

# Majestic Freeway Business Center (Building 17) (PPT220009) Noise and Vibration Analysis County of Riverside

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# **LIST OF ABBREVIATED TERMS**

(1) Reference

ANSI American National Standards Institute

Calveno California Vehicle Noise

CEQA California Environmental Quality Act
CNEL Community Noise Equivalent Level

dBA A-weighted decibels

EPA Environmental Protection Agency
FHWA Federal Highway Administration
FTA Federal Transit Administration

INCE Institute of Noise Control Engineering

L<sub>eq</sub> Equivalent continuous (average) sound level
L<sub>max</sub> Maximum level measured over the time interval

mph Miles per hour

PPV Peak Particle Velocity

Project Majestic Freeway Business Center (Building 17)

REMEL Reference Energy Mean Emission Level

RMS Root-mean-square VdB Vibration Decibels



# **EXECUTIVE SUMMARY**

Urban Crossroads, Inc. has prepared this noise study to determine the noise exposure and the necessary noise mitigation measures for the proposed Majestic Freeway Business Center (Building 17) development ("Project"). The Project site is located on the northeast corner of Harvill Avenue and America's Tire Drive in the County of Riverside. The Project is proposed to consist of the development of a 268,955 square foot warehouse building. This noise study has been prepared to satisfy applicable County of Riverside noise standards and significance criteria based on Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1)

The results of this Noise and Vibration Analysis are summarized below based on the significance criteria in Section 4 of this report consistent with Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1) Table ES-1 shows the findings of significance for each potential noise and/or vibration impact under CEQA before and after any required mitigation measures.

**TABLE ES-1: SUMMARY OF CEQA SIGNIFICANCE FINDINGS** 

Analysis	Report	Significance Findings		
Analysis	Section	Unmitigated	Mitigated	
Off-Site Traffic Noise	7	Less Than Significant	-	
Operational Noise	9	Less Than Significant	-	
Construction Noise		Less Than Significant	-	
Nighttime Concrete Pour	10	Less Than Significant	-	
Construction Vibration		Less Than Significant	-	



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# 1 INTRODUCTION

This noise analysis has been completed to determine the noise impacts associated with the development of the proposed Majestic Freeway Business Center (Building 17) ("Project"). This noise study briefly describes the proposed Project, provides information regarding noise fundamentals, sets out the local regulatory setting, presents the study methods and procedures for transportation related CNEL traffic noise analysis, and evaluates the future exterior noise environment. In addition, this study includes an analysis of the potential Project-related long-term stationary-source operational noise and short-term construction noise and vibration impacts.

# 1.1 SITE LOCATION

The proposed Project is located on the northeast corner of Harvill Avenue and America's Tire Drive County of Riverside, as shown on Exhibit 1-A.

# 1.2 PROJECT DESCRIPTION

A preliminary site plan for the proposed Project is shown on Exhibit 1-B. The Project is proposed to consist of the development of a 268,955 square foot warehouse building. The on-site Project-related noise sources are expected to include: loading dock activity, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements. This noise analysis is intended to describe the noise level impacts associated with the expected typical operational activities at the Project site.

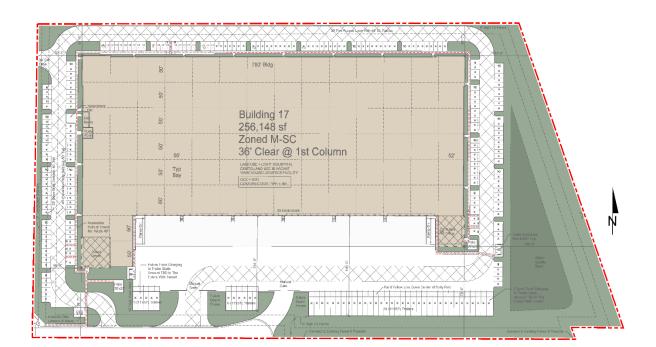


Site Val Verde

**EXHIBIT 1-A: LOCATION MAP** 



# **EXHIBIT 1-B: SITE PLAN**





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# **2 FUNDAMENTALS**

Noise is simply defined as "unwanted sound." Sound becomes unwanted when it interferes with normal activities, when it causes actual physical harm or when it has adverse effects on health. Noise is measured on a logarithmic scale of sound pressure level known as a decibel (dB). Aweighted decibels (dBA) approximate the subjective response of the human ear to broad frequency noise source by discriminating against very low and very high frequencies of the audible spectrum. They are adjusted to reflect only those frequencies which are audible to the human ear. Exhibit 2-A presents a summary of the typical noise levels and their subjective loudness and effects that are described in more detail below.

**EXHIBIT 2-A: TYPICAL NOISE LEVELS** 

COMMON OUTDOOR ACTIVITIES	COMMON INDOOR ACTIVITIES	A - WEIGHTED SOUND LEVEL dBA	SUBJECTIVE LOUDNESS	EFFECTS OF NOISE	
THRESHOLD OF PAIN		140			
NEAR JET ENGINE		130	INTOLERABLE OR		
		120	DEAFENING	HEARING LOSS	
JET FLY-OVER AT 300m (1000 ft)	ROCK BAND	110			
LOUD AUTO HORN		100			
GAS LAWN MOWER AT 1m (3 ft)		90	VERY NOISY		
DIESEL TRUCK AT 15m (50 ft), at 80 km/hr (50 mph)	FOOD BLENDER AT 1m (3 ft)	80	VERT NOIST		
NOISY URBAN AREA, DAYTIME	VACUUM CLEANER AT 3m (10 ft)	70	LOUD	SPEECH INTERFERENCE	
HEAVY TRAFFIC AT 90m (300 ft)	NORMAL SPEECH AT 1m (3 ft)	60	1000	INTERFERENCE	
QUIET URBAN DAYTIME	LARGE BUSINESS OFFICE	50	MODERATE	CLEED	
QUIET URBAN NIGHTTIME	THEATER, LARGE CONFERENCE ROOM (BACKGROUND)	40		SLEEP DISTURBANCE	
QUIET SUBURBAN NIGHTTIME	LIBRARY	30			
QUIET RURAL NIGHTTIME	BEDROOM AT NIGHT, CONCERT HALL (BACKGROUND)	20	FAINT		
	BROADCAST/RECORDING STUDIO	10	VERY FAINT	NO EFFECT	
LOWEST THRESHOLD OF HUMAN HEARING	LOWEST THRESHOLD OF HUMAN HEARING	0	VERT FAINT		

Source: Environmental Protection Agency Office of Noise Abatement and Control, Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety (EPA/ONAC 550/9-74-004) March 1974.

# 2.1 RANGE OF NOISE

Since the range of intensities that the human ear can detect is so large, the scale frequently used to measure intensity is a scale based on multiples of 10, the logarithmic scale. The scale for measuring intensity is the decibel scale. Each interval of 10 decibels indicates a sound energy ten times greater than before, which is perceived by the human ear as being roughly twice as loud. (2) The most common sounds vary between 40 dBA (very quiet) to 100 dBA (very loud). Normal conversation at three feet is roughly at 60 dBA, while loud jet engine noises equate to 110 dBA



at approximately 1,000 feet, which can cause serious discomfort. (3) Another important aspect of noise is the duration of the sound and the way it is described and distributed in time.

### 2.2 Noise Descriptors

Environmental noise descriptors are generally based on averages, rather than instantaneous, noise levels. The most used metric is the equivalent level ( $L_{eq}$ ). Equivalent sound levels are not measured directly but are calculated from sound pressure levels typically measured in Aweighted decibels (dBA). The equivalent sound level ( $L_{eq}$ ) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period and is commonly used to describe the "average" noise levels within the environment.

Peak hour or average noise levels, while useful, do not completely describe a given noise environment. Noise levels lower than peak hour may be disturbing if they occur during times when quiet is most desirable, namely evening and nighttime (sleeping) hours. To account for this, the Community Noise Equivalent Level (CNEL), representing a composite 24-hour noise level is utilized. The CNEL is the weighted average of the intensity of a sound, with corrections for time of day, and averaged over 24 hours. The time-of-day corrections require the addition of 5 decibels to dBA L<sub>eq</sub> sound levels in the evening from 7:00 p.m. to 10:00 p.m., and the addition of 10 decibels to dBA L<sub>eq</sub> sound levels at night between 10:00 p.m. and 7:00 a.m. These additions are made to account for the noise sensitive time periods during the evening and night hours when noise can become more intrusive. CNEL does not represent the actual sound level heard at any time, but rather represents the total sound exposure. The County of Riverside relies on the 24-hour CNEL level to assess land use compatibility with transportation related noise sources.

### 2.3 SOUND PROPAGATION

When sound propagates over a distance, it changes in level and frequency content. The way noise reduces with distance depends on the following factors.

# 2.3.1 GEOMETRIC SPREADING

Sound from a localized source (i.e., a stationary point source) propagates uniformly outward in a spherical pattern. The sound level attenuates (or decreases) at a rate of 6 dB for each doubling of distance from a point source. Highways consist of several localized noise sources on a defined path and hence can be treated as a line source, which approximates the effect of several point sources. Noise from a line source propagates outward in a cylindrical pattern, often referred to as cylindrical spreading. Sound levels attenuate at a rate of 3 dB for each doubling of distance from a line source. (2)

### 2.3.2 GROUND ABSORPTION

The propagation path of noise from a highway to a receiver is usually very close to the ground. Noise attenuation from ground absorption and reflective wave canceling adds to the attenuation associated with geometric spreading. Traditionally, the excess attenuation has also been expressed in terms of attenuation per doubling of distance. This approximation is usually



sufficiently accurate for distances of less than 200 ft. For acoustically hard sites (i.e., sites with a reflective surface between the source and the receiver, such as a parking lot or body of water), no excess ground attenuation is assumed. For acoustically absorptive or soft sites (i.e., those sites with an absorptive ground surface between the source and the receiver such as soft dirt, grass, or scattered bushes and trees), an excess ground attenuation value of 1.5 dB per doubling of distance is normally assumed. When added to the cylindrical spreading, the excess ground attenuation results in an overall drop-off rate of 4.5 dB per doubling of distance from a line source. (4)

### 2.3.3 ATMOSPHERIC EFFECTS

Receivers located downwind from a source can be exposed to increased noise levels relative to calm conditions, whereas locations upwind can have lowered noise levels. Sound levels can be increased at large distances (e.g., more than 500 feet) due to atmospheric temperature inversion (i.e., increasing temperature with elevation). Other factors such as air temperature, humidity, and turbulence can also have significant effects. (2)

### 2.3.4 SHIELDING

A large object or barrier in the path between a noise source and a receiver can substantially attenuate noise levels at the receiver. The amount of attenuation provided by shielding depends on the size of the object and the frequency content of the noise source. Shielding by trees and other such vegetation typically only has an "out of sight, out of mind" effect. That is, the perception of noise impact tends to decrease when vegetation blocks the line-of-sight to nearby residents. However, for vegetation to provide a substantial, or even noticeable, noise reduction, the vegetation area must be at least 15 feet in height, 100 feet wide and dense enough to completely obstruct the line-of-sight between the source and the receiver. This size of vegetation may provide up to 5 dBA of noise reduction. The Federal Highway Administration (FHWA) does not consider the planting of vegetation to be a noise abatement measure. (5)

### 2.4 Noise Control

Noise control is the process of obtaining an acceptable noise environment for an observation point or receiver by controlling the noise source, transmission path, receiver, or all three. This concept is known as the source-path-receiver concept. In general, noise control measures can be applied to these three elements.

# 2.5 Noise Barrier Attenuation

Effective noise barriers can reduce noise levels by 10 to 15 dBA, cutting the loudness of traffic noise in half. A noise barrier is most effective when placed close to the noise source or receiver. Noise barriers, however, do have limitations. For a noise barrier to work, it must block the line-of-sight path of sound from the noise source.



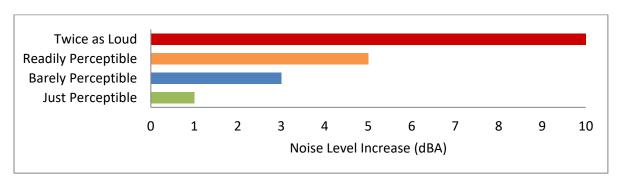
# 2.6 LAND USE COMPATIBILITY WITH NOISE

Some land uses are more tolerant of noise than others. For example, schools, hospitals, churches, and residences are more sensitive to noise intrusion than are commercial or industrial developments and related activities. As ambient noise levels affect the perceived amenity or livability of a development, so too can the mismanagement of noise impacts impair the economic health and growth potential of a community by reducing the area's desirability as a place to live, shop and work. For this reason, land use compatibility with the noise environment is an important consideration in the planning and design process. The FHWA encourages State and Local government to regulate land development in such a way that noise-sensitive land uses are either prohibited from being located adjacent to a highway, or that the developments are planned, designed, and constructed in such a way that noise impacts are minimized. (6)

# 2.7 COMMUNITY RESPONSE TO NOISE

Approximately sixteen percent of the population has a very low tolerance for noise and will object to any noise not of their making. Consequently, even in the quietest environment, some complaints may occur. Twenty to thirty percent of the population will not complain even in very severe noise environments. (7 pp. 8-6) Thus, a variety of reactions can be expected from people exposed to any given noise environment.

Surveys have shown that community response to noise varies from no reaction to vigorous action for newly introduced noises averaging from 10 dB below existing to 25 dB above existing. (8) According to research originally published in the Noise Effects Handbook (7), the percentage of high annoyance ranges from approximately 0 percent at 45 dB or less, 10 percent are highly annoyed around 60 dB, and increases rapidly to approximately 70 percent being highly annoyed at approximately 85 dB or greater. Despite this variability in behavior on an individual level, the population can be expected to exhibit the following responses to changes in noise levels as shown on Exhibit 2-B. A change of 3 dBA is considered barely perceptible, and changes of 5 dBA are considered readily perceptible. (4)



**EXHIBIT 2-B: NOISE LEVEL INCREASE PERCEPTION** 

# 2.8 VIBRATION

Per the Federal Transit Administration (FTA) *Transit Noise Impact and Vibration Impact Assessment Manual* (8), vibration is the periodic oscillation of a medium or object. The rumbling sound caused by the vibration of room surfaces is called structure-borne noise. Sources of ground-borne vibrations include natural phenomena (e.g., earthquakes, volcanic eruptions, sea waves, landslides) or human-made causes (e.g., explosions, machinery, traffic, trains, construction equipment). Vibration sources may be continuous, such as factory machinery, or transient, such as explosions. As is the case with airborne sound, ground-borne vibrations may be described by amplitude and frequency.

There are several different methods that are used to quantify vibration. The peak particle velocity (PPV) is defined as the maximum instantaneous peak of the vibration signal. The PPV is most frequently used to describe vibration impacts to buildings but is not always suitable for evaluating human response (annoyance) because it takes some time for the human body to respond to vibration signals. Instead, the human body responds to average vibration amplitude often described as the root mean square (RMS). The RMS amplitude is defined as the average of the squared amplitude of the signal and is most frequently used to describe the effect of vibration on the human body. Decibel notation (VdB) is commonly used to measure RMS. Decibel notation (VdB) serves to reduce the range of numbers used to describe human response to vibration. Typically, ground-borne vibration generated by man-made activities attenuates rapidly with distance from the source of the vibration. Sensitive receivers for vibration include structures (especially older masonry structures), people (especially residents, the elderly, and sick), and vibration-sensitive equipment and/or activities.

The background vibration-velocity level in residential areas is generally 50 VdB. Ground-borne vibration is normally perceptible to humans at approximately 65 VdB. For most people, a vibration-velocity level of 75 VdB is the approximate dividing line between barely perceptible and distinctly perceptible levels. Typical outdoor sources of perceptible ground-borne vibration are construction equipment, steel-wheeled trains, and traffic on rough roads. If a roadway is smooth, the ground-borne vibration is rarely perceptible. The range of interest is from approximately 50 VdB, which is the typical background vibration-velocity level, to 100 VdB, which is the general threshold where minor damage can occur in fragile buildings. Exhibit 2-C illustrates common vibration sources and the human and structural response to ground-borne vibration.



Velocity Typical Sources Level\* (50 ft from source) Human/Structural Response 100 Threshold, minor cosmetic damage Blasting from construction projects fragile buildings Bulldozers and other heavy tracked construction equipment Difficulty with tasks such as 90 reading a VDT screen Commuter rail, upper range 80 Residential annoyance, infrequent Rapid transit, upper range events (e.g. commuter rail) Commuter rail, typical Residential annoyance, frequent Bus or truck over bump events (e.g. rapid transit) Rapid transit, typical Limit for vibration sensitive equipment. Approx. threshold for Bus or truck, typical human perception of vibration 60 Typical background vibration 50

**EXHIBIT 2-C: TYPICAL LEVELS OF GROUND-BORNE VIBRATION** 

\* RMS Vibration Velocity Level in VdB relative to 10-6 inches/second

Source: Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual.



# 3 REGULATORY SETTING

To limit population exposure to physically and/or psychologically damaging as well as intrusive noise levels, the federal government, the State of California, various county governments, and most municipalities in the state have established standards and ordinances to control noise. In most areas, automobile and truck traffic is the major source of environmental noise. Traffic activity generally produces an average sound level that remains constant with time. Air and rail traffic, and commercial and industrial activities are also major sources of noise in some areas. Federal, state, and local agencies regulate different aspects of environmental noise. Federal and state agencies generally set noise standards for mobile sources such as aircraft and motor vehicles, while regulation of stationary sources is left to local agencies.

# 3.1 STATE OF CALIFORNIA NOISE REQUIREMENTS

The State of California regulates freeway noise, sets standards for sound transmission, provides occupational noise control criteria, identifies noise standards, and provides guidance for local land use compatibility. State law requires that each county and city adopt a General Plan that includes a Noise Element which is to be prepared per guidelines adopted by the Governor's Office of Planning and Research (OPR). (9) The purpose of the Noise Element is to *limit the exposure of the community to excessive noise levels*. In addition, the California Environmental Quality Act (CEQA) requires that all known environmental effects of a project be analyzed, including environmental noise impacts.

# 3.2 COUNTY OF RIVERSIDE GENERAL PLAN NOISE ELEMENT

The County of Riverside has adopted a Noise Element of the General Plan to control and abate environmental noise, and to protect the citizens of the County of Riverside from excessive exposure to noise. (10) The Noise Element specifies the maximum allowable exterior noise levels for new developments impacted by transportation noise sources such as arterial roads, freeways, airports, and railroads. In addition, the Noise Element identifies several polices to minimize the impacts of excessive noise levels throughout the community and establishes noise level requirements for all land uses. To protect County of Riverside residents from excessive noise, the Noise Element contains the following policies related to the Project:

- N 1.1 Protect noise-sensitive land uses from high levels of noise by restricting noise-producing land uses from these areas. If the noise-producing land use cannot be relocated, then noise buffers such as setbacks, landscaping, or block walls shall be used.
- N 1.3 Consider the following uses noise-sensitive and discourage these uses in areas in excess of 65 CNEL:
  - Schools
  - Hospitals
  - Rest Homes
  - Long Term Care Facilities
  - Mental Care Facilities
  - Residential Uses
  - Libraries



- Passive Recreation Uses
- Places of Worship
- N 1.5 Prevent and mitigate the adverse impacts of excessive noise exposure on the residents, employees, visitors, and noise-sensitive uses of Riverside County.
- N 4.1 Prohibit facility-related noise, received by any sensitive use, from exceeding the following worst-case noise levels:
  - a. 45 dBA 9-minute L<sub>eq</sub> between 10:00 p.m. and 7:00 a.m.;
  - b. 65 dBA 9-minute L<sub>eq</sub> between 7:00 a.m. and 10:00 p.m.
- N 13.1 Minimize the impacts of construction noise on adjacent uses within acceptable standards.
- N 13.2 Ensure that construction activities are regulated to establish hours of operation in order to prevent and/or mitigate the generation of excessive or adverse impacts on surrounding areas.
- N 13.3 Condition subdivision approval adjacent to developed/occupied noise-sensitive land uses (see policy N 1.3) by requiring the developer to submit a construction-related noise mitigation plan to the [County] for review and approval prior to issuance of a grading permit. The plan must depict the location of construction equipment and how the noise from this equipment will be mitigated during construction of this project, through the use of such methods as:
  - i. Temporary noise attenuation fences;
  - ii. Preferential location and equipment; and
  - iii. Use of current noise suppression technology and equipment.
- N 14.1 Enforce the California Building Standards that sets standards for building construction to mitigate interior noise levels to the tolerable 45 CNEL limit. These standards are utilized in conjunction with the Uniform Building Code by the County's Building Department to ensure that noise protection is provided to the public. Some design features may include extra-dense insulation, double-paned windows, and dense construction materials.
- N 16.3 Prohibit exposure of residential dwellings to perceptible ground vibration from passing trains as perceived at the ground or second floor. Perceptible motion shall be presumed to be a motion velocity of 0.01 inches/second over a range of 1 to 100 Hz.

To ensure noise-sensitive land uses are protected from high levels of noise (N 1.1), Table N-1 of the Noise Element identifies guidelines to evaluate proposed developments based on exterior and interior noise level limits for land uses and requires a noise analysis to determine needed mitigation measures if necessary. The Noise Element identifies residential use as a noise-sensitive land use (N 1.3) and discourages new development in areas with transportation related levels of 65 dBA CNEL or greater existing ambient noise levels. To prevent and mitigate noise impacts for its residents (N 1.5), County of Riverside requires exterior noise attenuation measures for sensitive land use exposed to transportation related noise levels higher than 65 dBA CNEL. In addition, the County of Riverside had adopted an interior noise level limit of 45 dBA CNEL (N 14.1).

Policy N 4.1 of the Noise Element sets a stationary-source exterior noise limit to not to be exceeded for a cumulative period of more than ten minutes in any hour of 65 dBA  $L_{eq}$  for daytime hours of 7:00 a.m. to 10:00 p.m., and 45 dBA  $L_{eq}$  during the noise-sensitive nighttime hours of 10:00 p.m. to 7:00 a.m. To prevent high levels of construction noise from impacting noise-



sensitive land uses, policies N 13.1 through 13.3 identify construction noise mitigation requirements for new development located near existing noise-sensitive land uses. (10)

### 3.2.1 LAND USE COMPATIBILITY GUIDELINES

The noise criteria identified in the County of Riverside Noise Element (Table N-1) are guidelines to evaluate the land use compatibility of transportation related noise. The compatibility criteria, shown on Exhibit 3-A, provides the County with a planning tool to gauge the compatibility of land uses relative to existing and future exterior noise levels.

The Land Use Compatibility for Community Noise Exposure matrix describes categories of compatibility and not specific noise standards. The warehouse/industrial use of the Project is considered normally acceptable with unmitigated exterior noise levels of less than 70 dBA CNEL based on the Industrial, Manufacturing, Utilities, Agriculture land use compatibility criteria shown on Exhibit 3-A. Residential designated land uses in the Project study area are considered normally acceptable with exterior noise levels below 60 dBA CNEL, and conditionally acceptable with exterior noise levels of up to 70 dBA CNEL. For conditionally acceptable exterior noise levels, of up to 80 dBA CNEL for Project land uses, new construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and the needed noise insulation features are included in the design. Conventional construction, but with closed windows and fresh air supply systems or air conditioning will normally suffice. (10)

### 3.3.2 COUNTY OF RIVERSIDE STATIONARY NOISE STANDARDS

The County of Riverside has set stationary-source hourly average L<sub>eq</sub> exterior noise limits to control loading dock activity, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements associated with the development of the proposed Majestic Freeway Business Center (Building 17). The County considers noise generated using motor vehicles to be a stationary noise source when operated on private property such as at a loading dock. These facility-related noises, as projected to any portion of any surrounding property containing a habitable dwelling, hospital, school, library or nursing home, must not exceed the following worst-case noise levels.

Policy N 4.1 of the County of Riverside General Plan Noise Element sets a stationary-source average  $L_{eq}$  exterior noise limit not to be exceeded for a cumulative period of more than ten minutes in any hour of 65 dBA  $L_{eq}$  for daytime hours of 7:00 a.m. to 10:00 p.m., and 45 dBA  $L_{eq}$  during the noise-sensitive nighttime hours of 10:00 p.m. to 7:00 a.m. (10)

The County of Riverside County Code Section 9.52.040 *General sound level standards* (included in Appendix 3.1) summarizing Ordinance No. 847 *Regulating Noise* identify lower, more restrictive exterior noise level standards, which for the purpose of this report, are used to evaluate potential Project-related operational noise level limits instead of the higher the General Plan exterior noise level standards previously identified. The County of Riverside County Code identifies residential exterior noise level limits of 55 dBA L<sub>eq</sub> during the daytime hours of 7:00 a.m. to 10:00 p.m., and 45 dBA L<sub>eq</sub> during the noise-sensitive nighttime hours of 10:00 p.m. to 7:00 a.m., commercial exterior noise level limits of 65 dBA L<sub>eq</sub> during the daytime hours, and 55 dBA L<sub>eq</sub> during the noise-sensitive nighttime hours, and public facility exterior noise level limits



of 65 dBA L<sub>eq</sub> during the daytime hours, and 45 dBA L<sub>eq</sub> during the noise-sensitive nighttime hours. (11).

LAND USE CATEGORY COMMUNITY NOISE EXPOSURE LEVEL Ldn or CNEL, dBA 70 75 80 60 65 Residential-Low Density Single Family, Duplex, Mobile Homes Residential-Multiple Family Transient Lodging-Motels, Hotels Schools, Libraries, Churches, Hospitals, **Nursing Homes** Auditoriums, Concert Halls, Amphitheaters Sports Arena, Outdoor Spectator Sports Playgrounds, Neighborhood Parks Golf Courses, Riding Stables, Water Recreation, Cemeteries Office Buildings, Businesses, Commercial, and Professional Industrial, Manufacturing, Utilities, Agriculture

**EXHIBIT 3-A: LAND USE COMPATIBILITY FOR COMMUNITY NOISE EXPOSURE** 

Source: County of Riverside General Plan Noise Element, Table N-1.



Clearly Unacceptable:

ew construction or development should merally not be undertaken. Construction sits to make the indoor environment couptable would be prohibitive and the indoor environment would not be usable.

Legend:

Normally Acceptable:

Source: California Office of Noise Control

Specified land use is satisfactory based upon the assumption that any buildings involved an of normal conventional construction, without any special noise insulation requirements.

New construction of excelopment should be undertaken only after a detailed analysis of the noise reduction requirements is made and needed noise insulation features included in the design. Conventional construction, but with closed windows and fresh air supply systems or air conditioning will normally suffice. Outdoor environment will seem noisy.

Conditionally Acceptable:

Normally Unacceptable:

Normany Unacceptable: New construction or development should generally be discouraged. If new construction or development does proceed, a detailed analysis of the noise reduction requirements must be made with needed

noise insulation features included in the design. Outdoor areas must be shielded.

Based on several discussions with the County of Riverside Department of Environmental Health (DEH), Office of Industrial Hygiene (OIH), it is important to recognize that the County of Riverside County Code noise level standards, incorrectly identify maximum noise level (L<sub>max</sub>) standards that should instead reflect the average L<sub>eq</sub> noise levels. Moreover, the County of Riverside DEH OIH's April 15<sup>th</sup>, 2015, Requirements for determining and mitigating, non-transportation noise source impacts to residential properties also identifies operational (stationary-source) noise level limits using the L<sub>eq</sub> metric, consistent with the direction of the County of Riverside General Plan guidelines and standards provided in the Noise Element. Therefore, this report has been prepared consistent with direction of the County of Riverside DEH OIH guidelines and standards using the average L<sub>eq</sub> noise level metric for stationary-source (operational) noise level evaluation.

# 3.3 CONSTRUCTION NOISE STANDARDS

To control noise impacts associated with the construction of the proposed Project, the County of Riverside has established limits to the hours of construction activities. Riverside County Ordinance No. 847 Regulating Noise Section 2i (Code Section 9.52.020[I]) indicates that noise associated with any private construction activity located within one-quarter of a mile from an inhabited dwelling is considered exempt between the hours of 6:00 a.m. and 6:00 p.m., during the months of June through September, and 7:00 a.m. and 6:00 p.m., during the months of October through May. (11) Neither the County's General Plan nor County Code establish numeric maximum acceptable construction source noise levels at potentially affected receivers for CEQA analysis purposes. Therefore, a numerical construction threshold based on Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment Manual* is used for analysis of daytime construction impacts, as discussed below.

According to the FTA, local noise ordinances are typically not very useful in evaluating construction noise. They usually relate to nuisance and hours of allowed activity, and sometimes specify limits in terms of maximum levels, but are generally not practical for assessing the impact of a construction project. Project construction noise criteria should account for the existing noise environment, the absolute noise levels during construction activities, the duration of the construction, and the adjacent land use. Due to the lack of standardized construction noise thresholds, the FTA provides guidelines that can be considered reasonable criteria for construction noise assessment. The FTA considers a daytime exterior construction noise level of 80 dBA L<sub>eq</sub> as a reasonable threshold for noise sensitive residential land use with a nighttime exterior construction noise level of 70 dBA L<sub>eq</sub> (8 p. 179).

# 3.4 Construction Vibration Standards

Construction activity can result in varying degrees of ground-borne vibration, depending on the equipment and methods used, distance to the affected structures and soil type. Construction vibration is generally associated with pile driving and rock blasting. Other construction equipment such as air compressors, light trucks, hydraulic loaders, etc., generates little or no ground vibration (8). To analyze vibration impacts originating from the operation and construction of the Majestic Freeway Business Center (Building 17), vibration-generating activities are appropriately evaluated against standards established under the Municipal Code, if



such standards exist. However, the County of Riverside does not identify specific construction vibration level limits. Therefore, for analysis purposes, the Caltrans *Transportation and Construction Vibration Guidance Manual*, (12 p. 38) Table 19, vibration damage are used in this noise study to assess potential temporary construction-related impacts at adjacent building locations. The nearest noise sensitive buildings adjacent to the Project site can best be described as "older residential structures" with a maximum acceptable continuous vibration threshold of 0.3 PPV (in/sec).

# 3.5 March Air Reserve Base/Inland Port Airport Land Use Compatibility

The March Air Reserve Base/Inland Port Airport (MARB/IPA) runway is located less than one mile east of the Project site. The *Riverside County Airport Land Use Compatibility Plan Policy Document* (RC ALUCP) includes the policies for determining the land use compatibility of the Project. Policy 4.1.5 *Noise Exposure for Other Land Uses* of the RC ALUCP requires that land uses, demonstrate compatibility with the acceptable noise levels on Table 2B. The Table 2B *Supporting Compatibility Criteria: Noise* matrix is shown on Exhibit 3-B and indicates that the Project's industrial land uses experience *clearly acceptable* exterior noise levels below 60 dBA CNEL. *Normally acceptable* noise levels for industrial land uses range from 60 to 65 dBA CNEL. *Marginally acceptable* noise levels at industrial land uses range from 65 to 70 dBA CNEL. (13)

The 70, 65 and 60 dBA CNEL noise contour boundaries used to determine the potential aircraft-related noise impacts at the Project site are found on Figure 6-9 of the March Air Reserve Base 2018 Final Air Installations Compatible Uses Zones Study and are presented on Exhibit 3-C of this report. Based on the 2018 noise level contours for the MARB/IPA, the Project development area is located outside the 60 dBA CNEL noise level contour boundaries and the Project's industrial land use is considered *clearly acceptable*.



**EXHIBIT 3-B: RC ALUCP SUPPORTING COMPATIBILITY CRITERIA: NOISE** 

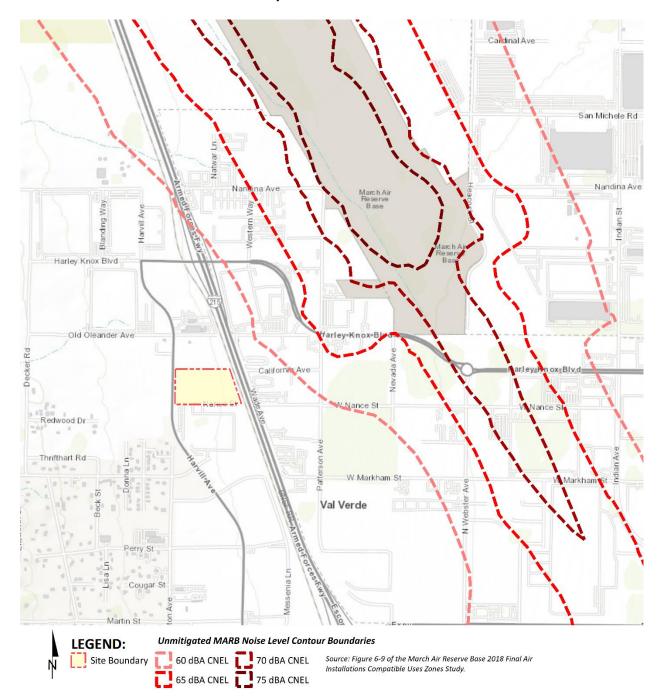
CNEL (dB
----------

Land Use Category	50–55	55–60	60–65	65–70	70–75
Residential *					
single-family, nursing homes, mobile homes	++	0	_		
multi-family, apartments, condominiums	++	+	0		
Public					
schools, libraries, hospitals	+	0	_		
churches, auditoriums, concert halls	+	0	0	_	
transportation, parking, cemeteries	++	++	++	+	0
Commercial and Industrial					
offices, retail trade	++	+	0	0	_
service commercial, wholesale trade, warehousing, light industrial	++	++	+	0	0
general manufacturing, utilities, extractive industry	++	++	++	+	+
Agricultural and Recreational					
cropland	++	++	++	++	+
livestock breeding	++	+	0	0	_
parks, playgrounds, zoos	++	+	+	0	_
golf courses, riding stables, water recreation	++	++	+	0	0
outdoor spectator sports	++	+	+	0	_
amphitheaters	+	0	_		

### Land Use Acceptability Interpretation/Comments Clearly Acceptable The activities associated with the specified land use can be carried out with essentially no interference from the noise exposure. Noise is a factor to be considered in that slight interference with outdoor activities may Normally Acceptable occur. Conventional construction methods will eliminate most noise intrusions upon indoor activities. Marginally Acceptable The indicated noise exposure will cause moderate interference with outdoor activities and with indoor activities when windows are open. The land use is acceptable on the conditions that outdoor activities are minimal and construction features which provide sufficient noise attenuation are used (e.g., installation of air conditioning so that windows can be kept closed). Under other circumstances, the land use should be discouraged. Normally Unacceptable Noise will create substantial interference with both outdoor and indoor activities. Noise intrusion upon indoor activities can be mitigated by requiring special noise insulation construction. Land uses which have conventionally constructed structures and/or involve outdoor activities which would be disrupted by noise should generally be avoided. Unacceptable noise intrusion upon land use activities will occur. Adequate structural Clearly Unacceptable noise insulation is not practical under most circumstances. The indicated land use should be avoided unless strong overriding factors prevail and it should be prohibited if outdoor activities are involved.

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<sup>\*</sup> Subtract 5 dB for low-activity outlying airports (Chiriaco Summit and Desert Center) Source: Riverside County Airport Land Use Compatibility Plan, Table 2B.



**EXHIBIT 3-C: MARB/IPA FUTURE AIRPORT NOISE CONTOURS** 



# 4 SIGNIFICANCE CRITERIA

The following significance criteria are based on currently adopted guidance provided by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1) For the purposes of this report, impacts would be potentially significant if the Project results in or causes:

- A. Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- B. Generation of excessive ground-borne vibration or ground-borne noise levels?
- C. For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

# 4.1 Noise Level Increases (Threshold A)

Noise level increases resulting from the Project are evaluated based on the Appendix G CEQA Guidelines described above at the closest sensitive receiver locations. Under CEQA, consideration must be given to the magnitude of the increase, the existing baseline ambient noise levels, and the location of noise-sensitive receivers to determine if a noise increase represents a significant adverse environmental impact. This approach recognizes that there is no single noise increase that renders a noise impact significant. (14) This is primarily because of the wide variation in individual thresholds of annoyance and differing individual experiences with noise. Thus, an important way of determining a person's subjective reaction to a new noise is the comparison of it to the existing environment to which one has adapted—the so-called ambient environment. In general, the more a new noise level exceeds the previously existing ambient noise level, the less acceptable the new noise level will typically be judged.

### 4.1.1 Noise-Sensitive Receivers

The Federal Interagency Committee on Noise (FICON) (15) developed guidance to be used for the assessment of project-generated increases in noise levels that consider the ambient noise level. The FICON recommendations are based on studies that relate aircraft noise levels to the percentage of persons highly annoyed by aircraft noise. Although the FICON recommendations were specifically developed to assess aircraft noise impacts, these recommendations are often used in environmental noise impact assessments involving the use of cumulative noise exposure metrics, such as the average-daily noise level (CNEL) and equivalent continuous noise level ( $L_{eq}$ ).

As previously stated, the approach used in this noise study recognizes that there is no single noise increase that renders a noise impact significant, based on a 2008 California Court of Appeal ruling on Gray v. County of Madera. (14) For example, if the ambient noise environment is quiet (<60 dBA) and the new noise source greatly increases the noise levels, an impact may occur if the noise criteria may be exceeded. Therefore, for this analysis, a readily perceptible 5 dBA or greater project-related noise level increase is considered a significant impact when the without project noise levels are below 60 dBA. Per the FICON, in areas where the without project noise levels



range from 60 to 65 dBA, a 3 dBA barely perceptible noise level increase appears to be appropriate for most people. When the without project noise levels already exceed 65 dBA, any increase in community noise louder than 1.5 dBA or greater is considered a significant impact if the noise criteria for a given land use is exceeded, since it likely contributes to an existing noise exposure exceedance. The FICON guidance provides an established source of criteria to assess the impacts of substantial temporary or permanent increase in baseline ambient noise levels. Based on the FICON criteria, the amount to which a given noise level increase is considered acceptable is reduced when the without Project (baseline) noise levels are already shown to exceed certain land-use specific exterior noise level criteria. The specific levels are based on typical responses to noise level increases of 5 dBA or readily perceptible, 3 dBA or barely perceptible, and 1.5 dBA depending on the underlying without Project noise levels for noise-sensitive uses. These levels of increases and their perceived acceptance are consistent with guidance provided by both the Federal Highway Administration (4 p. 9) and Caltrans (16 p. 2\_48).

### 4.1.2 Non-Noise-Sensitive Receivers

The County of Riverside General Plan Noise Element, Table N-1, Land Use Compatibility for Community Noise Exposure was used to establish the satisfactory noise levels of significance for non-noise-sensitive land uses in the Project study area. As previously shown on Exhibit 3-A, the normally acceptable exterior noise level for non-noise-sensitive land uses is 70 dBA CNEL. Noise levels greater than 70 dBA CNEL are considered conditionally acceptable per the Land Use Compatibility for Community Noise Exposure. (10)

To determine if Project-related traffic noise level increases are significant at off-site non-noise-sensitive land uses, a *barely perceptible* 3 dBA criteria is used. When the without Project noise levels are greater than the *normally acceptable* 70 dBA CNEL land use compatibility criteria, a *barely perceptible* 3 dBA or greater noise level increase is considered a significant impact since the noise level criteria is already exceeded. The noise level increases used to determine significant impacts for non-noise-sensitive land uses is generally consistent with the FICON noise level increase thresholds for noise-sensitive land uses but instead rely on the County of Riverside General Plan Noise Element, Table N-1, *Land Use Compatibility for Community Noise Exposure normally acceptable* 70 dBA CNEL exterior noise level criteria.

# 4.2 VIBRATION (THRESHOLD B)

As described in Section 3.4, the vibration impacts originating from the construction of Majestic Freeway Business Center (Building 17), vibration-generating activities are appropriately evaluated using the Caltrans vibration damage thresholds to assess potential temporary construction-related impacts at adjacent building locations. The nearest noise sensitive buildings adjacent to the Project site can best be described as "older residential structures" with a maximum acceptable continuous vibration threshold of 0.3 PPV (in/sec).



# 4.3 CEQA Guidelines Not Further Analyzed (Threshold C)

The closest airport which would require additional noise analysis under CEQA Appendix G Guideline C is the MARB/IPA. As previously indicated in Section 3.5, the noise contour boundaries of MARB/IPA are presented on Exhibit 3-C of this report and shows that the Project's industrial land uses are considered *normally acceptable* since the development area is located outside the 60 dBA CNEL contour. Therefore, the Project impacts are considered *less than significant*, and no further noise analysis is provided under CEQA Significance Criteria C.

### 4.4 SIGNIFICANCE CRITERIA SUMMARY

Noise impacts shall be considered significant if any of the following occur as a direct result of the proposed development. Table 4-1 shows the significance criteria summary matrix that includes the allowable criteria used to identify potentially significant incremental noise level increases.

**TABLE 4-1: SIGNIFICANCE CRITERIA SUMMARY** 

Amalysis	Receiving	Condition(s)	Significance Criteria		
Analysis	Land Use	Condition(s)	Daytime	Nighttime	
		If ambient is < 60 dBA CNEL	≥ 5 dBA CNEL F	Project increase	
	Noise- Sensitive <sup>1</sup>	If ambient is 60 - 65 dBA CNEL	≥ 3 dBA CNEL F	Project increase	
Off-Site	Schistive	If ambient is > 65 dBA CNEL	≥ 1.5 dBA CNEL	Project increase	
Traffic	Non-Noise- Sensitive <sup>2</sup>	If ambient is > 70 dBA CNEL	≥ 3 dBA CNEL Project increase		
		Exterior Noise Level Standards <sup>3</sup>	55 dBA L <sub>eq</sub>	45 dBA L <sub>eq</sub>	
Operational	Noise-	If ambient is < 60 dBA Leq <sup>1</sup>	≥ 5 dBA L <sub>eq</sub> Project increase		
Operational	Sensitive	If ambient is 60 - 65 dBA Leq <sup>1</sup>	≥ 3 dBA L <sub>eq</sub> Project increase		
		If ambient is > 65 dBA Leq <sup>1</sup>	≥ 1.5 dBA L <sub>eq</sub> Project increas		
Construction	Noise-	Noise Level Threshold <sup>4</sup>	80 dBA L <sub>eq</sub>	70 dBA L <sub>eq</sub>	
Construction	Sensitive	Vibration Level Threshold⁵	0.3 PPV (in/sec)		

<sup>&</sup>lt;sup>1</sup>FICON, 1992.



<sup>&</sup>lt;sup>2</sup>County of Riverside General Plan Noise Element, Table N-1.

 $<sup>^{3}</sup>$  County of Riverside General Plan Municipal Code, Section 9.52.040.

<sup>&</sup>lt;sup>4</sup> Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual.

 $<sup>^{\</sup>rm 5}$  Caltrans Transportation and Construction Vibration Manual, April 2020 Table 19

<sup>&</sup>quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

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# 5 EXISTING NOISE LEVEL MEASUREMENTS

To assess the existing noise level environment, 24-hour noise level measurements were taken at six locations in the Project study area. The receiver locations were selected to describe and document the existing noise environment within the Project study area. Exhibit 5-A provides the boundaries of the Project study area and the noise level measurement locations. To fully describe the existing noise conditions, noise level measurements were collected by Urban Crossroads, Inc. on Friday, August 5<sup>th</sup>, 2022, and Tuesday August 16<sup>th</sup>, 2022. Appendix 5.1 includes study area photos.

# 5.1 MEASUREMENT PROCEDURE AND CRITERIA

To describe the existing noise environment, the hourly noise levels were measured during typical weekday conditions over a 24-hour period. By collecting individual hourly noise level measurements, it is possible to describe the equivalent daytime and nighttime hourly noise levels and calculate the 24-hour CNEL. The long-term noise readings were recorded using Piccolo Type 2 integrating sound level meter and dataloggers. The Piccolo sound level meters were calibrated using a Larson-Davis calibrator, Model CAL 150. All noise meters were programmed in "slow" mode to record noise levels in "A" weighted form. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (17)

# **5.2** Noise Measurement Locations

The long-term noise level measurements were positioned as close to the nearest sensitive receiver locations as possible to assess the existing ambient hourly noise levels surrounding the Project site. Both Caltrans and the FTA recognize that it is not reasonable to collect noise level measurements that can fully represent every part of a private yard, patio, deck, or balcony normally used for human activity when estimating impacts for new development projects. This is demonstrated in the Caltrans general site location guidelines which indicate that, sites must be free of noise contamination by sources other than sources of interest. Avoid sites located near sources such as barking dogs, lawnmowers, pool pumps, and air conditioners unless it is the express intent of the analyst to measure these sources. (2) Further, FTA guidance states, that it is not necessary nor recommended that existing noise exposure be determined by measuring at every noise-sensitive location in the project area. Rather, the recommended approach is to characterize the noise environment for clusters of sites based on measurements or estimates at representative locations in the community. (8)

Based on recommendations of Caltrans and the FTA, it is not necessary to collect measurements at each individual building or residence, because each receiver measurement represents a group of buildings that share acoustical equivalence. (8) In other words, the area represented by the receiver shares similar shielding, terrain, and geometric relationship to the reference noise source. Receivers represent a location of noise sensitive areas and are used to estimate the future noise level impacts. Collecting reference ambient noise level measurements at the nearby



sensitive receiver locations allows for a comparison of the before and after Project noise levels and is necessary to assess potential noise impacts due to the Project's contribution to the ambient noise levels.

# 5.3 Noise Measurement Results

The noise measurements presented below focus on the equivalent or the energy average hourly sound levels ( $L_{eq}$ ). The equivalent sound level ( $L_{eq}$ ) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period. Table 5-1 identifies the hourly daytime (7:00 a.m. to 10:00 p.m.) and nighttime (10:00 p.m. to 7:00 a.m.) noise levels at each noise level measurement location.

**TABLE 5-1: AMBIENT NOISE LEVEL MEASUREMENTS** 

Location <sup>1</sup>	Description	Energy Average Noise Level (dBA L <sub>eq</sub> ) <sup>2</sup>		CNEL
		Daytime	Nighttime	
L1	Located north of the Project site near the existing residence at 22980 Peregrine Way.	57.2	55.8	62.8
L2	Located southwest of the Project placed near the residence at 22710 Redwood Drive.	60.0	49.4	59.9
L3	Located southwest of the Project placed near the residence at 22721 Redwood Drive.	50.2	45.2	53.7
L4	Located south of the Project site near the residence at 18412 Donna Lane.	58.6	50.6	59.6
L5	Located south of the Project site near the residence at 18391 Seaton Avenue.	59.6	56.7	63.9
L6	Located east of the Project site near the residence at 18100 California Avenue.	55.9	52.7	60.2

 $<sup>^{\</sup>rm 1}\,\mbox{See}$  Exhibit 5-A for the noise level measurement locations.

Table 5-1 provides the equivalent noise levels used to describe the daytime and nighttime ambient conditions. These daytime and nighttime energy average noise levels represent the average of all hourly noise levels observed during these time periods expressed as a single number. Appendix 5.2 provides summary worksheets of the noise levels for each hour as well as the minimum, maximum, L<sub>1</sub>, L<sub>2</sub>, L<sub>5</sub>, L<sub>8</sub>, L<sub>25</sub>, L<sub>50</sub>, L<sub>90</sub>, L<sub>95</sub>, and L<sub>99</sub> percentile noise levels observed during the daytime and nighttime periods.



<sup>&</sup>lt;sup>2</sup> Energy (logarithmic) average levels. The long-term 24-hour measurement worksheets are included in Appendix 5.2.

<sup>&</sup>quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

HARLEY KNOX BIVD Site MARKHAM ST

**EXHIBIT 5-A: NOISE MEASUREMENT LOCATIONS** 



**LEGEND:** 

Site Boundary A Measurement Locations

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# 6 TRAFFIC NOISE METHODS AND PROCEDURES

The following section outlines the methods and procedures used to estimate and analyze the future traffic noise environment. Consistent with County of Riverside Noise Guidelines for Land Use Planning (see Exhibit 3-A), all transportation related noise levels are presented in terms of the 24-hour CNEL's.

# 6.1 FHWA TRAFFIC NOISE PREDICTION MODEL

The expected roadway noise level increases from vehicular traffic were calculated by Urban Crossroads, Inc. using a computer program that replicates the Federal Highway Administration (FHWA) Traffic Noise Prediction Model- FHWA-RD-77-108. (18) The FHWA Model arrives at a predicted noise level through a series of adjustments to the Reference Energy Mean Emission Level (REMEL). In California the national REMELs are substituted with the California Vehicle Noise (Calveno) Emission Levels. (19) Adjustments are then made to the REMEL to account for: the roadway classification (e.g., collector, secondary, major or arterial), the roadway active width (i.e., the distance between the center of the outermost travel lanes on each side of the roadway), the total average daily traffic (ADT), the travel speed, the percentages of automobiles, medium trucks, and heavy trucks in the traffic volume, the roadway grade, the angle of view (e.g., whether the roadway view is blocked), the site conditions ("hard" or "soft" relates to the absorption of the ground, pavement, or landscaping), and the percentage of total ADT which flows each hour throughout a 24-hour period. Research conducted by Caltrans has shown that the use of soft site conditions is appropriate for the application of the FHWA traffic noise prediction model used in this analysis. (20)

### 6.1.1 OFF-SITE TRAFFIC NOISE PREDICTION MODEL INPUTS

Table 6-1 presents the roadway parameters used to assess the Project's off-site transportation noise impacts. Table 6-1 identifies the six off-site study area roadway segments, the distance from the centerline to adjacent land use based on the functional roadway classifications per the County of Riverside General Plan Circulation Element, and the vehicle speeds. The ADT volumes used in this study area presented on Table 6-2 are based on the *Majestic Freeway Business Center (Building 17) Traffic Analysis*, prepared by Urban Crossroads, Inc. for the following traffic scenarios (21).

- Existing (E)
- Existing plus Project (E+P)
- Existing plus Ambient Growth plus Cumulative (EAC) without Project Conditions
- Existing plus Ambient Growth plus Cumulative (EAPC) with Project Conditions

The ADT volumes vary for each roadway segment based on the existing traffic volumes and the combination of project traffic distributions. This analysis relies on a comparative evaluation of the off-site traffic noise impacts at the boundary of the right-of-way of the receiving adjacent land use, without and with project ADT traffic volumes from the Project traffic analysis. The



Project is anticipated to generate a net total of 378 two-way trips per day (actual vehicles) that includes 60 truck trips.

**TABLE 6-1: OFF-SITE ROADWAY PARAMETERS** 

ID	Roadway	Segment	Receiving Land Use <sup>1</sup>	Classification <sup>2</sup>	Distance from Centerline to Receiving Land Use (Feet) <sup>3</sup>	Vehicle Speed (mph)
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	Major	59'	50
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	Major	59'	50
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	Major	59'	50
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	Major	59'	50
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	Expressway	92'	50
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	Expressway	92'	50

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to adjacent residential land uses.

**TABLE 6-2: AVERAGE DAILY TRAFFIC VOLUMES** 

			Average Daily Traffic Volumes <sup>1</sup>				
ID	Roadway	Segment	Exis	ting	EAC (2025)		
שו			Without Project	With Project	Without Project	With Project	
1	Harvill Av.	n/o Old Oleander	8,466	8,679	24,657	24,870	
2	Harvill Av.	n/o Commerce Ctr. Dr.	9,371	9,626	25,486	25,741	
3	Harvill Av.	n/o Cajalco Expy	10,869	11,124	27,353	27,608	
4	Harvill Av.	s/o Cajalco Expy	13,086	13,145	28,239	28,298	
7	Cajalco Expy	w/o Harvill Av.	24,229	24,268	35,611	35,651	
8	Cajalco Expy	e/o Harvill Av.	27,043	27,199	53,559	53,715	

<sup>&</sup>lt;sup>1</sup> Majestic Freeway Business Center (Building 17) Traffic Analysis, Urban Crossroads, Inc.

To quantify the off-site noise levels, the Project related truck trips were added to the heavy truck category in the FHWA noise prediction model. The addition of the Project related truck trips increases the percentage of heavy trucks in the vehicle mix. This approach recognizes that the FHWA noise prediction model is significantly influenced by the number of heavy trucks in the vehicle mix. Table 6-3 provides the time of day (daytime, evening, and nighttime) vehicle splits. The daily Project truck trip-ends were assigned to the individual off-site study area roadway segments based on the Project truck trip distribution percentages documented in the *Majestic Freeway Business Center (Building 17) Traffic Analysis*. Using the Project truck trips in combination with the Project trip distribution, Urban Crossroads, Inc. calculated the number of additional Project truck trips and vehicle mix percentages for each of the study area roadway



<sup>&</sup>lt;sup>2</sup> County of Riverside General Plan Circulation Element functional roadway classification.

<sup>&</sup>lt;sup>3</sup> Distance to receiving land use is based upon the right-of-way distances.

segments. Table 6-4 shows the traffic flow by vehicle type (vehicle mix) used for all without Project traffic scenarios, and Tables 6-5 to 6-6 show the vehicle mixes used for the with Project traffic scenarios.

**TABLE 6-3: TIME OF DAY VEHICLE SPLITS** 

Vahiala Tura		Total of Time of		
Vehicle Type	Daytime	Evening	Nighttime	Day Splits
Autos	74.72%	7.70%	17.58%	100.00%
Medium Trucks	88.52%	1.11%	10.37%	100.00%
Heavy Trucks	75.08%	7.99%	16.93%	100.00%

<sup>&</sup>lt;sup>1</sup> Based on the August 2, 2022, 24-hour directional vehicle classification count collected on Harvill Avenue between Peregrine (Majestic Freeway Business Center (Building 17) Traffic Analysis, Urban Crossroads, Inc.)

**TABLE 6-4: WITHOUT PROJECT VEHICLE MIX** 

Classification	Classification Total % Traffic Flow <sup>1</sup>							
Classification	Autos	Medium Trucks	Heavy Trucks	Total				
All Segments	89.28%	3.19%	7.54%	100.00%				

<sup>&</sup>lt;sup>1</sup> Based on the August 2, 2022, 24-hour directional vehicle classification count collected on Harvill Avenue between Peregrine Way (Majestic Freeway Business Center (Building 17) Traffic Analysis, Urban Crossroads, Inc.)

Due to the added Project truck trips, the increase in Project traffic volumes and the distributions of trucks on the study area road segments, the percentage of autos, medium trucks and heavy trucks will vary for each of the traffic scenarios. This explains why the existing and future traffic volumes and vehicle mixes vary between seemingly identical study area roadway segments.

**TABLE 6-5: EXISTING WITH PROJECT VEHICLE MIX** 

			With Project <sup>1</sup>						
ID	Roadway	Segment	Autos	Medium Trucks	Heavy Trucks	Total <sup>2</sup>			
1	Harvill Av.	n/o Old Oleander	88.90%	3.21%	7.89%	100.00%			
2	Harvill Av.	n/o Commerce Ctr. Dr.	89.37%	3.14%	7.50%	100.00%			
3	Harvill Av.	n/o Cajalco Expy	89.35%	3.14%	7.50%	100.00%			
4	Harvill Av.	s/o Cajalco Expy	89.32%	3.17%	7.50%	100.00%			
7	Cajalco Expy	w/o Harvill Av.	89.29%	3.18%	7.52%	100.00%			
8	Cajalco Expy	e/o Harvill Av.	89.27%	3.18%	7.55%	100.00%			

<sup>&</sup>lt;sup>1</sup> Majestic Freeway Business Center (Building 17) Traffic Analysis, Urban Crossroads, Inc.



<sup>&</sup>quot;Daytime" = 7:00 a.m. to 7:00 p.m.; "Evening" = 7:00 p.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

<sup>&</sup>lt;sup>2</sup> Total of vehicle mix percentage values rounded to the nearest one-hundredth.

**TABLE 6-6: EAC WITH PROJECT VEHICLE MIX** 

			With Project <sup>1</sup>						
ID	Roadway	Segment	Autos	Medium Trucks	Heavy Trucks	Total <sup>2</sup>			
1	Harvill Av.	n/o Old Oleander	89.14%	3.20%	7.66%	100.00%			
2	Harvill Av.	n/o Commerce Ctr. Dr.	89.31%	3.17%	7.52%	100.00%			
3	Harvill Av.	n/o Cajalco Expy	89.31%	3.17%	7.52%	100.00%			
4	Harvill Av.	s/o Cajalco Expy	89.30%	3.18%	7.52%	100.00%			
7	Cajalco Expy	w/o Harvill Av.	89.29%	3.19%	7.53%	100.00%			
8	Cajalco Expy	e/o Harvill Av.	89.27%	3.19%	7.54%	100.00%			

<sup>&</sup>lt;sup>1</sup> Majestic Freeway Business Center (Building 17) Traffic Analysis, Urban Crossroads, Inc.



<sup>&</sup>lt;sup>2</sup> Total of vehicle mix percentage values rounded to the nearest one-hundredth.

### 7 OFF-SITE TRAFFIC NOISE ANALYSIS

To assess the off-site transportation CNEL noise level impacts associated with development of the proposed Project, noise contours were developed based on the Majestic Freeway Business Center (Building 17) Traffic Analysis prepared by Urban Crossroads, Inc. (21) Noise contour boundaries represent the equal levels of noise exposure and are measured in CNEL from the center of the roadway.

### 7.1 TRAFFIC NOISE CONTOURS

Noise contours were used to assess the Project's incremental traffic-related noise impacts at land uses adjacent to roadways conveying Project traffic. The noise contours represent the distance to noise levels of a constant value and are measured from the center of the roadway for the 70, 65, and 60 dBA noise levels. The noise contours do not consider the effect of any existing noise barriers or topography that may attenuate ambient noise levels. In addition, because the noise contours reflect modeling of vehicular noise on area roadways, they appropriately do not reflect noise contributions from the surrounding stationary noise sources within the Project study area. Tables 7-1 to 7-4 present a summary of the exterior traffic noise levels for each traffic condition. Appendix 7.1 includes the traffic noise level contours worksheets for each traffic condition.

TABLE 7-1: EXISTING WITHOUT PROJECT CONTOURS

10	Road	Commont	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)		
ID		Land Use <sup>1</sup>	Receiving Land Use (dBA) <sup>2</sup>	70 dBA CNEL	65 dBA CNEL	60 dBA CNEL	
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	71.5	75	161	346
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	72.0	80	172	371
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	72.6	88	190	409
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	73.4	100	215	463
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	73.8	165	356	767
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	74.3	178	383	825

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



<sup>&</sup>lt;sup>2</sup> The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

<sup>&</sup>quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

**TABLE 7-2: EXISTING WITH PROJECT CONTOURS** 

ID	Dood	6	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)		
טו	Road	Segment	Land Use <sup>1</sup>	(dBA) <sup>2</sup> CNEL CNEL		60 dBA CNEL	
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	71.8	77	167	359
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	72.1	81	175	376
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	72.7	89	192	414
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	73.4	100	215	463
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	73.8	165	356	767
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	74.3	179	385	829

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

**TABLE 7-3: EAC WITHOUT PROJECT CONTOURS** 

ID	Road	Sagment	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)			
טו	Road	Segment	(dBA) <sup>2</sup> CNEL		65 dBA CNEL	60 dBA CNEL		
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	76.2	152	328	706	
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	76.3	156	335	722	
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	76.6	163	351	757	
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	76.8	167	359	773	
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	75.5	214	460	992	
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	77.3	280	604	1302	

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



<sup>&</sup>lt;sup>2</sup> The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

<sup>&</sup>quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

<sup>&</sup>lt;sup>2</sup> The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

<sup>&</sup>quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

**TABLE 7-4: EAC WITH PROJECT CONTOURS** 

ID	Dood	Commont	Receiving	CNEL at Nearest	Distance to Contour from Centerline (Feet)			
טו	Road	Segment	(dBA) <sup>2</sup> CNEL CNE		65 dBA CNEL	60 dBA CNEL		
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	76.3	154	332	716	
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	76.4	156	337	726	
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	76.7	164	353	761	
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	76.8	167	359	774	
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	75.5	214	460	992	
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	77.3	281	606	1305	

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

### 7.2 EXISTING PROJECT TRAFFIC NOISE LEVEL INCREASES

An analysis of existing traffic noise levels plus traffic noise generated by the proposed Project has been included in this report for informational purposes and to fully analyze all the existing traffic scenarios identified in the Traffic Analysis prepared by Urban Crossroads, Inc. However, the analysis of existing off-site traffic noise levels plus traffic noise generated by the proposed Project scenario will not actually occur since the Project would not be fully constructed and operational until Year 2025 conditions. Table 7-1 shows the Existing without Project conditions CNEL noise levels. The Existing without Project exterior noise levels range from 71.5 to 74.3 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-2 shows the Existing with Project conditions ranging from 71.8 to 74.3 dBA CNEL. Table 7-5 shows that the Project off-site traffic noise level increases range from 0.0 to 0.3 dBA CNEL on the study area roadway segments.

### 7.3 EAC TRAFFIC NOISE LEVEL INCREASES

Table 7-3 presents the Existing plus Ambient Growth Plus Cumulative (EAC) without Project conditions CNEL noise levels. The EAC without Project exterior noise levels range from 75.5 to 77.3 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-4 shows that the EAC with Project conditions will range from 75.5 to 77.3 dBA CNEL. Table 7-6 shows that the Project off-site traffic noise level increases range from 0.0 to 0.1 dBA CNEL.



<sup>&</sup>lt;sup>2</sup> The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the nearest receiving land use.

<sup>&</sup>quot;RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-5: EXISTING WITH PROJECT TRAFFIC NOISE LEVEL INCREASES

ID	Road	Segment	Receiving		IEL at Receiv and Use (dBA	Incremental Noise Level Increase Threshold <sup>3</sup>		
			Land Use <sup>1</sup>	No Project	With Project	Project Increment	Limit	Exceeded?
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	71.5	71.8	0.3	3.0	No
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	72.0	72.1	0.1	3.0	No
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	72.6	72.7	0.1	3.0	No
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	73.4	73.4	0.0	3.0	No
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	73.8	73.8	0.0	3.0	No
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	74.3	74.3	0.0	3.0	No

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



<sup>&</sup>lt;sup>2</sup> The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

<sup>&</sup>lt;sup>3</sup> Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

<sup>&</sup>quot;n/a" Per the County of Riverside General Plan Noise Element Table N-1, a barely perceptible 3 dBA or greater noise level increase is considered a significant impact when the ambient non-noise sensitive noise level is greater than the normally acceptable 70 dBA CNEL land use compatibility criteria.

TABLE 7-6: EAC WITH PROJECT TRAFFIC NOISE LEVEL INCREASES

ID	Road	Segment	Receiving		IEL at Receiv and Use (dB <i>A</i>	Incremental Noise Level Increase Threshold <sup>3</sup>		
		ooge.it	Land Use <sup>1</sup>	No Project	With Project	Project Increment	Limit	Exceeded?
1	Harvill Av.	n/o Old Oleander	Non-Sensitive	76.2	76.3	0.1	3.0	No
2	Harvill Av.	n/o Commerce Ctr. Dr.	Non-Sensitive	76.3	76.4	0.1	3.0	No
3	Harvill Av.	n/o Cajalco Expy	Non-Sensitive	76.6	76.7	0.1	3.0	No
4	Harvill Av.	s/o Cajalco Expy	Non-Sensitive	76.8	76.8	0.0	3.0	No
7	Cajalco Expy	w/o Harvill Av.	Non-Sensitive	75.5	75.5	0.0	3.0	No
8	Cajalco Expy	e/o Harvill Av.	Non-Sensitive	77.3	77.3	0.0	3.0	No

<sup>&</sup>lt;sup>1</sup> Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.



<sup>&</sup>lt;sup>2</sup> The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

<sup>&</sup>lt;sup>3</sup> Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

<sup>&</sup>quot;n/a" Per the County of Riverside General Plan Noise Element Table N-1, a barely perceptible 3 dBA or greater noise level increase is considered a significant impact when the ambient non-noise sensitive noise level is greater than the normally acceptable 70 dBA CNEL land use compatibility criteria.

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# 8 SENSITIVE RECEIVER LOCATIONS

To assess the potential for long-term operational and short-term construction noise impacts, the following sensitive receiver locations, as shown on Exhibit 8-A, were identified as representative locations for analysis. Sensitive receivers are generally defined as locations where people reside or where the presence of unwanted sound could otherwise adversely affect the use of the land. Noise-sensitive land uses are generally considered to include schools, hospitals, single-family dwellings, mobile home parks, churches, libraries, and recreation areas. Moderately noise-sensitive land uses typically include multi-family dwellings, hotels, motels, dormitories, out-patient clinics, cemeteries, golf courses, country clubs, athletic/tennis clubs, and equestrian clubs. Land uses that are considered relatively insensitive to noise include business, commercial, and professional developments. Land uses that are typically not affected by noise include: industrial, manufacturing, utilities, agriculture, undeveloped land, parking lots, warehousing, liquid and solid waste facilities, salvage yards, and transit terminals.

To describe the potential off-site Project noise levels, seven receiver locations in the vicinity of the Project site were identified. The selection of receiver locations is based on FHWA guidelines and is consistent with additional guidance provided by Caltrans and the FTA, as previously described in Section 5.2. Other sensitive land uses in the Project study area that are located at greater distances than those identified in this noise study will experience lower noise levels than those presented in this report due to the additional attenuation from distance and the shielding of intervening structures. Distance is measured in a straight line from the project boundary to each receiver location.

- R1: Location R1 represents existing noise sensitive residence at 22980 Peregrine Way, approximately 76 feet north of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R1 is placed at the building façade. A 24-hour noise measurement was taken near this location, L1, to describe the existing ambient noise environment.
- R2: Location R2 represents the existing noise sensitive residence at 22710 Redwood Drive, approximately 999 feet west of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R2 is placed at the building façade. A 24-hour noise measurement was taken near this location, L2, to describe the existing ambient noise environment.
- R3: Location R3 represents the existing noise sensitive residence at 22721 Redwood Drive, approximately 801 feet southwest of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R3 is placed at the building façade. A 24-hour noise measurement was taken near this location, L3, to describe the existing ambient noise environment.
- R4: Location R4 represents the existing noise sensitive residence at 18412 Donna Lane, approximately 675 feet south of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R4 is placed at the building façade. A 24-hour noise measurement was taken near this location, L4, to describe the existing ambient noise environment.

HARLEY KNOX BUYD Site 1,721 1,473 MARKHAM ST

**EXHIBIT 8-A: RECEIVER LOCATIONS** 

**LEGEND:** 

Site Boundary Receiver Locations — Distance from receiver to Project site boundary (in feet)

- R5: Location R5 represents the existing noise sensitive residence at 22948 Markham Street, approximately 741 feet south of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R5 is placed at the building façade. A 24-hour noise measurement was taken near this location, L4, to describe the existing ambient noise environment.
- R6: Location R6 represents the existing noise sensitive residence at 18412 Donna Lane, approximately 700 feet south of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R6 is placed at the building façade. A 24-hour noise measurement was taken near this location, L5, to describe the existing ambient noise environment.
- R7: Location R7 represents the existing noise sensitive residence at 18100 California 395, approximately 1,691 feet east of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R7 is placed at the building façade. A 24-hour noise measurement was taken near this location, L6, to describe the existing ambient noise environment.

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### 9 OPERATIONAL NOISE IMPACTS

This section analyzes the potential stationary-source operational noise impacts at the nearest receiver locations, identified in Section 8, resulting from the operation of the proposed Majestic Freeway Business Center (Building 17) Project. Exhibit 9-A identifies the noise source locations used to assess the operational noise levels. The operational noise analysis includes the planned 12-foot-high screen walls near the western loading dock entrance. The screenwall shown on Exhibit 9-A is designed for screening, privacy, noise control, and security.

### 9.1 OPERATIONAL NOISE SOURCES

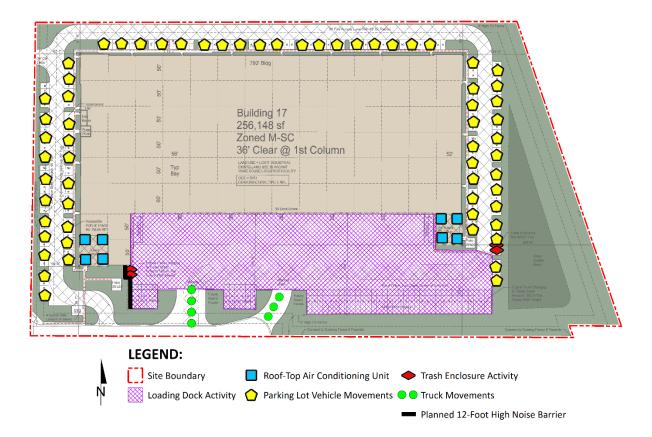
This operational noise analysis is intended to describe noise level impacts associated with the expected typical of daytime and nighttime activities at the Project site. Consistent with similar warehouse uses, the Project business operations would primarily be conducted within the enclosed building, except for traffic movement, parking, as well as loading and unloading of trucks at designated loading bays. The on-site Project-related noise sources are expected to include: loading dock activity, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements.

### 9.2 REFERENCE NOISE LEVELS

To estimate the Project operational noise impacts, reference noise level measurements were collected from similar types of activities to represent the noise levels expected with the development of the proposed Project. This section provides a detailed description of the reference noise level measurements shown on Table 9-1 used to estimate the Project operational noise impacts. It is important to note that the following projected noise levels assume the worst-case noise environment with the loading dock activity, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements all operating at the same time. These sources of noise activity will likely vary throughout the day.

#### 9.2.1 MEASUREMENT PROCEDURES

The reference noise level measurements presented in this section were collected using a Larson Davis LxT Type 1 precision sound level meter (serial number 01146). The LxT sound level meter was calibrated using a Larson-Davis calibrator, Model CAL 200, was programmed in "slow" mode to record noise levels in "A" weighted form and was located at approximately five feet above the ground elevation for each measurement. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (17)



**EXHIBIT 9-A: OPERATIONAL NOISE SOURCE LOCATIONS** 

**TABLE 9-1: REFERENCE NOISE LEVEL MEASUREMENTS** 

Noise Source <sup>1</sup>	Noise Source	Min./ Hour <sup>2</sup>		Reference Noise Level	Sound Power
Noise Source-	Height (Feet)	Day	Night	(dBA L <sub>eq</sub> ) @ 50 Feet	Level (dBA)³
Loading Dock Activity	8'	60	60	62.8	103.4
Roof-Top Air Conditioning Units	5'	39	28	57.2	88.9
Trash Enclosure Activity	5'	60	30	57.3	89.0
Parking Lot Vehicle Movements	5'	60	60	52.6	81.1
Truck Movements	8'	60	60	59.8	93.2

<sup>&</sup>lt;sup>1</sup> As measured by Urban Crossroads, Inc.

<sup>&</sup>lt;sup>2</sup> Anticipated duration (minutes within the hour) of noise activity during typical hourly conditions expected at the Project site.

<sup>&</sup>quot;Daytime" = 7:00 a.m. - 10:00 p.m.; "Nighttime" = 10:00 p.m. - 7:00 a.m.

<sup>&</sup>lt;sup>3</sup> Sound power level represents the total amount of acoustical energy (noise level) produced by a sound source independent of distance or surroundings. Sound power levels calculated using the CadnaA noise model at the reference distance to the noise source. Numbers may vary due to size differences between point and area noise sources.

#### 9.2.2 LOADING DOCK ACTIVITY

The reference loading dock activities are intended to describe the typical operational noise source levels associated with the Project. This includes truck idling, deliveries, backup alarms, unloading/loading, docking including a combination of tractor trailer semi-trucks, two-axle delivery trucks, and background forklift operations. At a uniform reference distance of 50 feet, Urban Crossroads collected a reference noise level of 62.8 dBA Leq. The loading dock activity noise level measurement was taken over a fifteen-minute period and represents multiple noise sources taken from the center of activity. The reference noise level measurement includes employees unloading a docked truck container included the squeaking of the truck's shocks when weight was removed from the truck, employees playing music over a radio, as well as a forklift horn and backup alarm. In addition, during the noise level measurement a truck entered the loading dock area and proceeded to reverse and dock in a nearby loading bay, adding truck engine, idling, air brakes noise, in addition to on-going idling of an already docked truck. Loading dock activity is estimated during all the daytime, evening, and nighttime hours.

#### 9.2.3 ROOF-TOP AIR CONDITIONING UNITS

The noise level measurements describe a single mechanical roof-top air conditioning unit. The reference noise level represents a Lennox SCA120 series 10-ton model packaged air conditioning unit. At the uniform reference distance of 50 feet, the reference noise levels are 57.2 dBA L<sub>eq</sub>. Based on the typical operating conditions observed over a four-day measurement period, the roof-top air conditioning units are estimated to operate for and average 39 minutes per hour during the daytime hours, and 28 minutes per hour during the nighttime hours. These operating conditions reflect peak summer cooling requirements with measured temperatures approaching 96 degrees Fahrenheit (°F) with average daytime temperatures of 82°F. For this noise analysis, the air conditioning units are expected to be located on the roof of the Project buildings.

#### 9.2.4 TRASH ENCLOSURE ACTIVITY

To describe the noise levels associated with a trash enclosure activity, Urban Crossroads collected a reference noise level measurement at an existing trash enclosure containing two dumpster bins. The trash enclosure noise levels describe metal gates opening and closing, metal scraping against concrete floor sounds, dumpster movement on metal wheels, and trash dropping into the metal dumpster. The reference noise levels describe trash enclosure noise activities when trash is dropped into an empty metal dumpster, as would occur at the Project Site. The measured reference noise level at the uniform 50-foot reference distance is 57.3 dBA L<sub>eq</sub> for the trash enclosure activity. The reference noise level describes the expected noise source activities associated with the trash enclosures for the Project's proposed building.

#### 9.2.5 PARKING LOT VEHICLE MOVEMENTS

To describe the on-site parking lot activity, a long-term 29-hour reference noise level measurement was collected in the center of activity within the staff parking lot of an Amazon warehouse distribution center. At 50 feet from the center of activity, the parking lot produced a reference noise level of 52.6 dBA  $L_{eq}$ . Parking activities are expected to take place during the full

hour (60 minutes) throughout the daytime and evening hours. The parking lot noise levels are mainly due cars pulling in and out of parking spaces in combination with car doors opening and closing.

#### 9.2.6 TRUCK MOVEMENTS

The truck movements reference noise level measurement was collected over a period of 1 hour and 28 minutes and represents multiple heavy trucks entering and exiting the outdoor loading dock area producing a reference noise level of  $59.8 \, \text{dBA} \, L_{eq}$  at  $50 \, \text{feet}$ . The noise sources included at this measurement location account for trucks entering and existing the Project driveways and maneuvering in and out of the outdoor loading dock activity area.

### 9.3 CADNAA NOISE PREDICTION MODEL

To fully describe the exterior operational noise levels from the Project, Urban Crossroads, Inc. developed a noise prediction model using the CadnaA (Computer Aided Noise Abatement) computer program. CadnaA can analyze multiple types of noise sources using the spatially accurate Project site plan, georeferenced Nearmap aerial imagery, topography, buildings, and barriers in its calculations to predict outdoor noise levels.

Using the ISO 9613-2 protocol, CadnaA will calculate the distance from each noise source to the noise receiver locations, using the ground absorption, distance, and barrier/building attenuation inputs to provide a summary of noise level at each receiver and the partial noise level contributions by noise source. Consistent with the ISO 9613-2 protocol, the CadnaA noise prediction model relies on the reference sound power level ( $L_w$ ) to describe individual noise sources. While sound pressure levels (e.g.,  $L_{eq}$ ) quantify in decibels the intensity of given sound sources at a reference distance, sound power levels ( $L_w$ ) are connected to the sound source and are independent of distance. Sound pressure levels vary substantially with distance from the source and diminish because of intervening obstacles and barriers, air absorption, wind, and other factors. Sound power is the acoustical energy emitted by the sound source and is an absolute value that is not affected by the environment.

The operational noise level calculations provided in this noise study account for the distance attenuation provided due to geometric spreading, when sound from a localized stationary source (i.e., a point source) propagates uniformly outward in a spherical pattern. A default ground attenuation factor of 0.5 was used in the CadnaA noise analysis to account for mixed ground representing a combination of hard and soft surfaces. Appendix 9.1 includes the detailed noise model inputs including the planned screenwall used to estimate the Project operational noise levels presented in this section.

### 9.4 Project Operational Noise Levels

Using the reference noise levels to represent the proposed Project operations that include loading dock activity, roof-top air conditioning units, trash enclosure activity, parking lot vehicle movements, and truck movements, Urban Crossroads, Inc. calculated the operational source noise levels that are expected to be generated at the Project site and the Project-related noise

level increases that would be experienced at each of the sensitive receiver locations. Table 9-2 shows the Project operational noise levels during the daytime hours of 7:00 a.m. to 10:00 p.m. The daytime hourly noise levels at the off-site receiver locations are expected to range from 33.2 to 42.5 dBA  $L_{\text{eq}}$ .

**TABLE 9-2: DAYTIME PROJECT OPERATIONAL NOISE LEVELS** 

Naise Coursel	Op	erational	Noise Leve	els by Rece	iver Locat	ion (dBA L	eq)
Noise Source <sup>1</sup>	R1	R2	R3	R4	R5	R6	R7
Loading Dock Activity	20.8	28.9	32.7	36.8	38.6	40.4	35.1
Roof-Top Air Conditioning Units	30.8	26.4	28.1	30.9	32.1	33.0	32.3
Trash Enclosure Activity	10.6	19.1	21.8	24.2	25.6	27.0	31.3
Parking Lot Vehicle Movements	37.2	26.0	26.8	29.2	30.2	31.3	35.2
Truck Movements	15.7	26.1	28.7	31.6	33.2	34.9	19.8
Total (All Noise Sources)	38.2	33.2	35.9	39.3	40.9	42.5	39.9

<sup>&</sup>lt;sup>1</sup> See Exhibit 9-A for the noise source locations. CadnaA noise model calculations are included in Appendix 9.1.

Table 9-3 shows the Project operational noise levels during the nighttime hours of 10:00 p.m. to 7:00 a.m. The nighttime hourly noise levels at the off-site receiver locations are expected to range from  $32.7 \text{ to } 42.2 \text{ dBA } L_{eq}$ . The differences between the daytime and nighttime noise levels are largely related to the estimated duration of noise activity as outlined in Table 9-1 and Appendix 9.1.

**TABLE 9-3: NIGHTTIME PROJECT OPERATIONAL NOISE LEVELS** 

Noise Source <sup>1</sup>	Op	Operational Noise Levels by Receiver Location (dBA Leq)							
Noise Source-	R1	R2	R3	R4	R5	R6	R7		
Loading Dock Activity	20.8	28.9	32.7	36.8	38.6	40.4	35.1		
Roof-Top Air Conditioning Units	28.4	24.0	25.7	28.5	29.7	30.6	29.9		
Trash Enclosure Activity	6.7	15.1	17.8	20.2	21.6	23.0	27.3		
Parking Lot Vehicle Movements	37.2	26.0	26.8	29.2	30.2	31.3	35.2		
Truck Movements	15.7	26.1	28.7	31.6	33.2	34.9	19.8		
Total (All Noise Sources)	37.9	32.7	35.5	39.0	40.6	42.2	39.1		

<sup>&</sup>lt;sup>1</sup> See Exhibit 9-A for the noise source locations. CadnaA noise model calculations are included in Appendix 9.1.

### 9.5 Project Operational Noise Level Compliance

To demonstrate compliance with local noise regulations, the Project-only operational noise levels are evaluated against exterior noise level thresholds based on the County of Riverside exterior noise level standards at nearby noise-sensitive receiver locations. Table 9-4 shows the operational noise levels associated with Majestic Freeway Business Center (Building 17) Project will not exceed the County of Riverside daytime and nighttime exterior noise level standards. Therefore, the operational noise impacts are considered *less than significant* at the nearby noise-sensitive receiver locations.

**TABLE 9-4: OPERATIONAL NOISE LEVEL COMPLIANCE** 

Receiver		perational s (dBA Leq) <sup>2</sup>		l Standards Leq) <sup>3</sup>	Noise Level Standards Exceeded? <sup>4</sup>		
Location	Daytime	Nighttime	Daytime	Nighttime	Daytime	Nighttime	
R1	38.2	37.9	55	45	No	No	
R2	33.2	32.7	55	45	No	No	
R3	35.9	35.5	55	45	No	No	
R4	39.3	39.0	55	45	No	No	
R5	40.9	40.6	55	45	No	No	
R6	42.5	42.2	55	45	No	No	
R7	39.9	39.1	55	45	No	No	

<sup>&</sup>lt;sup>1</sup> See Exhibit 8-A for the receiver locations.

### 9.5 Project Operational Noise Level Increases

To describe the Project operational noise level increases, the Project operational noise levels are combined with the existing ambient noise levels measurements for the nearby receiver locations potentially impacted by Project operational noise sources. Since the units used to measure noise, decibels (dB), are logarithmic units, the Project-operational and existing ambient noise levels cannot be combined using standard arithmetic equations. (2) Instead, they must be logarithmically added using the following base equation:

$$SPL_{Total} = 10log_{10}[10^{SPL1/10} + 10^{SPL2/10} + ... 10^{SPLn/10}]$$

Where "SPL1," "SPL2," etc. are equal to the sound pressure levels being combined, or in this case, the Project-operational and existing ambient noise levels. The difference between the combined Project and ambient noise levels describes the Project noise level increases to the existing ambient noise environment. Noise levels that would be experienced at receiver locations when Project-source noise is added to the daytime and nighttime ambient conditions are presented on Tables 9-5 and 9-6, respectively. As indicated on Table 9-5, the Project will generate a daytime operational noise level increases ranging from 0.0 to 0.2 dBA L<sub>eq</sub> at the nearest receiver locations. Table 9-6 shows that the Project will generate a nighttime operational noise level increases ranging from 0.1 to 0.4 dBA L<sub>eq</sub> at the nearest receiver locations. Project-related operational noise level increases will not exceed the operational noise level increase significance criteria presented in Table 4-1, and, therefore, the increases at the sensitive receiver locations will be *less than significant*.

<sup>&</sup>lt;sup>2</sup> Proposed Project operational noise levels as shown on Tables 9-2 and 9-3.

<sup>&</sup>lt;sup>3</sup> Exterior noise level standards, as shown on Table 4-1.

<sup>&</sup>lt;sup>4</sup> Do the estimated Project operational noise source activities exceed the noise level standards?

<sup>&</sup>lt;sup>5</sup> Receiver R2 represents the Temescal Valley Driving Range and does not include any noise sensitive nighttime receivers.

<sup>&</sup>quot;Daytime" = 7:00 a.m. - 10:00 p.m.; "Nighttime" = 10:00 p.m. - 7:00 a.m.

TABLE 9-5: DAYTIME PROJECT OPERATIONAL NOISE LEVEL INCREASES

Receiver Location <sup>1</sup>	Total Project Operational Noise Level <sup>2</sup>	Measurement Location <sup>3</sup>	Reference Ambient Noise Levels <sup>4</sup>	Combined Project and Ambient <sup>5</sup>	Project Increase <sup>6</sup>	Increase Criteria <sup>7</sup>	Increase Criteria Exceeded?
R1	38.2	L1	57.2	57.3	0.1	5.0	No
R2	33.2	L2	60.0	60.0	0.0	5.0	No
R3	35.9	L3	50.2	50.4	0.2	5.0	No
R4	39.3	L4	58.6	58.7	0.1	5.0	No
R5	40.9	L4	58.6	58.7	0.1	5.0	No
R6	42.5	L5	59.6	59.7	0.1	5.0	No
R7	39.9	L6	55.9	56.0	0.1	5.0	No

<sup>&</sup>lt;sup>1</sup> See Exhibit 8-A for the receiver locations.



<sup>&</sup>lt;sup>2</sup> Total Project daytime operational noise levels as shown on Table 9-2.

<sup>&</sup>lt;sup>3</sup> Reference noise level measurement locations as shown on Exhibit 5-A.

<sup>&</sup>lt;sup>4</sup> Observed daytime ambient noise levels as shown on Table 5-1.

<sup>&</sup>lt;sup>5</sup> Represents the combined ambient conditions plus the Project activities.

<sup>&</sup>lt;sup>6</sup> The noise level increase expected with the addition of the proposed Project activities.

<sup>&</sup>lt;sup>7</sup> Significance increase criteria as shown on Table 4-1.

TABLE 9-6: NIGHTTIME OPERATIONAL NOISE LEVEL INCREASES

Receiver Location <sup>1</sup>	Total Project Operational Noise Level <sup>2</sup>	Measurement Location <sup>3</sup>	Reference Ambient Noise Levels <sup>4</sup>	Combined Project and Ambient <sup>5</sup>	Project Increase <sup>6</sup>	Increase Criteria <sup>7</sup>	Increase Criteria Exceeded?
R1	37.9	L1	55.8	55.9	0.1	5.0	No
R2	32.7	L2	49.4	49.5	0.1	5.0	No
R3	35.5	L3	45.2	45.6	0.4	5.0	No
R4	39.0	L4	50.6	50.9	0.3	5.0	No
R5	40.6	L4	50.6	51.0	0.4	5.0	No
R6	42.2	L5	56.7	56.9	0.2	5.0	No
R7	39.1	L6	52.7	52.9	0.2	5.0	No

<sup>&</sup>lt;sup>1</sup> See Exhibit 8-A for the receiver locations.



<sup>&</sup>lt;sup>2</sup> Total Project nighttime operational noise levels as shown on Table 9-3.

<sup>&</sup>lt;sup>3</sup> Reference noise level measurement locations as shown on Exhibit 5-A.

<sup>&</sup>lt;sup>4</sup> Observed nighttime ambient noise levels as shown on Table 5-1.

<sup>&</sup>lt;sup>5</sup> Represents the combined ambient conditions plus the Project activities.

<sup>&</sup>lt;sup>6</sup> The noise level increase expected with the addition of the proposed Project activities.

<sup>&</sup>lt;sup>7</sup> Significance increase criteria as shown on Table 4-1.

### 10 CONSTRUCTION IMPACTS

This section analyzes potential impacts resulting from the short-term construction activities associated with the development of the Project. Exhibit 10-A shows the construction noise source locations in relation to the nearby sensitive receiver locations previously described in Section 8. According to Riverside County Ordinance No. 847 Regulating Noise Section 2i (Code Section 9.52.020[I]), noise associated with any private construction activity located within one-quarter of a mile from an inhabited dwelling is considered exempt between the hours of 6:00 a.m. and 6:00 p.m., during the months of June through September, and 7:00 a.m. and 6:00 p.m., during the months of October through May. (11)

In addition, neither the County of Riverside General Plan or County Code establish numeric maximum acceptable construction source noise levels at potentially affected receivers for CEQA analysis purposes. Therefore, a numerical construction threshold based on Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual is used for analysis of daytime construction impacts. The FTA considers a daytime exterior construction noise level of 80 dBA  $L_{eq}$  as a reasonable threshold for noise sensitive residential land use with a nighttime exterior construction noise level of 70 dBA  $L_{eq}$  (8 p. 179).

### **10.1** Construction Noise Levels

The FTA *Transit Noise and Vibration Impact Assessment Manual* recognizes that construction projects are accomplished in several different stages and outlines the procedures for assessing noise impacts during construction. Each stage has a specific equipment mix, depending on the work to be completed during that stage. As a result of the equipment mix, each stage has its own noise characteristics; some stages have higher continuous noise levels than others, and some have higher impact noise levels than others. The Project construction activities are expected to occur in the following stages:

- Site Preparation
- Grading
- Building Construction
- Paving
- Architectural Coating

#### 10.2 Construction Reference Noise Levels

To describe construction noise activities, this construction noise analysis was prepared using reference construction equipment noise levels from the Federal Highway Administration (FHWA) published the Roadway Construction Noise Model (RCNM), which includes a national database of construction equipment reference noise emission levels. (23) The RCNM equipment database, provides a comprehensive list of the noise generating characteristics for specific types of construction equipment. In addition, the database provides an acoustical usage factor to estimate the fraction of time each piece of construction equipment is operating at full power (i.e., its loudest condition) during a construction operation.



HARLEY KNOX BUYD 1,721 1,473 MARKHAM ST

**EXHIBIT 10-A: CONSTRUCTION NOISE SOURCE LOCATIONS** 



**LEGEND:** 

Construction Activity • Receiver Locations • Distance from receiver to Project site boundary (in feet)

### **10.3** Construction Noise Analysis

Using the reference construction equipment noise levels and the CadnaA noise prediction model, calculations of the Project construction noise level impacts at the nearby sensitive receiver locations were completed. Consistent with FTA guidance for general construction noise assessment, Table 10-1 presents the combined construction reference noise levels for the loudest construction equipment, assuming they operate at the same time. As shown on Table 10-2, the construction noise levels are expected to range from 49.3 to 64.7 dBA Leq at the nearby receiver locations. Appendix 10.1 includes the detailed CadnaA construction noise model inputs.

**TABLE 10-1: CONSTRUCTION REFERENCE NOISE LEVELS** 

Construction Stage	Reference Construction Activity	Reference Noise Level @ 50 Feet (dBA L <sub>eq</sub> ) <sup>1</sup>	Combined Noise Level (dBA L <sub>eq</sub> ) <sup>2</sup>	Combined Sound Power Level (PWL) <sup>3</sup>	
C'I	Crawler Tractors	78			
Site Preparation	Hauling Trucks	72	80	112	
Ru	Rubber Tired Dozers	75			
	Graders	81			
Grading	Excavators	77	83	115	
	Compactors	76			
5 11 11	Cranes	73		113	
Building Construction	Tractors	80	81		
Construction	Welders	70			
	Pavers	74			
Paving	Paving Equipment	82	83	115	
	Rollers	73			
	Cranes	73			
Architectural Coating	Air Compressors	74	77	109	
Couting	Generator Sets	70			

<sup>&</sup>lt;sup>1</sup> FHWA Roadway Construction Noise Model (RCNM).



<sup>&</sup>lt;sup>2</sup> Represents the combined noise level for all equipment assuming they operate at the same time consistent with FTA Transit Noise and Vibration Impact Assessment guidance.

<sup>&</sup>lt;sup>3</sup> Sound power level represents the total amount of acoustical energy (noise level) produced by a sound source independent of distance or surroundings. Sound power levels calibrated using the CadnaA noise model at the reference distance to the noise source.

**TABLE 10-2: CONSTRUCTION EQUIPMENT NOISE LEVEL SUMMARY** 

	Construction Noise Levels (dBA L <sub>eq</sub> )							
Receiver Location <sup>1</sup>	Site Preparation	Grading Pavi		Paving	Architectural Coating	Highest Levels <sup>2</sup>		
R1	61.7	64.7	62.7	64.7	58.7	64.7		
R2	52.3	55.3	53.3	55.3	49.3	55.3		
R3	53.2	56.2	54.2	56.2	50.2	56.2		
R4	55.6	58.6	56.6	58.6	52.6	58.6		
R5	56.8	59.8	57.8	59.8	53.8	59.8		
R6	58.0	61.0	59.0	61.0	55.0	61.0		
R7	59.3	62.3	60.3	62.3	56.3	62.3		

<sup>&</sup>lt;sup>1</sup>Construction noise source and receiver locations are shown on Exhibit 10-A.

# 10.4 CONSTRUCTION NOISE LEVEL COMPLIANCE

To evaluate whether the Project will generate potentially significant short-term noise levels at nearest receiver locations, a construction-related daytime noise level threshold of 80 dBA  $L_{eq}$  is used as a reasonable threshold to assess the daytime construction noise level impacts. The construction noise analysis shows that the nearest receiver locations will not exceed the reasonable daytime 80 dBA  $L_{eq}$  significance threshold during Project construction activities as shown on Table 10-3. Therefore, the noise impacts due to Project construction noise are considered *less than significant* at all receiver locations.

**TABLE 10-3: CONSTRUCTION NOISE LEVEL COMPLIANCE** 

D	Construction Noise Levels (dBA L <sub>eq</sub> )					
Receiver Location <sup>1</sup>	Highest Construction Noise Levels <sup>2</sup>	Threshold <sup>3</sup>	Threshold Exceeded? <sup>4</sup>			
R1	64.7	80	No			
R2	55.3	80	No			
R3	56.2	80	No			
R4	58.6	80	No			
R5	59.8	80	No			
R6	61.0	80	No			
R7	62.3	80	No			

<sup>&</sup>lt;sup>1</sup>Construction noise source and receiver locations are shown on Exhibit 10-A.



<sup>&</sup>lt;sup>2</sup> Construction noise level calculations based on distance from the construction activity, which is measured from the Project site boundary to the nearest receiver locations. CadnaA construction noise model inputs are included in Appendix 10.1.

<sup>&</sup>lt;sup>2</sup> Highest construction noise level calculations based on distance from the construction noise source activity to the nearest receiver locations as shown on Table 10-2.

<sup>&</sup>lt;sup>3</sup> Construction noise level thresholds as shown on Table 4-1.

<sup>&</sup>lt;sup>4</sup> Do the estimated Project construction noise levels exceed the construction noise level threshold?

### 10.5 NIGHTTIME CONCRETE POUR NOISE ANALYSIS

It is our understanding that nighttime concrete pouring activities will occur as a part of Project building construction activities. Nighttime concrete pouring activities are often used to support reduced concrete mixer truck transit times and lower air temperatures than during the daytime hours and are generally limited to the actual building pad area as shown on Exhibit 10-B. Since the nighttime concrete pours will take place outside the permitted by Riverside County Ordinance No. 847 Regulating Noise Section 2i (Code Section 9.52.020[I]), the Project Applicant will be required to obtain authorization for nighttime work from the County of Riverside. Any nighttime construction noise activities are evaluated against the FTA nighttime exterior construction noise level threshold of 70 dBA Leq for noise sensitive residential land use (8 p. 179).

#### 10.5.1 NIGHTTIME CONCRETE POUR REFERENCE NOISE LEVEL MEASUREMENTS

To estimate the noise levels due to nighttime concrete pour activities, sample reference noise level measurements were taken during a nighttime concrete pour at a construction site. Urban Crossroads, Inc. collected short-term nighttime concrete pour reference noise level measurements during the noise-sensitive nighttime hours between 1:00 a.m. to 2:00 a.m. at 27334 San Bernardino Avenue in the City of Redlands. The reference noise levels describe the expected concrete pour noise sources that may include concrete mixer truck movements and pouring activities, concrete paving equipment, rear mounted concrete mixer truck backup alarms, engine idling, air brakes, generators, and workers communicating/whistling.

To describe the nighttime concrete pour noise levels associated with the construction of the Majestic Freeway Business Center (Building 17), this analysis relies on reference sound pressure level of 67.7 dBA  $L_{eq}$  at 50 feet representing a sound power level of 100.3 dBA  $L_{w}$ . While the Project noise levels will depend on the actual duration of activities and specific equipment fleet in use at the time of construction, the reference sound power level of 100.3 dBA  $L_{w}$  is used to describe the expected Project nighttime concrete pour noise activities.

#### 10.5.2 NIGHTTIME CONCRETE POUR NOISE LEVEL COMPLIANCE

As shown on Table 10-4, the noise levels associated with the nighttime concrete pour activities are estimated to range from 40.5 to 49.5 dBA  $L_{\rm eq}$ . The analysis shows that the unmitigated nighttime concrete pour activities will not exceed the FTA 70 dBA  $L_{\rm eq}$  nighttime residential noise level threshold at all the nearest noise sensitive receiver locations. Therefore, the noise impacts due to Project construction nighttime concrete pour noise activity are considered *less than significant* at all receiver locations with prior authorization for nighttime work from the County of Riverside. Appendix 10.2 includes the CadnaA nighttime concrete pour noise model inputs.



HARLEY KNOX BUYD 1,826 1,611 MARKHAM ST **LEGEND:** Site Boundary Receiver Locations Nighttime Concrete Pour Activity — Distance from receiver to construction activity (in feet)

**EXHIBIT 10-B: NIGHTTIME CONCRETE POUR NOISE SOURCE AND RECEIVER LOCATIONS** 



TABLE 10-4: NIGHTTIME CONCRETE POUR NOISE LEVEL COMPLIANCE

D	Concrete Pour Construction Noise Levels (dBA L <sub>eq</sub> )						
Receiver Location <sup>1</sup>	Exterior Noise Levels <sup>2</sup>	Threshold <sup>3</sup>	Threshold Exceeded? <sup>4</sup>				
R1	49.5	70	No				
R2	40.5	70	No				
R3	41.3	70	No				
R4	43.7	70	No				
R5	44.8	70	No				
R6	46.1	70	No				
R7	46.8	70	No				

<sup>&</sup>lt;sup>1</sup> Construction noise source and receiver locations are shown on Exhibit 10-A.

#### 10.6 CONSTRUCTION VIBRATION ANALYSIS

Construction activity can result in varying degrees of ground vibration, depending on the equipment and methods employed. Operation of construction equipment causes ground vibrations that spread through the ground and diminish in strength with distance. Ground vibration levels associated with various types of construction equipment are summarized on Table 10-5. Based on the representative vibration levels presented for various construction equipment types, it is possible to estimate the potential for human response (annoyance) and building damage using the following vibration assessment methods defined by the FTA. To describe the vibration impacts the FTA provides the following equation:  $PPV_{equip} = PPV_{ref} \times (25/D)^{1.5}$ 

TABLE 10-5: VIBRATION SOURCE LEVELS FOR CONSTRUCTION EQUIPMENT

Equipment	PPV (in/sec) at 25 feet
Small bulldozer	0.003
Jackhammer	0.035
Loaded Trucks	0.076
Large bulldozer	0.089
Vibratory Roller	0.210

Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual



<sup>&</sup>lt;sup>2</sup> Nighttime Concrete Pour noise model inputs are included in Appendix 10.2.

<sup>&</sup>lt;sup>3</sup> Construction noise level thresholds as shown on Table 4-1.

<sup>&</sup>lt;sup>4</sup> Do the estimated Project construction noise levels exceed the construction noise level threshold?

Table 10-6 presents the expected Project related vibration levels at the nearby receiver locations. At distances ranging from 372 to 1,721 feet from Project construction activities, construction vibration velocity levels are estimated to range from 0.000 to 0.004 in/sec PPV. Based on maximum acceptable continuous vibration threshold of 0.3 PPV (in/sec), the typical Project construction vibration levels will fall below the building damage thresholds at all the noise sensitive receiver locations. Therefore, the Project-related vibration impacts are considered *less than significant* during typical construction activities at the Project site.

**TABLE 10-6: PROJECT CONSTRUCTION VIBRATION LEVELS** 

	Distance to		Typical Construction Vibration Levels PPV (in/sec) <sup>3</sup>						Thresholds
Location <sup>1</sup>	Activity	Small bulldozer	Jackhammer	Loaded Trucks	Large bulldozer	Vibratory Roller	Highest Vibration Level	PPV (in/sec) <sup>4</sup>	Exceeded? <sup>5</sup>
R1	372'	0.000	0.001	0.001	0.002	0.004	0.004	0.3	No
R2	1,721'	0.000	0.000	0.000	0.000	0.000	0.000	0.3	No
R3	1,473'	0.000	0.000	0.000	0.000	0.000	0.000	0.3	No
R4	1,014'	0.000	0.000	0.000	0.000	0.001	0.001	0.3	No
R5	856'	0.000	0.000	0.000	0.000	0.001	0.001	0.3	No
R6	718'	0.000	0.000	0.000	0.001	0.001	0.001	0.3	No
R7	613'	0.000	0.000	0.001	0.001	0.002	0.002	0.3	No

<sup>&</sup>lt;sup>1</sup> Construction noise source and receiver locations are shown on Exhibit 10-A.

Moreover, the vibration levels reported at the sensitive receiver locations are unlikely to be sustained during the entire construction period but will occur rather only during the times that heavy construction equipment is operating adjacent to the Project site perimeter.



<sup>&</sup>lt;sup>2</sup> Distance from receiver building facade to Project construction boundary (Project site boundary).

<sup>&</sup>lt;sup>3</sup> Based on the Vibration Source Levels of Construction Equipment (Table 10-5).

<sup>&</sup>lt;sup>4</sup> Caltrans Transportation and Construction Vibration Guidance Manual, April 2020, Table 19, p. 38.

<sup>&</sup>lt;sup>5</sup> Does the peak vibration exceed the acceptable vibration thresholds?

<sup>&</sup>quot;PPV" = Peak Particle Velocity

# 11 REFERENCES

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- 9. Office of Planning and Research. State of California General Plan Guidelines. 2019.
- 10. **County of Riverside.** *General Plan Noise Element.* December 2015.
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- 20. **California Department of Transportation.** *Traffic Noise Attenuation as a Function of Ground and Vegetation Final Report.* June 1995. FHWA/CA/TL-95/23.



- 21. **Urban Crossroads, Inc.** *Majestic Freeway Business Center (Building 17) Traffic Analysis.* November 2022.
- 22. U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning. FHWA Roadway Construction Noise Model. January, 2006.



# 12 CERTIFICATION

The contents of this noise study report represent an accurate depiction of the noise environment and impacts associated with the proposed Majestic Freeway Business Center (Building 17) Project. The information contained in this noise study report is based on the best available data at the time of preparation. If you have any questions, please contact me directly at (949) 584-3148.

Bill Lawson, P.E., INCE Principal URBAN CROSSROADS, INC. 1133 Camelback #8329 Newport Beach, CA 92658 (949) 581-3148 blawson@urbanxroads.com



#### **EDUCATION**

Master of Science in Civil and Environmental Engineering
California Polytechnic State University, San Luis Obispo • December, 1993

Bachelor of Science in City and Regional Planning California Polytechnic State University, San Luis Obispo • June, 1992

#### **PROFESSIONAL REGISTRATIONS**

PE – Registered Professional Traffic Engineer – TR 2537 • January, 2009

AICP – American Institute of Certified Planners – 013011 • June, 1997–January 1, 2012

PTP – Professional Transportation Planner • May, 2007 – May, 2013

INCE – Institute of Noise Control Engineering • March, 2004

#### **PROFESSIONAL AFFILIATIONS**

ASA – Acoustical Society of America ITE – Institute of Transportation Engineers

#### **PROFESSIONAL CERTIFICATIONS**

Certified Acoustical Consultant – County of San Diego • March, 2018
Certified Acoustical Consultant – County of Orange • February, 2011
FHWA-NHI-142051 Highway Traffic Noise Certificate of Training • February, 2013



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# **APPENDIX 3.1:**

**COUNTY OF RIVERSIDE MUNICIPAL CODE** 



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# **Chapter 9.52 NOISE REGULATION**

#### Sections:

#### 9.52.010 Intent.

At certain levels, sound becomes noise and may jeopardize the health, safety or general welfare of Riverside County residents and degrade their quality of life. Pursuant to its police power, the board of supervisors declares that noise shall be regulated in the manner described in this chapter. This chapter is intended to establish countywide standards regulating noise. This chapter is not intended to establish thresholds of significance for the purpose of any analysis required by the California Environmental Quality Act and no such thresholds are established.

(Ord. 847 § 1, 2006)

### **9.52.020 Exemptions.**

Sound emanating from the following sources is exempt from the provisions of this chapter:

- A. Facilities owned or operated by or for a governmental agency;
- B. Capital improvement projects of a governmental agency;
- C. The maintenance or repair of public properties;
- D. Public safety personnel in the course of executing their official duties, including, but not limited to, sworn peace officers, emergency personnel and public utility personnel. This exemption includes, without limitation, sound emanating from all equipment used by such personnel, whether stationary or mobile:
- E. Public or private schools and school-sponsored activities;
- F. Agricultural operations on land designated "Agriculture" in the Riverside County general plan, or land zoned A-I (light agriculture), A-P (light agriculture with poultry), A-2 (heavy agriculture), A-D (agriculture-dairy) or C/V (citrus/vineyard), provided such operations are carried out in a manner consistent with accepted industry standards. This exemption includes, without limitation, sound emanating from all equipment used during such operations, whether stationary or mobile;
- G. Wind energy conversion systems (WECS), provided such systems comply with the WECS noise provisions of Riverside County Ordinance No. 348;
- H. Private construction projects located one-quarter of a mile or more from an inhabited dwelling;
- I. Private construction projects located within one-quarter of a mile from an inhabited dwelling, provided that:
  - 1. Construction does not occur between the hours of six p.m. and six a.m. during the months of June through September, and
  - 2. Construction does not occur between the hours of six p.m. and seven a.m. during the months of October through May;
- J. Property maintenance, including, but not limited to, the operation of lawnmowers, leaf blowers, etc., provided such maintenance occurs between the hours of seven a.m. and eight p.m.;

- K. Motor vehicles, other than off-highway vehicles. This exemption does not include sound emanating from motor vehicle sound systems;
- L. Heating and air conditioning equipment;
- M. Safety, warning and alarm devices, including, but not limited to, house and car alarms, and other warning devices that are designed to protect the public health, safety, and welfare;
- N. The discharge of firearms consistent with all state laws.

(Ord. 847 § 2, 2006)

### 9.52.030 Definitions.

As used in this chapter, the following terms shall have the following meanings:

"Audio equipment" means a television, stereo, radio, tape player, compact disc player, mp3 player, I-POD or other similar device.

"Decibel (dB)" means a unit for measuring the relative amplitude of a sound equal approximately to the smallest difference normally detectable by the human ear, the range of which includes approximately one hundred thirty (130) decibels on a scale beginning with zero decibels for the faintest detectable sound. Decibels are measured with a sound level meter using different methodologies as defined below:

- 1. "A-weighting (dBA)" means the standard A-weighted frequency response of a sound level meter, which de-emphasizes low and high frequencies of sound in a manner similar to the human ear for moderate sounds.
- "Maximum sound level (L max)" means the maximum sound level measured on a sound level meter.

"Governmental agency" means the United States, the state of California, Riverside County, any city within Riverside County, any special district within Riverside County or any combination of these agencies.

"Land use permit" means a discretionary permit issued by Riverside County pursuant to Riverside County Ordinance No. 348.

"Motor vehicle" means a vehicle that is self-propelled.

"Motor vehicle sound system" means a stereo, radio, tape player, compact disc player, mp3 player, I-POD or other similar device.

"Noise" means any loud, discordant or disagreeable sound.

"Occupied property" means property upon which is located a residence, business or industrial or manufacturing use.

"Off-highway vehicle" means a motor vehicle designed to travel over any terrain.

"Public or private school" means an institution conducting academic instruction at the preschool, elementary school, junior high school, high school, or college level.

"Public property" means property owned by a governmental agency or held open to the public, including, but not limited to, parks, streets, sidewalks, and alleys.

"Sensitive receptor" means a land use that is identified as sensitive to noise in the noise element of the Riverside County general plan, including, but not limited to, residences, schools, hospitals, churches, rest homes, cemeteries or public libraries.

"Sound-amplifying equipment" means a loudspeaker, microphone, megaphone or other similar device.

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"Sound level meter" means an instrument meeting the standards of the American National Standards Institute for Type 1 or Type 2 sound level meters or an instrument that provides equivalent data.

(Ord. 847 § 3, 2006)

## 9.52.040 General sound level standards.

No person shall create any sound, or allow the creation of any sound, on any property that causes the exterior sound level on any other occupied property to exceed the sound level standards set forth in Table 1.

 $\label{eq:TABLE 1} \text{Sound Level Standards (Db $L_{max}$)}$ 

GENERAL	GENERAL PLAN	GENERAL PLAN LAND	DENSITY		M DECIBEL
PLAN	LAND USE	USE DESIGNATION		LEVEL	1
FOUNDATION	DESIGNATION	NAME		7 am—	10 pm—
COMPONENT				10 pm	7 am
Community	EDR	Estate Density	2 AC	55	45
Development		Residential			
	VLDR	Very Low Density	1 AC	55	45
		Residential			
	LDR	Low Density	1/2 AC	55	45
		Residential			
	MDR	Medium Density	2—5	55	45
		Residential			
	MHDR	Medium High Density	5—8	55	45
		Residential			
	HDR	High Density	8—14	55	45
		Residential			
	VHDR	Very High Density	14—20	55	45
		Residential			
	H'TDR	Highest Density	20+	55	45
		Residential			
	CR	Retail Commercial		65	55
	СО	Office Commercial		65	55
	СТ	Tourist Commercial		65	55
	CC	Community Center		65	55
	LI	Light Industrial		75	55
	HI	Heavy Industrial		75	75
	ВР	Business Park		65	45
	PF	Public Facility		65	45
	SP	Specific Plan-		55	45
		Residential			

		Specific Plan- Commercial		65	55
		Specific Plan-Light Industrial		75	55
		Specific Plan-Heavy Industrial		75	75
Rural Community	EDR	Estate Density Residential	2 AC	55	45
	VLDR	Very Low Density Residential	1 AC	55	45
	LDR	Low Density Residential	1/2 AC	55	45
Rural	RR	Rural Residential	5 AC	45	45
	RM	Rural Mountainous	10 AC	45	45
	RD	Rural Desert	10 AC	45	45
Agriculture	AG	Agriculture	10 AC	45	45
Open Space	С	Conservation		45	45
	CH	Conservation Habitat		45	45
	REC	Recreation		45	45
	RUR	Rural	20 AC	45	45
	W	Watershed		45	45
	MR	Mineral Resources		75	45

(Ord. 847 § 4, 2006)

## 9.52.050 Sound level measurement methodology.

Sound level measurements may be made anywhere within the boundaries of an occupied property. The actual location of a sound level measurement shall be at the discretion of the enforcement officials identified in Section 9.52.080 of this chapter. Sound level measurements shall be made with a sound level meter. Immediately before a measurement is made, the sound level meter shall be calibrated utilizing an acoustical calibrator meeting the standards of the American National Standards Institute. Following a sound level measurement, the calibration of the sound level meter shall be re-verified. Sound level meters and calibration equipment shall be certified annually.

(Ord. 847 § 5, 2006)

## 9.52.060 Special sound sources standards.

The general sound level standards set forth in Section 9.52.040 of this chapter apply to sound emanating from all sources, including the following special sound sources, and the person creating, or allowing the creation of, the sound is subject to the requirements of that section. The following special sound sources are also subject to the following additional standards, the failure to comply with which constitutes separate violations of this chapter:

#### A. Motor Vehicles.

- Off-Highway Vehicles.
  - a. No person shall operate an off-highway vehicle unless it is equipped with a USDA-qualified spark arrester and a constantly operating and properly maintained muffler. A muffler is not considered constantly operating and properly maintained if it is equipped with a cutout, bypass or similar device.
  - b. No person shall operate an off-highway vehicle unless the noise emitted by the vehicle is not more than ninety-six (96) dBA if the vehicle was manufactured on or after January 1, 1986 or is not more than one hundred one (101) dBA if the vehicle was manufactured before January 1, 1986. For purposes of this subsection, emitted noise shall be measured a distance of twenty (20) inches from the vehicle tailpipe using test procedures established by the Society of Automotive Engineers under Standard J-1287.
- 2. Sound Systems. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, between the hours of ten p.m. and eight a.m., such that the sound system is audible to the human ear inside any inhabited dwelling. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, at any other time such that the sound system is audible to the human ear at a distance greater than one hundred (100) feet from the vehicle.
- B. Power Tools and Equipment. No person shall operate any power tools or equipment between the hours of ten p.m. and eight a.m. such that the power tools or equipment are audible to the human ear inside an inhabited dwelling other than a dwelling in which the power tools or equipment may be located. No person shall operate any power tools or equipment at any other time such that the power tools or equipment are audible to the human ear at a distance greater than one hundred (100) feet from the power tools or equipment.
- C. Audio Equipment. No person shall operate any audio equipment, whether portable or not, between the hours of ten p.m. and eight a.m. such that the equipment is audible to the human ear inside an inhabited dwelling other than a dwelling in which the equipment may be located. No person shall operate any audio equipment, whether portable or not, at any other time such that the equipment is audible to the human ear at a distance greater than one hundred (100) feet from the equipment.
- D. Sound-Amplifying Equipment and Live Music. No person shall install, use or operate sound-amplifying equipment, or perform, or allow to be performed, live music unless such activities comply with the following requirements. To the extent that these requirements conflict with any conditions of approval attached to an underlying land use permit, these requirements shall control:
  - 1. Sound-amplifying equipment or live music is prohibited between the hours of ten p.m. and eight a.m.
  - Sound emanating from sound-amplifying equipment or live music at any other time shall not be audible to the human ear at a distance greater than two hundred (200) feet from the equipment or music.

(Ord. 847 § 6, 2006)

## 9.52.070 Exceptions.

Exceptions may be requested from the standards set forth in Section 9.52.040 or 9.52.060 of this chapter and may be characterized as construction-related, single-event or continuous-events exceptions.

#### A. Application and Processing.

- Construction-Related Exceptions. An application for a construction-related exception shall be made to and considered by the director of building and safety on forms provided by the building and safety department and shall be accompanied by the appropriate filing fee. No public hearing is required.
- 2. Single-Event Exceptions. An application for a single-event exception shall be made to and considered by the planning director on forms provided by the planning department and shall be accompanied by the appropriate filing fee. No public hearing is required.
- 3. Continuous-Events Exceptions. An application for a continuous-events exception shall be made to the planning director on forms provided by the planning department and shall be accompanied by the appropriate filing fee. Upon receipt of an application for a continuous-events exception, the planning director shall set the matter for public hearing before the planning commission, notice of which shall be given as provided in Section 18.26c of Riverside County Ordinance No. 348. Notwithstanding the above, an application for a continuous-events exception that is associated with an application for a land use permit shall be processed concurrently with the land use permit in the same manner that the land use permit is required to be processed.
- B. Requirements for Approval. The appropriate decisionmaking body or officer shall not approve an exception application unless the applicant demonstrates that the activities described in the application would not be detrimental to the health, safety or general welfare of the community. In determining whether activities are detrimental to the health, safety or general welfare of the community, the appropriate decisionmaking body or officer shall consider such factors as the proposed duration of the activities and their location in relation to sensitive receptors. If an exception application is approved, reasonable conditions may be imposed to minimize the public detriment, including, but not limited to, restrictions on sound level, sound duration and operating hours.
- C. Appeals. The director of building and safety's decision on an application for a construction-related exception is considered final. The planning director's decision on an application for a single-event exception is considered final. After making a decision on an application for a continuous-events exception, the appropriate decisionmaking body or officer shall mail notice of the decision to the applicant. Within ten (10) calendar days after the mailing of such notice, the applicant or an interested person may appeal the decision to the board of supervisors. Upon receipt of an appeal and payment of the appropriate appeal fee, the clerk of the board shall set the matter for hearing not less than five days nor more than thirty (30) days thereafter and shall give written notice of the hearing in the same manner as notice of the hearing was given by the appropriate hearing officer or body. The board of supervisors shall render its decision within thirty (30) days after the appeal hearing is closed.
- D. Effect of a Pending Continuous-Events Exception Application. For a period of one hundred eighty (180) days from the effective date of this chapter, no person creating any sound prohibited by this chapter shall be considered in violation of this chapter if the sound is related to a use that is operating pursuant to an approved land use permit, if an application for a continuous-events exception has been filed to sanction the sound and if a decision on the application is pending.

(Ord. 847 § 7, 2006)

#### 9.52.080 Enforcement.

The Riverside County sheriff and code enforcement shall have the primary responsibility for enforcing this chapter; provided, however, the sheriff and code enforcement may be assisted by the public health department. Violations shall be prosecuted as described in Section 9.52.100 of this chapter, but nothing in this chapter shall

prevent the sheriff, code enforcement or the department of public health from engaging in efforts to obtain voluntary compliance by means of warnings, notices, or educational programs.

(Ord. 847.1 § 1, 2007: Ord. 847 § 8, 2006)

## 9.52.090 Duty to cooperate.

No person shall refuse to cooperate with, or obstruct, the enforcement officials identified in Section 9.52.080 of this chapter when they are engaged in the process of enforcing the provisions of this chapter. This duty to cooperate may require a person to extinguish a sound source so that it can be determined whether sound emanating from the source violates the provisions of this chapter.

(Ord. 847 § 9, 2006)

### 9.52.100 Violations and penalties.

Any person who violates any provision of this chapter once or twice within a one hundred eighty (180) day period shall be guilty of an infraction. Any person who violates any provision of this chapter more than twice within a one hundred eighty (180) day period shall be guilty of a misdemeanor. Each day a violation is committed or permitted to continue shall constitute a separate offense and shall be punishable as such. Penalties shall not exceed the following amounts:

- A. For the first violation within a one hundred eighty (180) day period, the minimum mandatory fine shall be five hundred dollars (\$500.00).
- B. For the second violation within a one hundred eighty (180) day period, the minimum mandatory fine shall be seven hundred fifty dollars (\$750.00).
- C. For any further violations within a one hundred eighty (180) day period, the minimum mandatory fine shall be one thousand dollars (\$1,000.00) or imprisonment in the county jail for a period not exceeding six months, or both.

(Ord. 847 § 10, 2006)

# ORDINANCE NO. 847 (AS AMENDED THROUGH 847.1) AN ORDINANCE OF THE COUNTY OF RIVERSIDE AMENDING ORDINANCE NO. 847 REGULATING NOISE

The Board of Supervisors of the County of Riverside Ordains as Follows:

Section 1. INTENT. At certain levels, sound becomes noise and may jeopardize the health, safety or general welfare of Riverside County residents and degrade their quality of life. Pursuant to its police power, the Board of Supervisors hereby declares that noise shall be regulated in the manner described herein. This ordinance is intended to establish countywide standards regulating noise. This ordinance is not intended to establish thresholds of significance for the purpose of any analysis required by the California Environmental Quality Act and no such thresholds are hereby established.

Section 2. EXEMPTIONS. Sound emanating from the following sources is exempt from the provisions of this ordinance:

- a. Facilities owned or operated by or for a governmental agency.
- b. Capital improvement projects of a governmental agency.
- c. The maintenance or repair of public properties.
- d. Public safety personnel in the course of executing their official duties, including, but not limited to, sworn peace officers, emergency personnel and public utility personnel. This exemption includes, without limitation, sound emanating from all equipment used by such personnel, whether stationary or mobile.
- e. Public or private schools and school-sponsored activities
- f. Agricultural operations on land designated Agriculture in the Riverside County General Plan, or land zoned A-1 (Light Agriculture), A-P (Light Agriculture With Poultry), A-2 (Heavy Agriculture), A-D (Agriculture-Dairy) or C/V (Citrus/Vineyard), provided such operations are carried out in a manner consistent with accepted industry standards. This exemption includes, without limitation, sound emanating from all equipment used during such operations, whether stationary or mobile.
- g. Wind Energy Conversion Systems (WECS), provided such systems comply with the WECS noise provisions of Riverside County Ordinance No. 348.
- h. Private construction projects located one-quarter (1/4) of a mile or more from an inhabited dwelling.
- i. Private construction projects located within one-quarter (1/4) of a mile from an inhabited dwelling, provided that:
  - 1. Construction does not occur between the hours of 6:00 p.m. and 6:00 a.m. during the months of June through September; and
  - 2. Construction does not occur between the hours of 6:00 p.m. and 7:00 a.m. during the months of October through May.

- j. Property maintenance, including, but not limited to, the operation of lawnmowers, leaf blowers, etc., provided such maintenance occurs between the hours of 7 a.m. and 8 p.m.
- Motor vehicles, other than off-highway vehicles. This exemption does not include sound emanating from motor vehicle sound systems
- I. Heating and air conditioning equipment.
- m. Safety, warning and alarm devices, including, but not limited to, house and car alarms, and other warning devices that are designed to protect the public health, safety, and welfare.
- n. The discharge of firearms consistent with all state laws.

<u>Section 3</u>. DEFINITIONS. As used in this ordinance, the following terms shall have the following meanings:

- a. <u>Audio Equipment</u>. A television, stereo, radio, tape player, compact disc player, mp3 player, I-POD or other similar device.
- b. <u>Decibel (dB)</u>. A unit for measuring the relative amplitude of a sound equal approximately to the smallest difference normally detectable by the human ear, the range of which includes approximately one hundred thirty (130) decibels on a scale beginning with zero decibels for the faintest detectable sound. Decibels are measured with a sound level meter using different methodologies as defined below:
  - 1. A-weighting (dBA) means the standard A-weighted frequency response of a sound level meter, which de-emphasizes low and high frequencies of sound in a manner similar to the human ear for moderate sounds.
  - 2. Maximum Sound level (L<sub>max</sub>) means the maximum sound level measured on a sound level meter.
- c. <u>Governmental Agency</u>. The United States, the State of California, Riverside County, any city within Riverside County, any special district within Riverside County or any combination of these agencies.
- d. <u>Land Use Permit</u>. A discretionary permit issued by Riverside County pursuant to Riverside County Ordinance No. 348.
- e. <u>Motor Vehicle</u>. A vehicle that is self-propelled.
- f. <u>Motor Vehicle Sound System</u>. A stereo, radio, tape player, compact disc player, mp3 player, I-POD or other similar device.
- g. Noise. Any loud, discordant or disagreeable sound.
- h. <u>Occupied Property</u>. Property upon which is located a residence, business or industrial or manufacturing use.
- i. <u>Off-Highway Vehicle</u>. A motor vehicle designed to travel over any terrain.
- j. <u>Public Property</u>. Property owned by a governmental agency or held open to the public, including, but not limited to, parks, streets, sidewalks, and alleys.

- k. <u>Public or Private School</u>. An institution conducting academic instruction at the preschool, elementary school, junior high school, high school, or college level.
- I. <u>Sensitive Receptor</u>. A land use that is identified as sensitive to noise in the Noise Element of the Riverside County General Plan, including, but not limited to, residences, schools, hospitals, churches, rest homes, cemeteries or public libraries.
- m. <u>Sound Level Meter</u>. An instrument meeting the standards of the American National Standards Institute for Type 1 or Type 2 sound level meters or an instrument that provides equivalent data.
- n. <u>Sound Amplifying Equipment</u>. A loudspeaker, microphone, megaphone or other similar device.

Section 4. GENERAL SOUND LEVEL STANDARDS. No person shall create any sound, or allow the creation of any sound, on any property that causes the exterior sound level on any other occupied property to exceed the sound level standards set forth in Table 1.

		TABLE 1 SOUND LEVEL STANDARDS ( Db	Lmay )		
GENERAL	GENERAL PLAN	GENERAL PLAN LAND	-max /		/I DECIBEL VEL
PLAN FOUNDATION COMPONENT	LAND USE DESIGNATION	USE DESIGNATION NAME	DENSITY	7am- 10pm	10pm- 7am
	EDR	Estate Density Residential	2 AC	55	45
	VLDR	Very Low density	1 AC	55	45
	LDR	Low Density Residential	1/2 AC	55	45
	MDR	Medium Density	25	55	45
	MHDR	Medium High Density	58	55	45
	HDR	High Density Residential	814	55	45
	VHDR	Very High Density	14-20	55	45
	H'TDR	Residential Highest Density	20+	55	45
	CR	Retail Commercial	201	65	55
Community Development	CO	Office Commercial		65	55
Development	СТ	Tourist Commercial		65	55
	CC	Community Center		65	55
	LI	Light Industrial		75	55
	HI	Hoovy Industrial		75	75
	BP	Heavy Industrial		-	45
		Business Park		65	
	PF	Public Facility		65	45
		Specific Plan-Residential Specific Plan-		55	45
	SP	Commercial Specific Plan-Light		65	55
		Specific Plan-Heavy		75	55
Rural		Estate Density		75	75
Community	EDR	Very Low Density	2 ac	55	45
	VLDR	Pesidential	1 ac	55	45
Rural	LDR	Low Density Residential	1/2 ac	55	45
Itulai	RR	Rural Residential	5 ac	45	45
	RM	Rural Mountainous	10 ac	45	45
A	RD	Rural Desert	10 ac	45	45
Agriculture	AG	Agriculture	10 AC	45	45
Onen Charr	С	Conservation		45	45
Open Space	СН	Conservation Habitat		45	45
	REC	Recreation		45	45
	RUR	Rural	20 AC	45	45
	W	Watershed		45	45
	MR	Mineral Resources		75	45

Section 5. SOUND LEVEL MEASUREMENT METHODOLOGY. Sound level measurements may be made anywhere within the boundaries of an occupied property. The actual location of a sound level measurement shall be at the discretion of the enforcement officials identified in Section 8. of this ordinance. Sound level measurements shall be made with a sound level meter. Immediately before a measurement is made, the sound level meter shall be calibrated utilizing an acoustical calibrator meeting the standards of the American National Standards Institute. Following a sound level measurement, the calibration of the sound level meter shall be re-verified. Sound level meters and calibration equipment shall be certified annually.

Section 6. SPECIAL SOUND SOURCES STANDARDS. The general sound level standards set forth in Section 4. of this ordinance apply to sound emanating from all sources, including the following special sound sources, and the person creating, or allowing the creation of, the sound is subject to the requirements of that section. The following special sound sources are also subject to the following additional standards, the failure to comply with which constitute separate violations of this ordinance.

- a. Motor Vehicles.
  - 1. Off-Highway Vehicles.
    - i. No person shall operate an off-highway vehicle unless it is equipped with a USDA qualified spark arrester and a constantly operating and properly maintained muffler. A muffler is not considered constantly operating and properly maintained if it is equipped with a cutout, bypass or similar device.
    - ii. No person shall operate an off-highway vehicle unless the noise emitted by the vehicle is not more than 96 dBA if the vehicle was manufactured on or after January 1, 1986 or is not more that 101 dBA if the vehicle was manufactured before January 1, 1986. For purposes of this subsection, emitted noise shall be measured a distance of twenty (20) inches from the vehicle tailpipe using test procedures established by the Society of Automotive Engineers under Standard J-1287.
  - 2. Sound Systems. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, between the hours of 10:00 p.m. and 8:00 a.m., such that the sound system is audible to the human ear inside any inhabited dwelling. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, at any other time such that the sound system is audible to the human ear at a distance greater than one hundred (100) feet from the vehicle.
- b. Power Tools and Equipment. No person shall operate any power tools or equipment between the hours of 10:00 p.m. and 8:00 a.m. such that the power tools or equipment are audible to the human ear inside an inhabited dwelling other than a dwelling in which the power tools or equipment may be located. No person shall operate any power tools or equipment at any other time such that the power tools

- or equipment are audible to the human ear at a distance greater than one hundred (100) feet from the power tools or equipment.
- c. Audio Equipment. No person shall operate any audio equipment, whether portable or not, between the hours of 10:00 p.m. and 8:00 a.m. such that the equipment is audible to the human ear inside an inhabited dwelling other than a dwelling in which the equipment may be located. No person shall operate any audio equipment, whether portable or not, at any other time such that the equipment is audible to the human ear at a distance greater than one hundred (100) feet from the equipment.
- d. Sound Amplifying Equipment and Live Music. No person shall install, use or operate sound amplifying equipment, or perform, or allow to be performed, live music unless such activities comply with the following requirements. To the extent that these requirements conflict with any conditions of approval attached to an underlying land use permit, these requirements shall control.
  - 1. Sound amplifying equipment or live music is prohibited between the hours of 10:00 p.m. and 8:00 a.m.
  - 2. Sound emanating from sound amplifying equipment or live music at any other time shall not be audible to the human ear at a distance greater than two hundred (200) feet from the equipment or music.

Section 7. EXCEPTIONS. Exceptions may be requested from the standards set forth in Sections 4. or 6. of this ordinance and may be characterized as construction-related, single event or continuous events exceptions.

- a. Application and Processing.
  - Construction-Related Exceptions. An application for a construction-related exception shall be made to and considered by the Director of Building and Safety on forms provided by the Building and Safety Department and shall be accompanied by the appropriate filing fee. No public hearing is required.
  - 2. Single Event Exceptions. An application for a single event exception shall be made to and considered by the Planning Director on forms provided by the Planning Department and shall be accompanied by the appropriate filing fee. No public hearing is required.
  - 3. Continuous Events Exceptions. An application for a continuous events exception shall be made to the Planning Director on forms provided by the Planning Department and shall be accompanied by the appropriate filing fee. Upon receipt of an application for a continuous events exception, the Planning Director shall set the matter for public hearing before the Planning Commission, notice of which shall be given as provided in Section 18.26.c. of Riverside County Ordinance No. 348. Notwithstanding the above, an application for a

continuous events exception that is associated with an application for a land use permit shall be processed concurrently with the land use permit in the same manner that the land use permit is required to be processed.

- b. Requirements for Approval. The appropriate decision making body or officer shall not approve an exception application unless the applicant demonstrates that the activities described in the application would not be detrimental to the health, safety or general welfare of the community. In determining whether activities are detrimental to the health, safety or general welfare of the community, the appropriate decision making body or officer shall consider such factors as the proposed duration of the activities and their location in relation to sensitive receptors. If an exception application is approved, reasonable conditions may be imposed to minimize the public detriment, including, but not limited to, restrictions on sound level, sound duration and operating hours.
- The Director of Building and Safety's decision on an C. Appeals. application for a construction-related exception is considered final. The Planning Director's decision on an application for a single event exception is considered final. After making a decision on an application for a continuous events exception, the appropriate decision making body or officer shall mail notice of the decision to the applicant. Within ten (10) calendar days after the mailing of such notice, the applicant or an interested person may appeal the decision to the Board of Supervisors. Upon receipt of an appeal and payment of the appropriate appeal fee, the Clerk of the Board shall set the matter for hearing not less than five (5) days nor more than thirty (30) days thereafter and shall give written notice of the hearing in the same manner as notice of the hearing was given by the appropriate hearing officer or body. The Board of Supervisors shall render its decision within thirty (30) days after the appeal hearing is closed.
- d. Effect of a Pending Continuous Events Exception Application. For a period of one hundred and eighty (180) days from the effective date of this ordinance, no person creating any sound prohibited by this ordinance shall be considered in violation of this ordinance if the sound is related to a use that is operating pursuant to an approved land use permit, if an application for a continuous events exception has been filed to sanction the sound and if a decision on the application is pending.

Section 8. ENFORCEMENT. The Riverside County Sheriff and Code Enforcement shall have the primary responsibility for enforcing this ordinance; provided, however, the Sheriff and Code Enforcement may be assisted by the Public Health Department. Violations shall be prosecuted as described in Section 10. of this ordinance, but nothing in this ordinance shall prevent the Sheriff, Code Enforcement or the Department of Public Health from engaging in efforts to obtain voluntary compliance by means of warnings, notices, or educational programs.

Section 9. DUTY TO COOPERATE. No person shall refuse to cooperate with, or obstruct, the enforcement officials identified in Section 8. of this ordinance when they are engaged in the process of enforcing the provisions of this ordinance. This duty to cooperate may require a person to extinguish a sound source so that it can be determined whether sound emanating from the source violates the provisions of this ordinance.

Section 10. VIOLATIONS AND PENALTIES. Any person who violates any provision of this ordinance once or twice within a one hundred and eighty (180) day period shall be guilty of an infraction. Any person who violates any provision of this ordinance more than twice within a one hundred and eighty (180) day period shall be guilty of a misdemeanor. Each day a violation is committed or permitted to continue shall constitute a separate offense and shall be punishable as such. Penalties shall not exceed the following amounts.

- a. For the first violation within a one hundred and eighty (180) day period the minimum mandatory fine shall be five hundred dollars (\$500).
- b. For the second violation within a one hundred and eighty (180) day period the minimum mandatory fine shall be seven hundred and fifty dollars (\$750).
- c. For any further violations within a one hundred and eighty (180) day period the minimum mandatory fine shall be one thousand dollars (\$1,000) or imprisonment in the County jail for a period not exceeding six (6) months, or both.

<u>Section 11</u>. SEVERABILITY. If any provision of this ordinance, or the application thereof to any person or circumstance, is held invalid, such invalidity shall not affect the remainder of the ordinance or the application of such provision(s) to other persons or circumstances.

Section 12. SAVINGS CLAUSE. The adoption of this ordinance shall not in any manner affect the prosecution of ordinance violations, which violations were committed prior to the effective date of this ordinance, nor be construed as a waiver of any permit, license, penalty or penal provisions applicable to such violations. The provisions of this ordinance, insofar as they are substantially the same as ordinance provisions previously adopted by Riverside County relating to the same subject matter, shall be construed as restatements and continuations, and not as new enactments.

Section 13. EFFECTIVE DATE. This ordinance shall take effect 30 days after its adoption.

**Adopted:** 847 Item 3.19 of 04/04/2006 (Eff: 05/04/2006) **Amended:** 847.1 Item 3.4 of 06/19/2007 (Eff: 07/19/2007)

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**APPENDIX 5.1:** 

**STUDY AREA PHOTOS** 



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13697\_L01\_Q\_E 33, 51' 28.750000"117, 15' 43.640000"



13697\_L01\_Q\_S 33, 51' 28.750000"117, 15' 43.640000"



13697\_L01\_Q\_N 33, 51' 28.750000"117, 15' 43.640000"



13697\_L01\_Q\_W 33, 51' 28.750000"117, 15' 43.640000"



13697\_L02\_O\_E 33, 51' 16.630000"117, 16' 12.450000"



13697\_L02\_O\_S 33, 51' 16.630000"117, 16' 12.450000"



13697\_L02\_O\_N 33, 51' 16.630000"117, 16' 12.450000"



13697\_L02\_O\_W 33, 51' 16.630000"117, 16' 12.450000"



13697\_L03\_D\_E 33, 51' 16.360000"117, 15' 57.290000"



13697\_L03\_D\_S 33, 51' 16.360000"117, 15' 57.290000"



13697\_L03\_D\_N 33, 51' 16.360000"117, 15' 57.290000"



13697\_L03\_D\_W 33, 51' 16.360000"117, 15' 57.290000"



13697\_L04 A 1.North 33, 51' 12.680000"117, 15' 51.110000"



13697\_L04 A 3.East 33, 51' 12.590000"117, 15' 51.110000"



13697\_L04 A 2.South 33, 51' 12.550000"117, 15' 51.170000"



13697\_L04 A 4.West 33, 51' 12.600000"117, 15' 51.140000"



13697\_L05 G 1.North 33, 51' 13.230000"117, 15' 42.790000"



13697\_L05 G 3.East 33, 51' 13.290000"117, 15' 42.740000"



13697\_L05 G 2.South 33, 51' 13.260000"117, 15' 42.760000"



13697\_L05 G 4.West 33, 51' 13.260000"117, 15' 42.790000"



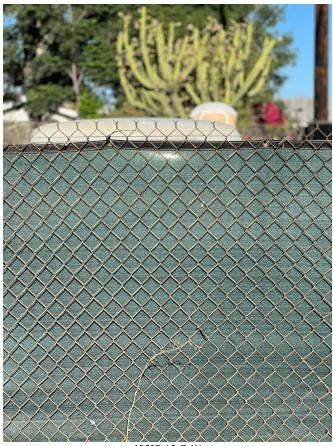
13697\_L6\_T\_E 33, 51' 32.280000"117, 15' 17.500000"



13697\_L6\_T\_S 33, 51' 32.280000"117, 15' 17.500000"



13697\_L6\_T\_N 33, 51' 32.280000"117, 15' 17.500000"



13697\_L6\_T\_W 33, 51' 32.280000"117, 15' 17.500000"

# APPENDIX 5.2:

**NOISE LEVEL MEASUREMENT WORKSHEETS** 



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#### 24-Hour Noise Level Measurement Summary Location: L1 - Located north of the Project site near the existing JN: 13697 Date: Friday, August 5, 2022 Meter: Piccolo II Project: MFBC Source: residence at 22980 Peregrine Way. Analyst: A. Shami Hourly L ea dBA Readings (unadjusted) 80.0 75.0 70.0 65.0 60.0 55.0 50.0 Hourly 58.0 6 45.0 40.0 57 56. 27 35.0 2 5 7 8 9 10 13 15 17 18 19 20 21 22 23 0 1 3 4 6 11 12 14 16 **Hour Beginning** L2% L8% L<sub>eq</sub> Adj. L <sub>eq</sub> Timeframe Hour L min L1% L5% L25% L50% L90% L95% L99% Adj. $L_{eq}$ L max 52.2 48.3 57.9 48.7 62.2 61.4 61.0 60.4 55.8 51.3 49.8 48.6 48.4 52.2 10.0 1 51.5 60.5 47.8 60.0 59.4 57.5 55.8 48.7 48.2 48.0 47.9 10.0 61.5 50.4 51.5 2 55.2 62.5 48.4 61.9 61.4 60.0 59.1 55.7 53.4 50.4 49.7 49.0 55.2 10.0 65.2 53.1 62.2 47.2 59.4 57.6 47.9 63.1 Night 3 61.7 61.2 52.8 49.8 47.6 47.3 53.1 10.0 57.8 69.5 48.1 69.1 68.1 65.2 62.6 55.7 52.1 49.0 48.6 48.2 57.8 10.0 67.8 4 5 56.2 64.4 50.0 64.0 63.3 61.6 60.2 56.7 53.8 50.8 50.4 50.1 56.2 10.0 66.2 6 60.5 70.6 52.3 70.2 69.6 67.5 64.9 59.6 56.3 53.2 52.8 52.4 60.5 10.0 70.5 68.4 53.8 68.0 67.5 65.7 64.1 59.9 57.7 54.9 54.5 54.0 59.9 0.0 59.9 59.9 8 59.0 66.6 53.0 66.2 65.7 64.2 63.1 59.6 56.6 53.9 53.5 53.1 59.0 0.0 59.0 9 55.2 52.3 58.0 66.9 51.8 66.7 66.1 64.0 61.7 57.7 52.7 52.0 58.0 0.0 58.0 10 56.3 52.0 63.8 63.2 59.6 54.5 52.8 52.5 0.0 56.3 64.1 61.4 56.4 52.1 56.3 55.6 50.6 51.5 51.1 11 63.7 63.2 62.6 60.6 59.0 55.7 53.8 50.7 55.6 0.0 55.6 12 54.5 62.8 49.4 62.4 61.8 59.9 58.5 54.5 52.3 50.2 49.8 49.5 54.5 0.0 54.5 13 54.7 62.5 49.8 62.2 61.5 59.7 58.5 54.9 52.8 50.7 50.3 49.9 54.7 0.0 54.7 Day 14 59.7 68.5 51.0 68.3 67.9 66.9 65.7 59.3 54.6 51.9 51.5 51.1 59.7 0.0 59.7 65.0 48.7 64.1 49.7 49.2 15 56.7 64.7 62.6 61.3 57.5 53.7 48.8 56.7 0.0 56.7 16 54.6 64.1 49.1 63.5 62.6 60.0 58.0 54.3 52.1 49.9 49.6 49.2 54.6 0.0 54.6 17 55.6 65.4 49.6 65.0 64.3 62.1 60.1 54.3 52.4 50.3 50.0 49.7 55.6 0.0 55.6 51.4 18 57.3 66.0 51.0 65.6 64.9 63.1 61.3 57.7 54.6 51.7 57.3 0.0 57.3 51.1 19 57.3 67.1 50.2 66.6 65.8 63.3 61.4 57.1 54.0 51.1 50.7 50.3 57.3 5.0 62.3 20 48.8 64.5 49.8 48.9 61.5 56.5 65.6 65.1 62.6 61.3 56.5 52.6 49.3 56.5 5.0 21 57.3 48.0 68.3 67.5 64.3 62.2 55.0 52.0 48.9 48.4 48.1 57.3 5.0 62.3 22 58.2 50.3 47.5 10.0 63.9 53.9 63.5 47.0 63.1 62.3 60.2 53.6 47.8 47.1 53.9 Night 23 52.9 63.8 46.1 63.1 62.0 58.9 57.1 52.2 49.1 46.7 46.5 46.2 52.9 10.0 62.9 L min L1% L2% L5% L8% L25% L50% L90% L95% L99% Leq (dBA) **Timeframe** Hour $L_{eq}$ L max 24-Hour Min 54.5 62.5 48.0 62.2 61.5 59.7 58.0 54.3 52.0 48.9 48.4 48.1 Daytime Nighttime **CNEL** Day 59.9 68.7 67.9 65.7 59.9 57.7 54.9 54.5 54.0 (7am-10pm) Max 53.8 68.3 66.9 (10pm-7am) 57.2 Average 65.3 64.7 62.7 61.1 56.7 53.9 51.3 50.9 50.6 **Energy Average 57.2** 55.8 **62.8** 51.5 60.0 59.4 57.5 55.8 50.4 48.7 46.7 46.5 46.2 Min 60.5 46.1 Night Max 60.5 70.6 52.3 70.2 69.6 67.5 64.9 59.6 56.3 53.2 52.8 52.4 **Energy Average** 55.8 Average: 63.8 63.1 60.9 59.0 54.2 51.5 49.2 48.8 48.5



#### 24-Hour Noise Level Measurement Summary JN: 13697 Date: Friday, August 5, 2022 Location: L2 - Located southwest of the Project placed near the Meter: Piccolo II Project: MFBC Source: residence at 22710 Redwood Drive. Analyst: A. Shami Hourly L ea dBA Readings (unadjusted) 80.0 75.0 70.0 65.0 66.0 Hourly 1 55.0 55.0 45.0 40.0 8 50.0 9 45.1 45.0 40.0 35.0 2 6 7 8 9 10 13 19 23 0 1 3 4 5 11 12 14 15 16 17 18 20 21 22 **Hour Beginning** L2% L8% Adj. L eq Timeframe Hour L min L1% L5% L25% L50% L90% L95% L99% $L_{eq}$ L max Adj. $L_{eq}$ 46.2 45.9 44.6 47.4 43.1 47.1 46.8 45.0 44.4 43.6 43.5 43.3 44.6 10.0 54.6 1 44.3 46.9 43.1 46.6 46.3 45.7 45.3 44.1 43.5 43.2 10.0 54.3 44.6 43.4 44.3 2 48.6 53.2 45.4 53.0 52.7 52.1 51.7 49.4 47.3 46.0 45.8 45.5 48.6 10.0 58.6 49.0 48.8 48.5 48.1 47.9 45.5 56.7 Night 3 46.7 45.0 47.2 46.6 45.3 45.1 46.7 10.0 51.2 45.7 51.0 50.7 49.7 49.1 47.4 46.3 46.1 45.9 10.0 57.7 4 47.7 48.1 47.7 5 51.2 55.5 47.2 55.2 54.7 54.1 53.6 51.9 50.7 48.4 47.9 47.4 51.2 10.0 61.2 6 54.6 62.4 50.1 62.0 61.6 60.1 58.5 54.3 52.6 50.8 50.5 50.2 54.6 10.0 64.6 72.9 57.1 72.4 71.9 71.1 70.5 67.7 64.3 59.1 58.2 57.2 66.2 0.0 66.2 66.2 8 60.9 67.6 55.0 67.0 66.4 65.2 64.6 62.2 59.2 56.1 55.6 55.2 60.9 0.0 60.9 9 71.1 57.9 63.2 70.5 69.7 67.4 66.2 63.6 61.9 59.3 58.8 58.1 63.2 0.0 63.2 10 63.7 70.2 57.4 69.7 69.1 67.5 66.7 59.3 58.5 0.0 63.7 64.5 62.6 57.7 63.7 69.9 68.7 55.8 11 64.0 54.8 69.7 69.5 69.1 65.4 61.4 55.4 54.9 64.0 0.0 64.0 12 57.7 64.1 51.0 63.1 62.1 60.9 60.6 59.1 57.9 52.1 51.7 51.2 57.7 0.0 57.7 13 55.4 60.5 50.9 60.2 59.8 59.1 58.6 56.5 54.3 52.0 51.5 51.1 55.4 0.0 55.4 Day 14 52.4 60.7 46.4 59.7 58.8 57.2 56.3 53.1 50.3 47.4 47.0 46.5 52.4 0.0 52.4 44.5 57.7 56.9 55.5 54.7 15 51.2 58.6 52.1 49.8 46.5 45.7 44.8 51.2 0.0 51.2 16 51.9 59.6 45.2 58.8 57.9 56.2 55.4 52.8 50.3 46.9 46.2 45.4 51.9 0.0 51.9 17 50.0 58.6 43.3 57.7 56.9 55.0 53.8 50.5 47.8 44.6 44.1 43.5 50.0 0.0 50.0 18 59.4 69.8 43.7 69.3 68.8 67.4 65.8 58.1 49.9 45.2 44.0 59.4 0.0 59.4 44.6 19 54.5 64.3 41.4 63.8 63.5 61.4 60.1 54.6 46.8 42.6 41.9 41.6 54.5 5.0 59.5 20 40.7 50.3 47.4 42.9 40.8 49.3 44.3 52.3 51.2 48.6 44.6 41.2 41.0 44.3 5.0 50.1 21 42.4 49.4 47.9 47.1 45.5 44.3 43.1 42.8 42.5 45.1 5.0 22 46.4 10.0 47.6 50.9 46.0 50.5 50.0 49.3 48.9 48.0 47.3 46.5 46.2 47.6 57.6 Night 23 48.3 51.2 46.8 50.9 50.6 50.0 49.7 48.7 48.0 47.2 47.1 46.9 48.3 10.0 58.3 L1% L5% L8% L25% L50% L90% L95% L99% Leq (dBA) **Timeframe** Hour $L_{eq}$ L max L min L2% 24-Hour Min 44.3 51.1 40.7 50.1 49.4 47.9 47.1 44.6 42.9 41.2 41.0 40.8 Daytime Nighttime **CNEL** Day 66.2 72.9 57.9 72.4 71.9 70.5 59.3 58.1 (7am-10pm) Max 71.1 67.7 64.3 58.8 (10pm-7am) 60.0 Average 62.7 62.1 60.6 59.8 56.7 53.6 50.1 49.5 49.0 **Energy Average** 49.4 **59.9** 60.0 44.3 46.6 46.3 45.7 45.3 44.6 44.1 43.5 43.4 43.2 Min 46.9 43.1 Night Max 54.6 62.4 50.1 62.0 61.6 60.1 58.5 54.3 52.6 50.8 50.5 50.2



50.1

48.6

47.6

46.5

46.2

46.0

Average:

51.7

51.3

50.6

**Energy Average** 

49.4

#### 24-Hour Noise Level Measurement Summary JN: 13697 Date: Friday, August 5, 2022 Location: L3 - Located southwest of the Project placed near the Meter: Piccolo II Project: MFBC Source: residence at 22721 Redwood Drive. Analyst: A. Shami Hourly L ea dBA Readings (unadjusted) 80.0 75.0 70.0 65.0 60.0 Hourly L 55.0 50.0 45.0 40.0 49.7 48.4 45.0 40.0 50. 45. 43 35.0 2 7 8 19 23 0 1 3 4 5 6 9 10 12 13 14 15 16 17 18 20 21 22 11 **Hour Beginning** L2% Adj. L <sub>eq</sub> Timeframe Hour L min L1% L5% L8% L25% L50% L90% L95% L99% $L_{eq}$ L max Adj. $L_{eq}$ 42.2 44.4 43.7 43.3 52.2 44.6 40.6 44.2 42.5 41.9 41.2 41.0 40.8 42.2 10.0 1 47.6 57.2 40.2 56.8 56.1 54.1 52.4 47.1 41.0 40.8 40.4 10.0 57.6 44.1 47.6 2 42.5 46.1 40.7 45.8 45.5 44.6 44.1 42.7 42.0 41.2 41.1 40.8 42.5 10.0 52.5 43.4 42.3 40.5 51.3 Night 3 41.3 40.0 43.2 43.0 42.6 41.6 41.2 40.4 40.2 41.3 10.0 50.2 40.2 42.4 38.7 42.2 42.0 41.6 41.4 40.0 39.2 39.1 38.8 40.2 10.0 4 40.6 5 42.7 54.1 36.7 53.4 52.5 49.5 47.1 40.1 38.2 37.1 37.0 36.8 42.7 10.0 52.7 50.1 60.2 37.3 59.8 59.0 56.5 54.5 50.5 45.8 37.8 37.6 37.4 50.1 10.0 60.1 6 48.4 57.8 38.9 57.4 56.8 54.8 53.2 48.9 44.8 39.7 39.4 39.0 48.4 0.0 48.4 8 45.7 51.7 42.8 51.1 50.6 49.4 48.6 45.8 44.6 43.5 43.2 43.0 45.7 0.0 45.7 9 51.4 58.2 46.7 57.6 56.9 55.1 53.9 52.0 50.5 48.0 47.5 47.0 51.4 0.0 51.4 10 50.7 56.6 46.0 56.1 55.4 54.0 53.3 49.9 47.3 46.8 0.0 50.7 51.4 46.2 50.7 55.6 53.6 47.9 50.6 11 50.6 46.8 55.2 54.7 53.0 51.2 49.9 47.6 47.1 50.6 0.0 12 49.7 54.0 46.3 53.7 53.4 52.4 51.8 50.5 49.1 47.3 47.0 46.5 49.7 0.0 49.7 13 49.7 54.4 45.7 54.0 53.6 52.8 52.4 50.7 48.9 46.7 46.4 45.9 49.7 0.0 49.7 Day 14 47.7 52.4 44.3 52.0 51.5 50.3 49.8 48.5 47.3 45.2 44.8 44.4 47.7 0.0 47.7 54.7 47.0 52.7 49.7 47.9 47.5 15 50.2 54.2 53.7 52.2 50.9 47.1 50.2 0.0 50.2 16 50.6 55.2 46.4 54.8 54.5 53.6 53.1 51.5 50.1 47.8 47.3 46.7 50.6 0.0 50.6 17 49.7 57.4 42.7 57.1 56.6 55.7 54.5 51.1 45.7 43.5 43.2 42.9 49.7 0.0 49.7 18 47.3 52.8 43.5 52.2 51.7 50.6 50.1 48.2 46.5 44.3 44.0 43.6 47.3 0.0 47.3 19 48.4 53.9 44.3 53.6 53.1 52.0 51.3 49.3 47.4 45.3 44.9 44.5 48.4 5.0 53.4 20 59.9 49.7 59.5 54.5 63.3 45.3 62.7 62.1 60.9 54.6 46.5 46.0 45.5 54.5 5.0 21 59.0 46.1 58.6 58.3 56.5 55.7 51.8 48.8 46.8 46.5 46.2 5.0 56.4 22 50.0 49.1 48.3 43.5 43.3 10.0 55.5 45.5 51.0 43.0 50.5 45.8 44.7 43.1 45.5 Night 23 43.7 49.7 40.6 49.1 48.6 47.4 46.6 44.2 42.7 41.2 41.0 40.7 43.7 10.0 53.7 L1% L5% L8% L25% L50% L90% L95% L99% Leq (dBA) **Timeframe** Hour $L_{eq}$ L max L min L2% 24-Hour Min 45.7 51.7 38.9 51.1 50.6 49.4 48.6 45.8 44.6 39.7 39.4 39.0 Daytime Nighttime **CNEL** Day 47.0 59.9 50.5 48.0 47.6 47.1 (7am-10pm) Max 54.5 63.3 62.7 62.1 60.9 54.6 (10pm-7am) 50.2 Average 55.4 54.9 53.6 52.8 50.4 48.2 45.8 45.5 45.0 **Energy Average** 50.2 45.2 **53.7** 40.2 42.4 42.2 42.0 41.6 41.4 40.1 38.2 37.1 37.0 36.8 Min 36.7 Night Max 50.1 60.2 43.0 59.8 59.0 56.5 54.5 50.5 45.8 43.5 43.3 43.1



46.7

43.9

42.3

40.3

40.1

39.9

Average:

49.5

49.0

47.7

**Energy Average** 

45.2

#### 24-Hour Noise Level Measurement Summary JN: 13697 Date: Tuesday, August 16, 2022 Location: L4 - Located south of the Project site near the residence at Meter: Piccolo II Project: MFBC Source: 18412 Donna Ln. Analyst: A. Shami Hourly L eq dBA Readings (unadjusted) 80.0 75.0 70.0 65.0 60.0 Hourly L 55.0 50.0 45.0 40.0 9 45.0 40.0 43 50. 45. 35.0 2 5 7 8 13 19 23 0 1 3 4 6 9 10 11 12 14 15 16 17 18 20 21 22 **Hour Beginning** L2% L8% Adj. L <sub>eq</sub> Timeframe Hour L min L1% L5% L25% L50% L90% L95% L99% $L_{eq}$ L max Adj. $L_{eq}$ 50.0 49.4 49.0 47.0 50.5 44.5 50.2 47.8 46.6 45.1 44.9 44.6 47.0 10.0 57.0 1 45.4 49.4 42.6 49.2 48.9 48.0 47.5 44.9 43.3 42.7 10.0 55.4 46.1 43.0 45.4 2 44.6 47.7 42.3 47.4 47.2 46.7 46.4 45.3 44.4 42.9 42.7 42.4 44.6 10.0 54.6 44.6 50.9 50.2 45.4 57.5 Night 3 47.5 51.4 51.1 49.6 48.0 46.9 45.1 44.7 47.5 10.0 52.7 55.5 50.6 55.3 55.1 54.7 54.3 53.3 52.5 51.2 51.0 50.7 52.7 10.0 62.7 4 5 54.5 56.7 52.8 56.5 56.4 56.0 55.8 54.9 54.3 53.3 53.1 52.8 54.5 10.0 64.5 6 53.7 56.3 52.0 56.0 55.8 55.2 54.9 54.2 53.5 52.5 52.3 52.1 53.7 10.0 63.7 58.5 63.7 54.0 63.1 62.5 61.5 61.0 59.4 57.9 55.4 54.9 54.3 58.5 0.0 58.5 8 62.7 71.4 56.7 70.6 69.9 68.3 67.1 62.7 60.0 57.5 57.2 56.8 62.7 0.0 62.7 9 69.1 58.2 59.2 58.8 62.7 68.4 67.8 66.9 66.1 63.3 61.4 58.3 62.7 0.0 62.7 10 63.6 71.7 57.6 70.9 70.4 69.5 68.7 60.6 58.5 58.2 0.0 63.6 63.4 57.8 63.6 60.2 69.1 67.2 57.9 53.3 60.2 11 52.0 68.1 65.5 64.4 60.6 54.2 52.3 60.2 0.0 12 60.2 60.2 66.8 55.9 66.2 65.6 64.6 63.8 60.6 58.6 56.8 56.5 56.0 60.2 0.0 13 56.3 63.1 50.1 62.2 61.7 60.5 59.9 57.6 54.3 51.4 50.9 50.4 56.3 0.0 56.3 Day 14 55.1 62.2 49.3 61.2 60.4 59.2 58.4 56.1 53.9 50.8 50.2 49.5 55.1 0.0 55.1 55.5 60.3 59.0 49.8 15 64.7 49.1 63.6 62.4 56.0 53.8 50.4 49.3 55.5 0.0 55.5 16 56.3 63.6 50.0 62.9 62.2 60.9 60.0 57.4 54.5 51.3 50.7 50.1 56.3 0.0 56.3 17 53.0 61.3 46.8 60.5 59.7 58.0 56.9 53.4 51.0 48.1 47.6 47.0 53.0 0.0 53.0 18 47.7 53.0 44.3 52.5 52.0 51.0 50.3 48.3 46.9 45.2 44.8 47.7 0.0 47.7 44.4 19 50.2 59.7 46.2 58.2 56.8 54.3 53.1 50.2 48.8 47.0 46.6 46.3 50.2 5.0 55.2 20 55.5 55.5 50.5 56.3 46.1 55.8 54.6 53.9 51.4 49.1 46.8 46.5 46.2 50.5 5.0 48.7 21 43.7 47.5 47.2 46.9 45.6 44.3 43.1 41.9 41.7 43.7 5.0 41.3 46.1 41.4 22 43.4 10.0 60.9 50.9 56.5 43.0 56.3 56.1 55.6 55.2 53.0 48.4 43.8 43.1 50.9 Night 23 45.9 49.1 43.5 48.8 48.6 48.0 47.6 46.5 45.6 44.2 43.9 43.6 45.9 10.0 55.9 L max L min L1% L5% L8% L25% L50% L90% L95% L99% Leq (dBA) **Timeframe** Hour $L_{eq}$ L2% 24-Hour Min 43.7 47.5 41.3 47.2 46.9 46.1 45.6 44.3 43.1 41.9 41.7 41.4 Daytime Nighttime **CNEL** Day 63.6 70.4 69.5 68.7 59.2 58.8 58.3 (7am-10pm) Max 71.7 58.2 70.9 63.4 61.4 (10pm-7am) 58.6 Average 62.1 61.4 60.1 59.2 56.3 54.1 51.6 51.2 50.7 **Energy Average** 58.6 **59.6** 50.6 44.6 47.4 47.2 46.7 46.4 45.3 44.4 42.9 42.7 42.4 Min 47.7 42.3 Night Max 54.5 56.7 52.8 56.5 56.4 56.0 55.8 54.9 54.3 53.3 53.1 52.8 **Energy Average** 50.6 Average: 52.3 52.1 51.5 51.1 49.9 48.6 46.9 46.6 46.3



#### 24-Hour Noise Level Measurement Summary JN: 13697 Date: Tuesday, August 16, 2022 Location: L5 - Located south of the Project site near the residence at Meter: Piccolo II Project: MFBC Source: 18391 Seaton Avenue. Analyst: A. Shami Hourly L eq dBA Readings (unadjusted) 80.0 75.0 70.0 65.0 66.0 55.0 50.0 Hourly 61 59 45.0 40.0 57 56. 35.0 2 5 7 8 9 10 13 17 18 19 20 21 22 23 0 1 3 4 6 11 12 14 15 16 **Hour Beginning** L2% L8% Adj. L <sub>eq</sub> Timeframe Hour L min L1% L5% L25% L50% L90% L95% L99% $L_{eq}$ L max $L_{eq}$ Adj. 53.9 59.3 58.0 63.9 61.5 47.8 61.1 60.5 54.5 51.5 48.7 48.3 47.9 53.9 10.0 1 50.8 57.5 46.1 57.2 56.7 54.7 49.1 46.9 46.2 10.0 60.8 55.5 51.2 46.6 50.8 2 52.0 59.1 45.2 58.7 58.3 57.5 56.8 52.8 49.0 45.9 45.6 45.3 52.0 10.0 62.0 55.3 62.1 48.3 60.5 59.5 49.4 65.3 Night 3 61.8 61.5 56.1 53.4 48.9 48.4 55.3 10.0 59.2 65.6 53.8 65.2 64.6 63.4 62.7 57.8 54.8 54.3 53.9 59.2 10.0 69.2 4 60.1 5 60.1 65.0 55.9 64.8 64.6 63.9 63.3 61.0 59.1 56.7 56.3 56.0 60.1 10.0 70.1 61.0 6 60.2 64.8 56.4 64.6 64.4 63.8 63.1 59.4 57.2 56.8 56.5 60.2 10.0 70.2 68.4 59.5 67.1 63.2 60.7 60.2 59.7 0.0 63.6 63.6 67.8 66.3 65.7 64.4 63.6 8 59.8 66.7 53.7 65.9 65.2 63.7 63.0 60.7 58.7 55.3 54.7 54.0 59.8 0.0 59.8 9 58.3 60.2 69.4 52.4 68.3 67.4 65.2 64.0 60.8 54.3 53.6 52.7 60.2 0.0 60.2 10 59.4 53.6 64.9 64.3 63.2 62.5 58.4 55.3 54.6 0.0 59.4 65.6 60.5 53.9 59.4 60.8 55.7 57.3 56.6 60.8 11 65.9 65.5 64.9 64.0 63.6 61.7 60.2 55.9 60.8 0.0 12 58.5 64.8 53.6 64.1 63.4 62.4 61.7 59.2 57.4 54.9 54.4 53.8 58.5 0.0 58.5 13 60.3 66.0 56.0 65.3 64.7 63.6 63.0 61.0 59.6 57.2 56.8 56.2 60.3 0.0 60.3 Day 14 61.4 67.1 56.3 66.5 66.0 65.1 64.5 62.4 60.5 57.6 57.1 56.5 61.4 0.0 61.4 58.8 62.5 58.3 55.5 15 63.3 54.8 62.9 61.7 61.3 59.5 56.0 55.0 58.8 0.0 58.8 16 59.7 65.5 54.6 65.1 64.5 63.4 62.8 60.7 58.6 56.0 55.5 54.8 59.7 0.0 59.7 17 57.8 63.0 52.5 62.7 62.3 61.5 60.9 58.7 57.0 53.9 53.4 52.7 57.8 0.0 57.8 18 56.0 61.0 50.8 60.7 60.4 59.6 59.0 57.1 55.2 52.2 51.6 0.0 56.0 51.0 56.0 19 56.9 62.9 50.8 62.6 62.2 61.1 60.4 58.1 55.5 52.1 51.4 50.9 56.9 5.0 61.9 20 50.5 62.5 60.6 56.7 63.2 62.9 61.5 57.5 54.9 51.5 51.1 50.6 56.7 5.0 61.7 60.7 21 66.2 47.2 64.7 63.4 61.0 59.8 56.2 52.2 48.6 48.1 47 4 55.7 5.0 22 52.1 48.0 10.0 55.0 61.6 47.4 61.4 61.2 60.3 59.8 56.3 48.5 47.5 55.0 65.0 Night 23 50.9 56.2 46.4 56.0 55.8 55.1 54.5 52.0 49.5 47.0 46.7 46.5 50.9 10.0 60.9 L min L1% L2% L5% L8% L25% L50% L90% L95% L99% Leq (dBA) **Timeframe** Hour $L_{eq}$ L max 24-Hour 48.1 Min 55.7 61.0 47.2 60.7 60.4 59.6 59.0 56.2 52.2 48.6 47.4 Daytime Nighttime **CNEL** Day 63.6 59.5 67.4 65.7 60.7 59.7 (7am-10pm) Max 69.4 68.3 66.3 64.4 63.2 60.2 (10pm-7am) 59.6 Average 64.7 64.0 62.9 62.2 59.9 57.9 54.9 54.3 53.7 **Energy Average** 59.6 56.7 63.9 50.8 56.0 55.8 55.1 54.5 51.2 49.0 45.9 45.6 45.3 Min 56.2 45.2 Night Max 60.2 65.6 56.4 65.2 64.6 63.9 63.3 61.0 59.4 57.2 56.8 56.5 **Energy Average** 56.7 Average: 61.2 60.8 59.9 59.2 56.1 53.4 50.6 50.2 49.8



#### 24-Hour Noise Level Measurement Summary Location: L6 - Located east of the Project site near the residence at JN: 13697 Date: Friday, August 5, 2022 Meter: Piccolo II Project: MFBC Source: 18100 California 395. Analyst: A. Shami Hourly L eq dBA Readings (unadjusted) 80.0 75.0 70.0 65.0 660.0 Hourly 1 55.0 55.0 45.0 40.0 58. 45.0 40.0 57 57 35.0 7 2 5 6 8 9 10 13 17 19 21 23 0 1 3 4 11 12 14 15 16 18 20 22 **Hour Beginning** L2% L8% Adj. L eq Timeframe Hour L min L1% L5% L25% L50% L90% L95% L99% L eq $L_{eq}$ L max Adj. 48.5 54.3 52.2 58.5 54.7 44.4 53.8 51.2 49.0 47.4 45.5 45.1 44.7 48.5 10.0 1 47.7 53.8 42.9 53.3 52.8 51.9 51.2 46.3 44.1 43.7 43.2 47.7 10.0 57.7 48.4 2 47.8 53.7 43.6 53.2 52.7 51.6 50.9 48.5 46.8 44.7 44.3 43.8 47.8 10.0 57.8 56.4 56.1 55.6 54.1 53.3 59.8 Night 3 49.8 45.0 50.4 48.5 46.1 45.6 45.2 49.8 10.0 51.6 57.4 46.7 57.0 56.6 55.4 54.7 52.3 50.5 47.8 47.4 10.0 61.6 4 46.9 51.6 5 53.5 61.0 48.2 60.4 59.8 58.0 56.5 54.0 52.1 49.3 48.8 48.4 53.5 10.0 63.5 58.9 68.5 50.4 67.7 67.2 65.3 64.2 58.0 55.2 51.5 51.1 50.6 58.9 10.0 68.9 6 55.8 51.0 63.1 62.4 61.0 59.5 55.9 54.1 51.8 51.5 51.1 55.8 0.0 55.8 63.6 8 55.1 63.1 48.8 62.8 62.2 60.7 59.5 55.2 52.5 49.8 49.4 48.9 55.1 0.0 55.1 9 57.3 66.4 51.6 65.9 65.3 62.8 61.2 56.9 54.8 52.4 52.1 51.7 57.3 0.0 57.3 10 57.3 65.1 52.2 64.7 64.2 62.5 60.9 55.2 53.3 52.8 0.0 57.3 57.5 52.3 57.3 57.1 63.6 60.5 52.7 57.1 11 64.1 51.6 63.1 61.6 57.7 56.0 52.3 51.8 57.1 0.0 12 55.6 65.9 50.2 65.3 64.2 61.4 59.0 54.8 52.8 50.9 50.6 50.4 55.6 0.0 55.6 13 57.0 67.2 50.1 66.8 66.2 63.6 61.6 55.3 52.6 50.7 50.5 50.2 57.0 0.0 57.0 Day 14 57.5 68.1 51.0 67.4 66.5 63.8 62.1 56.2 53.9 52.0 51.6 51.1 57.5 0.0 57.5 60.3 58.7 48.9 15 53.3 61.2 48.4 60.8 56.9 53.4 51.5 49.2 48.6 53.3 0.0 53.3 16 53.1 60.9 48.9 60.6 60.2 58.2 56.2 52.8 51.4 49.7 49.4 49.0 53.1 0.0 53.1 17 54.5 63.3 50.0 62.8 62.1 60.0 57.7 54.0 52.5 50.7 50.4 50.1 54.5 0.0 54.5 18 55.0 63.1 50.5 62.8 62.3 60.2 58.0 53.2 51.3 51.0 50.6 55.0 0.0 55.0 54.9 19 57.8 68.5 51.9 67.8 66.7 63.4 61.2 57.4 54.3 52.6 52.3 52.0 57.8 5.0 62.8 20 49.1 60.8 59.1 50.0 59.1 54.1 61.7 61.3 57.9 54.7 52.1 49.6 49.2 54.1 5.0 21 54.4 63.6 48.2 62.9 59.1 53.3 51.2 49.0 48.7 48.3 54.4 5.0 59.4 63.3 61.0 22 54.8 49.8 47.0 10.0 51.6 60.0 46.5 59.6 58.8 56.5 51.8 47.4 46.7 51.6 61.6 Night 23 49.4 55.9 45.0 55.5 55.0 53.5 52.5 50.0 48.0 45.9 45.6 45.1 49.4 10.0 59.4 L max L1% L2% L5% L8% L25% L50% L90% L95% L99% Leq (dBA) **Timeframe** Hour $L_{eq}$ L min 24-Hour 48.7 Min 53.1 60.9 48.2 60.6 60.2 58.2 56.2 52.8 51.2 49.0 48.3 Daytime Nighttime **CNEL** Day 57.8 66.7 57.7 53.3 52.3 (7am-10pm) Max 68.5 52.2 67.8 63.8 62.1 56.0 52.8 (10pm-7am) 55.9 Average 63.9 63.3 61.2 59.4 55.3 53.2 51.1 50.7 50.4 **Energy Average** 55.9 52.7 60.2 47.7 53.2 52.7 51.6 50.9 48.4 46.3 44.1 43.7 43.2 Min 53.7 42.9 Night Max 58.9 68.5 50.4 67.7 67.2 65.3 64.2 58.0 55.2 51.5 51.1 50.6 **Energy Average** 52.7 Average: 57.5 56.9 55.4 54.4 51.4 49.4 46.9 46.5 46.1



# **APPENDIX 7.1:**

**OFF-SITE TRAFFIC NOISE LEVEL CALCULATIONS** 



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	FHWA-RE	D-77-108 HIGH	WAY I	NOISE	PREDIC	TION	MODEL	(9/12/2	2021)			
	rio: E ne: Harvill Av. nt: n/o Old Ole	eander					t Name: Number:		C (Building	17)		
	SPECIFIC IN	IPUT DATA							EL INPUT	s		
Highway Data					Site Con	ditions	(Hard =	: 10, S	oft = 15)			
Average Daily	Traffic (Adt):	8,466 vehicle	es					Autos	: 15			
Peak Hour	Percentage:	7.00%			Me	dium T	rucks (2	Axles)	: 15			
Peak H	lour Volume:	593 vehicle	S		He	avy Tru	icks (3+	Axles)	: 15			
Ve	hicle Speed:	50 mph		ŀ	Vehicle I	/lix						
Near/Far La	ne Distance:	48 feet		ŀ		cleTyp	e	Day	Evening	Nigi	nt	Daily
Site Data							Autos:	74.79		17.		89.28%
Ra	rrier Height:	0.0 feet			Me	edium 1	rucks:	88.5	% 1.1%	10.	4%	3.19%
Barrier Type (0-W		0.0			F	leavy 1	rucks:	75.19	% 8.0%	16.	9%	7.54%
Centerline Di		59.0 feet		ŀ	Noise Sc			- /:	E4)			
Centerline Dist.	to Observer:	59.0 feet		ŀ	Noise Sc				eet)			
Barrier Distance	to Observer:	0.0 feet			A de eller	Auto n Truci		.000				
Observer Height	(Above Pad):	5.0 feet						.297	Grade Ad	livetm	ant.	2.0
P	ad Elevation:	0.0 feet			Heav	y Truci	KS: 8	.004	Grade At	ijusuri	ciii. (	J.U
Ro	ad Elevation:	0.0 feet			Lane Equ	ıivalen	t Distan	ce (in	feet)			
	Road Grade:	0.0%				Auto	os: 54	.129				
	Left View:	-90.0 degree	es		Mediui	n Truci	ks: 53	.966				
	Right View:	90.0 degree	es		Heav	y Truci	ks: 53	.982				
FHWA Noise Mod	el Calculation	s										
VehicleType	REMEL	Traffic Flow	Dist	tance	Finite	Road	Fres	nel	Barrier At	ten .	Berm	Atten
Autos:	70.20	-5.06		-0.6	32	-1.20		-4.69	0.	000		0.000
Medium Trucks:	81.00	-19.53		-0.6	30	-1.20		-4.88	0.	000		0.000
Heavy Trucks:	85.38	-15.80		-0.6	30	-1.20		-5.35	0.	000		0.000
Unmitigated Noise	e Levels (with	out Topo and	barrie	r atter	nuation)							
VehicleType	Leq Peak Hou	ır Leq Day	,	Leq E	vening	Leg	Night		Ldn		CNE	ΞL
Autos:	00	1.3	62.8		59.0		57.	8	65.	2		65.5
Medium Trucks:	00	1.7	59.9		46.9		51.	8	60.	3		60.3
Heavy Trucks:			67.3		63.6		62.	1	69.	_		69.8
Vehicle Noise:	69	0.6	69.2		64.9		63.	7	71.	3		71.5
Centerline Distant	ce to Noise Co	ontour (in feet	)									
				70	dBA	65	dBA		60 dBA		55 d	
			Ldn:		72		154	-	333			716
		C	VEL:		75		16	I	346	6		746

		D-77-108 HIGH	WAI	NOISE	TREDIC			,					
	io: EAC								(Building 1	17)			
	e: Harvill Av.					Job N	umber:	13697					
Road Segmei	nt: n/o Old Ole	eander											
	SPECIFIC IN	IPUT DATA							L INPUT	S			
Highway Data					Site Con	ditions	(Hard :	= 10, S	oft = 15)				
Average Daily	Traffic (Adt):	24,657 vehicl	les		Autos: 15								
Peak Hour	Percentage:	7.00%			Me	dium Tr	ucks (2	Axles)	15				
Peak H	lour Volume:	1,726 vehicle	es		He	avy Tru	cks (3+	Axles).	15				
Ve	hicle Speed:	50 mph		F	Vehicle I	Wix							
Near/Far La	ne Distance:	48 feet		1		icleType		Day	Evening	Night	Daily		
Site Data							Autos:	74.79	6 7.7%	17.6%	89.28%		
Rai	rrier Height:	0.0 feet			M	edium T	rucks:	88.59	6 1.1%	10.4%	3.19%		
Barrier Type (0-W		0.0			I	Heavy T	rucks:	75.19	8.0%	16.9%	7.54%		
Centerline Dis		59.0 feet		-	Noise Sc	roo E	ovetio	na (in f	not)				
Centerline Dist.	to Observer:	59.0 feet		F	Noise 30	Auto		.000	eet)				
Barrier Distance	to Observer:	0.0 feet			Modius	m Truck		.297					
Observer Height (	Above Pad):	5.0 feet				y Truck		1.004	Grade Ad	iuctman	t: 0.0		
Pa	ad Elevation:	0.0 feet			пеач	ry ITUCK	s. c	.004	Grade Au	jusunen	1. 0.0		
Ros	ad Elevation:	0.0 feet			Lane Eq	uivalen	Distar	nce (in	feet)				
1	Road Grade:	0.0%				Auto	s: 54	1.129					
	Left View:	-90.0 degre	es		Mediu	m Truck	s: 53	3.966					
	Right View:	90.0 degre	es		Heav	ry Truck	s: 53	3.982					
FHWA Noise Mode	el Calculation	s											
VehicleType	REMEL	Traffic Flow		stance		Road	Fres		Barrier Att		rm Atten		
Autos:	70.20	-0.42	-	-0.6		-1.20		-4.69		000	0.000		
Medium Trucks:	81.00			-0.6		-1.20		-4.88		000	0.000		
Heavy Trucks:	85.38	-11.15	5	-0.6	30	-1.20		-5.35	0.0	000	0.000		
Unmitigated Noise										,			
VehicleType	Leq Peak Hou		,	Leq E	vening		Night		Ldn		NEL		
Autos:	68		67.5		63.6		62		69.8	-	70.		
Medium Trucks:	64		64.5		51.5		56		64.9		65.0		
Heavy Trucks: Vehicle Noise:	72	1.4	71.9		68.2 69.6		66 68		74.1 75.9		74.		
Centerline Distance													
cemeriine Distant	e to Noise Co	nitour (iii fee	9	70	dBA	65	dBA		60 dBA	55	dBA		
			Ldn:		146		31	5	678	,	1,461		

	FHWA-RD	-77-108 HIGH	WAY I	NOISE	PREDIC	TION N	IODEL (	9/12/2	021)				
Scenario	o: E+P					Project	Name:	MFBC	(Building 1	17)			
	e: Harvill Av.					Job ∧	lumber:	13697					
Road Segmen	t: n/o Old Ole	ander											
SITE S Highway Data	SPECIFIC IN	PUT DATA			NOISE MODEL INPUTS Site Conditions (Hard = 10, Soft = 15)								
	F 65 (4 11)	0.070			site Con	uitions							
Average Daily	. ,	8,679 vehicle	es			-ti T		Autos:					
Peak Hour I		7.00%					ucks (2 /	,					
	our Volume:	608 vehicle	8		HE	avy iru	cks (3+ )	4xies).	15				
	nicle Speed:	50 mph		١	/ehicle	Mix							
Near/Far Lar	e Distance:	48 feet			Veh	icleType		Day	Evening	Night	Daily		
Site Data							Autos:	74.7%	7.7%	17.6%	88.90		
Bar	rier Height:	0.0 feet			М	edium T	rucks:	88.5%	1.1%	10.4%	3.21		
Barrier Type (0-Wa	all, 1-Berm):	0.0				Heavy T	rucks:	75.1%	8.0%	16.9%	7.89		
Centerline Dis		59.0 feet		,	Voise S	ource E	levation	s (in f	eet)				
Centerline Dist. t		59.0 feet				Auto		000	,				
Barrier Distance t	o Observer:	0.0 feet			Mediu	m Truck		297					
Observer Height (/	Above Pad):	5.0 feet				/y Truck		004	Grade Ad	iustmen	: 0.0		
Pa	d Elevation:	0.0 feet				•							
Roa	d Elevation:	0.0 feet		L	.ane Eq		t Distan		feet)				
F	Road Grade:	0.0%				Auto		129					
	Left View:	-90.0 degree	es			m Truck	00.	966					
	Right View:	90.0 degree	es		Heav	y Truck	s: 53.	982					
FHWA Noise Mode													
VehicleType	REMEL	Traffic Flow	Dist	ance		Road	Fresr		Barrier Att		m Atter		
Autos:	70.20	-4.97		-0.62		-1.20		-4.69		000	0.00		
Medium Trucks:	81.00	-19.39		-0.60	-	-1.20		-4.88		000	0.00		
Heavy Trucks:	85.38	-15.49		-0.60		-1.20		-5.35	0.0	000	0.00		
Unmitigated Noise	-						A Control	_	I do	_	NIT!		
VehicleType Autos:	Leq Peak Hou			Leq Ev			Night		Ldn	_	NEL		
Medium Trucks:	63.	-	62.9 60.0		59.1 47.0		57.9 52.0		65.3 60.4		65		
Heavy Trucks:	59.							-			60		
Vehicle Noise:	68. 69.		67.6 69.4		63.9 65.2		62.4		69.9 71.5		70 71		
Centerline Distanc	e to Noise Co	ntour (in feet	)										
		. ,		70 d	iBA	65	dBA		60 dBA	55	dBA		
			Ldn:		74		160		345	;	74		

Saturday, December 3, 2022

	FHWA-RI	D-77-108 HIG	HWAY	NOIS	E PREDIC	TION M	ODEL	. (9/12/2	021)		
Road Nan	rio: EAC+P ne: Harvill Av. nt: n/o Old Ol	eander						: MFBC :: 13697	(Building	17)	
	SPECIFIC IN	IPUT DATA							L INPUT	s	
Highway Data					Site Con	ditions (	Hard	= 10, Sc	oft = 15)		
Average Daily	Traffic (Adt):	24,870 vehic	les					Autos:	15		
Peak Hour	Percentage:	7.00%			Ме	dium Tru	icks (2	2 Axles):	15		
Peak F	lour Volume:	1,741 vehicle	es		He	avy Truc	ks (3-	+ Axles):	15		
Ve	ehicle Speed:	50 mph			Vehicle I	Miv					
Near/Far La	ne Distance:	48 feet				icleType	П	Dav	Evening	Night	Dailv
Site Data							utos:	74.7%	-	17.6%	. ,
	rrier Heiaht:	0.0 feet			Me	edium Tr	ucks:	88.5%	1.1%	10.4%	
Barrier Type (0-V		0.0 reet 0.0				leavy Tr			8.0%	16.9%	
	ist. to Barrier:	59.0 feet			Noise Sc		41-	( 6	41		
Centerline Dist.	to Observer:	59.0 feet			Noise Sc			_ •	eet)		
Barrier Distance	to Observer:	0.0 feet				Autos m Trucks		0.000			
Observer Height	(Above Pad):	5.0 feet						2.297	0	···	
P	ad Elevation:	0.0 feet			Heav	y Trucks		8.004	Grade Ad	justrnent	. 0.0
Ro	ad Elevation:	0.0 feet			Lane Equ	uivalent	Dista	nce (in	feet)		
	Road Grade:	0.0%				Autos	: 5	4.129			
	Left View:	-90.0 degre	ees		Mediui	m Trucks	: 5	3.966			
	Right View:	90.0 degre	ees		Heav	y Trucks	: 5	3.982			
FHWA Noise Mod	el Calculation	s									
VehicleType	REMEL	Traffic Flow	Di	stance	Finite	Road	Fre	snel	Barrier Att	en Ber	m Atten
Autos:	70.20	-0.3	9	-0.0	62	-1.20		-4.69	0.	000	0.000
Medium Trucks:	81.00	-14.8	4	-0.6	60	-1.20		-4.88	0.	000	0.000
Heavy Trucks:	85.38	-11.0	5	-0.0	30	-1.20		-5.35	0.	000	0.000
Unmitigated Nois	e Levels (with	out Topo and	l barri	ier atte	nuation)						
VehicleType	Leq Peak Hou	ır Leq Da	iy .	Leq E	vening	Leq I	Vight		Ldn		NEL
Autos:		3.0	67.5		63.6			2.5	69.	9	70.1
Medium Trucks:	64	.4	64.6		51.6		56	3.5	65.	0	65.0
Heavy Trucks:	72	2.5	72.0		68.3		66	8.8	74.	3	74.6
Vehicle Noise:	74	1.3	73.9		69.7		68	3.5	76.	0	76.3
Centerline Distan	ce to Noise Co	ontour (in fee	t)								
				70	dBA	65 c			60 dBA		dBA
			Ldn:		148		31		687		1,480
		(	NEL:		154		33	32	716	3	1,542

Saturday, December 3, 2022

	FHWA-RI	D-77-108 HIGH	IWAY	NOISE	PREDIC	CTION N	MODEL (	9/12/2	021)		
	io: E ne: Harvill Av. nt: n/o Comm	erce Ctr. Dr.					t Name: lumber:		(Building 1	17)	
	SPECIFIC IN	IPUT DATA							L INPUT	S	
Highway Data					Site Cor	ditions	(Hard =	10, S	oft = 15)		
Average Daily	Traffic (Adt):	9,371 vehicle	es					Autos.	15		
Peak Hour	Percentage:	7.00%			Me	edium Tr	ucks (2	Axles)	: 15		
Peak H	lour Volume:	656 vehicle	S		He	eavy Tru	cks (3+	Axles).	15		
Ve	hicle Speed:	50 mph		ŀ	Vehicle	Miv					
Near/Far La	ne Distance:	48 feet		ŀ		icleType	9	Day	Evening	Night	Daily
Site Data							Autos:	74.79	6 7.7%	17.6	% 89.28%
Ra	rrier Height:	0.0 feet			М	edium T	rucks:	88.59	6 1.1%	10.4	% 3.19%
Barrier Type (0-W		0.0				Heavy T	rucks:	75.19	6 8.0%	16.9	% 7.54%
Centerline Di		59.0 feet									
Centerline Dist	to Observer:	59.0 feet			Noise S				eet)		
Barrier Distance	to Observer:	0.0 feet				Auto		.000			
Observer Height	(Above Pad):	5.0 feet				m Truck		297	0	·	-4.00
	ad Elevation:	0.0 feet			Hea	vy Truck	s: 8	.004	Grade Ad	justme	nt: 0.0
Roi	ad Elevation:	0.0 feet		ı	Lane Eq	uivalen	t Distan	ce (in	feet)		
	Road Grade:	0.0%		ı		Auto	s: 54	.129			
	Left View:	-90.0 degree	es		Mediu	m Truck	s: 53	.966			
	Right View:	90.0 degree	es		Hea	vy Truck	s: 53	.982			
FHWA Noise Mode	el Calculation	s									
VehicleType	REMEL	Traffic Flow	Dis	tance	Finite	Road	Fresi	nel	Barrier Att	en B	erm Atten
Autos:	70.20	-4.62		-0.6	-	-1.20		-4.69		000	0.000
Medium Trucks:				-0.6		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-15.35		-0.6	30	-1.20		-5.35	0.0	000	0.000
Unmitigated Noise	e Levels (with	out Topo and	barrie	er atter	nuation)						
VehicleType	Leq Peak Hou	ır Leq Day	/	Leq E	vening	Leq	Night		Ldn		CNEL
Autos:	63		63.3		59.4		58.	_	65.6	-	65.9
Medium Trucks:	60	1.1	60.3		47.3		52.	3	60.7	7	60.8
Heavy Trucks:	68		67.7		64.0		62.	-	70.0	-	70.3
Vehicle Noise:			69.6		65.4	•	64.	2	71.	/	72.0
Centerline Distant	ce to Noise Co	ontour (in feet	)	70				1			
			L	70	dBA 77	65	dBA	_	60 dBA		55 dBA
			Ldn:		77		165		356		767
		C	NEL:		80		172	<u>'</u>	371		798

	FHWA-RI	0-77-108 HIGH	TWAY	NOISE	PREDIC	CTION N	IODEL	(9/12/2	021)				
Road Nam	io: EAC ne: Harvill Av. nt: n/o Comm	erce Ctr. Dr.						MFBC 13697	(Building 1	7)			
	SPECIFIC IN	IPUT DATA							L INPUT	S			
Highway Data					Site Con	ditions	(Hard	= 10, S	oft = 15)				
Average Daily	Traffic (Adt):	25,486 vehicl	les		Autos: 15								
Peak Hour	Percentage:	7.00%			Me	edium Tr	ucks (2	Axles).	15				
Peak H	lour Volume:	1,784 vehicle	es		He	eavy Tru	cks (3+	Axles):	15				
Ve	hicle Speed:	50 mph		,	Vehicle	Mix							
Near/Far La	ne Distance:	48 feet		ľ		icleType		Day	Evening	Night	Daily		
Site Data							Autos:	74.7%	6 7.7%	17.6%	89.28%		
Bai	rrier Height:	0.0 feet			М	edium T	rucks:	88.5%	6 1.1%	10.4%	3.19%		
Barrier Type (0-W		0.0			- 1	Heavy T	rucks:	75.1%	8.0%	16.9%	7.54%		
Centerline Dis	st. to Barrier:	59.0 feet		-	Noise So	ourco E	lovatio	ne (in f	not)				
Centerline Dist.	to Observer:	59.0 feet		ľ	V0/36 30	Auto		0.000	eei)				
Barrier Distance	to Observer:	0.0 feet			Modiu	m Truck		2.297					
Observer Height (	Above Pad):	5.0 feet				vy Truck		3.004	Grade Ad	iustment	. 0 0		
Pa	ad Elevation:	0.0 feet								0011110111	. 0.0		
Ros	ad Elevation:	0.0 feet		1	Lane Eq				feet)				
ı	Road Grade:	0.0%				Auto		1.129					
	Left View:	-90.0 degre				m Truck		3.966					
	Right View:	90.0 degre	es		Heav	vy Truck	s: 53	3.982					
FHWA Noise Mode	el Calculation	s											
VehicleType	REMEL	Traffic Flow		stance		Road	Fres		Barrier Att		m Atten		
Autos:	70.20	-0.27		-0.6		-1.20		-4.69		000	0.000		
Medium Trucks:		-14.74		-0.6	-	-1.20		-4.88		000	0.000		
Heavy Trucks:	85.38	-11.01		-0.6	-	-1.20		-5.35	0.0	000	0.00		
Unmitigated Noise										_			
VehicleType	Leq Peak Hou		,	Leq E		,	Night		Ldn 70.0		NEL 70.2		
Autos: Medium Trucks:	68 64		67.6 64.7		63.8 51.7		62 56		70.0 65.1	-	65.		
Heavy Trucks:	72		72.1		68.4		66		74.		74.6		
Vehicle Noise:	74		74.0		69.7		68		76.		76.3		
Centerline Distance	ce to Noise Co	ontour (in fee	t)										
		(	,	70 c	dBA	65	dBA	-	60 dBA	55	dBA		
			Ldn:		149		32	2	693		1,494		
		_	NEL:		156		33		722		1,556		

Road Nam	io: E+P ne: Harvill Av. nt: n/o Comme	erce Ctr. Dr.						: MFBC :: 13697	(Building	17)	
	SPECIFIC IN	PUT DATA			24- 0				L INPUT	S	
Highway Data	- ~	0.000 1:1		3	site Con	ditions	(Hara	Autos:			
Average Daily	. ,	9,626 vehicles			140	dium Tr	uaka (				
	Percentage:	7.00%					(	,			
	lour Volume:	674 vehicles			HE	avy Tru	CKS (31	Axies):	15		
	hicle Speed:	50 mph		l	/ehicle	Mix					
Near/Far La	ne Distance:	48 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data						,	Autos:	74.7%	7.7%	17.6%	89.379
Ba	rrier Height:	0.0 feet			М	edium T	rucks:	88.5%	1.1%	10.4%	3.149
Barrier Type (0-W	/all, 1-Berm):	0.0				Heavy T	rucks:	75.1%	8.0%	16.9%	7.509
Centerline Di	st. to Barrier:	59.0 feet			Vaina C	ource E	lovestic	na (in f	2041		
Centerline Dist.	to Observer:	59.0 feet		-	V0/36 30	Auto		0.000	ei)		
Barrier Distance	to Observer:	0.0 feet			Modiu	m Truck		2.297			
Observer Height	(Above Pad):	5.0 feet				n Truck vy Truck		8.004	Grade Ad	liustment	. 0 0
P	ad Elevation:	0.0 feet			rical	ry IIUCK	S. 1	0.004	0,000,10	jaoumom	0.0
Ro	ad Elevation:	0.0 feet		L	ane Eq	uivalen	t Dista	nce (in	feet)		
	Road Grade:	0.0%				Auto	s: 5	4.129			
	Left View:	-90.0 degrees			Mediu	m Truck	s: 5	3.966			
	Right View:	90.0 degrees			Hear	y Truck	s: 5	3.982			
FHWA Noise Mod			D: /		T =- ''				5		
VehicleType Autos:	REMEL 70.20	Traffic Flow -4.50	Dista	-0.62		-1.20	Fre.	snel -4.69	Barrier Att		m Atten
Medium Trucks:		-4.50 -19.05		-0.60	_	-1.20		-4.88		000 000	0.00
Heavy Trucks:		-15.26		-0.60	-	-1.20		-5.35		000	0.00
Unmitigated Noise	e Levels (with	out Topo and b	arrier	atteni	uation)						
VehicleType	Leg Peak Hou	r Leg Day	I	Leg Ev	ening	Leq	Night		Ldn	C	NEL
Autos:	63.	9 6	3.4		59.5		- 58	3.3	65.	8	66
Medium Trucks:	60.	.2 6	0.4		47.4		52	2.3	60.	8	60
Heavy Trucks:	68.	.3 6	7.8		64.1		62	2.6	70.	1	70
Vehicle Noise:	70.	.1 6	9.7		65.5		64	1.3	71.	8	72
Centerline Distanc	ce to Noise Co	ntour (in feet)									
				70 d		65	dBA		60 dBA		dBA
			de.		70		4.0		201		77

Saturday, December 3, 2022

	FHWA-RI	D-77-108 H	IIGHWA	Y NOISI	E PREDIC	TION M	ODEL	. (9/12/2	021)		
Road Nan	nio: EAC+P ne: Harvill Av. nt: n/o Comm	erce Ctr. E	r.					:: MFBC :: 13697	(Building	17)	
	SPECIFIC IN	IPUT DA	TA						L INPUT	S	
Highway Data					Site Con	ditions (	Hard	= 10, Sc	oft = 15)		
Average Daily	Traffic (Adt):	25,741 ve	ehicles					Autos:	15		
Peak Hour	Percentage:	7.00%				dium Tru					
Peak F	lour Volume:	1,802 vel	nicles		He	avy Truc	ks (3-	+ Axles):	15		
Ve	hicle Speed:	50 mp	h		Vehicle I	Miv					
Near/Far La	ne Distance:	48 fee	t			icleType	П	Dav	Evening	Night	Daily
Site Data							utos:	74.7%	-	17.6%	
Pa	rrier Height:	0.0 fe	ot		М	edium Tri	ucks:	88.5%	1.1%	10.4%	3.17%
Barrier Type (0-W		0.0	eı		F	Heavy Tr	ucks:	75.1%	8.0%	16.9%	7.52%
Centerline Di		59.0 fe	et		M-: 0-	51	45-	(: 6	41		
Centerline Dist.	to Observer:	59.0 fe	et		Noise Sc			_ •	eet)		
Barrier Distance	to Observer:	0.0 fe	et			Autos m Trucks		0.000			
Observer Height	(Above Pad):	5.0 fe	et					2.297	0	···	
-	ad Elevation:	0.0 fe	et		Heav	y Trucks		8.004	Grade Ad	justment	0.0
Ro	ad Elevation:	0.0 fe	et		Lane Equ	uivalent	Dista	nce (in	feet)		
	Road Grade:	0.0%				Autos	: 5	4.129			
	Left View:	-90.0 de	egrees		Mediui	m Trucks	: 5	3.966			
	Right View:	90.0 de	egrees		Heav	y Trucks	: 5	3.982			
FHWA Noise Mod	el Calculation	s			!						
VehicleType	REMEL	Traffic FI	ow D	istance	Finite		Fre	snel	Barrier Att	en Ber	m Atten
Autos:	70.20		0.23	-0.		-1.20		-4.69		000	0.000
Medium Trucks:			4.73	-0.		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-10	0.97	-0.	60	-1.20		-5.35	0.	000	0.000
Unmitigated Noise	e Levels (with	out Topo	and barı	rier atte	nuation)						
VehicleType	Leq Peak Hou	ır Leq	Day	Leq E	Evening	Leq N	light		Ldn		NEL
Autos:	68		67.6		63.8			2.6	70.	-	70.3
Medium Trucks:	64		64.7		51.7			3.6	65.		65.1
Heavy Trucks:		2.6	72.1		68.4			3.9	74.		74.7
Vehicle Noise:	74	.4	74.0	)	69.8		68	3.6	76.	1	76.4
Centerline Distan	ce to Noise Co	ontour (in	feet)								
					dBA	65 d			60 dBA		dBA
			Ldn		150		-	24	697		1,502
			CNEL	:	156		33	37	726	3	1,564

Saturday, December 3, 2022

	FHWA-RI	D-77-108 HIGH	WAY I	NOISE	PREDIC	CTION N	ODEL	(9/12/2	021)		
	rio: E ne: Harvill Av. nt: n/o Cajalco	э Ехру					t Name: lumber:		(Building	17)	
SITE	SPECIFIC IN	IPUT DATA							L INPUT	s	
Highway Data					Site Con	nditions	(Hard =	: 10, S	oft = 15)		
Average Daily	Traffic (Adt):	10,869 vehicl	es					Autos:	15		
Peak Hour	Percentage:	7.00%			Me	edium Tr	ucks (2	Axles).	15		
Peak F	lour Volume:	761 vehicle	s		He	eavy Tru	cks (3+	Axles):	15		
Ve	ehicle Speed:	50 mph		H	Vehicle	Miv					
Near/Far La	ne Distance:	48 feet		-		icleType		Dav	Evening	Night	Daily
Site Data							Autos:	74.7%	-	17.6	
Ra	rrier Height:	0.0 feet			М	edium T	rucks:	88.5%	1.1%	10.49	% 3.19%
Barrier Type (0-W		0.0				Heavy T	rucks:	75.1%	8.0%	16.99	% 7.54%
	ist. to Barrier:	59.0 feet		L							
Centerline Dist		59.0 feet			Noise So				eet)		
Barrier Distance	to Observer:	0.0 feet				Auto		.000			
Observer Height		5.0 feet				m Truck		.297			
	ad Elevation:	0.0 feet			Heav	vy Truck	s: 8	.004	Grade Ad	justmei	nt: 0.0
	ad Flevation:	0.0 feet			Lane Eq	uivalen	t Distan	ce (in	feet)		
	Road Grade:	0.0%				Auto	s: 54	.129	,		
	Left View:	-90.0 degre	29		Mediu	m Truck	s: 53	966			
	Right View:	90.0 degre			Heav	vy Truck	s: 53	.982			
FHWA Noise Mod	el Calculation	s									
VehicleType	REMEL	Traffic Flow	Dist	ance	Finite	Road	Fres	nel	Barrier Att	en B	erm Atten
Autos:		-3.97		-0.6	_	-1.20		-4.69		000	0.000
Medium Trucks:				-0.6	-	-1.20		-4.88	0.0	000	0.000
Heavy Trucks:	85.38	-14.71		-0.6	0	-1.20		-5.35	0.0	000	0.000
Unmitigated Nois	e Levels (with	out Topo and	barrie	r atten	uation)						
VehicleType	Leq Peak Hou	ır Leq Daj	/	Leq E	vening	Leq	Night		Ldn	(	CNEL
Autos:		.4	63.9		60.1		58.	9	66.	3	66.5
Medium Trucks:	60	1.8	61.0		48.0		52.	9	61.	4	61.4
Heavy Trucks:		-	68.4		64.7		63.		70.		70.9
Vehicle Noise:	70	1.7	70.2		66.0		64.	8	72.	3	72.6
Centerline Distan	ce to Noise Co	ontour (in feet	)								
				70	dBA	65	dBA	_	60 dBA		5 dBA
			Ldn:		85		182		393		846
		С	NEL:		88		190	)	409	1	881

		0-77-108 HIGH	/1	110101	- I WEDIC			•					
	io: EAC								(Building	17)			
	e: Harvill Av.					Job N	umber	13697					
Road Segme	nt: n/o Cajalco	Expy											
	SPECIFIC IN	IPUT DATA			NOISE MODEL INPUTS Site Conditions (Hard = 10, Soft = 15)								
Highway Data					Site Con	ditions	Hard	= 10, S	oft = 15)				
Average Daily	Traffic (Adt):	27,353 vehicl	es					Autos:	15				
Peak Hour	Percentage:	7.00%			Medium Trucks (2 Axles): 15								
Peak H	lour Volume:	1,915 vehicle	:S		He	avy Truc	ks (3+	Axles):	15				
Ve	hicle Speed:	50 mph			Vehicle	Miv							
Near/Far La	Near/Far Lane Distance: 48 feet				VehicleType Day Evening Night Daily								
Site Data						- /	lutos:	74.7%	7.7%	17.6%	89.28%		
Rai	rrier Height:	0.0 feet			М	edium Tı	ucks:	88.5%	6 1.1%	10.4%	3.19%		
Barrier Type (0-W		0.0				Heavy Ti	ucks:	75.1%	8.0%	16.9%	7.54%		
Centerline Dis		59.0 feet			Noise So		41-	// #	41				
Centerline Dist. to Observer: 59.0 feet					Noise S				eet)				
Barrier Distance to Observer: 0.0 feet					A decedio	Auto: m Truck:		0.000					
Observer Height (	Above Pad):	5.0 feet						2.297	Grade Ad	ii ratma ni			
Pa	ad Elevation:	0.0 feet			Heat	y Truck	5. 6	3.004	Grade Ad	justriierii	. 0.0		
Roa	ad Elevation:	0.0 feet			Lane Eq	uivalent	Dista	nce (in	feet)				
1	Road Grade:	0.0%			Autos: 54.129								
	Left View:	-90.0 degre	es		Mediu	m Trucks	s: 5	3.966					
	Right View:	90.0 degre	es		Heavy Trucks: 53.982								
FHWA Noise Mode	el Calculation	s											
VehicleType	REMEL	Traffic Flow		stance		Road	Fres		Barrier Att		m Atten		
Autos:	70.20	0.03		-0.		-1.20		-4.69		000	0.000		
Medium Trucks:	81.00	-14.44		-0.		-1.20		-4.88		000	0.000		
Heavy Trucks:	85.38	-10.70		-0.	60	-1.20		-5.35	0.0	000	0.000		
Unmitigated Noise													
VehicleType	Leq Peak Hou			Leq E	vening		Night		Ldn		NEL		
Autos:	68		67.9		64.1		62		70.	-	70.6 65.4		
Medium Trucks:	64		65.0		52.0		56						
Heavy Trucks: Vehicle Noise:		72.9 72.4 74.7 74.3			68.7 67. 70.0 68.					74.9			
Centerline Distance					70.0		- 00		70.	•	70.		
Centernine Distant	e to Noise Co	nitour (in reet	y	70	dBA	65	dBA		60 dBA	55	dBA		
			Ldn:		157		33	7	727		1,566		
											1,631		

Road Nan	io: E+P ne: Harvill Av. nt: n/o Cajalco	Ехру						: MFBC : 13697	(Building	17)			
	SPECIFIC IN	PUT DATA			NOISE MODEL INPUTS Site Conditions (Hard = 10, Soft = 15)								
Highway Data					Site Co	naitions	(Hara						
Average Daily	, ,	11,124 vehicle	S					Autos:					
	Percentage:	7.00%				ledium Ti		,					
	lour Volume:	779 vehicles			-	leavy Tru	icks (3+	Axies):	15				
	hicle Speed:	50 mph			Vehicle	Mix							
Near/Far La	ne Distance:	48 feet		ĺ	Ve	hicleTyp	е	Day	Evening	Night	Daily		
Site Data							Autos:	74.7%	7.7%	17.6%	89.35		
Ва	rrier Height:	0.0 feet			1	Medium 1	rucks:	88.5%	1.1%	10.4%	3.14		
Barrier Type (0-V	-	0.0				Heavy 7	rucks:	75.1%	8.0%	16.9%	7.50		
	st. to Barrier:	59.0 feet		-	M-1	<b>5</b>			41				
Centerline Dist.	to Observer:	59.0 feet		-	Noise :	Source E		_	eet)				
Barrier Distance	to Observer:	0.0 feet				Auto		0.000					
Observer Height	(Above Pad):	5.0 feet				um Truck		2.297	Grade Ad	livatmant			
P	ad Elevation:	0.0 feet			не	avy Truck	(S. C	3.004	Grade Ad	jusuneni	. 0.0		
Ro	ad Elevation:	0.0 feet			Lane E	quivalen	t Dista	nce (in	feet)				
	Road Grade:	0.0%				Auto	s: 5	1.129					
	Left View:	-90.0 degree	s		Medi	um Truck	ks: 5	3.966					
	Right View:	90.0 degree	s		He	avy Truck	ks: 5	3.982					
FHWA Noise Mod													
VehicleType	REMEL	Traffic Flow	Di	istance	_	e Road	Fres		Barrier Att	_	m Atter		
Autos:		-3.87		-0.6		-1.20		-4.69		000	0.0		
Medium Trucks:		-18.41		-0.6		-1.20		-4.88		000	0.00		
Heavy Trucks:		-14.63		-0.6		-1.20		-5.35	0.	000	0.0		
Unmitigated Nois			$\overline{}$	-				_					
VehicleType	Leq Peak Hou		_	Leq E	vening		Night	_	Ldn		NEL		
Autos: Medium Trucks:	0.1		34.0		60.	_	59		66.		66		
	00		31.0		48.	-	53		61.		61		
Heavy Trucks: Vehicle Noise:			70.3		64.		63 64		70. 72.		71 72		
Centerline Distan	ce to Noise Co	ntour (in feet)											
				70	dBA	65	dBA	(	60 dBA	55	dBA		
			dn:	-	0.0		10	_	300		96		

Saturday, December 3, 2022

	FHWA-RI	D-77-108 HIGH	WAY	NOISI	E PREDIC	TION M	ODEL	(9/12/2	021)					
	o: EAC+P e: Harvill Av. nt: n/o Cajalo	о Ехру			Project Name: MFBC (Building 17) Job Number: 13697									
	SPECIFIC IN	NPUT DATA							L INPUT	s				
Highway Data					Site Con	ditions (	Hard	= 10, S	oft = 15)					
Average Daily	Traffic (Adt):	27,608 vehicle	es					Autos:	15					
Peak Hour Percentage: 7.00%					dium Tru									
Peak H	our Volume:	1,933 vehicle	S		He	avy Truc	ks (3+	Axles):	15					
Ve	hicle Speed:	50 mph			Vehicle I	Miv								
Near/Far La	ne Distance:	48 feet				cleType		Day	Evening	Night	Daily			
Site Data							utos:	74.7%	-	17.6%				
Rai	rier Height:	0.0 feet			Me	edium Tr	ucks:	88.5%	1.1%	10.4%	3.17%			
Barrier Type (0-W		0.0			F	leavy Tr	ucks:	75.1%	8.0%	16.9%	7.52%			
Centerline Dis	. ,	59.0 feet			Noise Source Elevations (in feet)									
Centerline Dist.	to Observer:	59.0 feet			Noise So			_ •	eet)					
Barrier Distance	to Observer:	0.0 feet				Autos		0.000						
Observer Height (Above Pad): 5.0 feet						n Trucks	-	2.297	0	·				
Pad Elevation: 0.0 feet					Heav	y Trucks	: 8	3.004	Grade Ad	ijustment	0.0			
Road Elevation: 0.0 feet					Lane Equ	uivalent	Dista	nce (in	feet)					
1	Road Grade:	0.0%				Autos	: 5	1.129						
	Left View:	-90.0 degree	es		Mediur	n Trucks	: 5	3.966						
	Right View:	90.0 degree	es		Heavy Trucks: 53.982									
FHWA Noise Mode	el Calculation	ıs												
VehicleType	REMEL	Traffic Flow	Dis	stance	Finite	Road	Fres	snel	Barrier Att	ten Ber	m Atten			
Autos:	70.20	0.08		-0.6	62	-1.20		-4.69	0.	000	0.000			
Medium Trucks:	81.00	-14.42		-0.6	60	-1.20		-4.88	0.	000	0.000			
Heavy Trucks:	85.38	-10.67		-0.0	60	-1.20		-5.35	0.	000	0.000			
Unmitigated Noise	Levels (with	out Topo and	barri	er atte	nuation)									
	Leq Peak Ho			Leq E	vening	Leq N	-		Ldn		NEL			
Autos:			68.0		64.1		62		70.		70.6			
Medium Trucks:	-		65.0		52.0		56		65.		65.4			
Heavy Trucks:				68.7		67.2		74.7		75.0				
Vehicle Noise:	74	1.7	74.3		70.1		68	.9	76.	4	76.7			
Centerline Distanc	e to Noise C	ontour (in feet	)											
			L	70	dBA	65 d			60 dBA		dBA			
			Ldn:		157		33	-	730	-	1,574			
		C	NEL:		164		35	3	761	1	1,639			

Saturday, December 3, 2022

	FHWA-RI	D-77-108 HIGH	IWAY N	IOISE	PREDIC	TION N	MODEL	(9/12/2	021)					
Scenar									(Building	17)				
	ne: Harvill Av. nt: s/o Cajalco	Evny				JOD I	lumber:	13697						
Road Segille	ni. s/o Cajaico	Ехру												
	SPECIFIC IN	IPUT DATA			NOISE MODEL INPUTS Site Conditions (Hard = 10, Soft = 15)									
Highway Data					Site Con	aitions	(Hara =							
Average Daily	. ,	13,086 vehicl	es					Autos:						
	Percentage:	7.00%				dium Tr								
Peak F	lour Volume:	916 vehicle	S		He	avy Tru	cks (3+	Axles):	15					
Ve	ehicle Speed:	50 mph		1	Vehicle	Mix								
Near/Far La	Near/Far Lane Distance:			H	Veh	icleType	9	Day	Evening	Night	Daily			
Site Data							Autos:	74.7%	6 7.7%	17.6	% 89.28%			
Ra	rrier Height:	0.0 feet			М	edium T	rucks:	88.5%	6 1.1%	10.4	% 3.19%			
Barrier Type (0-W		0.0			- 1	Heavy T	rucks:	75.1%	8.0%	16.9	% 7.54%			
	ist. to Barrier:	59.0 feet		<u> </u>										
Centerline Dist		59.0 feet		1	Noise So				eet)					
Barrier Distance	to Observer:	0.0 feet				Auto		.000						
Observer Height		5.0 feet				m Truck		.297						
-	ad Elevation:	0.0 feet			Heav	y Truck	s: 8	.004	Grade Ad	justme	nt: 0.0			
	ad Flevation:	0.0 feet		1	Lane Eq	uivalen	t Distar	ce (in	feet)					
	Road Grade:	0.0%				Auto	s: 54	.129	,					
	Left View:	-90.0 degre	29		Mediu	m Truck	s: 53	966						
	Right View:	90.0 degre			Heav	y Truck	s: 53	.982						
FHWA Noise Mod	el Calculation	s												
VehicleType	REMEL	Traffic Flow	Dista	ance	Finite	Road	Fres	nel	Barrier Att	en B	erm Atten			
Autos:	70.20	-3.17		-0.6	2	-1.20		-4.69	0.0	000	0.000			
Medium Trucks:	81.00	-17.64		-0.6	0	-1.20		-4.88	0.0	000	0.000			
Heavy Trucks:	85.38	-13.90		-0.6	0	-1.20		-5.35	0.0	000	0.000			
Unmitigated Noise	e Levels (with	out Topo and	barrier	atten	uation)									
VehicleType	Leq Peak Hou	ır Leq Daj	/	Leq E	vening	Leq	Night		Ldn		CNEL			
Autos:	65	i.2	64.7		60.9		59	7	67.	1	67.4			
Medium Trucks:	61	.6	61.8		48.8		53	7	62.	2	62.2			
Heavy Trucks:			69.2		65.5		64	0	71.		71.7			
Vehicle Noise:	71	.5	71.1		66.8		65	6	73.	2	73.4			
Centerline Distant	ce to Noise Co	ontour (in feet	)											
				70 c		65	dBA	_	60 dBA		i5 dBA			
			Ldn:		96		20	-	445		958			
		С	NEL:		100		21	5	463	3	998			

	FHWA-RI	D-77-108 HIG	HWAY	NOISE	PREDIC	CTION N	IODEL	(9/12/2	021)				
Road Nam	io: EAC ne: Harvill Av. nt: s/o Cajalco	Ехру			Project Name: MFBC (Building 17) Job Number: 13697								
	SPECIFIC IN	IPUT DATA			NOISE MODEL INPUTS								
Highway Data					Site Conditions (Hard = 10, Soft = 15)								
Average Daily	Traffic (Adt):	28,239 vehic	les					Autos:	15				
Peak Hour	Percentage:	7.00%			Medium Trucks (2 Axles): 15								
Peak H	lour Volume:	1,977 vehicle	es		He	eavy Tru	cks (3+	Axles):	15				
Ve	50 mph	50 mph			Mix								
Near/Far La	ne Distance:	48 feet				icleType	•	Day	Evening	Night	Daily		
Site Data							Autos:	74.7%	7.7%	17.6%	89.28%		
Bai	rrier Height:	0.0 feet			М	edium T	rucks:	88.5%	1.1%	10.4%	3.19%		
Barrier Type (0-W		0.0			1	Heavy T	rucks:	75.1%	8.0%	16.9%	7.54%		
Centerline Dis	st. to Barrier:	59.0 feet		,	Voise So	nurce F	levatio	ns (in f	oet)				
Centerline Dist.	to Observer:	59.0 feet		· · · · · · · ·	10/36 00	Auto		0.000	501)				
Barrier Distance	Barrier Distance to Observer: 0.0 feet					m Truck		2.297					
Observer Height (	Observer Height (Above Pad): 5.0 feet					vy Truck		3.004	Grade Ad	iustment	. 0 0		
Pa	ad Elevation:	0.0 feet								4011110111	. 0.0		
Ros	ad Elevation:	0.0 feet		L	Lane Eq	uivalen	t Distai	nce (in	feet)				
ı	Road Grade:	0.0%				Auto	s: 54	1.129					
	Left View:	-90.0 degre	ees		Medium Trucks: 53.966								
	Right View:	90.0 degre	ees		Heav	vy Truck	s: 50	3.982					
FHWA Noise Mode	el Calculation	s											
VehicleType	REMEL	Traffic Flow	Di	stance	Finite	Road	Fres	snel	Barrier Att	en Bei	m Atten		
Autos:	70.20	0.17	7	-0.62	2	-1.20		-4.69	0.0	000	0.00		
Medium Trucks:	81.00	-14.30	)	-0.60	0	-1.20		-4.88	0.0	000	0.00		
Heavy Trucks:	85.38	-10.56	3	-0.60	0	-1.20		-5.35	0.0	000	0.000		
Unmitigated Noise													
VehicleType	Leq Peak Hou		,	Leq Ev		,	Night		Ldn		NEL		
Autos:	68		68.0		64.2		63		70.4		70.		
Medium Trucks:		.9 65.1			52.1		57.1		65.5				
Heavy Trucks: Vehicle Noise:	Heavy Trucks:         73.0         72.5           Vehicle Noise:         74.8         74.4			68.8 67.3 74.8 70.2 69.0 76.5					75.1 76.1				
					70.2		00	.0	70.0		70.		
Centerline Distanc	ce to Noise Co	ontour (in fee	ij	70 c	iBA	65	dBA	Т.	60 dBA	55	dBA		
			Ldn:		160		34		742	1	1.599		

Road Nan	io: E+P ne: Harvill Av. nt: s/o Cajalco	Ехру			Project Name: MFBC (Building 17) Job Number: 13697								
	SPECIFIC IN	IPUT DATA			NOISE MODEL INPUTS								
Highway Data					Site Conditions (Hard = 10, Soft = 15)								
Average Daily	. ,	13,145 vehicle	S					Autos.					
	Percentage:	7.00%				edium Ti		,					
Peak F	lour Volume:	920 vehicles	;		Н	eavy Tru	cks (3-	+ Axles).	15				
	hicle Speed:	50 mph			Vehicle	Mix							
Near/Far La	ne Distance:	48 feet			Ve	hicleType	9	Day	Evening	Night	Daily		
Site Data							Autos:	74.79	7.7%	17.6%	89.329		
Ra	rrier Height:	0.0 feet			٨	1edium 7	rucks:	88.5%	1.1%	10.4%	3.179		
Barrier Type (0-W		0.0				Heavy 7	rucks:	75.19	8.0%	16.9%	7.509		
Centerline Di		59.0 feet											
Centerline Dist.	to Observer:	59.0 feet			Noise S	ource E		_ •	eet)				
Barrier Distance		0.0 feet				Auto		0.000					
Observer Height	(Above Pad):	5.0 feet				ım Truck		2.297	0	···	4.00		
P	ad Elevation:	0.0 feet			неа	vy Truck	is:	8.004	Grade Ad	jusimen	ι. υ.υ		
Ro	ad Elevation:	0.0 feet			Lane E	quivalen	t Dista	nce (in	feet)				
	Road Grade:	0.0%				Auto	s: 5	4.129					
	Left View:	-90.0 degree	s		Medi	ım Truck	s: 5	3.966					
	Right View:	90.0 degree	s		Hea	vy Truck	rs: 5	3.982					
FHWA Noise Mod													
VehicleType	REMEL	Traffic Flow	Di	stance		Road	Fre	snel	Barrier Att		rm Atter		
Autos:	70.20	-3.15		-0.6		-1.20		-4.69		000	0.00		
Medium Trucks:	81.00	-17.64		-0.6		-1.20		-4.88		000	0.00		
Heavy Trucks:		-13.90		-0.6		-1.20		-5.35	0.	000	0.00		
Unmitigated Nois						1				1			
VehicleType	Leq Peak Hou	.,.,		Leq E	vening		Night		Ldn		NEL		
Autos:	65		64.7		60.			9.7	67.		67.		
Medium Trucks:	61		61.8		48.	-		3.7	62.	_	62.		
Heavy Trucks:	69		69.2		65.			1.0	71.		71.		
Vehicle Noise:			71.1		66.	5	65	5.6	73.	2	73.		
Centerline Distan	ce to Noise Co	ontour (in feet)		70	dBA	65	dBA		50 dBA	5.6	5 dBA		
			Ldn:		96		20	_	445		95		

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	FHWA-RI	D-77-108 HIGH	WAY	NOIS	E PREDIC	TION M	ODEL	. (9/12/2	021)				
Road Nar	rio: EAC+P ne: Harvill Av. ent: s/o Cajalco	Ехру			Project Name: MFBC (Building 17) Job Number: 13697								
	SPECIFIC IN	IPUT DATA							L INPUT	s			
Highway Data					Site Con	ditions	Hard	= 10, S	oft = 15)				
Average Daily	Traffic (Adt):	28,298 vehicle	es					Autos.	15				
Peak Hou	Percentage:	7.00%			Me	dium Tru	icks (2	Axles).	15				
Peak I	Hour Volume:	1,981 vehicle	s		He	avy Truc	ks (3+	Axles).	15				
Ve	ehicle Speed:	50 mph			Vehicle I	Miss							
Near/Far La	ane Distance:	48 feet				icleType		Dav	Evening	Night	Daily		
Site Data							utos:	74.79	-	17.6%			
	rrier Heiaht:	0.0 feet			Ме	edium Tr		88.5%		10.4%			
Barrier Type (0-V		0.0 feet			F	leavy Tr	ucks:	75.19	8.0%	16.9%	7.52%		
	ist to Barrier:	59.0 feet											
Centerline Dist.		59.0 feet			Noise So			_ •	eet)				
Barrier Distance		0.0 feet				Autos		0.000					
Observer Height		5.0 feet				m Trucks		2.297					
-	ad Elevation:	0.0 feet			Heav	y Trucks	3.	8.004	Grade Ad	justment	: 0.0		
	ad Elevation:	0.0 feet			Lane Equ	uivalent	Dista	nce (in	feet)				
	Road Grade:	0.0%				Autos	s: 5	4.129					
	Left View:	-90.0 degree	es		Mediur	m Trucks	: 5	3.966					
	Right View:	90.0 degree			Heav	y Trucks	s: 5	3.982					
FHWA Noise Mod	lel Calculation	s											
VehicleType	REMEL	Traffic Flow	Dis	stance	Finite		Fre.		Barrier Att		m Atten		
Autos:				-0.		-1.20		-4.69		000	0.000		
Medium Trucks:				-0.		-1.20		-4.88		000	0.000		
Heavy Trucks:	85.38	-10.56		-0.	60	-1.20		-5.35	0.0	000	0.000		
Unmitigated Nois	e Levels (with	out Topo and	barri	er atte	nuation)								
VehicleType	Leq Peak Hou	ur Leq Day	′	Leq E	vening	Leq	Vight		Ldn		NEL		
Autos:			68.1		64.2			3.0	70.4		70.7		
Medium Trucks:	-	1.9	65.1		52.1		57		65.	-	65.6		
Heavy Trucks:		3.0	72.5		68.8			7.3	74.	-	75.1		
Vehicle Noise:	74	1.8	74.4		70.2		69	9.0	76.	5	76.8		
Centerline Distan	ce to Noise Co	ontour (in feet	)										
			L	70	dBA	65 (			60 dBA		dBA		
			Ldn:		160		34	-	743		1,600		
		C	NEL:		167		35	59	774		1,666		

Saturday, December 3, 2022

FHWA:	RD-7	77-108 HIGH	IWAY	NOISE	E PREDI	CTION I	<b>IODEL</b>	(9/12/2	021)		
Scenario: E Road Name: Cajalco Road Segment: w/o Harv		r.					t Name: Number:		(Building	17)	
SITE SPECIFIC	INP	UT DATA			0				L INPUT	S	
Highway Data					Site Cor	naitions	(Hara =				
Average Daily Traffic (Adt)		4,229 vehicle	es					Autos:			
Peak Hour Percentage		7.00%				edium Ti					
Peak Hour Volume		,696 vehicle:	S		He	eavy Tru	icks (3+	Axles):	15		
Vehicle Speed		50 mph		ı	Vehicle	Mix					
Near/Far Lane Distance	:	102 feet		ı	Vel	nicleType	е	Day	Evening	Nigh	Daily
Site Data							Autos:	74.7%	7.7%	17.6	% 89.28%
Barrier Height		0.0 feet			N	1edium 7	rucks:	88.5%	1.1%	10.4	% 3.19%
Barrier Type (0-Wall, 1-Berm)	:	0.0				Heavy 1	rucks:	75.1%	8.0%	16.9	% 7.54%
Centerline Dist. to Barrier		92.0 feet			Noise S	ource E	levation	ns (in fe	eet)		
Centerline Dist. to Observer		92.0 feet		ı		Auto	os: 0	.000	,		
Barrier Distance to Observer											
	Observer Height (Above Pad): 5.0 feet								Grade Ad	justme	ent: 0.0
Pad Elevation		0.0 feet				vy Truck					
Road Elevation	-	0.0 feet			Lane Eq				reet)		
Road Grade	-	0.0%				Auto		.733			
Left View	-	-90.0 degree				ım Truck		.618			
Right View	-	90.0 degree	es		неа	vy Truci	(S: 76	.629			
FHWA Noise Model Calculati	ons										
VehicleType REMEL	7	raffic Flow	Di	stance	Finite	Road	Fres	nel	Barrier Att	en E	Berm Atten
Autos: 70.	20	-0.49		-2.8		-1.20		-4.76	0.0	000	0.000
Medium Trucks: 81.	00	-14.96		-2.8	88	-1.20		-4.88	0.0	000	0.000
Heavy Trucks: 85.	38	-11.23		-2.8	88	-1.20		-5.18	0.0	000	0.000
Unmitigated Noise Levels (w.	thou	t Topo and	barri	er atte	nuation)						
VehicleType Leq Peak F		Leq Day		Leq E	ening 61.3		Night		Ldn	_	CNEL
	Autos: 65.6 65.1							1	67.		67.8
Medium Trucks:		49.2 65.9	-	54		62.	-	62.6			
Heavy Trucks:	Heavy Trucks:         70.1         69.6           Vehicle Noise:         71.9         71.5							4	71.		72.1 73.8
			67.2	<u> </u>	66	0	73.	b	/3.8		
Centerline Distance to Noise	Con	tour (in feet	)	70	dBA	65	dBA	1 6	60 dBA	1 .	55 dBA
			Ldn:	- , ,	159		34:	_	737	_	1.587
	CNEL:								767		1,653

Saturday, December 3, 2022

	FHWA-RI	D-77-108 HIGH	WAY N	OISE	PREDIC	TION MO	DDEL	(9/12/2	021)		
Road Nan	rio: EAC ne: Cajalco Ex nt: w/o Harvill .					Project i Job Nu			(Building 1	17)	
	SPECIFIC IN	IPUT DATA							L INPUT	s	
Highway Data					Site Con	ditions (	Hard =	= 10, S	oft = 15)		
Average Daily	Traffic (Adt):	35,611 vehicle	es					Autos	15		
Peak Hour	Percentage:	7.00%			Me	dium Tru	cks (2	Axles)	15		
Peak F	lour Volume:	2,493 vehicles	3		He	avy Truc	ks (3+	Axles).	15		
Ve	ehicle Speed:	50 mph			Vehicle I	Miv					
Near/Far La	ne Distance:	102 feet		F		icleType	П	Dav	Evening	Night	Daily
Site Data							utos:	74.79		17.6	
Ra	rrier Heiaht:	0.0 feet			M	edium Tri	ucks:	88.59	6 1.1%	10.4	% 3.19%
Barrier Type (0-W		0.0			1	Heavy Tri	ucks:	75.19	8.0%	16.9	% 7.54%
	ist. to Barrier:	92.0 feet		-	M-: 0-		47	/: 4	41		
Centerline Dist.	to Observer:	92.0 feet		H	Noise Sc	ource Ele			eet)		
Barrier Distance	to Observer:			Autos m Trucks		.000					
Observer Height	(Above Pad):	5.0 feet					-	.297	0	·	-4.00
	ad Elevation:	0.0 feet			Heav	y Trucks	: 8	.004	Grade Ad	justme	nt: U.U
Ro	ad Elevation:	0.0 feet		Ī	Lane Eq	uivalent	Distar	ice (in	feet)		
	Road Grade:	0.0%				Autos	: 76	.733			
	Left View:	-90.0 degree	es		Mediu	m Trucks	: 76	.618			
	Right View:	90.0 degree	es		Heav	y Trucks	: 76	.629			
FHWA Noise Mod	el Calculation	s									
VehicleType	REMEL	Traffic Flow	Dista	ance		Road	Fres		Barrier Att		erm Atten
Autos:		1.18		-2.8	-	-1.20		-4.76		000	0.000
Medium Trucks:				-2.8	-	-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-9.56		-2.8	8	-1.20		-5.18	0.0	000	0.000
Inmitigated Nois								,		,	
VehicleType	Leq Peak Hou			Leq E	vening	Leq N	-		Ldn	1	CNEL
Autos:		66.8		62.9		61		69.2	_	69.4	
Medium Trucks:		63.9		50.9 67.5		55	-	64.2	_	64.3	
Heavy Trucks:	Heavy Trucks:         71.7         71.2           Vehicle Noise:         73.5         73.1						66	-	73.	-	73.8
			68.9		67	./	75.	2	75.5		
Centerline Distan	ce to Noise Co	70	dBA	65 a	IDΛ		60 dBA		55 dBA		
	Ldn:					03 0	BA 44:		952 952		2.051
	Lan: CNEL:						46	_	992		2,031
		CI	VLL.		214		40	U	992		2,137

Scenari Road Nam Road Segmer	e: Cajalco Exp						Name: umber:		(Building 1	7)	
	SPECIFIC IN	IPUT DATA			2:4				L INPUT	S	
Highway Data				- 1	Site Con	aitions		-,-	/		
Average Daily	. ,	24,268 vehicle	es			ationa Ta		Autos:			
	Percentage:	7.00%				dium Tru		,			
	our Volume:	1,699 vehicles	3		HE	avy Truc	KS (3+ )	axies).	15		
	hicle Speed:	50 mph		١	Vehicle I	Mix					
Near/Far Lai	ne Distance:	102 feet			Veh	icleType		Day	Evening	Night	Daily
Site Data						F	lutos:	74.7%	7.7%	17.6%	89.29
Bar	rier Height:	0.0 feet			М	edium Ti	ucks:	88.5%	1.1%	10.4%	3.18
Barrier Type (0-W		0.0				Heavy Ti	ucks:	75.1%	8.0%	16.9%	7.52
Centerline Dis		92.0 feet		١.	O			- /: #	4		
Centerline Dist.	to Observer:	92.0 feet	,	Noise S			•	eet)			
Barrier Distance	to Observer:	0.0 feet			Auto		000				
Observer Height (	Above Pad):	5.0 feet				m Truck		297	0	4	
Pa	d Elevation:	0.0 feet			Heav	y Truck	s: 8.	004	Grade Adj	usimeni	0.0
Roa	d Elevation:	0.0 feet		I	Lane Eq	uivalent	Distant	ce (in	feet)		
ŀ	Road Grade:	0.0%				Auto	s: 76.	733			
	Left View:	-90.0 degree	es		Mediu	m Truck	s: 76.	618			
	Right View:	90.0 degree	es		Hear	y Truck	s: 76.	629			
FHWA Noise Mode	l Calculation	s									
VehicleType	REMEL	Traffic Flow	Dista			Road	Fresn	_	Barrier Atte	en Bei	m Atter
Autos:	70.20	-0.49		-2.89	9	-1.20		-4.76	0.0	000	0.0
Medium Trucks:	81.00	-14.96		-2.8	8	-1.20		-4.88	0.0	000	0.00
Heavy Trucks:	85.38			-2.8	-	-1.20		-5.18	0.0	000	0.0
Inmitigated Noise								1		_	
VehicleType Autos:	Leq Peak Hou	. , . ,	65.1	Leq E	vening		Night		Ldn		NEL
Medium Trucks:	62		65.1 62.2		61.3 49.2		60.1 54.1		67.5 62.6		67 62
Heavy Trucks:	70		62.2 69.6		49.2 65.9				71.8		
Vehicle Noise:							66.0		73.6		72 73
Centerline Distanc	e to Noise Co										
		70 c	dBA	65	dBA		60 dBA		dBA		
Ldn:					159		342		737		1,58
			165		356		767		1.65		

Saturday, December 3, 2022

	FHWA-R	D-77-108 HIGH	WAY	NOISE I	PREDIC	TION M	ODEL	(9/12/2	021)		
Road Nan	rio: EAC+P ne: Cajalco Ex nt: w/o Harvill							MFBC 13697	(Building 1	17)	
	SPECIFIC II	NPUT DATA							L INPUT	S	
Highway Data				S	ite Con	ditions	(Hard :				
Average Daily	. ,	35,651 vehicle	es					Autos:			
	Percentage:	7.00%				dium Tri		,			
	lour Volume:	2,496 vehicles	3		He	avy Truc	cks (3+	Axles):	15		
Vé	ehicle Speed:	50 mph		ν	ehicle l	Mix					
Near/Far La	ne Distance:	102 feet		F		icleType		Day	Evening	Night	Daily
Site Data						- /	Autos:	74.7%	7.7%	17.6%	89.29%
Ra	rrier Height:	0.0 feet			Me	edium Ti	rucks:	88.5%	1.1%	10.4%	3.19%
Barrier Type (0-V		0.0			F	Heavy Ti	rucks:	75.1%	8.0%	16.9%	7.53%
** '	ist. to Barrier:	92.0 feet			laiaa Ce	urce El	ovetio	na (in f	2041		
Centerline Dist.	to Observer:	92.0 feet			oise sc	Auto:		0.000	et)		
Barrier Distance	to Observer:	0.0 feet			A de eller	Auto: m Truck:		2.297			
Observer Height	(Above Pad):	5.0 feet				η Truck: γ Truck:		3.004	Grade Ad	livetmen	
P	ad Elevation:	0.0 feet			пеач	y ITUCK	s. c	.004	Grade Au	jusunem	. 0.0
Ro	ad Elevation:	0.0 feet		L	ane Eq	uivalent	Distar	nce (in :	feet)		
	Road Grade:	0.0%				Auto	s: 76	6.733			
	Left View:	-90.0 degree	es		Mediui	m Truck	s: 76	6.618			
	Right View:	90.0 degree	es		Heav	y Truck	s: 76	6.629			
FHWA Noise Mod	el Calculation	ıs									
VehicleType	REMEL	Traffic Flow	Dis	stance	Finite	Road	Fres	inel	Barrier Att	en Bei	rm Atten
Autos:	70.20	1.18		-2.89	1	-1.20		-4.76	0.0	000	0.000
Medium Trucks:	81.00	-13.29		-2.88		-1.20		-4.88	0.0	000	0.000
Heavy Trucks:	85.38	-9.56		-2.88		-1.20		-5.18	0.0	000	0.000
Unmitigated Nois	e Levels (with	out Topo and	barri	er attenu	ıation)						
VehicleType	Leq Peak Ho			Leq Ev		Leq	Night		Ldn		NEL
Autos:			66.8		62.9		61		69.	_	69.4
Medium Trucks:	-		63.9		50.9		55		64.	_	64.3
Heavy Trucks:			71.2		67.5		66		73.		73.8
Vehicle Noise:	73	3.5	73.1		68.9		67	.7	75.	2	75.5
Centerline Distan	ce to Noise C	ontour (in feet)	) _								
			L	70 d		65	dBA		60 dBA		dBA
			Ldn:		205		44	-	952	-	2,052
		CI	VEL:		214		46	0	992	2	2,137

Saturday, December 3, 2022

Saturday, December 3, 2022

	FHWA-R	D-77-108 HIG	HWAY	NOISE	PREDIC	CTION MC	DDEL (	9/12/2	021)		
	io: E ne: Cajalco Ex nt: e/o Harvill.					Project I Job Nu			(Building	17)	
	SPECIFIC II	NPUT DATA	١						L INPUT	s	
Highway Data					Site Cor	nditions (i					
Average Daily	. ,	27,043 vehi	cles					Autos:			
	Percentage:	7.00%				edium Tru					
	lour Volume:	1,893 vehic	les		He	eavy Truck	(S (3+ A	axies):	15		
	hicle Speed:	50 mph			Vehicle	Mix					
Near/Far La	ne Distance:	102 feet			Ver	icleType		Day	Evening	Night	Daily
Site Data							utos:	74.7%	7.7%	17.69	6 89.28%
Bai	rrier Height:	0.0 feet				ledium Tru		88.5%		10.49	
Barrier Type (0-W	/all, 1-Berm):	0.0				Heavy Tru	icks:	75.1%	8.0%	16.99	6 7.54%
Centerline Dis		92.0 feet		-	Noise S	ource Ele	vation	s (in fe	eet)		
Centerline Dist.		92.0 feet		ľ		Autos		000	,		
Barrier Distance		0.0 feet			Mediu	m Trucks.	2.	297			
Observer Height (		5.0 feet			Hea	vv Trucks.	8.0	004	Grade Ad	justmen	t: 0.0
	ad Elevation:	0.0 feet		-							
	ad Elevation:	0.0 feet		ŀ	Lane Eq	uivalent i			reet)		
,	Road Grade:	0.0%				Autos.		733			
	Left View:	-90.0 deg				m Trucks.		618			
	Right View:	90.0 deg	ees		неа	vy Trucks.	76.	629			
FHWA Noise Mode	el Calculation										
VehicleType	REMEL	Traffic Flow		stance		Road	Fresn	_	Barrier Att		rm Atten
Autos:	70.20	-0.0	12	-2.8		-1.20		-4.76	0.0	000	0.000
Medium Trucks:	81.00		-	-2.8		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-10.7	5	-2.8	38	-1.20		-5.18	0.0	000	0.000
Unmitigated Noise				er attei	nuation)						
VehicleType	Leq Peak Ho		,	Leq E	vening	Leq ∧	-		Ldn		CNEL
Autos:	66	65.6 62.7		61.7		60.6		68.		68.2	
Medium Trucks:	62		49.7		54.6		63.	-	63.1		
Heavy Trucks:		0.5	70.1		66.3		64.8		72.		72.6
Vehicle Noise:	72		67.7		66.5	5	74.	0	74.3		
Centerline Distance	ce to Noise C		dBA								
	L						BA	6	60 dBA		5 dBA
			Ldn: CNFL:		171 178		368 383		793 825		1,707
			CIVEL:		1/8		383		825	)	1,778

Saturday, December 3, 2022

	FHWA-KL	0-77-108 HIGH	WAY	NOISI	PREDIC	TION M	ODEL	(9/12/2	<del>02</del> 1)		
Road Nam	io: EAC ne: Cajalco Exp nt: e/o Harvill A							: MFBC : 13697	(Building	17)	
SITE	SPECIFIC IN	PUT DATA				N	OISE	MODE	L INPUT	s	
Highway Data					Site Cor	ditions	(Hard	= 10, S	oft = 15)		
Average Daily	Traffic (Adt):	53,559 vehicle	es					Autos	15		
Peak Hour	Percentage:	7.00%			Me	edium Tro	icks (2	Axles)	15		
Peak H	lour Volume:	3,749 vehicle	s		He	avy Truc	ks (3+	Axles).	15		
Ve	hicle Speed:	50 mph			Vehicle						
Near/Far La	ne Distance:	102 feet				icleType		Dav	Evening	Night	Daily
Site Data					V C//		lutos:	74.79	-	17.6%	. ,
					M	edium Ti		88.59			
	rrier Height:	0.0 feet 0.0				Heavy Ti		75.19			
Barrier Type (0-W Centerline Dis		0.0 92.0 feet				1001) 11	dono.	70.17	0.070	10.07	7.017
Centerline Dist.		92.0 feet			Noise S	ource El	evatio	ns (in f	eet)		
Barrier Distance		0.0 feet				Auto	s: (	0.000			
Observer Height (		5.0 feet				m Truck		2.297			
	ad Elevation:	0.0 feet			Hea	vy Truck	s: 8	3.004	Grade Ad	ljustmen	t: 0.0
	ad Elevation:	0.0 feet			Lane Eq	uivalent	Dista	nce (in	feet)		
	Road Grade:	0.0%				Auto	s: 70	3.733			
	Left View:	-90.0 degree	es		Mediu	m Trucks	s: 70	3.618			
	Right View:	90.0 degree			Hea	vy Truck	s: 70	6.629			
FHWA Noise Mode	el Calculation	s									
VehicleType	REMEL	Traffic Flow	Di	stance	Finite	Road	Fres	snel	Barrier At	ten Be	rm Atten
Autos:	70.20	2.95		-2.	89	-1.20		-4.76	0.	000	0.00
Medium Trucks:	81.00	-11.52		-2.	88	-1.20		-4.88	0.	000	0.00
Heavy Trucks:	85.38	-7.78		-2.	88	-1.20		-5.18	0.	000	0.000
Unmitigated Noise	e Levels (with	out Topo and	barri	er atte	nuation)						
VehicleType	Leq Peak Hou	ır Leq Day	/	Leq E	vening	Leq	Night		Ldn	С	NEL
Autos:	69	.1	68.6		64.7		63	.5	70.	9	71.2
Medium Trucks:	65		65.6		52.6		57		66.		66.
Heavy Trucks:	73		73.0		69.3		67		75.		75.0
Vehicle Noise:	75	.3	74.9		70.7	'	69	1.5	77.	0	77.3
Centerline Distand	ce to Noise Co	ontour (in feet	)								
			[	70	dBA	65	dBA 		60 dBA		dBA
		_	Ldn:		269		58	-	1,250		2,693
		C	NEL:		280		60	14	1,302	<u> </u>	2,805

	o: E+P e: Cajalco Expy t: e/o Harvill Av						! Name: I lumber: 1		(Building 1	7)	
	PECIFIC INP	UT DATA							L INPUT	S	
Highway Data				- 1	Site Con	ditions	(Hard =				
Average Daily	raffic (Adt): 2	7,199 vehicle	S					Autos.			
Peak Hour I	-	7.00%					ucks (2 A	,			
Peak Ho	our Volume: 1	,904 vehicles			He	avy Tru	cks (3+ A	(xles	15		
Vel	icle Speed:	50 mph		- 1	Vehicle I	Mix					
Near/Far Lar	e Distance:	102 feet		F		icleType	•	Dav	Evening	Night	Daily
Site Data								74.79	-	17.6%	
	rier Height:	0.0 feet			М	edium T		88.5%		10.4%	
Barrier Type (0-Wa		0.0 feet			- 1	Heavy T	rucks:	75.19	8.0%	16.9%	7.55%
Centerline Dis		92.0 feet		L		,					
Centerline Dist. 1		92.0 feet		1	Noise So	ource E	levations	s (in f	eet)		
Barrier Distance t		0.0 feet				Auto	s: 0.0	000			
Observer Height (		5.0 feet			Mediu	m Truck	s: 2.2	297			
	d Elevation:	0.0 feet			Heav	y Truck	s: 8.0	004	Grade Adj	iustment	0.0
	d Elevation:	0.0 feet		- 1	l ano Fa	uivalon	t Distanc	o (in	foot)		
		0.0 reet		ľ	Lane Ly	Auto			1001)		
r	Left View:		_		Modiu	m Truck					
	Right View:	-90.0 degree 90.0 degree				y Truck					
		50.0 degree	3		77001	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0. 70.	020			
FHWA Noise Mode					1			. 1			
VehicleType		Traffic Flow	Dist	ance		Road	Fresn		Barrier Att		rm Atten
Autos:	70.20	0.01		-2.8	-	-1.20		-4.76		000	0.00
Medium Trucks:	81.00	-14.47		-2.8	-	-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-10.72		-2.8		-1.20		-5.18	0.0	000	0.000
Unmitigated Noise VehicleType	<b>Levels (withoι</b> Lea Peak Hour		parrie				A 17 1- 4		Ldn		NEL
Autos:	Leq Peak Hour 66.1	Leq Day	35.6	Leq E	vening 61.8		Night 60.6		Lan 68.0		NEL 68.3
Medium Trucks:	62.4		49.7		54.6		63.1		63.		
Heavy Trucks:	70.6		66.4		64.9		72.3		72.0		
Vehicle Noise:	70.6		67.7		66.5		74.1		74.		
Centerline Distanc	e to Noise Con										
		70 (	dBA	65	dBA		60 dBA	55	dBA		
			dn:		172		370		796		1,715

Saturday, December 3, 2022

	FHWA-RE	D-77-108 HIGH	WAY	NOISE	PREDIC	TION MO	DDEL (	9/12/2	021)		
Scenario: Road Name: Road Segment:	Cajalco Exp					Project I Job Nu			(Building 1	7)	
SITE SP	ECIFIC IN	IPUT DATA				N	DISE	MODE	L INPUT	s	
Highway Data					Site Con	ditions (i	Hard =	10, Sc	oft = 15)		
Average Daily Tra	affic (Adt):	53,715 vehicle	es					Autos:	15		
Peak Hour Pe	rcentage:	7.00%			Me	dium Tru	cks (2.	Axles):	15		
Peak Hou	r Volume:	3,760 vehicles	3		He	avy Truci	ks (3+	Axles):	15		
Vehic	le Speed:	50 mph		H	Vehicle	Miss					
Near/Far Lane	Distance:	102 feet		ŀ		icleType		Day	Evening	Night	Daily
Site Data					VEII		utos:	74.7%	-	17.6%	89.27%
					M	edium Tri		88.5%		10.4%	3.19%
	r Height:	0.0 feet				Heavy Tru		75.1%		16.9%	7.54%
Barrier Type (0-Wall, Centerline Dist. 1	,	0.0 92.0 feet								10.570	7.5470
Centerline Dist. to		92.0 feet		Ŀ	Noise S	ource Ele	vation	s (in f	eet)		
Barrier Distance to		0.0 feet				Autos.	0.	000			
Observer Height (Ab				m Trucks.	_	297					
		Heav	y Trucks.	8.	004	Grade Adj	justment.	0.0			
	Pad Elevation: 0.0 feet  Road Elevation: 0.0 feet							ce (in	feet)		
	ad Grade:	0.0%		ŀ		Autos		733	,		
	Left View:	-90.0 degree	20		Mediu	m Trucks		618			
-	ight View:	90.0 degree				y Trucks.		629			
FHWA Noise Model C	Calculation	•									
	REMEL	Traffic Flow	Die	tance	Finite	Road	Fresi	nel le	Barrier Atte	en Rer	m Atten
Autos:	70.20	2.96	Dis	-2.8		-1.20	1100	-4.76		000	0.000
Medium Trucks:	81.00	-11.51		-2.8		-1.20		-4.88		000	0.000
Heavy Trucks:	85.38	-7.77		-2.8	8	-1.20		-5.18	0.0	000	0.000
Unmitigated Noise Lo	evels (with	out Topo and I	barrie	r atten	uation)						
VehicleType Le	q Peak Hou	ır Leq Day		Leq E	vening	Leq N	light		Ldn	CI	VEL
Autos:	69	.1 (	68.6		64.7		63.	5	70.9	9	71.2
Medium Trucks:	Medium Trucks: 65.4 65.6						57.	6	66.0	)	66.1
Heavy Trucks:	Heavy Trucks: 73.5 73.0						67.	В	75.3	3	75.6
Vehicle Noise:	Vehicle Noise: 75.3 74.9							5	77.0	)	77.3
Centerline Distance t	Centerline Distance to Noise Contour (in feet)										
			L	70	dBA	65 d			60 dBA		dBA
			Ldn:		270 281		581		1,253		2,699
	CNEL:						606	i	1,305		2,811

Saturday, December 3, 2022

Saturday, December 3, 2022

## APPENDIX 9.1:

**CADNAA OPERATIONAL NOISE MODEL INPUTS** 





13697 - MFBC Building 17 CadnaA Noise Prediction Model: 13697-02 bldg 17.cna

Date: 03.12.22 Analyst: B. Lawson

**Calculation Configuration** 

Parameter   Value	Configurat	ion
Max. Error (dB) 0.00  Max. Search Radius (#(Unit,LEN)) 2000.01  Min. Dist Src to Rcvr 0.00  Partition 0.50  Max. Length of Section (#(Unit,LEN)) 999.99  Min. Length of Section (#(Unit,LEN)) 1.01  Min. Length of Section (#(Unit,LEN)) 0.00  Proj. Line Sources 0n  Proj. Area Sources 0n  Ref. Time 0.00  Reference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 10.00  Dinth 10.00  DTM 5  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection max. Order of Reflection 2		
Max. Search Radius (#(Unit,LEN))  Min. Dist Src to Rcvr  Partition  Raster Factor  Max. Length of Section (#(Unit,LEN))  Min. Length of Section (#(Unit,LEN))  Min. Length of Section (#(Unit,LEN))  Min. Length of Section (%)  Do  Proj. Line Sources  On  Proj. Area Sources  On  Ref. Time  Reference Time Day (min)  Reference Time Night (min)  Daytime Penalty (dB)  Scool  Night-time Penalty (dB)  DTM  Standard Height (m)  Model of Terrain  Reflection  max. Order of Reflection  2	General	
Min. Dist Src to Rcvr 0.00  Partition 0.50  Raster Factor 0.50  Max. Length of Section (#(Unit,LEN)) 999.99  Min. Length of Section (#(Unit,LEN)) 1.01  Min. Length of Section (%) 0.00  Proj. Line Sources On  Proj. Area Sources On  Ref. Time  Reference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Max. Error (dB)	0.00
Partition  Raster Factor  0.50  Max. Length of Section (#(Unit,LEN)) 999.99  Min. Length of Section (#(Unit,LEN)) 1.01  Min. Length of Section (%) 0.00  Proj. Line Sources  On  Proj. Area Sources  On  Ref. Time  Reference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Max. Search Radius (#(Unit,LEN))	2000.01
Raster Factor         0.50           Max. Length of Section (#(Unit,LEN))         999.99           Min. Length of Section (#(Unit,LEN))         1.01           Min. Length of Section (%)         0.00           Proj. Line Sources         On           Proj. Area Sources         On           Ref. Time         Reference Time Day (min)         960.00           Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         Standard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection         2	Min. Dist Src to Rcvr	0.00
Max. Length of Section (#(Unit,LEN))         999.99           Min. Length of Section (#(Unit,LEN))         1.01           Min. Length of Section (%)         0.00           Proj. Line Sources         On           Proj. Area Sources         On           Ref. Time         86.00           Reference Time Day (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection         2	Partition	
Min. Length of Section (#(Unit, LEN)) 1.01  Min. Length of Section (%) 0.00  Proj. Line Sources On  Proj. Area Sources On  Ref. Time  Reference Time Day (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM 5tandard Height (m) 0.00  Model of Terrain Triangulation  Reflection max. Order of Reflection 2	Raster Factor	0.50
Min. Length of Section (%) 0.00  Proj. Line Sources On  Proj. Area Sources On  Ref. Time Seference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM 5tandard Height (m) 0.00  Model of Terrain Triangulation  Reflection max. Order of Reflection 2	Max. Length of Section (#(Unit,LEN))	999.99
Proj. Line Sources         On           Proj. Area Sources         On           Ref. Time         960.00           Reference Time Day (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Standard Height (m)         0.00           Model of Terrain         Triangulation           Reflection         ax. Order of Reflection	Min. Length of Section (#(Unit,LEN))	1.01
Proj. Area Sources         On           Ref. Time         960.00           Reference Time Day (min)         480.00           Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Standard Height (m)         0.00           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Min. Length of Section (%)	0.00
Ref. Time       960.00         Reference Time Day (min)       960.00         Reference Time Night (min)       480.00         Daytime Penalty (dB)       0.00         Recr. Time Penalty (dB)       5.00         Night-time Penalty (dB)       10.00         DTM       5tandard Height (m)         Standard Height (m)       0.00         Model of Terrain       Triangulation         Reflection       max. Order of Reflection	Proj. Line Sources	On
Reference Time Day (min)         960.00           Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         Standard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Proj. Area Sources	On
Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Ref. Time	
Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DSTAND         0.00           Standard Height (m)         0.00           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Reference Time Day (min)	960.00
Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Reference Time Night (min)	480.00
Night-time Penalty (dB) 10.00  DTM 0.00  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection 2	Daytime Penalty (dB)	0.00
DTM Standard Height (m) Model of Terrain Reflection max. Order of Reflection 2	Recr. Time Penalty (dB)	5.00
Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Night-time Penalty (dB)	10.00
Model of Terrain Triangulation Reflection max. Order of Reflection 2	DTM	
Reflection 2 2	Standard Height (m)	0.00
max. Order of Reflection 2	Model of Terrain	Triangulation
	Reflection	
C	max. Order of Reflection	2
Search Radius Src   100.00	Search Radius Src	100.00
Search Radius Rcvr 100.00	Search Radius Rcvr	100.00
Max. Distance Source - Rcvr 1000.00 1000.00	Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector 1.00 1.00	Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector 0.10	Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	Industrial (ISO 9613)	
Lateral Diffraction some Obj	Lateral Diffraction	some Obj
Obst. within Area Src do not shield On	Obst. within Area Src do not shield	On
Screening Incl. Ground Att. over Barrier	Screening	Incl. Ground Att. over Barrier
Dz with limit (20/25)		Dz with limit (20/25)
Barrier Coefficients C1,2,3 3.0 20.0 0.0	Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP)) 10	Temperature (#(Unit,TEMP))	10
rel. Humidity (%) 70	rel. Humidity (%)	70
Ground Absorption G 0.50	Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED)) 3.0	Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	Roads (TNM)	
Railways (FTA/FRA)	Railways (FTA/FRA)	
Aircraft (???)	Aircraft (???)	
Strictly acc. to AzB	Strictly acc. to AzB	

### **Receiver Noise Levels**

Name	М.	ID		Level Lr		Lir	nit. Val	ue		Land	Use	Height		Co	oordinates	
			Day	Night	CNEL	Day	Night	CNEL	Туре	Auto	Noise Type			Х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	38.2	37.9	44.5	55.0	45.0	0.0				5.00	а	6254523.18	2257379.43	5.00
RECEIVERS		R2	33.2	32.7	39.4	55.0	45.0	0.0				5.00	а	6252919.34	2256408.68	5.00
RECEIVERS		R3	35.9	35.5	42.1	55.0	45.0	0.0				5.00	а	6253214.27	2256016.68	5.00
RECEIVERS		R4	39.3	39.0	45.7	55.0	45.0	0.0				5.00	а	6253873.08	2255725.53	5.00
RECEIVERS		R5	40.9	40.6	47.3	55.0	45.0	0.0				5.00	а	6254202.08	2255653.20	5.00
RECEIVERS		R6	42.5	42.3	48.9	55.0	45.0	0.0				5.00	а	6254474.43	2255690.47	5.00
RECEIVERS		R7	39.9	39.1	45.8	55.0	45.0	0.0				5.00	а	6256247.45	2257053.56	5.00

## Point Source(s)

Name	М.	ID	R	esult. PW	'L		Lw/L	i	Ор	erating Ti	me	Heigh	t	Co	oordinates	
			Day	Evening	Night	Туре	Value	norm.	Day	Special	Night			Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(ft)		(ft)	(ft)	(ft)
BLDG17		AC01	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6255482.53	2256588.98	50.00
BLDG17		AC02	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6255512.80	2256587.23	50.00
BLDG17		AC03	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6255512.80	2256627.98	50.00
BLDG17		AC04	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6255480.21	2256627.98	50.00
BLDG17		AC05	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6254753.27	2256544.75	50.00
BLDG17		AC06	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6254788.19	2256545.91	50.00
BLDG17		AC07	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6254787.61	2256585.49	50.00
BLDG17		AC08	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	5.00	g	6254752.11	2256585.49	50.00
BLDG17		CAR01	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.70	2256502.26	5.00
BLDG17		CAR02	81.1	81.1	81.1	Lw	81.1					5.00	а	6255591.95	2256530.20	5.00
BLDG17		CAR03	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.70	2256587.23	5.00

Name	М.	ID	R	esult. PW	'L		Lw/L	i	Ope	erating Ti	ime	Heigh	t	Co	oordinates	
			Day	Evening	Night	Туре	Value		Day	Special	Night	- 0		Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(ft)		(ft)	(ft)	(ft)
BLDG17		CAR04	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.12	2256616.33	5.00
BLDG17		CAR05	81.1	81.1	81.1	Lw	81.1					5.00	а	6255544.81	2256606.44	5.00
BLDG17		CAR06	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.12	2256654.17	5.00
BLDG17		CAR07	81.1	81.1	81.1	Lw	81.1					5.00	а	6255544.81	2256637.87	5.00
BLDG17		CAR08	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.70	2256688.50	5.00
BLDG17		CAR09	81.1	81.1	81.1	Lw	81.1					5.00	а	6255544.81	2256670.46	5.00
BLDG17		CAR10	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.12	2256719.35	5.00
BLDG17		CAR11	81.1	81.1	81.1	Lw	81.1					5.00	а	6255545.97	2256710.62	5.00
BLDG17		CAR12	81.1	81.1	81.1	Lw	81.1					5.00	а	6255593.70	2256758.93	5.00
BLDG17		CAR13	81.1	81.1	81.1	Lw	81.1					5.00		6255544.23	2256743.21	5.00
BLDG17		CAR14	81.1	81.1	81.1	Lw	81.1					5.00	а	6255594.86	2256793.27	5.00
BLDG17		CAR15	81.1	81.1	81.1	Lw	81.1					5.00	a	6255545.39	2256776.97	5.00
BLDG17		CAR16	81.1	81.1	81.1	Lw	81.1					5.00	a	6255595.44	2256831.68	5.00
BLDG17		CAR17	81.1	81.1 81.1	81.1 81.1	Lw	81.1					5.00	a	6255546.56	2256827.02 2256868.93	5.00
BLDG17 BLDG17		CAR18 CAR19	81.1	81.1	81.1	Lw	81.1					5.00	a	6255594.28 6255544.23	2256861.36	5.00
BLDG17		CAR20	81.1	81.1	81.1	Lw	81.1					5.00	a	6255594.86	2256900.94	5.00
BLDG17		CAR21	81.1	81.1	81.1	Lw	81.1					5.00	а	6255545.97	2256895.12	5.00
BLDG17		CAR22	81.1	81.1	81.1	Lw	81.1					5.00	a	6255596.03	2256932.37	5.00
BLDG17		CAR23	81.1	81.1	81.1	Lw	81.1					5.00	а	6255545.39	2256948.08	5.00
BLDG17		CAR24	81.1	81.1	81.1	Lw	81.1					5.00	а	6255457.51	2256985.33	5.00
BLDG17		CAR25	81.1	81.1	81.1	Lw	81.1					5.00	а	6255420.26	2256985.33	5.00
BLDG17		CAR26	81.1	81.1	81.1	Lw	81.1					5.00	а	6255380.68	2256984.75	5.00
BLDG17		CAR27	81.1	81.1	81.1	Lw	81.1					5.00	а	6255344.60	2256985.91	5.00
BLDG17		CAR28	81.1	81.1	81.1	Lw	81.1					5.00	а	6255308.51	2256985.91	5.00
BLDG17		CAR29	81.1	81.1	81.1	Lw	81.1					5.00	а	6255267.77	2256984.75	5.00
BLDG17		CAR30	81.1	81.1	81.1	Lw	81.1					5.00	а	6255230.52	2256984.17	5.00
BLDG17		CAR31	81.1	81.1	81.1	Lw	81.1					5.00	а	6255196.18	2256984.17	5.00
BLDG17		CAR32	81.1	81.1	81.1	Lw	81.1					5.00	а	6255144.97	2256985.33	5.00
BLDG17		CAR33	81.1	81.1	81.1	Lw	81.1					5.00	а	6255109.46	2256984.17	5.00
BLDG17		CAR34	81.1	81.1	81.1	Lw	81.1					5.00	а	6255069.30	2256985.33	5.00
BLDG17		CAR35	81.1	81.1	81.1	Lw	81.1					5.00	а	6255032.64	2256984.17	5.00
BLDG17		CAR36	81.1	81.1	81.1	Lw	81.1					5.00	а	6254996.55	2256984.75	5.00
BLDG17		CAR37	81.1	81.1	81.1	Lw	81.1					5.00	a	6254948.83	2256986.50	5.00
BLDG17 BLDG17		CAR38 CAR39	81.1	81.1 81.1	81.1 81.1	Lw	81.1					5.00	a	6254909.25 6254865.60	2256986.50 2256986.50	5.00
BLDG17		CAR40	81.1	81.1	81.1	Lw	81.1					5.00	a	6254826.61	2256987.08	5.00
BLDG17		CAR41	81.1	81.1	81.1	Lw	81.1					5.00	a	6254790.52	2256986.50	5.00
BLDG17		CAR42	81.1	81.1	81.1	Lw	81.1					5.00	а	6254718.35	2256946.92	5.00
BLDG17		CAR43	81.1	81.1	81.1	Lw	81.1					5.00	а	6254719.51	2256914.91	5.00
BLDG17		CAR44	81.1	81.1	81.1	Lw	81.1					5.00	а	6254670.63	2256874.75	5.00
BLDG17		CAR45	81.1	81.1	81.1	Lw	81.1					5.00	а	6254717.77	2256879.40	5.00
BLDG17		CAR46	81.1	81.1	81.1	Lw	81.1					5.00	а	6254719.51	2256822.95	5.00
BLDG17		CAR47	81.1	81.1	81.1	Lw	81.1					5.00	а	6254671.79	2256832.84	5.00
BLDG17		CAR48	81.1	81.1	81.1	Lw	81.1					5.00	а	6254671.79	2256795.01	5.00
BLDG17		CAR49	81.1	81.1	81.1	Lw	81.1					5.00	а	6254718.93	2256789.19	5.00
BLDG17		CAR50	81.1	81.1	81.1	Lw	81.1					5.00	а	6254719.51	2256754.27	5.00
BLDG17		CAR51	81.1	81.1	81.1	Lw	81.1					5.00	а	6254670.63	2256755.44	5.00
BLDG17		CAR52	81.1	81.1	81.1	Lw	81.1					5.00			2256710.04	5.00
BLDG17		CAR53	81.1	81.1	81.1	Lw	81.1					5.00		6254671.21	2256666.39	5.00
BLDG17		CAR54	81.1	81.1	81.1	Lw	81.1					5.00		6254718.35	2256701.31	5.00
BLDG17		CAR55	81.1	81.1	81.1	Lw	81.1					5.00		6254717.77	2256659.99	5.00
BLDG17		CAR56	81.1	81.1	81.1	Lw	81.1					5.00	a	6254716.60		5.00
BLDG17		CAR57	81.1	81.1	81.1	Lw	81.1					5.00		6254715.44	2256580.25	5.00
BLDG17 BLDG17	$\vdash$	CAR58 CAR59	81.1	81.1 81.1	81.1 81.1	Lw	81.1					5.00		6254718.35 6254670.63	2256545.33 2256623.32	5.00
BLDG17		CAR60	81.1	81.1	81.1	Lw	81.1					5.00		6254670.04	2256592.47	5.00
BLDG17		CAR61	81.1	81.1	81.1	Lw	81.1					5.00			2256554.64	5.00
BLDG17		CAR62	81.1	81.1	81.1	Lw	81.1					5.00			2256511.57	5.00
BLDG17		CAR63	81.1	81.1	81.1	Lw	81.1					5.00		6254670.04		5.00
BLDG17		TRASH01	89.0	89.0	89.0	Lw	89		900.00	0.00	270.00	5.00		6255593.70		5.00
BLDG17	П	TRASH02	89.0	89.0	89.0	Lw	89		900.00	0.00		5.00		6255593.12	2256574.43	5.00
BLDG17		TRASH03	89.0	89.0	89.0	Lw	89		900.00	0.00	270.00	5.00		6254844.34	2256513.36	5.00
BLDG17		TRASH04	89.0	89.0	89.0	Lw	89		900.00	0.00	270.00	5.00	а	6254844.19	2256524.42	5.00
	_												_			

#### Line Source(s)

Name	M.	ID	R	esult. PW	'L	R	esult. PW	L'		Lw / L	i	Op	erating Ti	me		Moving	Pt. Src		Heigh	nt
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night		Number		Speed		
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	Day	Evening	Night	(mph)	(ft)	
BLDG17		TRUCK01	93.2	93.2	93.2	79.6	79.6	79.6	Lw	93.2									8	а
BLDG17		TRUCK02	93.2	93.2	93.2	79.5	79.5	79.5	Lw	93.2									8	а

Name	ID	H	lei	ght		Coordinat	es	
		Begin		End	х	у	Z	Ground
		(ft)		(ft)	(ft)	(ft)	(ft)	(ft)
BLDG17	TRUCK01	8.00	а		6254969.80	2256484.20	8.00	0.00

Name	ID	ŀ	lei	ght		Coordinat	es	
		Begin		End	х	у	z	Ground
		(ft)		(ft)	(ft)	(ft)	(ft)	(ft)
					6254969.78	2256408.56	8.00	0.00
BLDG17	TRUCK02	8.00	a		6255157.20	2256483.00	8.00	0.00
			Г		6255119.94	2256416.70	8.00	0.00

Area Source(s)

Name	M.	ID	R	esult. PW	'L	Re	esult. PW	L''		Lw/L	i	Ор	erating Ti	me	Height	t
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)	
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)		
BLDG17		DOCK01	103.4	103.4	103.4	62.6	62.6	62.6	Lw	103.4					8	а

Name	ID	ŀ	lei	ght			Coordinat	es	
		Begin		End		х	у	z	Ground
		(ft)		(ft)		(ft)	(ft)	(ft)	(ft)
BLDG17	DOCK01	8.00	а		Ī	6254844.65	2256638.45	8.00	0.00
						6255469.73	2256637.87	8.00	0.00
						6255467.98	2256564.54	8.00	0.00
					Ī	6255552.38	2256563.95	8.00	0.00
						6255584.97	2256553.48	8.00	0.00
						6255584.39	2256434.16	8.00	0.00
						6255206.66	2256433.58	8.00	0.00
						6255204.91	2256482.47	8.00	0.00
						6255098.99	2256483.64	8.00	0.00
						6255100.73	2256442.89	8.00	0.00
						6255035.55	2256444.64	8.00	0.00
					Ī	6255036.13	2256483.64	8.00	0.00
						6254899.36	2256484.80	8.00	0.00
						6254899.94	2256444.64	8.00	0.00
						6254845.23	2256445.22	8.00	0.00
						6254844.07	2256534.27	8.00	0.00

Barrier(s)

	- (-	_													
Name	Sel.	M.	ID	Abso	rption	Z-Ext.	Canti	lever	Н	lei	ght		Coordinat	es	
				left	right		horz.	vert.	Begin		End	х	у	Z	Ground
						(ft)	(ft)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)	(ft)
BLDG17			0						12.00	а		6254833.72	2256533.20	12.00	0.00
												6254833.72	2256507.51	12.00	0.00
												6254844.42	2256507.52	12.00	0.00
												6254844.62	2256443.45	12.00	0.00

Building(s)

	0	۱-,										
Name	Sel.	M.	ID	RB	Residents	Absorption	Height	t		Coordinat	es	
							Begin		х	У	Z	Ground
							(ft)		(ft)	(ft)	(ft)	(ft)
BLDG17			BUILDING00008	х	0		45.00	а	6254741.05	2256964.38	45.00	0.00
									6255523.27	2256964.96	45.00	0.00
									6255522.11	2256575.59	45.00	0.00
									6255469.73	2256576.18	45.00	0.00
									6255469.73	2256637.87	45.00	0.00
									6254844.65	2256638.45	45.00	0.00
									6254844.07	2256534.27	45.00	0.00
									6254739.30	2256531.94	45.00	0.00

Urban Crossroads, Inc.



## **APPENDIX 10.1:**

**CADNAA CONSTRUCTION NOISE MODEL INPUTS** 





## 13697 - MFBC Building 17

CadnaA Noise Prediction Model: 13697-02 bldg 17 Construction.cna

Date: 29.11.22 Analyst: B. Lawson

**Calculation Configuration** 

Parameter   Value	Configurat	ion
Max. Error (dB) 0.00  Max. Search Radius (#(Unit,LEN)) 2000.01  Min. Dist Src to Rcvr 0.00  Partition 0.50  Max. Length of Section (#(Unit,LEN)) 999.99  Min. Length of Section (#(Unit,LEN)) 1.01  Min. Length of Section (#(Unit,LEN)) 0.00  Proj. Line Sources 0n  Proj. Area Sources 0n  Ref. Time 0.00  Reference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 10.00  Dinth 10.00  DTM 5  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection max. Order of Reflection 2		
Max. Search Radius (#(Unit,LEN))  Min. Dist Src to Rcvr  Partition  Raster Factor  Max. Length of Section (#(Unit,LEN))  Min. Length of Section (#(Unit,LEN))  Min. Length of Section (#(Unit,LEN))  Min. Length of Section (%)  Do  Proj. Line Sources  On  Proj. Area Sources  On  Ref. Time  Reference Time Day (min)  Reference Time Night (min)  Daytime Penalty (dB)  Scool  Night-time Penalty (dB)  DTM  Standard Height (m)  Model of Terrain  Reflection  max. Order of Reflection  2	General	
Min. Dist Src to Rcvr 0.00  Partition 0.50  Raster Factor 0.50  Max. Length of Section (#(Unit,LEN)) 999.99  Min. Length of Section (#(Unit,LEN)) 1.01  Min. Length of Section (%) 0.00  Proj. Line Sources On  Proj. Area Sources On  Ref. Time  Reference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Max. Error (dB)	0.00
Partition  Raster Factor  0.50  Max. Length of Section (#(Unit,LEN)) 999.99  Min. Length of Section (#(Unit,LEN)) 1.01  Min. Length of Section (%) 0.00  Proj. Line Sources  On  Proj. Area Sources  On  Ref. Time  Reference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Max. Search Radius (#(Unit,LEN))	2000.01
Raster Factor         0.50           Max. Length of Section (#(Unit,LEN))         999.99           Min. Length of Section (#(Unit,LEN))         1.01           Min. Length of Section (%)         0.00           Proj. Line Sources         On           Proj. Area Sources         On           Ref. Time         Reference Time Day (min)         960.00           Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         Standard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection         2	Min. Dist Src to Rcvr	0.00
Max. Length of Section (#(Unit,LEN))         999.99           Min. Length of Section (#(Unit,LEN))         1.01           Min. Length of Section (%)         0.00           Proj. Line Sources         On           Proj. Area Sources         On           Ref. Time         86.00           Reference Time Day (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection         2	Partition	
Min. Length of Section (#(Unit, LEN)) 1.01  Min. Length of Section (%) 0.00  Proj. Line Sources On  Proj. Area Sources On  Ref. Time  Reference Time Day (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM 5tandard Height (m) 0.00  Model of Terrain Triangulation  Reflection max. Order of Reflection 2	Raster Factor	0.50
Min. Length of Section (%) 0.00  Proj. Line Sources On  Proj. Area Sources On  Ref. Time Seference Time Day (min) 960.00  Reference Time Night (min) 480.00  Daytime Penalty (dB) 0.00  Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM 5tandard Height (m) 0.00  Model of Terrain Triangulation  Reflection max. Order of Reflection 2	Max. Length of Section (#(Unit,LEN))	999.99
Proj. Line Sources         On           Proj. Area Sources         On           Ref. Time         960.00           Reference Time Day (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Standard Height (m)         0.00           Model of Terrain         Triangulation           Reflection         ax. Order of Reflection	Min. Length of Section (#(Unit,LEN))	1.01
Proj. Area Sources         On           Ref. Time         960.00           Reference Time Day (min)         480.00           Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Standard Height (m)         0.00           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Min. Length of Section (%)	0.00
Ref. Time       960.00         Reference Time Day (min)       960.00         Reference Time Night (min)       480.00         Daytime Penalty (dB)       0.00         Recr. Time Penalty (dB)       5.00         Night-time Penalty (dB)       10.00         DTM       5tandard Height (m)         Standard Height (m)       0.00         Model of Terrain       Triangulation         Reflection       max. Order of Reflection	Proj. Line Sources	On
Reference Time Day (min)         960.00           Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         Standard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Proj. Area Sources	On
Reference Time Night (min)         480.00           Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DTM         5tandard Height (m)           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Ref. Time	
Daytime Penalty (dB)         0.00           Recr. Time Penalty (dB)         5.00           Night-time Penalty (dB)         10.00           DSTAND         0.00           Standard Height (m)         0.00           Model of Terrain         Triangulation           Reflection         max. Order of Reflection	Reference Time Day (min)	960.00
Recr. Time Penalty (dB) 5.00  Night-time Penalty (dB) 10.00  DTM  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Reference Time Night (min)	480.00
Night-time Penalty (dB) 10.00  DTM 0.00  Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection 2	Daytime Penalty (dB)	0.00
DTM Standard Height (m) Model of Terrain Reflection max. Order of Reflection 2	Recr. Time Penalty (dB)	5.00
Standard Height (m) 0.00  Model of Terrain Triangulation  Reflection  max. Order of Reflection 2	Night-time Penalty (dB)	10.00
Model of Terrain Triangulation Reflection max. Order of Reflection 2	DTM	
Reflection 2 2	Standard Height (m)	0.00
max. Order of Reflection 2	Model of Terrain	Triangulation
	Reflection	
C	max. Order of Reflection	2
Search Radius Src   100.00	Search Radius Src	100.00
Search Radius Rcvr 100.00	Search Radius Rcvr	100.00
Max. Distance Source - Rcvr 1000.00 1000.00	Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector 1.00 1.00	Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector 0.10	Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	Industrial (ISO 9613)	
Lateral Diffraction some Obj	Lateral Diffraction	some Obj
Obst. within Area Src do not shield On	Obst. within Area Src do not shield	On
Screening Incl. Ground Att. over Barrier	Screening	Incl. Ground Att. over Barrier
Dz with limit (20/25)		Dz with limit (20/25)
Barrier Coefficients C1,2,3 3.0 20.0 0.0	Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP)) 10	Temperature (#(Unit,TEMP))	10
rel. Humidity (%) 70	rel. Humidity (%)	70
Ground Absorption G 0.50	Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED)) 3.0	Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	Roads (TNM)	
Railways (FTA/FRA)	Railways (FTA/FRA)	
Aircraft (???)	Aircraft (???)	
Strictly acc. to AzB	Strictly acc. to AzB	

#### **Receiver Noise Levels**

Name	М.	ID		Level Lr		Lir	nit. Val	ue		Land	Use	Height		Co	oordinates	
			Day	Night	CNEL	Day	Night	CNEL	Туре	Auto	Noise Type			Х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	64.7	61.9	69.0	55.0	45.0	0.0				5.00	а	6254523.18	2257379.43	5.00
RECEIVERS		R2	55.3	51.7	58.9	55.0	45.0	0.0				5.00	а	6252919.34	2256408.68	5.00
RECEIVERS		R3	56.2	52.6	59.9	55.0	45.0	0.0				5.00	а	6253214.27	2256016.68	5.00
RECEIVERS		R4	58.6	55.0	62.3	55.0	45.0	0.0				5.00	а	6253873.08	2255725.53	5.00
RECEIVERS		R5	59.8	56.1	63.4	55.0	45.0	0.0				5.00	а	6254202.08	2255653.20	5.00
RECEIVERS		R6	61.0	57.4	64.6	55.0	45.0	0.0				5.00	а	6254474.43	2255690.47	5.00
RECEIVERS		R7	62.3	58.4	65.7	55.0	45.0	0.0				5.00	а	6256247.45	2257053.56	5.00

## Point Source(s)

Name	М.	ID	R	esult. PW	'L		Lw/L	i	Ор	erating Ti	me	Heigh	t	Co	oordinates	
			Day	Evening	Night	Туре	Value	norm.	Day	Special	Night			Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(ft)		(ft)	(ft)	(ft)
		CONS01	115.0	115.0	115.0	Lw	115					8.00	а	6254679.82	2256995.93	8.00
		CONS02	115.0	115.0	115.0	Lw	115					8.00	а	6255624.51	2256961.75	8.00
		CONS03	115.0	115.0	115.0	Lw	115					8.00	а	6254682.26	2256432.04	8.00

Area Source(s)

		(-)														
Name	M.	ID	R	esult. PW	/L	Re	esult. PW	L"		Lw / Li		Op	erating T	ime	Height	t
			Day	Evening	Night	Day	Evening	Night	Type	Value	norm.	Day	Special	Night	(ft)	Г
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)		Г
SITEBOUNDARY		CONSTRUCTION	122.0	15.0	15.0	73.8	-33.2	-33.2	PWL-Pt	115					8	a

Name	ŀ	lei	ght			Coordinat	es	
	Begin		End		х	у	Z	Ground
	(ft)		(ft)		(ft)	(ft)	(ft)	(ft)
SITEBOUNDARY	8.00	а			6254650.62	2257029.73	8.00	0.00
					6255635.05	2257031.71	8.00	0.00
					6255848.73	2256408.34	8.00	0.00
					6255742.18	2256409.43	8.00	0.00
				Г	6255750.89	2256385.30	8.00	0.00
				Г	6254639.79	2256388.75	8.00	0.00

Urban Crossroads, Inc.

## **APPENDIX 10.2:**

**NIGHTTIME CONCRETE POUR NOISE MODEL INPUTS** 





# 13697 - MFBC Building 17

CadnaA Noise Prediction Model: 13697-02 bldg 17 Concrete.cna

Date: 02.12.22 Analyst: B. Lawson

**Calculation Configuration** 

Configuration									
Parameter	Value								
General									
Max. Error (dB)	0.00								
Max. Search Radius (#(Unit,LEN))	2000.01								
Min. Dist Src to Rcvr	0.00								
Partition									
Raster Factor	0.50								
Max. Length of Section (#(Unit,LEN))	999.99								
Min. Length of Section (#(Unit,LEN))	1.01								
Min. Length of Section (%)	0.00								
Proj. Line Sources	On								
Proj. Area Sources	On								
Ref. Time									
Reference Time Day (min)	960.00								
Reference Time Night (min)	480.00								
Daytime Penalty (dB)	0.00								
Recr. Time Penalty (dB)	5.00								
Night-time Penalty (dB)	10.00								
DTM									
Standard Height (m)	0.00								
Model of Terrain	Triangulation								
Reflection									
max. Order of Reflection	2								
Search Radius Src	100.00								
Search Radius Rcvr	100.00								
Max. Distance Source - Rcvr	1000.00 1000.00								
Min. Distance Rvcr - Reflector	1.00 1.00								
Min. Distance Source - Reflector	0.10								
Industrial (ISO 9613)									
Lateral Diffraction	some Obj								
Obst. within Area Src do not shield	On								
Screening	Incl. Ground Att. over Barrier								
	Dz with limit (20/25)								
Barrier Coefficients C1,2,3	3.0 20.0 0.0								
Temperature (#(Unit,TEMP))	10								
rel. Humidity (%)	70								
Ground Absorption G	0.50								
Wind Speed for Dir. (#(Unit,SPEED))	3.0								
TIME SPECE IOI DITT ("(OTHE, ST LED))									
Roads (TNM)									
Roads (TNM)									

#### **Receiver Noise Levels**

Name	M.	ID	Level Lr			Limit. Value			Land Use			Height		Coordinates		
			Day	Night	CNEL	Day	Night	CNEL	Туре	Auto	Noise Type			х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	49.5	46.2	53.4	55.0	45.0	0.0				5.00	а	6254523.18	2257379.43	5.00
RECEIVERS		R2	40.5	36.6	43.9	55.0	45.0	0.0				5.00	а	6252919.34	2256408.68	5.00
RECEIVERS		R3	41.3	37.4	44.7	55.0	45.0	0.0				5.00	а	6253214.27	2256016.68	5.00
RECEIVERS		R4	43.7	39.7	47.0	55.0	45.0	0.0				5.00	а	6253873.08	2255725.53	5.00
RECEIVERS		R5	44.8	40.8	48.2	55.0	45.0	0.0				5.00	а	6254202.08	2255653.20	5.00
RECEIVERS		R6	46.1	42.2	49.5	55.0	45.0	0.0				5.00	а	6254474.43	2255690.47	5.00
RECEIVERS		R7	46.8	42.7	50.0	55.0	45.0	0.0				5.00	а	6256247.45	2257053.56	5.00

## Point Source(s)

Name	M.	ID	Result. PWL			Lw / Li			Ор	ime	Height		Coordinates			
			Day	Evening	Night	Туре	Value	norm.	Day	Special	Night			Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(ft)		(ft)	(ft)	(ft)
		CONCRETE01	100.3	100.3	100.3	Lw	100.3					8.00	а	6254761.76	2256938.96	8.00
		CONCRETE02	100.3	100.3	100.3	Lw	100.3					8.00	а	6255490.43	2256934.01	8.00
		CONCRETE03	100.3	100.3	100.3	Lw	100.3					8.00	а	6254870.82	2256475.49	8.00

Area Source(s)

		(-)														
Name	М.	ID	Result. PWL			Result. PWL"			Lw / Li			Op	Height			
			Day	Evening	Night	Day	Evening	Night	Type	Value	norm.	Day	Special	Night	(ft)	Ī
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)		Γ
CONCRETE		CONCRETE	107.3	0.3	0.3	61.5	-45.5	-45.5	PWL-Pt	100.3					8	а

Name	ID	H	lei	ght	Coordinates						
		Begin		End	х	у	z	Ground			
		(ft)		(ft)	(ft)	(ft)	(ft)	(ft)			
CONCRETE	CONCRETE	8.00	а		6254741.50	2256965.38	8.00	0.00			
					6255522.42	2256965.38	8.00	0.00			
					6255522.76	2256563.32	8.00	0.00			
					6255552.83	2256563.32	8.00	0.00			
					6255584.40	2256543.03	8.00	0.00			
					6255600.19	2256541.52	8.00	0.00			
					6255599.44	2256494.16	8.00	0.00			
					6255581.81	2256489.57	8.00	0.00			
					6255582.15	2256433.27	8.00	0.00			
					6255204.77	2256433.27	8.00	0.00			
					6255206.28	2256482.14	8.00	0.00			
					6255176.21	2256481.38	8.00	0.00			
					6255173.20	2256467.10	8.00	0.00			
					6255158.92	2256436.28	8.00	0.00			
					6255140.12	2256411.47	8.00	0.00			
					6255133.36	2256392.68	8.00	0.00			
					6255128.09	2256406.21	8.00	0.00			
					6255116.82	2256422.00	8.00	0.00			
					6255095.02	2256428.76	8.00	0.00			
					6255113.81	2256444.55	8.00	0.00			
					6255130.35	2256461.84	8.00	0.00			
					6255136.36	2256484.39	8.00	0.00			
					6255100.28	2256481.38	8.00	0.00			
					6255101.78	2256444.55	8.00	0.00			
					6255036.38	2256446.05	8.00	0.00			
					6255036.38	2256483.64	8.00	0.00			
					6254997.29	2256482.89	8.00	0.00			
					6254997.29	2256415.98	8.00	0.00			
					6254904.07	2256416.73	8.00	0.00			
					6254925.12	2256433.27	8.00	0.00			
					6254937.15	2256454.32	8.00	0.00			
					6254939.41	2256483.64	8.00	0.00			
					6254898.81	2256482.89	8.00	0.00			
			П		6254898.81	2256444.55	8.00	0.00			
					6254844.69	2256443.80	8.00	0.00			
					6254849.08	2256534.30	8.00	0.00			
					6254740.77	2256532.84	8.00	0.00			