	0.21	0.110	O				0.80
27.917	0.00	0.21	0.108	O				0.79
28.000	0.00	0.21	0.107	O				0.79
28.083	0.00	0.21	0.105	O				0.78
28.167	0.00	0.21	0.104	O				0.77
28.250	0.00	0.21	0.103	O				0.77
28.333	0.00	0.20	0.101	O				0.76
28.417	0.00	0.20	0.100	O				0.76
28.500	0.00	0.20	0.098	O				0.75
28.583	0.00	0.20	0.097	O				0.74
28.667	0.00	0.20	0.096	O				0.74
28.750	0.00	0.20	0.094	O				0.73
28.833	0.00	0.20	0.093	O				0.72
28.917	0.00	0.20	0.091	O				0.72
29.000	0.00	0.20	0.090	O				0.71
29.083	0.00	0.20	0.089	O				0.70
29.167	0.00	0.20	0.087	O				0.70

29.250	0.00	0.20	0.086	O	|	|	|	0.69
29.333	0.00	0.19	0.085	O	|	|	|	0.69
29.417	0.00	0.19	0.083	O	|	|	|	0.68
29.500	0.00	0.19	0.082	O	|	|	|	0.67
29.583	0.00	0.19	0.081	O	|	|	|	0.67
29.667	0.00	0.19	0.079	O	|	|	|	0.66
29.750	0.00	0.19	0.078	O	|	|	|	0.66
29.833	0.00	0.19	0.077	O	|	|	|	0.65
29.917	0.00	0.19	0.075	O	|	|	|	0.64
30.000	0.00	0.19	0.074	O	|	|	|	0.64
30.083	0.00	0.19	0.073	O	|	|	|	0.63
30.167	0.00	0.19	0.072	O	|	|	|	0.63
30.250	0.00	0.19	0.070	O	|	|	|	0.62
30.333	0.00	0.18	0.069	O	|	|	|	0.61
30.417	0.00	0.18	0.068	O	|	|	|	0.61
30.500	0.00	0.18	0.067	O	|	|	|	0.60
30.583	0.00	0.18	0.065	O	|	|	|	0.60
30.667	0.00	0.18	0.064	O	|	|	|	0.59
30.750	0.00	0.18	0.063	O	|	|	|	0.58
30.833	0.00	0.18	0.062	O	|	|	|	0.58
30.917	0.00	0.18	0.060	O	|	|	|	0.57
31.000	0.00	0.18	0.059	O	|	|	|	0.57
31.083	0.00	0.18	0.058	O	|	|	|	0.56
31.167	0.00	0.18	0.057	O	|	|	|	0.55
31.250	0.00	0.17	0.055	O	|	|	|	0.55
31.333	0.00	0.17	0.054	O	|	|	|	0.54
31.417	0.00	0.17	0.053	O	|	|	|	0.54
31.500	0.00	0.17	0.052	O	|	|	|	0.53
31.583	0.00	0.17	0.051	O	|	|	|	0.52
31.667	0.00	0.17	0.049	O	|	|	|	0.52
31.750	0.00	0.17	0.048	O	|	|	|	0.51
31.833	0.00	0.17	0.047	O	|	|	|	0.51
31.917	0.00	0.17	0.046	O	|	|	|	0.50
32.000	0.00	0.17	0.045	O	|	|	|	0.49
32.083	0.00	0.16	0.044	O	|	|	|	0.48
32.167	0.00	0.16	0.043	O	|	|	|	0.48
32.250	0.00	0.16	0.041	O	|	|	|	0.47
32.333	0.00	0.16	0.040	O	|	|	|	0.46
32.417	0.00	0.16	0.039	O	|	|	|	0.45
32.500	0.00	0.16	0.038	O	|	|	|	0.44
32.583	0.00	0.15	0.037	O	|	|	|	0.44
32.667	0.00	0.15	0.036	O	|	|	|	0.43
32.750	0.00	0.15	0.035	O	|	|	|	0.42
32.833	0.00	0.15	0.034	O	|	|	|	0.41
32.917	0.00	0.15	0.033	O	|	|	|	0.41
33.000	0.00	0.15	0.032	O	|	|	|	0.40
33.083	0.00	0.15	0.031	O	|	|	|	0.39
33.167	0.00	0.14	0.030	O	|	|	|	0.39
33.250	0.00	0.14	0.029	O	|	|	|	0.38
33.333	0.00	0.14	0.028	O	|	|	|	0.37
33.417	0.00	0.14	0.027	O	|	|	|	0.36
33.500	0.00	0.14	0.026	O	|	|	|	0.36
33.583	0.00	0.14	0.025	O	|	|	|	0.35
33.667	0.00	0.14	0.024	O	|	|	|	0.34
33.750	0.00	0.14	0.023	O	|	|	|	0.34
33.833	0.00	0.13	0.022	O	|	|	|	0.33
33.917	0.00	0.13	0.021	O	|	|	|	0.32
34.000	0.00	0.13	0.020	O	|	|	|	0.32
34.083	0.00	0.13	0.020	O	|	|	|	0.31
34.167	0.00	0.13	0.019	O	|	|	|	0.30
34.250	0.00	0.13	0.018	O	|	|	|	0.30
34.333	0.00	0.13	0.017	O	|	|	|	0.29
34.417	0.00	0.13	0.016	O	|	|	|	0.29
34.500	0.00	0.12	0.015	O	|	|	|	0.28
34.583	0.00	0.12	0.014	O	|	|	|	0.27
34.667	0.00	0.12	0.013	O	|	|	|	0.27
34.750	0.00	0.12	0.013	O	|	|	|	0.26
34.833	0.00	0.12	0.012	O	|	|	|	0.26
34.917	0.00	0.12	0.011	O	|	|	|	0.25
35.000	0.00	0.11	0.010	O	|	|	|	0.23
35.083	0.00	0.10	0.010	O	|	|	|	0.22
35.167	0.00	0.09	0.009	O	|	|	|	0.20

35.250	0.00	0.09	0.008	O	|	|	|	|	0.19
35.333	0.00	0.08	0.008	O	|	|	|	|	0.17
35.417	0.00	0.08	0.007	O	|	|	|	|	0.16
35.500	0.00	0.07	0.007	O	|	|	|	|	0.15
35.583	0.00	0.07	0.006	O	|	|	|	|	0.14
35.667	0.00	0.06	0.006	O	|	|	|	|	0.13
35.750	0.00	0.06	0.005	O	|	|	|	|	0.12
35.833	0.00	0.05	0.005	O	|	|	|	|	0.11
35.917	0.00	0.05	0.005	O	|	|	|	|	0.10
36.000	0.00	0.05	0.004	O	|	|	|	|	0.10
36.083	0.00	0.04	0.004	O	|	|	|	|	0.09
36.167	0.00	0.04	0.004	O	|	|	|	|	0.08
36.250	0.00	0.04	0.003	O	|	|	|	|	0.08
36.333	0.00	0.03	0.003	O	|	|	|	|	0.07
36.417	0.00	0.03	0.003	O	|	|	|	|	0.07
36.500	0.00	0.03	0.003	O	|	|	|	|	0.06
36.583	0.00	0.03	0.003	O	|	|	|	|	0.06
36.667	0.00	0.03	0.002	O	|	|	|	|	0.05
36.750	0.00	0.02	0.002	O	|	|	|	|	0.05
36.833	0.00	0.02	0.002	O	|	|	|	|	0.05
36.917	0.00	0.02	0.002	O	|	|	|	|	0.04
37.000	0.00	0.02	0.002	O	|	|	|	|	0.04
37.083	0.00	0.02	0.002	O	|	|	|	|	0.04
37.167	0.00	0.02	0.001	O	|	|	|	|	0.03
37.250	0.00	0.01	0.001	O	|	|	|	|	0.03
37.333	0.00	0.01	0.001	O	|	|	|	|	0.03
37.417	0.00	0.01	0.001	O	|	|	|	|	0.03
37.500	0.00	0.01	0.001	O	|	|	|	|	0.03
37.583	0.00	0.01	0.001	O	|	|	|	|	0.02
37.667	0.00	0.01	0.001	O	|	|	|	|	0.02
37.750	0.00	0.01	0.001	O	|	|	|	|	0.02
37.833	0.00	0.01	0.001	O	|	|	|	|	0.02
37.917	0.00	0.01	0.001	O	|	|	|	|	0.02
38.000	0.00	0.01	0.001	O	|	|	|	|	0.02
38.083	0.00	0.01	0.001	O	|	|	|	|	0.02
38.167	0.00	0.01	0.001	O	|	|	|	|	0.01
38.250	0.00	0.01	0.001	O	|	|	|	|	0.01
38.333	0.00	0.01	0.001	O	|	|	|	|	0.01
38.417	0.00	0.01	0.000	O	|	|	|	|	0.01
38.500	0.00	0.00	0.000	O	|	|	|	|	0.01
38.583	0.00	0.00	0.000	O	|	|	|	|	0.01
38.667	0.00	0.00	0.000	O	|	|	|	|	0.01
38.750	0.00	0.00	0.000	O	|	|	|	|	0.01
38.833	0.00	0.00	0.000	O	|	|	|	|	0.01
38.917	0.00	0.00	0.000	O	|	|	|	|	0.01
39.000	0.00	0.00	0.000	O	|	|	|	|	0.01
39.083	0.00	0.00	0.000	O	|	|	|	|	0.01
39.167	0.00	0.00	0.000	O	|	|	|	|	0.01
39.250	0.00	0.00	0.000	O	|	|	|	|	0.01
39.333	0.00	0.00	0.000	O	|	|	|	|	0.00
39.417	0.00	0.00	0.000	O	|	|	|	|	0.00
39.500	0.00	0.00	0.000	O	|	|	|	|	0.00
39.583	0.00	0.00	0.000	O	|	|	|	|	0.00
39.667	0.00	0.00	0.000	O	|	|	|	|	0.00
39.750	0.00	0.00	0.000	O	|	|	|	|	0.00
39.833	0.00	0.00	0.000	O	|	|	|	|	0.00
39.917	0.00	0.00	0.000	O	|	|	|	|	0.00
40.000	0.00	0.00	0.000	O	|	|	|	|	0.00
40.083	0.00	0.00	0.000	O	|	|	|	|	0.00
40.167	0.00	0.00	0.000	O	|	|	|	|	0.00
40.250	0.00	0.00	0.000	O	|	|	|	|	0.00
40.333	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 484
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.443 (CFS)
Total volume = 0.826 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
3-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD10310.rte
**********HYDROGRAPH DATA**********
Number of intervals = 37
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 8.167 (CFS)
Total volume = 0.648 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 37
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991	
5.600	0.979	5.490	0.960	0.998	

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 2.0 4.08 6.13 8.17	Depth (Ft.)
0.083	0.87	0.03	0.003	O I | | | | |	0.07
0.167	1.17	0.10	0.009	O I | | | | |	0.22
0.250	1.04	0.13	0.016	O I | | | | |	0.29
0.333	1.26	0.14	0.023	O I | | | | |	0.34
0.417	1.35	0.15	0.031	O I | | | | |	0.40
0.500	1.55	0.16	0.040	O I | | | | |	0.46
0.583	1.42	0.17	0.049	O I | | | | |	0.52
0.667	1.55	0.18	0.058	O I | | | | |	0.56
0.750	1.62	0.18	0.068	O I | | | | |	0.61
0.833	1.42	0.19	0.077	O I | | | | |	0.65
0.917	1.42	0.20	0.086	O I | | | | |	0.69
1.000	1.58	0.20	0.095	O I | | | | |	0.73
1.083	1.89	0.21	0.105	O I | | | | |	0.78
1.167	1.98	0.21	0.117	O I | | | | |	0.84
1.250	1.98	0.22	0.129	O I | | | | |	0.89
1.333	1.85	0.23	0.141	O I | | | | |	0.94
1.417	2.21	0.24	0.153	O I | | | |	1.00
1.500	2.41	0.24	0.168	O |I | | | |	1.07
1.583	2.23	0.25	0.182	O I | | | |	1.13
1.667	2.36	0.26	0.196	|O |I | | | |	1.20
1.750	2.88	0.26	0.212	|O | I | | | |	1.27
1.833	2.87	0.27	0.230	|O | I | | | |	1.35
1.917	2.66	0.28	0.247	|O | I | | | |	1.43
2.000	2.68	0.29	0.264	|O | I | | | |	1.50
2.083	2.79	0.30	0.281	|O | I | | | |	1.58
2.167	3.71	0.31	0.301	|O | | I | | |	1.68
2.250	4.68	0.32	0.328	|O | | | I | |	1.80
2.333	3.67	0.33	0.354	|O | | I | | |	1.92
2.417	5.96	0.34	0.385	|O | | | I | |	2.05
2.500	7.29	0.35	0.428	|O | | | | I |	2.25
2.583	8.17	0.37	0.479	|O | | | | | I	2.48
2.667	6.53	0.39	0.527	|O | | | I | |	2.71
2.750	2.84	0.40	0.557	|O | I | | | |	2.84
2.833	1.67	0.40	0.569	|O | I | | | |	2.90
2.917	1.62	0.41	0.578	|O | I | | | |	2.94
3.000	0.82	0.41	0.584	|O I | | | |	2.97
3.083	0.14	0.41	0.584	IO | | | |	2.97
3.167	0.00	0.41	0.582	IO | | | |	2.96
3.250	0.00	0.41	0.579	IO | | | |	2.95
3.333	0.00	0.40	0.576	IO | | | |	2.93
3.417	0.00	0.40	0.573	IO | | | |	2.92
3.500	0.00	0.40	0.571	IO | | | |	2.91
3.583	0.00	0.40	0.568	IO | | | |	2.90
3.667	0.00	0.40	0.565	IO | | | |	2.88
3.750	0.00	0.40	0.562	IO | | | |	2.87
3.833	0.00	0.40	0.559	IO | | | |	2.86
3.917	0.00	0.40	0.557	IO | | | |	2.84
4.000	0.00	0.40	0.554	IO | | | |	2.83
4.083	0.00	0.40	0.551	IO | | | |	2.82
4.167	0.00	0.40	0.549	IO | | | |	2.81
4.250	0.00	0.39	0.546	IO | | | |	2.79
4.333	0.00	0.39	0.543	IO | | | |	2.78
4.417	0.00	0.39	0.540	IO | | | |	2.77
4.500	0.00	0.39	0.538	IO | | | |	2.76
4.583	0.00	0.39	0.535	IO | | | |	2.74
4.667	0.00	0.39	0.532	IO | | | |	2.73
4.750	0.00	0.39	0.530	IO | | | |	2.72
4.833	0.00	0.39	0.527	IO | | | |	2.71
4.917	0.00	0.39	0.524	IO | | | |	2.69
5.000	0.00	0.39	0.522	IO | | | |	2.68
5.083	0.00	0.39	0.519	IO | | | |	2.67
5.167	0.00	0.38	0.516	IO | | | |	2.66

5.250	0.00	0.38	0.514	IO				2.64
5.333	0.00	0.38	0.511	IO				2.63
5.417	0.00	0.38	0.508	IO				2.62
5.500	0.00	0.38	0.506	IO				2.61
5.583	0.00	0.38	0.503	IO				2.59
5.667	0.00	0.38	0.500	IO				2.58
5.750	0.00	0.38	0.498	IO				2.57
5.833	0.00	0.38	0.495	IO				2.56
5.917	0.00	0.38	0.493	IO				2.55
6.000	0.00	0.38	0.490	IO				2.53
6.083	0.00	0.38	0.487	IO				2.52
6.167	0.00	0.37	0.485	IO				2.51
6.250	0.00	0.37	0.482	IO				2.50
6.333	0.00	0.37	0.480	IO				2.49
6.417	0.00	0.37	0.477	IO				2.47
6.500	0.00	0.37	0.475	IO				2.46
6.583	0.00	0.37	0.472	IO				2.45
6.667	0.00	0.37	0.470	IO				2.44
6.750	0.00	0.37	0.467	IO				2.43
6.833	0.00	0.37	0.464	IO				2.42
6.917	0.00	0.37	0.462	IO				2.40
7.000	0.00	0.37	0.459	IO				2.39
7.083	0.00	0.36	0.457	IO				2.38
7.167	0.00	0.36	0.454	IO				2.37
7.250	0.00	0.36	0.452	IO				2.36
7.333	0.00	0.36	0.449	IO				2.35
7.417	0.00	0.36	0.447	IO				2.34
7.500	0.00	0.36	0.444	IO				2.32
7.583	0.00	0.36	0.442	IO				2.31
7.667	0.00	0.36	0.439	IO				2.30
7.750	0.00	0.36	0.437	IO				2.29
7.833	0.00	0.36	0.435	IO				2.28
7.917	0.00	0.36	0.432	IO				2.27
8.000	0.00	0.35	0.430	IO				2.26
8.083	0.00	0.35	0.427	IO				2.25
8.167	0.00	0.35	0.425	IO				2.24
8.250	0.00	0.35	0.422	IO				2.22
8.333	0.00	0.35	0.420	IO				2.21
8.417	0.00	0.35	0.418	IO				2.20
8.500	0.00	0.35	0.415	IO				2.19
8.583	0.00	0.35	0.413	IO				2.18
8.667	0.00	0.35	0.410	IO				2.17
8.750	0.00	0.35	0.408	IO				2.16
8.833	0.00	0.35	0.406	IO				2.15
8.917	0.00	0.34	0.403	IO				2.14
9.000	0.00	0.34	0.401	IO				2.13
9.083	0.00	0.34	0.398	IO				2.12
9.167	0.00	0.34	0.396	IO				2.10
9.250	0.00	0.34	0.394	IO				2.09
9.333	0.00	0.34	0.391	IO				2.08
9.417	0.00	0.34	0.389	IO				2.07
9.500	0.00	0.34	0.387	IO				2.06
9.583	0.00	0.34	0.384	IO				2.05
9.667	0.00	0.34	0.382	IO				2.04
9.750	0.00	0.34	0.380	IO				2.03
9.833	0.00	0.34	0.377	IO				2.02
9.917	0.00	0.33	0.375	IO				2.01
10.000	0.00	0.33	0.373	IO				2.00
10.083	0.00	0.33	0.370	IO				1.99
10.167	0.00	0.33	0.368	IO				1.98
10.250	0.00	0.33	0.366	IO				1.97
10.333	0.00	0.33	0.364	IO				1.96
10.417	0.00	0.33	0.361	IO				1.95
10.500	0.00	0.33	0.359	IO				1.94
10.583	0.00	0.33	0.357	IO				1.93
10.667	0.00	0.33	0.355	IO				1.92
10.750	0.00	0.33	0.352	IO				1.91
10.833	0.00	0.33	0.350	IO				1.90
10.917	0.00	0.32	0.348	IO				1.89
11.000	0.00	0.32	0.346	IO				1.88
11.083	0.00	0.32	0.343	IO				1.87
11.167	0.00	0.32	0.341	IO				1.86

11.250	0.00	0.32	0.339	IO				1.85
11.333	0.00	0.32	0.337	IO				1.84
11.417	0.00	0.32	0.335	IO				1.83
11.500	0.00	0.32	0.332	IO				1.82
11.583	0.00	0.32	0.330	IO				1.81
11.667	0.00	0.32	0.328	IO				1.80
11.750	0.00	0.32	0.326	IO				1.79
11.833	0.00	0.32	0.324	IO				1.78
11.917	0.00	0.31	0.321	IO				1.77
12.000	0.00	0.31	0.319	IO				1.76
12.083	0.00	0.31	0.317	IO				1.75
12.167	0.00	0.31	0.315	IO				1.74
12.250	0.00	0.31	0.313	IO				1.73
12.333	0.00	0.31	0.311	IO				1.72
12.417	0.00	0.31	0.309	IO				1.71
12.500	0.00	0.31	0.306	IO				1.70
12.583	0.00	0.31	0.304	IO				1.69
12.667	0.00	0.31	0.302	IO				1.68
12.750	0.00	0.31	0.300	IO				1.67
12.833	0.00	0.30	0.298	IO				1.66
12.917	0.00	0.30	0.296	IO				1.65
13.000	0.00	0.30	0.294	IO				1.64
13.083	0.00	0.30	0.292	IO				1.63
13.167	0.00	0.30	0.290	IO				1.62
13.250	0.00	0.30	0.288	IO				1.61
13.333	0.00	0.30	0.286	IO				1.60
13.417	0.00	0.30	0.283	IO				1.59
13.500	0.00	0.30	0.281	IO				1.59
13.583	0.00	0.30	0.279	IO				1.58
13.667	0.00	0.30	0.277	IO				1.57
13.750	0.00	0.29	0.275	IO				1.56
13.833	0.00	0.29	0.273	IO				1.55
13.917	0.00	0.29	0.271	IO				1.54
14.000	0.00	0.29	0.269	IO				1.53
14.083	0.00	0.29	0.267	IO				1.52
14.167	0.00	0.29	0.265	IO				1.51
14.250	0.00	0.29	0.263	IO				1.50
14.333	0.00	0.29	0.261	IO				1.49
14.417	0.00	0.29	0.259	IO				1.48
14.500	0.00	0.29	0.257	IO				1.47
14.583	0.00	0.29	0.255	IO				1.47
14.667	0.00	0.28	0.253	IO				1.46
14.750	0.00	0.28	0.251	IO				1.45
14.833	0.00	0.28	0.250	IO				1.44
14.917	0.00	0.28	0.248	IO				1.43
15.000	0.00	0.28	0.246	IO				1.42
15.083	0.00	0.28	0.244	IO				1.41
15.167	0.00	0.28	0.242	IO				1.40
15.250	0.00	0.28	0.240	IO				1.39
15.333	0.00	0.28	0.238	IO				1.39
15.417	0.00	0.28	0.236	IO				1.38
15.500	0.00	0.28	0.234	IO				1.37
15.583	0.00	0.27	0.232	IO				1.36
15.667	0.00	0.27	0.230	IO				1.35
15.750	0.00	0.27	0.228	IO				1.34
15.833	0.00	0.27	0.227	IO				1.33
15.917	0.00	0.27	0.225	IO				1.33
16.000	0.00	0.27	0.223	IO				1.32
16.083	0.00	0.27	0.221	IO				1.31
16.167	0.00	0.27	0.219	IO				1.30
16.250	0.00	0.27	0.217	IO				1.29
16.333	0.00	0.27	0.216	IO				1.28
16.417	0.00	0.27	0.214	IO				1.28
16.500	0.00	0.26	0.212	IO				1.27
16.583	0.00	0.26	0.210	IO				1.26
16.667	0.00	0.26	0.208	IO				1.25
16.750	0.00	0.26	0.206	IO				1.24
16.833	0.00	0.26	0.205	IO				1.23
16.917	0.00	0.26	0.203	IO				1.23
17.000	0.00	0.26	0.201	IO				1.22
17.083	0.00	0.26	0.199	IO				1.21
17.167	0.00	0.26	0.197	IO				1.20

17.250	0.00	0.26	0.196	IO				1.19
17.333	0.00	0.26	0.194	IO				1.19
17.417	0.00	0.25	0.192	O				1.18
17.500	0.00	0.25	0.190	O				1.17
17.583	0.00	0.25	0.189	O				1.16
17.667	0.00	0.25	0.187	O				1.15
17.750	0.00	0.25	0.185	O				1.15
17.833	0.00	0.25	0.183	O				1.14
17.917	0.00	0.25	0.182	O				1.13
18.000	0.00	0.25	0.180	O				1.12
18.083	0.00	0.25	0.178	O				1.12
18.167	0.00	0.25	0.177	O				1.11
18.250	0.00	0.25	0.175	O				1.10
18.333	0.00	0.25	0.173	O				1.09
18.417	0.00	0.24	0.172	O				1.08
18.500	0.00	0.24	0.170	O				1.08
18.583	0.00	0.24	0.168	O				1.07
18.667	0.00	0.24	0.167	O				1.06
18.750	0.00	0.24	0.165	O				1.05
18.833	0.00	0.24	0.163	O				1.05
18.917	0.00	0.24	0.162	O				1.04
19.000	0.00	0.24	0.160	O				1.03
19.083	0.00	0.24	0.158	O				1.02
19.167	0.00	0.24	0.157	O				1.02
19.250	0.00	0.24	0.155	O				1.01
19.333	0.00	0.24	0.153	O				1.00
19.417	0.00	0.24	0.152	O				0.99
19.500	0.00	0.23	0.150	O				0.99
19.583	0.00	0.23	0.148	O				0.98
19.667	0.00	0.23	0.147	O				0.97
19.750	0.00	0.23	0.145	O				0.96
19.833	0.00	0.23	0.144	O				0.96
19.917	0.00	0.23	0.142	O				0.95
20.000	0.00	0.23	0.141	O				0.94
20.083	0.00	0.23	0.139	O				0.94
20.167	0.00	0.23	0.137	O				0.93
20.250	0.00	0.23	0.136	O				0.92
20.333	0.00	0.22	0.134	O				0.91
20.417	0.00	0.22	0.133	O				0.91
20.500	0.00	0.22	0.131	O				0.90
20.583	0.00	0.22	0.130	O				0.89
20.667	0.00	0.22	0.128	O				0.89
20.750	0.00	0.22	0.127	O				0.88
20.833	0.00	0.22	0.125	O				0.87
20.917	0.00	0.22	0.124	O				0.86
21.000	0.00	0.22	0.122	O				0.86
21.083	0.00	0.22	0.121	O				0.85
21.167	0.00	0.22	0.119	O				0.84
21.250	0.00	0.21	0.118	O				0.84
21.333	0.00	0.21	0.116	O				0.83
21.417	0.00	0.21	0.115	O				0.82
21.500	0.00	0.21	0.113	O				0.82
21.583	0.00	0.21	0.112	O				0.81
21.667	0.00	0.21	0.110	O				0.80
21.750	0.00	0.21	0.109	O				0.80
21.833	0.00	0.21	0.107	O				0.79
21.917	0.00	0.21	0.106	O				0.78
22.000	0.00	0.21	0.105	O				0.78
22.083	0.00	0.21	0.103	O				0.77
22.167	0.00	0.20	0.102	O				0.76
22.250	0.00	0.20	0.100	O				0.76
22.333	0.00	0.20	0.099	O				0.75
22.417	0.00	0.20	0.098	O				0.75
22.500	0.00	0.20	0.096	O				0.74
22.583	0.00	0.20	0.095	O				0.73
22.667	0.00	0.20	0.093	O				0.73
22.750	0.00	0.20	0.092	O				0.72
22.833	0.00	0.20	0.091	O				0.71
22.917	0.00	0.20	0.089	O				0.71
23.000	0.00	0.20	0.088	O				0.70
23.083	0.00	0.20	0.087	O				0.69
23.167	0.00	0.19	0.085	O				0.69

23.250	0.00	0.19	0.084	O	|	|	|	0.68
23.333	0.00	0.19	0.083	O	|	|	|	0.68
23.417	0.00	0.19	0.081	O	|	|	|	0.67
23.500	0.00	0.19	0.080	O	|	|	|	0.66
23.583	0.00	0.19	0.079	O	|	|	|	0.66
23.667	0.00	0.19	0.077	O	|	|	|	0.65
23.750	0.00	0.19	0.076	O	|	|	|	0.65
23.833	0.00	0.19	0.075	O	|	|	|	0.64
23.917	0.00	0.19	0.073	O	|	|	|	0.63
24.000	0.00	0.19	0.072	O	|	|	|	0.63
24.083	0.00	0.19	0.071	O	|	|	|	0.62
24.167	0.00	0.19	0.070	O	|	|	|	0.62
24.250	0.00	0.18	0.068	O	|	|	|	0.61
24.333	0.00	0.18	0.067	O	|	|	|	0.60
24.417	0.00	0.18	0.066	O	|	|	|	0.60
24.500	0.00	0.18	0.065	O	|	|	|	0.59
24.583	0.00	0.18	0.063	O	|	|	|	0.59
24.667	0.00	0.18	0.062	O	|	|	|	0.58
24.750	0.00	0.18	0.061	O	|	|	|	0.57
24.833	0.00	0.18	0.060	O	|	|	|	0.57
24.917	0.00	0.18	0.058	O	|	|	|	0.56
25.000	0.00	0.18	0.057	O	|	|	|	0.56
25.083	0.00	0.17	0.056	O	|	|	|	0.55
25.167	0.00	0.17	0.055	O	|	|	|	0.54
25.250	0.00	0.17	0.054	O	|	|	|	0.54
25.333	0.00	0.17	0.052	O	|	|	|	0.53
25.417	0.00	0.17	0.051	O	|	|	|	0.53
25.500	0.00	0.17	0.050	O	|	|	|	0.52
25.583	0.00	0.17	0.049	O	|	|	|	0.51
25.667	0.00	0.17	0.048	O	|	|	|	0.51
25.750	0.00	0.17	0.046	O	|	|	|	0.50
25.833	0.00	0.17	0.045	O	|	|	|	0.50
25.917	0.00	0.16	0.044	O	|	|	|	0.49
26.000	0.00	0.16	0.043	O	|	|	|	0.48
26.083	0.00	0.16	0.042	O	|	|	|	0.47
26.167	0.00	0.16	0.041	O	|	|	|	0.46
26.250	0.00	0.16	0.040	O	|	|	|	0.46
26.333	0.00	0.16	0.039	O	|	|	|	0.45
26.417	0.00	0.16	0.038	O	|	|	|	0.44
26.500	0.00	0.15	0.037	O	|	|	|	0.43
26.583	0.00	0.15	0.035	O	|	|	|	0.42
26.667	0.00	0.15	0.034	O	|	|	|	0.42
26.750	0.00	0.15	0.033	O	|	|	|	0.41
26.833	0.00	0.15	0.032	O	|	|	|	0.40
26.917	0.00	0.15	0.031	O	|	|	|	0.40
27.000	0.00	0.15	0.030	O	|	|	|	0.39
27.083	0.00	0.14	0.029	O	|	|	|	0.38
27.167	0.00	0.14	0.028	O	|	|	|	0.37
27.250	0.00	0.14	0.027	O	|	|	|	0.37
27.333	0.00	0.14	0.026	O	|	|	|	0.36
27.417	0.00	0.14	0.025	O	|	|	|	0.35
27.500	0.00	0.14	0.025	O	|	|	|	0.35
27.583	0.00	0.14	0.024	O	|	|	|	0.34
27.667	0.00	0.13	0.023	O	|	|	|	0.33
27.750	0.00	0.13	0.022	O	|	|	|	0.33
27.833	0.00	0.13	0.021	O	|	|	|	0.32
27.917	0.00	0.13	0.020	O	|	|	|	0.31
28.000	0.00	0.13	0.019	O	|	|	|	0.31
28.083	0.00	0.13	0.018	O	|	|	|	0.30
28.167	0.00	0.13	0.017	O	|	|	|	0.29
28.250	0.00	0.13	0.016	O	|	|	|	0.29
28.333	0.00	0.12	0.016	O	|	|	|	0.28
28.417	0.00	0.12	0.015	O	|	|	|	0.28
28.500	0.00	0.12	0.014	O	|	|	|	0.27
28.583	0.00	0.12	0.013	O	|	|	|	0.26
28.667	0.00	0.12	0.012	O	|	|	|	0.26
28.750	0.00	0.12	0.011	O	|	|	|	0.25
28.833	0.00	0.11	0.011	O	|	|	|	0.24
28.917	0.00	0.11	0.010	O	|	|	|	0.22
29.000	0.00	0.10	0.009	O	|	|	|	0.21
29.083	0.00	0.09	0.008	O	|	|	|	0.19
29.167	0.00	0.08	0.008	O	|	|	|	0.18

29.250	0.00	0.08	0.007	O	|	|	|	|	0.17
29.333	0.00	0.07	0.007	O	|	|	|	|	0.15
29.417	0.00	0.07	0.006	O	|	|	|	|	0.14
29.500	0.00	0.06	0.006	O	|	|	|	|	0.13
29.583	0.00	0.06	0.005	O	|	|	|	|	0.12
29.667	0.00	0.05	0.005	O	|	|	|	|	0.11
29.750	0.00	0.05	0.005	O	|	|	|	|	0.11
29.833	0.00	0.05	0.004	O	|	|	|	|	0.10
29.917	0.00	0.04	0.004	O	|	|	|	|	0.09
30.000	0.00	0.04	0.004	O	|	|	|	|	0.09
30.083	0.00	0.04	0.003	O	|	|	|	|	0.08
30.167	0.00	0.03	0.003	O	|	|	|	|	0.07
30.250	0.00	0.03	0.003	O	|	|	|	|	0.07
30.333	0.00	0.03	0.003	O	|	|	|	|	0.06
30.417	0.00	0.03	0.003	O	|	|	|	|	0.06
30.500	0.00	0.03	0.002	O	|	|	|	|	0.05
30.583	0.00	0.02	0.002	O	|	|	|	|	0.05
30.667	0.00	0.02	0.002	O	|	|	|	|	0.05
30.750	0.00	0.02	0.002	O	|	|	|	|	0.04
30.833	0.00	0.02	0.002	O	|	|	|	|	0.04
30.917	0.00	0.02	0.002	O	|	|	|	|	0.04
31.000	0.00	0.02	0.002	O	|	|	|	|	0.04
31.083	0.00	0.02	0.001	O	|	|	|	|	0.03
31.167	0.00	0.01	0.001	O	|	|	|	|	0.03
31.250	0.00	0.01	0.001	O	|	|	|	|	0.03
31.333	0.00	0.01	0.001	O	|	|	|	|	0.03
31.417	0.00	0.01	0.001	O	|	|	|	|	0.02
31.500	0.00	0.01	0.001	O	|	|	|	|	0.02
31.583	0.00	0.01	0.001	O	|	|	|	|	0.02
31.667	0.00	0.01	0.001	O	|	|	|	|	0.02
31.750	0.00	0.01	0.001	O	|	|	|	|	0.02
31.833	0.00	0.01	0.001	O	|	|	|	|	0.02
31.917	0.00	0.01	0.001	O	|	|	|	|	0.02
32.000	0.00	0.01	0.001	O	|	|	|	|	0.01
32.083	0.00	0.01	0.001	O	|	|	|	|	0.01
32.167	0.00	0.01	0.001	O	|	|	|	|	0.01
32.250	0.00	0.01	0.001	O	|	|	|	|	0.01
32.333	0.00	0.01	0.000	O	|	|	|	|	0.01
32.417	0.00	0.00	0.000	O	|	|	|	|	0.01
32.500	0.00	0.00	0.000	O	|	|	|	|	0.01
32.583	0.00	0.00	0.000	O	|	|	|	|	0.01
32.667	0.00	0.00	0.000	O	|	|	|	|	0.01
32.750	0.00	0.00	0.000	O	|	|	|	|	0.01
32.833	0.00	0.00	0.000	O	|	|	|	|	0.01
32.917	0.00	0.00	0.000	O	|	|	|	|	0.01
33.000	0.00	0.00	0.000	O	|	|	|	|	0.01
33.083	0.00	0.00	0.000	O	|	|	|	|	0.01
33.167	0.00	0.00	0.000	O	|	|	|	|	0.01
33.250	0.00	0.00	0.000	O	|	|	|	|	0.00
33.333	0.00	0.00	0.000	O	|	|	|	|	0.00
33.417	0.00	0.00	0.000	O	|	|	|	|	0.00
33.500	0.00	0.00	0.000	O	|	|	|	|	0.00
33.583	0.00	0.00	0.000	O	|	|	|	|	0.00
33.667	0.00	0.00	0.000	O	|	|	|	|	0.00
33.750	0.00	0.00	0.000	O	|	|	|	|	0.00
33.833	0.00	0.00	0.000	O	|	|	|	|	0.00
33.917	0.00	0.00	0.000	O	|	|	|	|	0.00
34.000	0.00	0.00	0.000	O	|	|	|	|	0.00
34.083	0.00	0.00	0.000	O	|	|	|	|	0.00
34.167	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 410
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.407 (CFS)
Total volume = 0.648 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 01/06/23

TEMESCAL CANYON SELF STORAGE - RIVERSIDE COUNTY
PROPOSED CONDITION - NODES 140-161
MITIGATION ANALYSIS
1-HOUR - 10-YEAR

Program License Serial Number 6310

********** HYDROGRAPH INFORMATION **********

From study/file name: 2216PD10110.rte
**********HYDROGRAPH DATA**********
Number of intervals = 13
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 13.804 (CFS)
Total volume = 0.396 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

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Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 13
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.250	0.011	0.118	0.011	0.011
0.500	0.046	0.167	0.045	0.047
0.600	0.066	0.183	0.065	0.067
1.000	0.153	0.236	0.152	0.154
1.500	0.263	0.289	0.262	0.264
1.810	0.330	0.318	0.329	0.331
2.000	0.373	0.334	0.372	0.374
2.500	0.483	0.374	0.482	0.484
3.000	0.590	0.409	0.589	0.591
3.500	0.694	0.442	0.692	0.696
3.900	0.772	0.467	0.770	0.774
4.000	0.793	0.535	0.791	0.795
4.500	0.882	2.336	0.874	0.890
4.900	0.933	4.305	0.918	0.948
5.000	0.947	4.495	0.932	0.962

5.500	0.973	5.338	0.955	0.991
5.600	0.979	5.490	0.960	0.998

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 3.5 6.90 10.35 13.80	Depth (Ft.)
0.083	1.73	0.06	0.006	O I | | | |	0.13
0.167	2.36	0.13	0.019	O I | | | |	0.31
0.250	2.76	0.15	0.036	O I | | | |	0.43
0.333	2.89	0.17	0.054	O I | | | |	0.54
0.417	3.03	0.19	0.073	O I| | | |	0.63
0.500	3.42	0.20	0.094	O I| | | |	0.73
0.583	4.25	0.22	0.119	O |I | | |	0.84
0.667	5.07	0.23	0.150	O | I | | |	0.98
0.750	7.05	0.25	0.190	O | |I | |	1.17
0.833	13.80	0.29	0.260	O | | | I|	1.48
0.917	7.40	0.32	0.331	O | |I | |	1.81
1.000	3.07	0.33	0.364	O I| | | |	1.96
1.083	0.66	0.33	0.375	OI | | | |	2.01
1.167	0.00	0.33	0.375	O | | | |	2.01
1.250	0.00	0.33	0.373	O | | | |	2.00
1.333	0.00	0.33	0.370	O | | | |	1.99
1.417	0.00	0.33	0.368	O | | | |	1.98
1.500	0.00	0.33	0.366	O | | | |	1.97
1.583	0.00	0.33	0.363	O | | | |	1.96
1.667	0.00	0.33	0.361	O | | | |	1.95
1.750	0.00	0.33	0.359	O | | | |	1.94
1.833	0.00	0.33	0.357	O | | | |	1.93
1.917	0.00	0.33	0.354	O | | | |	1.92
2.000	0.00	0.33	0.352	O | | | |	1.91
2.083	0.00	0.33	0.350	O | | | |	1.90
2.167	0.00	0.32	0.348	O | | | |	1.89
2.250	0.00	0.32	0.345	O | | | |	1.88
2.333	0.00	0.32	0.343	O | | | |	1.87
2.417	0.00	0.32	0.341	O | | | |	1.86
2.500	0.00	0.32	0.339	O | | | |	1.85
2.583	0.00	0.32	0.337	O | | | |	1.84
2.667	0.00	0.32	0.334	O | | | |	1.83
2.750	0.00	0.32	0.332	O | | | |	1.82
2.833	0.00	0.32	0.330	O | | | |	1.81
2.917	0.00	0.32	0.328	O | | | |	1.80
3.000	0.00	0.32	0.326	O | | | |	1.79
3.083	0.00	0.32	0.323	O | | | |	1.78
3.167	0.00	0.31	0.321	O | | | |	1.77
3.250	0.00	0.31	0.319	O | | | |	1.76
3.333	0.00	0.31	0.317	O | | | |	1.75
3.417	0.00	0.31	0.315	O | | | |	1.74
3.500	0.00	0.31	0.313	O | | | |	1.73
3.583	0.00	0.31	0.311	O | | | |	1.72
3.667	0.00	0.31	0.308	O | | | |	1.71
3.750	0.00	0.31	0.306	O | | | |	1.70
3.833	0.00	0.31	0.304	O | | | |	1.69
3.917	0.00	0.31	0.302	O | | | |	1.68
4.000	0.00	0.31	0.300	O | | | |	1.67
4.083	0.00	0.30	0.298	O | | | |	1.66
4.167	0.00	0.30	0.296	O | | | |	1.65
4.250	0.00	0.30	0.294	O | | | |	1.64
4.333	0.00	0.30	0.292	O | | | |	1.63
4.417	0.00	0.30	0.290	O | | | |	1.62
4.500	0.00	0.30	0.287	O | | | |	1.61
4.583	0.00	0.30	0.285	O | | | |	1.60
4.667	0.00	0.30	0.283	O | | | |	1.59
4.750	0.00	0.30	0.281	O | | | |	1.58
4.833	0.00	0.30	0.279	O | | | |	1.58
4.917	0.00	0.30	0.277	O | | | |	1.57
5.000	0.00	0.29	0.275	O | | | |	1.56
5.083	0.00	0.29	0.273	O | | | |	1.55
5.167	0.00	0.29	0.271	O | | | |	1.54

5.250	0.00	0.29	0.269	O	|	|	|	1.53
5.333	0.00	0.29	0.267	O	|	|	|	1.52
5.417	0.00	0.29	0.265	O	|	|	|	1.51
5.500	0.00	0.29	0.263	O	|	|	|	1.50
5.583	0.00	0.29	0.261	O	|	|	|	1.49
5.667	0.00	0.29	0.259	O	|	|	|	1.48
5.750	0.00	0.29	0.257	O	|	|	|	1.47
5.833	0.00	0.29	0.255	O	|	|	|	1.46
5.917	0.00	0.28	0.253	O	|	|	|	1.46
6.000	0.00	0.28	0.251	O	|	|	|	1.45
6.083	0.00	0.28	0.249	O	|	|	|	1.44
6.167	0.00	0.28	0.247	O	|	|	|	1.43
6.250	0.00	0.28	0.246	O	|	|	|	1.42
6.333	0.00	0.28	0.244	O	|	|	|	1.41
6.417	0.00	0.28	0.242	O	|	|	|	1.40
6.500	0.00	0.28	0.240	O	|	|	|	1.39
6.583	0.00	0.28	0.238	O	|	|	|	1.39
6.667	0.00	0.28	0.236	O	|	|	|	1.38
6.750	0.00	0.28	0.234	O	|	|	|	1.37
6.833	0.00	0.27	0.232	O	|	|	|	1.36
6.917	0.00	0.27	0.230	O	|	|	|	1.35
7.000	0.00	0.27	0.228	O	|	|	|	1.34
7.083	0.00	0.27	0.226	O	|	|	|	1.33
7.167	0.00	0.27	0.225	O	|	|	|	1.33
7.250	0.00	0.27	0.223	O	|	|	|	1.32
7.333	0.00	0.27	0.221	O	|	|	|	1.31
7.417	0.00	0.27	0.219	O	|	|	|	1.30
7.500	0.00	0.27	0.217	O	|	|	|	1.29
7.583	0.00	0.27	0.215	O	|	|	|	1.28
7.667	0.00	0.27	0.214	O	|	|	|	1.28
7.750	0.00	0.26	0.212	O	|	|	|	1.27
7.833	0.00	0.26	0.210	O	|	|	|	1.26
7.917	0.00	0.26	0.208	O	|	|	|	1.25
8.000	0.00	0.26	0.206	O	|	|	|	1.24
8.083	0.00	0.26	0.205	O	|	|	|	1.23
8.167	0.00	0.26	0.203	O	|	|	|	1.23
8.250	0.00	0.26	0.201	O	|	|	|	1.22
8.333	0.00	0.26	0.199	O	|	|	|	1.21
8.417	0.00	0.26	0.197	O	|	|	|	1.20
8.500	0.00	0.26	0.196	O	|	|	|	1.19
8.583	0.00	0.26	0.194	O	|	|	|	1.19
8.667	0.00	0.25	0.192	O	|	|	|	1.18
8.750	0.00	0.25	0.190	O	|	|	|	1.17
8.833	0.00	0.25	0.189	O	|	|	|	1.16
8.917	0.00	0.25	0.187	O	|	|	|	1.15
9.000	0.00	0.25	0.185	O	|	|	|	1.15
9.083	0.00	0.25	0.183	O	|	|	|	1.14
9.167	0.00	0.25	0.182	O	|	|	|	1.13
9.250	0.00	0.25	0.180	O	|	|	|	1.12
9.333	0.00	0.25	0.178	O	|	|	|	1.11
9.417	0.00	0.25	0.177	O	|	|	|	1.11
9.500	0.00	0.25	0.175	O	|	|	|	1.10
9.583	0.00	0.25	0.173	O	|	|	|	1.09
9.667	0.00	0.24	0.171	O	|	|	|	1.08
9.750	0.00	0.24	0.170	O	|	|	|	1.08
9.833	0.00	0.24	0.168	O	|	|	|	1.07
9.917	0.00	0.24	0.166	O	|	|	|	1.06
10.000	0.00	0.24	0.165	O	|	|	|	1.05
10.083	0.00	0.24	0.163	O	|	|	|	1.05
10.167	0.00	0.24	0.161	O	|	|	|	1.04
10.250	0.00	0.24	0.160	O	|	|	|	1.03
10.333	0.00	0.24	0.158	O	|	|	|	1.02
10.417	0.00	0.24	0.156	O	|	|	|	1.02
10.500	0.00	0.24	0.155	O	|	|	|	1.01
10.583	0.00	0.24	0.153	O	|	|	|	1.00
10.667	0.00	0.24	0.152	O	|	|	|	0.99
10.750	0.00	0.23	0.150	O	|	|	|	0.99
10.833	0.00	0.23	0.148	O	|	|	|	0.98
10.917	0.00	0.23	0.147	O	|	|	|	0.97
11.000	0.00	0.23	0.145	O	|	|	|	0.96
11.083	0.00	0.23	0.144	O	|	|	|	0.96
11.167	0.00	0.23	0.142	O	|	|	|	0.95

11.250	0.00	0.23	0.140	O	|	|	|	0.94
11.333	0.00	0.23	0.139	O	|	|	|	0.93
11.417	0.00	0.23	0.137	O	|	|	|	0.93
11.500	0.00	0.23	0.136	O	|	|	|	0.92
11.583	0.00	0.22	0.134	O	|	|	|	0.91
11.667	0.00	0.22	0.133	O	|	|	|	0.91
11.750	0.00	0.22	0.131	O	|	|	|	0.90
11.833	0.00	0.22	0.130	O	|	|	|	0.89
11.917	0.00	0.22	0.128	O	|	|	|	0.89
12.000	0.00	0.22	0.127	O	|	|	|	0.88
12.083	0.00	0.22	0.125	O	|	|	|	0.87
12.167	0.00	0.22	0.124	O	|	|	|	0.86
12.250	0.00	0.22	0.122	O	|	|	|	0.86
12.333	0.00	0.22	0.121	O	|	|	|	0.85
12.417	0.00	0.22	0.119	O	|	|	|	0.84
12.500	0.00	0.21	0.118	O	|	|	|	0.84
12.583	0.00	0.21	0.116	O	|	|	|	0.83
12.667	0.00	0.21	0.115	O	|	|	|	0.82
12.750	0.00	0.21	0.113	O	|	|	|	0.82
12.833	0.00	0.21	0.112	O	|	|	|	0.81
12.917	0.00	0.21	0.110	O	|	|	|	0.80
13.000	0.00	0.21	0.109	O	|	|	|	0.80
13.083	0.00	0.21	0.107	O	|	|	|	0.79
13.167	0.00	0.21	0.106	O	|	|	|	0.78
13.250	0.00	0.21	0.105	O	|	|	|	0.78
13.333	0.00	0.21	0.103	O	|	|	|	0.77
13.417	0.00	0.20	0.102	O	|	|	|	0.76
13.500	0.00	0.20	0.100	O	|	|	|	0.76
13.583	0.00	0.20	0.099	O	|	|	|	0.75
13.667	0.00	0.20	0.097	O	|	|	|	0.74
13.750	0.00	0.20	0.096	O	|	|	|	0.74
13.833	0.00	0.20	0.095	O	|	|	|	0.73
13.917	0.00	0.20	0.093	O	|	|	|	0.73
14.000	0.00	0.20	0.092	O	|	|	|	0.72
14.083	0.00	0.20	0.091	O	|	|	|	0.71
14.167	0.00	0.20	0.089	O	|	|	|	0.71
14.250	0.00	0.20	0.088	O	|	|	|	0.70
14.333	0.00	0.20	0.087	O	|	|	|	0.69
14.417	0.00	0.19	0.085	O	|	|	|	0.69
14.500	0.00	0.19	0.084	O	|	|	|	0.68
14.583	0.00	0.19	0.083	O	|	|	|	0.68
14.667	0.00	0.19	0.081	O	|	|	|	0.67
14.750	0.00	0.19	0.080	O	|	|	|	0.66
14.833	0.00	0.19	0.079	O	|	|	|	0.66
14.917	0.00	0.19	0.077	O	|	|	|	0.65
15.000	0.00	0.19	0.076	O	|	|	|	0.65
15.083	0.00	0.19	0.075	O	|	|	|	0.64
15.167	0.00	0.19	0.073	O	|	|	|	0.63
15.250	0.00	0.19	0.072	O	|	|	|	0.63
15.333	0.00	0.19	0.071	O	|	|	|	0.62
15.417	0.00	0.19	0.069	O	|	|	|	0.62
15.500	0.00	0.18	0.068	O	|	|	|	0.61
15.583	0.00	0.18	0.067	O	|	|	|	0.60
15.667	0.00	0.18	0.066	O	|	|	|	0.60
15.750	0.00	0.18	0.064	O	|	|	|	0.59
15.833	0.00	0.18	0.063	O	|	|	|	0.59
15.917	0.00	0.18	0.062	O	|	|	|	0.58
16.000	0.00	0.18	0.061	O	|	|	|	0.57
16.083	0.00	0.18	0.059	O	|	|	|	0.57
16.167	0.00	0.18	0.058	O	|	|	|	0.56
16.250	0.00	0.18	0.057	O	|	|	|	0.56
16.333	0.00	0.17	0.056	O	|	|	|	0.55
16.417	0.00	0.17	0.055	O	|	|	|	0.54
16.500	0.00	0.17	0.053	O	|	|	|	0.54
16.583	0.00	0.17	0.052	O	|	|	|	0.53
16.667	0.00	0.17	0.051	O	|	|	|	0.53
16.750	0.00	0.17	0.050	O	|	|	|	0.52
16.833	0.00	0.17	0.049	O	|	|	|	0.51
16.917	0.00	0.17	0.048	O	|	|	|	0.51
17.000	0.00	0.17	0.046	O	|	|	|	0.50
17.083	0.00	0.17	0.045	O	|	|	|	0.49
17.167	0.00	0.16	0.044	O	|	|	|	0.49

17.250	0.00	0.16	0.043	O	|	|	|	0.48
17.333	0.00	0.16	0.042	O	|	|	|	0.47
17.417	0.00	0.16	0.041	O	|	|	|	0.46
17.500	0.00	0.16	0.040	O	|	|	|	0.45
17.583	0.00	0.16	0.039	O	|	|	|	0.45
17.667	0.00	0.16	0.038	O	|	|	|	0.44
17.750	0.00	0.15	0.036	O	|	|	|	0.43
17.833	0.00	0.15	0.035	O	|	|	|	0.42
17.917	0.00	0.15	0.034	O	|	|	|	0.42
18.000	0.00	0.15	0.033	O	|	|	|	0.41
18.083	0.00	0.15	0.032	O	|	|	|	0.40
18.167	0.00	0.15	0.031	O	|	|	|	0.40
18.250	0.00	0.15	0.030	O	|	|	|	0.39
18.333	0.00	0.14	0.029	O	|	|	|	0.38
18.417	0.00	0.14	0.028	O	|	|	|	0.37
18.500	0.00	0.14	0.027	O	|	|	|	0.37
18.583	0.00	0.14	0.026	O	|	|	|	0.36
18.667	0.00	0.14	0.025	O	|	|	|	0.35
18.750	0.00	0.14	0.024	O	|	|	|	0.35
18.833	0.00	0.14	0.024	O	|	|	|	0.34
18.917	0.00	0.13	0.023	O	|	|	|	0.33
19.000	0.00	0.13	0.022	O	|	|	|	0.33
19.083	0.00	0.13	0.021	O	|	|	|	0.32
19.167	0.00	0.13	0.020	O	|	|	|	0.31
19.250	0.00	0.13	0.019	O	|	|	|	0.31
19.333	0.00	0.13	0.018	O	|	|	|	0.30
19.417	0.00	0.13	0.017	O	|	|	|	0.29
19.500	0.00	0.13	0.016	O	|	|	|	0.29
19.583	0.00	0.12	0.015	O	|	|	|	0.28
19.667	0.00	0.12	0.015	O	|	|	|	0.28
19.750	0.00	0.12	0.014	O	|	|	|	0.27
19.833	0.00	0.12	0.013	O	|	|	|	0.26
19.917	0.00	0.12	0.012	O	|	|	|	0.26
20.000	0.00	0.12	0.011	O	|	|	|	0.25
20.083	0.00	0.11	0.011	O	|	|	|	0.24
20.167	0.00	0.10	0.010	O	|	|	|	0.22
20.250	0.00	0.10	0.009	O	|	|	|	0.21
20.333	0.00	0.09	0.008	O	|	|	|	0.19
20.417	0.00	0.08	0.008	O	|	|	|	0.18
20.500	0.00	0.08	0.007	O	|	|	|	0.17
20.583	0.00	0.07	0.007	O	|	|	|	0.15
20.667	0.00	0.07	0.006	O	|	|	|	0.14
20.750	0.00	0.06	0.006	O	|	|	|	0.13
20.833	0.00	0.06	0.005	O	|	|	|	0.12
20.917	0.00	0.05	0.005	O	|	|	|	0.11
21.000	0.00	0.05	0.005	O	|	|	|	0.11
21.083	0.00	0.05	0.004	O	|	|	|	0.10
21.167	0.00	0.04	0.004	O	|	|	|	0.09
21.250	0.00	0.04	0.004	O	|	|	|	0.08
21.333	0.00	0.04	0.003	O	|	|	|	0.08
21.417	0.00	0.03	0.003	O	|	|	|	0.07
21.500	0.00	0.03	0.003	O	|	|	|	0.07
21.583	0.00	0.03	0.003	O	|	|	|	0.06
21.667	0.00	0.03	0.003	O	|	|	|	0.06
21.750	0.00	0.03	0.002	O	|	|	|	0.05
21.833	0.00	0.02	0.002	O	|	|	|	0.05
21.917	0.00	0.02	0.002	O	|	|	|	0.05
22.000	0.00	0.02	0.002	O	|	|	|	0.04
22.083	0.00	0.02	0.002	O	|	|	|	0.04
22.167	0.00	0.02	0.002	O	|	|	|	0.04
22.250	0.00	0.02	0.002	O	|	|	|	0.03
22.333	0.00	0.02	0.001	O	|	|	|	0.03
22.417	0.00	0.01	0.001	O	|	|	|	0.03
22.500	0.00	0.01	0.001	O	|	|	|	0.03
22.583	0.00	0.01	0.001	O	|	|	|	0.03
22.667	0.00	0.01	0.001	O	|	|	|	0.02
22.750	0.00	0.01	0.001	O	|	|	|	0.02
22.833	0.00	0.01	0.001	O	|	|	|	0.02
22.917	0.00	0.01	0.001	O	|	|	|	0.02
23.000	0.00	0.01	0.001	O	|	|	|	0.02
23.083	0.00	0.01	0.001	O	|	|	|	0.02
23.167	0.00	0.01	0.001	O	|	|	|	0.02

```
23.250    0.00    0.01      0.001  O       |       |       |       |      0.01
23.333    0.00    0.01      0.001  O       |       |       |       |      0.01
23.417    0.00    0.01      0.001  O       |       |       |       |      0.01
23.500    0.00    0.01      0.001  O       |       |       |       |      0.01
23.583    0.00    0.01      0.000  O       |       |       |       |      0.01
23.667    0.00    0.00      0.000  O       |       |       |       |      0.01
23.750    0.00    0.00      0.000  O       |       |       |       |      0.01
23.833    0.00    0.00      0.000  O       |       |       |       |      0.01
23.917    0.00    0.00      0.000  O       |       |       |       |      0.01
24.000    0.00    0.00      0.000  O       |       |       |       |      0.01
24.083    0.00    0.00      0.000  O       |       |       |       |      0.01
24.167    0.00    0.00      0.000  O       |       |       |       |      0.01
24.250    0.00    0.00      0.000  O       |       |       |       |      0.01
24.333    0.00    0.00      0.000  O       |       |       |       |      0.01
24.417    0.00    0.00      0.000  O       |       |       |       |      0.01
24.500    0.00    0.00      0.000  O       |       |       |       |      0.00
24.583    0.00    0.00      0.000  O       |       |       |       |      0.00
24.667    0.00    0.00      0.000  O       |       |       |       |      0.00
24.750    0.00    0.00      0.000  O       |       |       |       |      0.00
24.833    0.00    0.00      0.000  O       |       |       |       |      0.00
24.917    0.00    0.00      0.000  O       |       |       |       |      0.00
25.000    0.00    0.00      0.000  O       |       |       |       |      0.00
25.083    0.00    0.00      0.000  O       |       |       |       |      0.00
25.167    0.00    0.00      0.000  O       |       |       |       |      0.00
25.250    0.00    0.00      0.000  O       |       |       |       |      0.00
25.333    0.00    0.00      0.000  O       |       |       |       |      0.00
25.417    0.00    0.00      0.000  O       |       |       |       |      0.00

        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =   305
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.335 (CFS)
                      Total volume =       0.396 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

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```
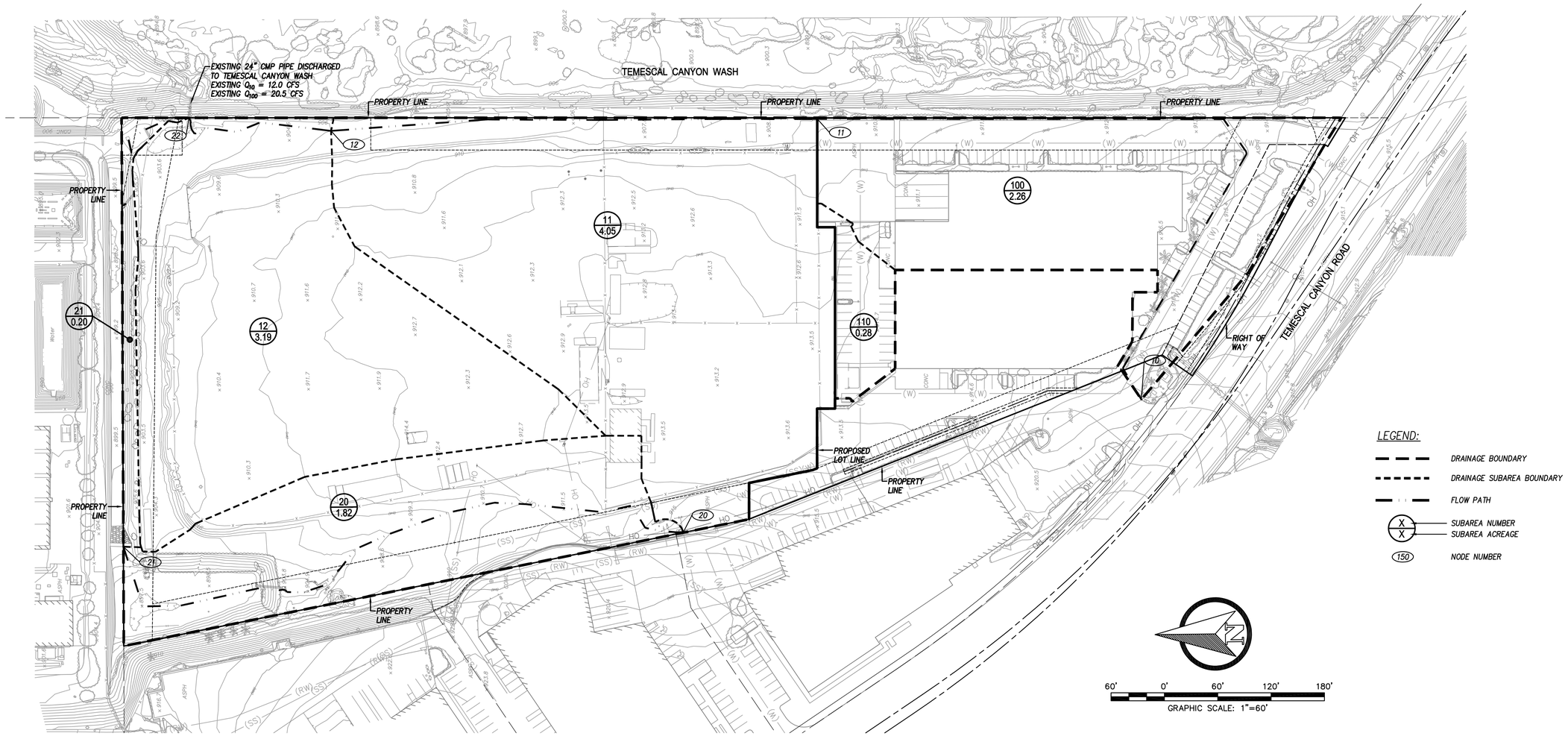

Technical Appendix G

Hydrology Maps



160 S. Old Springs Road
Suite 210
Anaheim Hills, CA 92808
714-685-6860

DRC Engineering, Inc.
Civil Engineering/Land Surveying/Land Planning

GREGORY R. COOKE R.C.E. 39478 DATE

NOT FOR CONSTRUCTION

NO:	REVISION:	DATE:

PROJECT:
PALISADE TEMESCAL CANYON
22740 TEMESCAL CANYON RD.
UNINCORPORATED COUNTY OF RIVERSIDE

DRAWING NAME:
EXISTING HYDROLOGY MAP

ISSUE:	PRELIMINARY
DATE:	2023/1/10
CHECKED: JH	DRAWN: MS
DRAWING FILE:	21143EXHM
PROJECT NO.:	21-143
SHEET NUMBER:	1
OF	1 SHEETS
SCALE:	AS SHOWN

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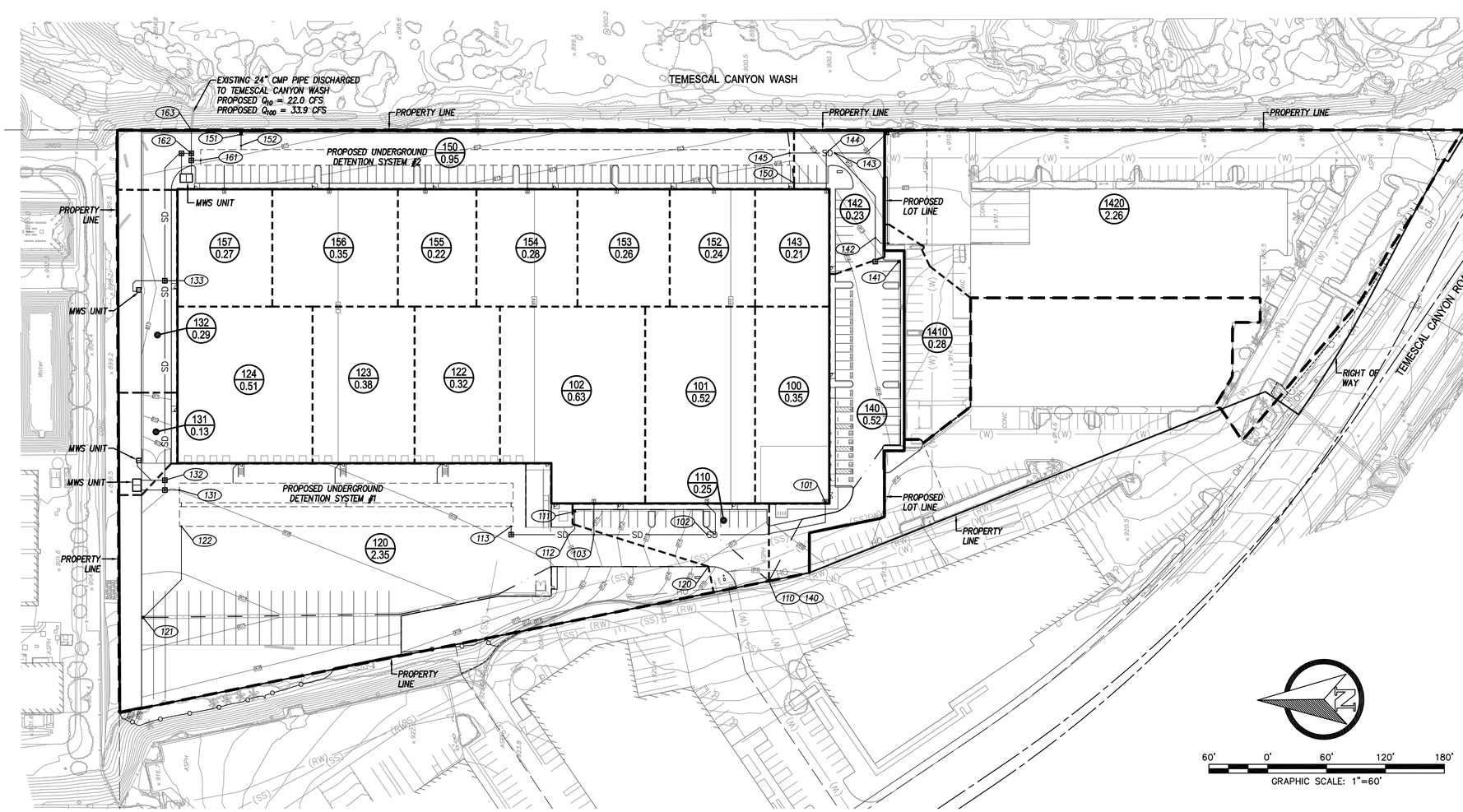

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DRC Engineering, Inc.
Civil Engineering/Land Surveying/Land Planning

GREGORY R. COOKE R.C.E. 39478 DATE

NOT FOR CONSTRUCTION

NO.:	REVISION:	DATE:

PROPOSE HYDROLOGY MAP

PROJECT: PALISADE TEMESCAL CANYON
22740 TEMESCAL CANYON RD.
UNINCORPORATED COUNTY OF RIVERSIDE

DRAWING NAME:

ISSUE:	PRELIMINARY
DATE:	2023/1/10
CHECKED: JH	DRAWN: JH
DRAWING FILE:	21143PRHM
PROJECT NO.:	21-143
SHEET NUMBER:	1
OF	1 SHEETS
SCALE:	AS SHOWN

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